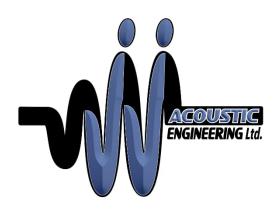


Road Traffic and Stationary Noise Impact Study

785 Gordon Street, Guelph, Ontario

JJ-00239-NIS1

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March 21, 2022

Reference No. JJ-00239-NIS1

Caitlin Aitchison srm Architects Inc. 279 King Street West, Suite 200 Kitchener, Ontario N2G 1B1

Dear Ms. Aitchison:

Re: Feasibility Road Traffic and Stationary Noise Impact Study 785 Gordon Street, Guelph, Ontario

1. Introduction

JJ Acoustic Engineering Ltd. (JJAE) was retained to complete a Feasibility Road Traffic and Stationary Noise Impact Study (Study) for the residential development located at 785 Gordon Street in Guelph, Ontario (Site). The Site will be developed into a 10-storey residential building. JJAE has provided a copy of the most up-to-date Site Plan in Attachment A.

The Study was prepared consistent with Ontario Ministry of the Environment, Conservation and Parks (MOECP) NPC 300, "Environmental Noise Guideline, Stationary and Transportation Sources– Approval and Planning", August 2013 as well as the Guelph Noise Control Guidelines (GNCG).

This Study has determined that the potential environmental noise impact from road traffic noise is significant. The stationary noise impacts from the neighboring buildings to the Site were below MOECP and GNCG guidelines. The proposed development will require a requirement for central air-conditioning, noise warning clauses and special building components. Road traffic noise control requirements for the Site were determined based on road traffic volumes provided by the City of Guelph (City) forecasted to 2031.

JJ Acoustic Engineering Ltd. joey@jjae.ca 226-346-6473 The following attachments were included with this Study:

- Attachment A Site Plan
- Attachment B Traffic Data, Traffic Data Summary Table, STC Calculations and Sample Stamson Traffic Model Outputs
- Attachment C Stationary Noise Impact Figures
- Attachment D Stationary Noise Impact Source Table

2. Road Traffic Analysis

2.1 Road Traffic Noise Modeling Methodology

The road traffic noise impact was conducted using STAMSON, the MOECP's computerized model of ORNAMENT. The Application of the model for the site was consistent with the ORNAMENT technical documents. The computer model input parameters include, among other data, the number of road segments, number of house rows, the positional relationship of the receptor to a noise source or barrier in terms of distance, elevation and angle of exposure to the source, the basic site topography, the ground surface type, traffic volumes, traffic composition and speed limit.

The predicted sound level is based on the 1-hour equivalent sound level, designated as Leq, and is adjusted by the STAMSON program to the 16-hour daytime and the 8-hour nighttime equivalent sound level. The applicable noise criteria for noise sensitive spaces are specified in terms of the 16-hour daytime period (7:00 a.m. to 11:00 p.m.) and 8-hour nighttime period (11:00 p.m. to 7:00 a.m.) enabling a direct comparison between the STAMSON model output and the noise limits.

2.2 Road Traffic Model Input Parameters

This section describes the STAMSON model input parameters used to predict road traffic noise impact for the Site.

The Site has two significant roadways in the vicinity of the development: Gordon Street approximately 15 meters to the East and Harvard Road approximately 15 meters to the North. Where there are intervening and off-site structures that provide line-of-sight obstruction to the roads, JJAE did not include line-of-sight obstruction in our analysis as to calculate worst-case noise impact.

2.2.1 Road Traffic Parameters

The traffic data provided by the City has been summarized below:

Gordon Street:

- Current AADT (2019) (Calculated): $(({}^{1}AM Peak) + ({}^{1}PM Peak)) \ge 20,585$
- Forecast AADT (2031) (Calculated)²: 27,684
- Commercial Vehicle Rates (Assumed 5.18% Total³): 3.11% medium trucks and 2.08% heavy trucks
- Posted Speed Limit: 60 km/h
- Day Night Splits: 90% day and 10% night based on common practice in acoustic engineering

Harvard Road:

- Current AADT (2019) (Calculated): $(({}^{1}AM Peak) + ({}^{1}PM Peak)) \ge 5 = 2420$
- Future AADT (2031) (Calculated)²: 3069
- Commercial Vehicle Rates (Assumed 3.11% Total³): 1.87% medium trucks and 1.24% heavy trucks
- Posted Speed Limit: 50 km/h
- Day Night Splits: 90% day and 10% night based on common practice in acoustic engineering

JJAE was provided with traffic data for 2019 from the City to use in our calculations. JJAE used a very conservative 2.5% growth increase over 12 years which would exceed most municipalities growth potential for roadways similar to Gordon Street. Therefore, JJAE believes that this data is suitable and acceptable in terms of calculating future potential noise impacts.

The traffic data is the foundation of this analysis and the Study will be updated if the values change. Traffic data was supplied by the City. The City's AADT report for this Noise Studies report has been supplied in Attachment B.

¹ No AADT data was supplied but AM and PM Peak values were supplied. JJAE has used a very conservative calculations method which takes the sum of the AM Peak and PM Peak values for the roadway and multiplies that by 5. This approach is used by traffic engineers as a conservative calculation of the AADT for a roadway and is the calculation method used in this report.

² Future AADT was calculated using a 2.5% increase over 12 years to estimate the 2031 Future Traffic Volume.

³ Percentages of Commercial Vehicles Rate was calculated using the worst-case truck traffic volumes for both the AM and PM peak and dividing by the total traffic to calculate the 5.18% total for Gordon Street and 3.11% total for Harvard Road. JJAE used a conservative 60% medium truck to 40% heavy truck ratio to calculate the 3.11% medium truck and 2.08% heavy truck volumes for Gordon Street and 1.87% medium truck and 1.24% heavy truck volumes for Harvester Road.

2.3 Road Traffic Noise Modeling Results

JJAE calculated the Plane of Window (POW) noise exposure for each floor at the Site for the separate daytime and nighttime periods.

The STAMSON road traffic model outputs are provided in Attachment B.

2.4 Road Traffic Modeling Discussion

Noise control requirements will be defined based on NPC 300.

Daytime Outdoor Living Area Assessment (NPC 300, Section C7.1.1)

NPC 300 section A5 (pages 13-14) defines an Outdoor Living Area (OLA). As part of this definition, a balcony or terrace is considered an OLA if it has a minimum depth of 4 meters. All balconies are less than 4 m in depth and therefore will not be considered as OLAs. This can also be seen in the definitions section of the GNCG.

JJAE has identified several potential OLA locations. OLA locations are indicated on Attachment A.

Plane of a Window – Ventilation Requirements (NPC 300, Section C7.1.2)

The predicted daytime and nighttime Plane of Window (POW) noise impact assumes a worst-case and direct line of sight noise exposure to both roads, unless the building itself blocks line-of-sight (full or partial).

JJAE has used the following criteria, which is a summary of NPC 300 requirements, to evaluate the Site noise impacts from road traffic noise:

Daytime Level (dBA)	Nighttime Level (dBA)	Ventilation Requirements and Warning Clauses	Special Building Components
55	50	Not Required	Not Required
55 - 65	50 - 60	Yes, with Type C Warning Clause	Not Required
66 or more	60 or more	Yes, with Type D Warning Clause	Yes

Table B.1 summarizes the predicted worst-case sound levels and the requirements for the units. The following warning clause is required:

"The Transferee of 785 Gordon Street, for himself, his heirs, executors, administrators, successors and assigns acknowledge being advised that despite the inclusion of noise control features in the development and/or within the building unit sound levels due to increasing road traffic may occasionally interfere with some indoor and/or outdoor activities of each dwelling occupants as the sound levels may at times exceed the sound level limits of the municipal and provincial noise criteria."

"This development includes a number of measures to help reduce noise impacts, listed below. To ensure the provincial and municipal sound level limits are not exceeded and/or to keep sound levels as low as possible it is important to maintain the sound attenuation features provided."

"This development includes building and street orientation to help increase setback distances to major noise sources and shield OLA from excessive noise levels."

"Each dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the municipal and provincial sound level limits."

"The building components of each dwelling unit (walls, windows and exterior doors) have been designed to provide acoustic insulation so that, when windows and exterior doors are closed, the indoor sound levels are within the municipal and provincial sound level limits. The details of this building component design are available by contacting the builder of this unit."

Indoor Living Areas – Building Components (NPC 300, Section C7.1.3)

At minimum, the building must be constructed to standard Ontario Building Code requirements. JJAE has assumed 35% window to floor area coverage and that windows are thick and operable.

3. Stationary Noise Impact Analysis

3.1 Stationary Noise Impact Sound Level Criteria

The general criteria for stationary noise sources are defined by NPC 300. The criteria defined in Table C-5 and C-6, "Exclusion Limit Values of One-Hour Equivalent Sound Level (Leq, dBA) Outdoor Points of Reception" and "Exclusion Limit Values of One-Hour Equivalent Sound Level (Leq, dBA) Plane of Window of Noise Sensitive Spaces" are used to evaluate the noise impact at the proposed development.

Receiver Category	Time Period	Stationary Noise Criteria
Outdoor Living Area (OLA)	Day = 7:00 to 23:00	Leq = 50 dBA
Plane of Window (POW)	Day = 7:00 to 23:00	Leq = 50 dBA
	Night = 23:00 to 7:00	Leq = 45 dBA

The criteria for a Class 1 area have been summarized below:

3.2 Modelling Methodology

The stationary noise impact was evaluated using the CADNA A acoustic modelling software that is based on the ISO 9613-2 standard. The data for all potential stationary noise sources was summarized in Attachment D.

4. Noise Impact Summary – From Site

The noise from the Site to the neighboring buildings could not be accounted for because the site has not undergone mechanical design yet. A detailed report should be completed once a mechanical design is done to account for noise from the Site to the neighboring building.

5. Noise Impact Summary – From Environment to Site

There are several buildings near the site. JJAE has identified several potential stationary noise sources including:

- HVAC 2 Fan
- Small HVAC Unit
- Representative MUA
- Representative Chiller

A summary of the noise sources used in our modelling is provided in Attachment D.

JJAE modelled the noise impact from all significant noise sources to the Site. The results are summarized in the table below and illustrated on Figure 1.

Facade	Worst Case Daytime Sound Level (dBA)	Daytime Noise Limit (dBA)	Worst Case Nighttime Sound Level (dBA)	Nighttime Noise Limit (dBA)	Limits met
North	48	50	44	45	Yes
East	46	50	43	45	Yes
South	45	50	41	45	Yes
West	48	50	45	45	Yes
OLA #1	25	55			Yes
OLA #2	23	55			Yes
OLA #3	24	55			Yes

From the table above it can be seen that all façades meet noise limits.

6. Recommendations

The road traffic noise impacts were above the NPC 300 and GNCG requirements. JJAE requires noise mitigation measures including requirements for air conditioning, noise warning clauses (Stated in Section 2.4) and special building components, which have been summarized in Attachment B under Table B1.

The stationary noise impacts from to the site were evaluated and the sound level predictions were determined to be below the noise limits for all façades.

7. Conclusions

The results of this Study indicate that the potential environmental impact from road traffic sources are significant. Mitigation measures will be required including ventilation requirements, special building components and noise warning clauses for each unit.

Should you have any questions on the above, please do not hesitate to contact us.

Yours truly,

Written by:

Reviewed by:

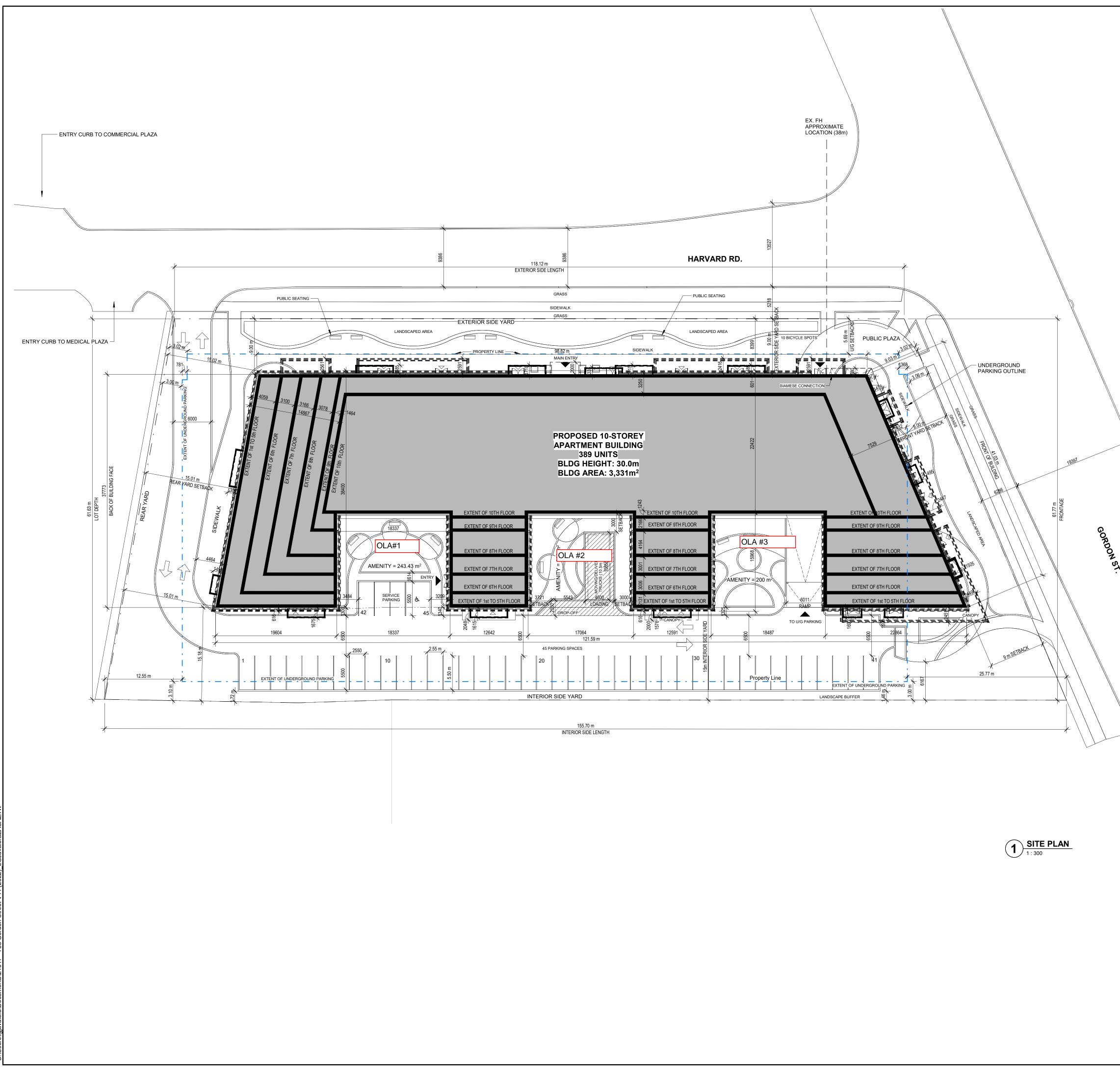
March 21, 2021

Cum Schighis

Emmanuel Ghiorghis, Acoustic Technician

Joey Jraige, P.Eng., B.A.Sc. President

ATTACHMENT A



Sľ	TE DATA			
785	Gordon Street, Guelph, Ontario			
DA	ТА	REQUIRED	PROVIDED	
ZON	ling	SC.1-11 w/requested change to R.4B Specia		
MIN	LOT AREA (m²)	650m ² 8462.2m ²		
MIN	LOT FRONTAGE (m)	15.0m	61.77m	
	FRONT YARD (meters)	6.0m, except as defined by section 4.24 15.0m	9.0m	
SETBACKS	INTERIOR SIDE YARD (m)	1/2 Bldg H, 7.5m min =15.0m OR 20% of Depth @midpoint = 27.38m	27.38m	
SEI	EXTERIOR SIDE YARD (m)	6.0m	9.0m	
	REAR YARD (m)	Greatest of 20% of <i>Lot</i> Depth OR 1/2 Bldg H, 7.5m min =12.3m or 15.0m	15.0m	
	UNDERGROUND PARKING (m)	3.0m	3.0 - 25.77m	

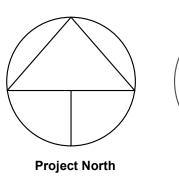
BUILDING DATA REQUIRED PROVIDED DATA TOTAL BEDS 520 beds ----150uph @ 0.85ha = **127.5 units** TOTAL NO OF UNITS 389 units BUILDING AREA (m²) 3,331m² / 35,845 SF ---28,877.44m² / GROSS FLOOR AREA (m²) ----310,834.18 SF FLOOR SPACE INDEX (FSI) 1.5 3.0 NUMBER OF STOREYS 10 10 Required when abutting w/another Residential zone Provided, at Front yard BUFFER STRIP portion of Interior Side Yard varies, 45° angular 30.0m, 52° @Gordon St BUILDING HEIGHT (m) plane from street 30.0m, 46° @Harvard St 586.46 m² / 6213 SF COMMERCIAL/RETAIL AREA (m²) ----Within main Bldg, or any accessory building; GARBAGE, REFUSE STORAGE In Building, AND COMPOSTERS n container located in a Private pick up side or rear yard. 70m² in rear yard, ACCESORY BUILDING (m²) setback 0.6m from lot none provided lines, 3.6m height

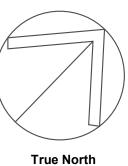
LANDSCAPING DATA					
DATA	REQUIRED	PROVIDED			
OUTDOOR LANDSCAPED AREA	40% of lot area = 3,384.9 m ²	49% (4,146.1 m²)			
LOT AREA	SOFTSCAPE AREA	20% (1,700.5 m²)			
LOTAREA	HARDSCAPE AREA	16% (1361.6 m²)			
PUBLIC AREA	SOFTSCAPE AREA	9% (763.5 m²)			
(*ADD'L LANDSCAPE NOT REQ.)	HARDSCAPE AREA	4% (332.9 m²)			
PAVED AREA & CURBS		25% (2104.4 m²)			
BUILDING AREA		39% (3,331 m²)			
TOTAL (LOT AREA)		100% (8,462.2 m ²)			

AMENITY DATA					
DATA	REQUIRED	PROVIDED			
BALCONIES		443.66 m² / 4,776 SF			
TERRACES		1,427.31m ² / 15,363SF			
OUTDOOR LANDSCAPED AREA		4,141.70 m² / 44,581 SF			
INDOOR AMENITY AREA		712.84m² / 7,677 SF			
TOTAL AMENITY AREA (m ²) **Not in Front & Exterior Side Yard	30m²/unit (0-20) +20m²/unit (21+) MIN 50m²/area 389 units = 7,980m ²	6,725.51 m² / 71,856 SF			

VEHICLE PARKING DATA					
DATA	REQUIRED	PROVIDED			
COMMERCIAL PARKING (1/2 AS OFFICE)	1 / 7.5m ² - commercial (@293.23m ² = 9) 1 / 33m ² - office (@293.23m ² = 40) = 49	50			
RESIDENTIAL PARKING	1.5 / Unit (0-20), 1.25 / Unit (>20), so 30+470 = 500	0.25/bed @520beds = 130			
RESIDENTIAL VISITOR PARKING *On provided. (Included in Count)	20% of total proposed = 26	26			
BARRIER FREE PARKING *On provided. (Included in Count)	For 201-300spots = 4	SURFACE - 1 U/G - 6			
PROPOSEI	D PARKING SUBTOTAL	179			
	FLEXIBLE PARKING	40			
TOTAL	549	220			

DATA	REQUIRED	PROVIDED
RESIDENTIAL BICYCLE PARKING		428
SHORT TERM		0.1 / unit = 39
LONG TERM		1 / unit = 389
COMMERCIAL BICYCLE PARKING		4
SHORT TERM		0.2 / 100m ² GFA or 2 min = 2
LONG TERM		0.2/100m ² GFA office or 2min = 2
TOTAL SHORT TERM SPOTS		41
TOTAL LONG TERM SPOTS		391
TOTAL	432	432





GENERAL NOTES

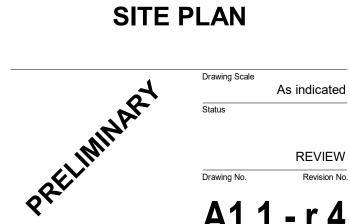
1. DO NOT SCALE DRAWINGS. WRITTEN DIMENSIONS SHALL HAVE PRECEDENCE OVER SCALED DIMENSIONS.

- 2. ALL WORK SHALL COMPLY WITH THE 2012 ONTARIO BUILDING CODE AND AMENDMENTS.
- 3. CONTRACTORS MUST CHECK AND VERIFY ALL DIMENSIONS AND SPECIFICATIONS AND REPORT ANY DISCREPANCIES TO THE ARCHITECT BEFORE PROCEEDING WITH THE WORK.
- 4. ALL CONTRACTORS AND SUB-CONTRACTORS SHALL HAVE A SET OF APPROVED CONSTRUCTION DOCUMENTS ON SITE AT ALL TIMES.
- 5. ALL DOCUMENTS REMAIN THE PROPERTY OF THE ARCHITECT. UNAUTHORIZED USE, MODIFICATION, AND/OR REPRODUCTION OF THESE DOCUMENTS IS PROHIBITED WITHOUT WRITTEN PERMISSION. THE CONTRACT DOCUMENTS WERE PREPARED BY THE CONSULTANT FOR THE ACCOUNT OF THE OWNER.
- 6. THE MATERIAL CONTAINED HEREIN REFLECTS THE CONSULTANTS BEST JUDGEMENT IN LIGHT OF THE INFORMATION AVAILABLE TO HIM AT THE TIME OF PREPARATION. ANY USE WHICH A THIRD PARTY MAKES OF THE CONTRACT DOCUMENTS, OR ANY RELIANCE ON/OR DECISIONS TO BE MADE BASED ON THEM ARE THE RESPONSIBILITY OF SUCH THIRD PARTIES.
- 7. THE CONSULTANT ACCEPTS NO RESPONSIBILITY FOR DAMAGES, IF ANY, SUFFERED BY ANY THIRD PARTY AS A RESULT OF DECISIONS MADE OR ACTIONS BASED ON THE CONTRACT DOCUMENTS.

No.	Date	Revision
1	2021-10-18	Issued for Pre-construction
2	2022-02-18	Issued for Coordination
3	2022-03-07	Issued for Coordination
4	2022-03-18	Issued for OPA/ZBA

Project Date	2021-11-0
	2021110
Drawn by	LG
Checked by	MY
ARCHITECTS INC. Plot Date / Time 2022-03	-18 4:18:05 PN

21017 **785 GORDON STREET**



REVIEW

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ATTACHMENT B

Table B1

Road Traffic Noise Levels and Mitigation Measures Summary 785 Gordon Street, Guelph, Ontario

Point of Reception	Road Sound Level Daytime (dBA)	Road Sound Level Nighttime (dBA)	Ventilation Requirements NPC 300	Warning Clauses From NPC 300	Special Building Components
North Facade		<u> </u>	•		
Plane of Window Level 1	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 4	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 5	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 6	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 7	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 8	63 (dBA)	56 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 9	63 (dBA)	56 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 10	63 (dBA)	56 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
East Facade					
Plane of Window Level 1	70 (dBA)	64 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 31
Plane of Window Level 2	70 (dBA)	63 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 31
Plane of Window Level 3	69 (dBA)	63 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 30
Plane of Window Level 4	69 (dBA)	63 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 30
Plane of Window Level 5	69 (dBA)	62 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 30
Plane of Window Level 6	68 (dBA)	62 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 29
Plane of Window Level 7	68 (dBA)	61 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 29
Plane of Window Level 8	67 (dBA)	61 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 28
Plane of Window Level 9	67 (dBA)	60 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 28
Plane of Window Level 10	67 (dBA)	60 (dBA)	Requirement for Air Conditioning	Type D	Minimum Window STC Rating of 28

Table B1

Road Traffic Noise Levels and Mitigation Measures Summary 785 Gordon Street, Guelph, Ontario

Point of Reception	Road Sound Level Daytime (dBA)	Road Sound Level Nighttime (dBA)	Ventilation Requirements NPC 300	Warning Clauses From NPC 300	Special Building Components
South Facade	Daytime (uDA)	(up)		1101111100000	Special Zuntung Components
Plane of Window Level 1	65 (dBA)	58 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 2	65 (dBA)	58 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 3	65 (dBA)	58 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 4	64 (dBA)	58 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 5	64 (dBA)	58 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 6	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 7	64 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 8	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 9	63 (dBA)	57 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
Plane of Window Level 10	63 (dBA)	56 (dBA)	Requirement for Air Conditioning	Type C	Compliance with Ontario Building Code
West Facade					
Plane of Window Level 1	55 (dBA)	48 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 2	55 (dBA)	48 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 3	54 (dBA)	48 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 4	54 (dBA)	47 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 5	53 (dBA)	47 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 6	53 (dBA)	46 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 7	53 (dBA)	46 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 8	52 (dBA)	46 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 9	52 (dBA)	45 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Plane of Window Level 10	()				
Plane of window Level To	51 (dBA)	45 (dBA)	Not Required	Not Required	Compliance with Ontario Building Code
Outdoor Living Area (1)					
OLA #1	47 (dBA)	N/A	N/A	N/A	N/A
OLA #2	48 (dBA)	N/A	N/A	N/A	N/A
OLA #3	51 (dBA)	N/A	N/A	N/A	N/A

Note:1

All OLA locations are shielded by the building, JJAE has assumed a conservative 10 dBA reduction in sound level from our stamson model for road traffic.

Outdoor Sound Level Indoor Sound Level Noise Reduction	65 45 23	Day/Night Day Road/Rail Road
Angle of Sound	60 to 90 Degrees	Angle Correction 3
		Sum 26
Component	Window	Sum 26
Sound Energy Transmitted	100 %	Table 3 0
Component Area Room Floor Area Room Absorption Category	35 % Floor Area 100 31 Intermediate	Table 4 -4
Noise Spectrum Type Component Category	Mixed Road Traffic, Distance Aircraft Openable Thick Window	Table 5 4
RE	QUIRED STC FOR COMPONENT	26
Component	Exterior Wall	Sum 26
Sound Energy Transmitted	10 %	Table 3 10
Component Area Room Floor Area	65 % Floor Area 100 63	
Room Absorption Category	Intermediate	Table 4 -1
Noise Spectrum Type Component Category	Mixed Road Traffic, Distance Aircraft Exterior Wall	Table 5 7



	raffic Inc.
Morning Peak Diagram	Specified Period One Hour Peak From: 7:00:00 From: 8:00:00 To: 9:00:00 To: 9:00:00
Municipality:GuelphSite #:1906000021Intersection:Gordon St & Harvard RdTFR File #:1Count date:22-Oct-19	Weather conditions: RainyPerson counted:EvgeniiPPerson prepared: Person checked:
** Signalized Intersection **	Major Road: Gordon St runs N/S
North Entering: 611 Trucks 6 32 0	4 Cyclists 18 East Leg Total: 8 38 Trucks 51 East Entering: 4 569 Totals 1088 Peds Cross: Χ
Cyclists Trucks Cars Totals 1 6 137 144 Harvard Rd	Gordon St $ \begin{array}{ccccccccccccccccccccccccccccccccccc$
Cyclists Trucks Cars Totals	Harvard Rd
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	s Cars Trucks Cyclists Totals 4 0 0 4
Peds Cross: X Cars 497 C West Peds: 34 Trucks 33 Tru West Entering: 205 Cyclists 3 Cyclists	Cars 32 862 1 895 Peds Cross: ▶ ucks 0 45 0 45 South Peds: 6 lists 0 9 0 9 South Entering: 949 tatls 32 916 1 South Leg Total: 1482
Com	ments



Mid-day Peak Diagram Municipality: Guelph Site #: 1906000021 Intersection: Gordon St & Harvard Rd TFR File #: 1 Count date: 22-Oct-19 ** Signalized Intersection ** North Leg Total: 1950 North Entering: 969 North Peds: 26	ጎ ሰ [°]
Site #: 1906000021 Intersection: Gordon St & Harvard Rd TFR File #: 1 Count date: 22-Oct-19 ** Signalized Intersection ** North Leg Total: 1950 North Entering: 969	Rainy Person counted: EvgeniiP Person prepared: Person checked: Major Road: Gordon St runs N/S Cyclists 5 East Leg Total: 13
North Leg Total: 1950 Cyclists 3 0 6 North Entering: 969 Trucks 6 36 0 4	Cyclists 5 East Leg Total: 13
North Entering: 969 Trucks 6 36 0 4	
Peds Cross: M Totals 169 799 1	2 Trucks 45 East Entering: 11 21 Cars 931 East Peds: 17 Totals 981 Peds Cross: X
Cyclists Trucks Cars Totals	Fordon St Cars Trucks Cyclists Total 9 0 0 9 0 0 0 9 0 0 0 1 1 0 2 E
Cyclists Trucks Cars Totals	Harvard Rd
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Cars Trucks Cyclists Total
West Peds: 45 Trucks 43 Truc West Entering: 270 Cyclists 3 Cycli	ars 80 758 0 838 Peds Cross: M cks 1 41 0 42 South Peds: 7 sts 0 3 0 3 South Entering: 883 als 81 802 0 South Leg Total: 1783
Comr	nents



Afternoon Peak Diagram	Specified Period One Hour Peak
	From: 15:00:00 From: 16:45:00 To: 18:00:00 To: 17:45:00
Municipality:GuelphSite #:1906000021Intersection:Gordon St & Harvard RdTFR File #:1Count date:22-Oct-19	Weather conditions: Rainy Person counted: EvgeniiP Person prepared: Person checked:
North Entering: 1482 Trucks 6 31 0 3 North Peds: 40 Cars 221 1205 3 1 Peds Cross: 🛏 Totals 232 1247 3	Major Road: Gordon St runs N/S 6 Cyclists 8 87 Trucks 37 429 Cars 1100 Totals 1145 Peds Cross: X
Cyclists Trucks Cars Totals	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
Cyclists Trucks Cars Totals 5 3 181 1 0 1 2 1 1 0 102 7 3 284	Harvard Rd Cars Trucks Cyclists Totals 6 0 1 7
West Peds:64Trucks 31TruWest Entering:294Cyclists 13Cycl	ars 86 916 2 1004 Peds Cross: ► cks 3 34 0 37 South Peds: 7 ists 1 3 0 4 South Entering: 1045 tals 90 953 2 South Leg Total: 2396
Com	nents



Accu-Traffic Inc.

Eight Hour	Peak Dia	agram			Eight Hour Peak From: 8:00:00 To: 16:00:00
	000021 on St & Harvard	Rd	Weather of Rainy Person co Person pr Person ch	repared:	EvgeniiP
** Signalized Inters	ection **		Major Roa	ad: Gordon S	St runs N/S
North Leg Total: 9401 North Entering: 4540 North Peds: 103 Peds Cross: ►	Cyclists 11 Trucks 25 Cars 763 Totals 799	16 0 27 161 1 18 3553 10 43 3730 11	ጎ ሰ	Cyclists 45 Trucks 216 Cars 4600 Totals 4861	East Leg Total: 45 East Entering: 24 East Peds: 86 Peds Cross: X
Cyclists Trucks Cars Tota 11 31 1076 1114 Har	1		erdon St		Cars Trucks Cyclists Totals 20 1 0 21 0 0 0 0 1 1 3 21 2 1
Cyclists Trucks Cars Total 20 26 724 770 1 0 5 6 0 8 372 380		S	5		ard Rd
21 34 1101	\checkmark	Gordon St		\Box	19 1 1 21
Peds Cross:XWest Peds:171West Entering:1156West Leg Total:2274	Cars 3926 Trucks 170 Cyclists 17 Totals 4113	Truc	rs 313 3856 ks 6 189 sts <u>0 25</u> ils <u>319 4070</u>	0 195 0 25	Peds Cross: South Peds: 26 South Entering: 4393 South Leg Total: 8506
		Comn	nents		
-	Cyclists 17	•	ıls 319 4070		-



Accu-Traffic Inc.

Total Count Diagram

	000021 on St & Harvard F	٦d	Weather of Rainy Person co Person pi Person ch	repared:	EvgeniiP
** Signalized Inters	ection **		Major Roa	ad: Gordon St	runs N/S
North Leg Total: 15452 North Entering: 7771 North Peds: 180 Peds Cross: ►	Trucks 41 2 Cars 1236 6	253 1 2	⁵⁵ 1995 1421	Cyclists 63 Trucks 330 Cars 7288 Totals 7681	East Leg Total: 67 East Entering: 32 East Peds: 145 Peds Cross: X
Cyclists Trucks Cars Tota 21 52 1735 180	•	↓ Ŀ `	N E	$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array}\\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\$	0 0 0 1 2 6
Cyclists Trucks Cars Total 28 41 1097 116 2 0 7 9	4 ک		S	Harvard	d Rd
1 11 590 602 31 52 1694	Ţ.	Gordon Si			ars Trucks Cyclists Totals 2 1 2 35
Peds Cross:XWest Peds:293West Entering:1777West Leg Total:3585	Cars 6763 Trucks 265 Cyclists 38 Totals 7066	Tru Cycl	ars 499 6166 cks 11 288 ists <u>1 35</u> als 511 6489	0 299 0 36	Peds Cross:►South Peds:50South Entering:7010South Leg Total:14076
		Com	ments		



Accu-Traffic Inc. Traffic Count Summary

				IIAI		ount 3						
Intersection:	Gordon	St & Ha	rvard Rd	l	Count [Date: 22-Oct-19) Mu	^{nicipality:} Gl	lelph			
	Nort	h Appro	ach Tot	als		North/South	I	Sout	h Appro	oach Tot	tals	
Hour	Includ	es Cars, T	rucks, & C		Total	Total	Hour	Includ	es Cars, T	rucks, & C		Total
Ending	Left	Thru	Right	Grand Total	Peds	Approaches	Ending	Left	Thru	Right	Grand Total	Peds
7:00:00	0	0	0	0	0	0	7:00:00	0	0	0	0	0
8:00:00	1	357	43	401	5	1035	8:00:00		621	0	634	1
9:00:00	2	497	112	611	11	1560	9:00:00	32	916	1	949	6
11:00:00	0	0	0	0	0	0	11:00:00	0 0	0	0	0	0
12:00:00	2	741	177	920	9	1780	12:00:00		797	1	860	2
13:00:00	2	786	174	962	18	1823	13:00:00		784	0	861	5
14:00:00	1	729	166	896	34	1666	14:00:00		706	1	770	6
15:00:00	0	0	0	0	2	0	15:00:00		0	0	0	0
16:00:00	4	977	170	1151	29	2104	16:00:00		867	1	953	7
17:00:00	2	1200	239	1441	38	2430	17:00:00		898	6	989	13
18:00:00	2	1171	216	1389	34	2383	18:00:00	94	900	0	994	10
Totals:	16	6458	1297	7771	180	14781	S Totals		6489	10	7010	50
		t Appro a es Cars, T				East/West				ach Tot rucks, & C		
Hour Ending	menuu			Grand	Total Peds	Total	Hour Ending	Includ			Grand	Total Peds
-	Left	Thru	Right	Total		Approaches		Left	Thru	Right	Total	1 645
7:00:00	0	0	0	0	0	0	7:00:00		0	0	0	0
8:00:00	1	0	1	2	6	64	8:00:00		0	16	62	15
9:00:00	0	0	4	4	26	209	9:00:00		1	36	205	34
11:00:00	0	0	0	0	0	0	11:00:00		0	0	0	0
12:00:00	0	0	6	6	6	186	12:00:00		2	67	180	37
13:00:00 14:00:00	1 2	0	4 5	5 7	15 12	239 273	13:00:00 14:00:00		0 2	80 100	234 266	36 29
15:00:00	2		0	0	0	0	15:00:00		0		200	29
16:00:00	0	0	2	2	27	273	16:00:00		1	97	271	35
17:00:00	1		2	3	29	273	17:00:00		1	93	255	48
18:00:00	1	Ö	2	3	24	307	18:00:00		2	113	304	59
10.00.00	,	Ŭ	-	Ŭ	21	007	10.00.00		-		007	00
Totolo	e		26	32	145	1809		1166	9	602	1777	293
Totals:	6	0					W Totals			602	1777	293
	a allas se	0.00				or Traffic Cr	-	-		10.00		
Hours E		8:00	9:00 186	12:00 124	13:00 178		14:00 208	16:00 210	17:00 214	18:00 236		
Crossing	y values	. 03	100	124	1/0		200	210	214	230		

STAMSON 5.0 NORMAL REPORT Date: 18-11-2021 13:12:37 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: northf1.te Time Period: Day/Night 16/8 hours Description: North Facade Floor 1 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume : 3.11 Heavy Truck % of Total Volume : 2.08 Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods.) : No of house rows 0 / 0 (Reflective ground surface) Surface : 2 Receiver source distance : 40.00 / 40.00 m Receiver height : 2.00 / 2.00 m Topography 1 (Flat/gentle slope; no barrier) : Reference angle : 0.00 ♠ Road data, segment # 2: Harvard Rd (day/night) _____ Car traffic volume : 2838/315 veh/TimePeriod * Medium truck volume : 55/6 veh/TimePeriod * 36/4 Heavy truck volume : veh/TimePeriod * Posted speed limit : 50 km/h 0% Road gradient : Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 2420 Percentage of Annual Growth : 2.50

Number of Years of Growth: 12.00Medium Truck % of Total Volume: 1.87Heavy Truck % of Total Volume: 1.24 Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Harvard Rd (day/night) -----Angle1Angle2: -90.00 deg90.00 degWood depth: 0(No woods)No of house rows: 0 / 0Surface: 2(Reflective) (No woods.) (Reflective ground surface) Receiver source distance : 15.00 / 15.00 m Receiver height: 2.00 / 2.00 mTopography: 1 (Flat/gentle slope; no barrier) Reference angle : 0.00 ♠ Results segment # 1: Gordon St (day) ------Source height = 1.20 mROAD (0.00 + 62.76 + 0.00) = 62.76 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 0 90 0.00 70.03 0.00 -4.26 -3.01 0.00 0.00 0.00 62.76 -----Segment Leq : 62.76 dBA ♠ Results segment # 2: Harvard Rd (day) Source height = 1.05 m ROAD $(0.00 + 57.77 + 0.00) = 57.77 \, dBA$ Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _____ Segment Leq : 57.77 dBA Total Leq All Segments: 63.96 dBA Results segment # 1: Gordon St (night)

Source height = 1.20 m ROAD (0.00 + 56.24 + 0.00) = 56.24 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ 0 90 0.00 63.51 0.00 -4.26 -3.01 0.00 0.00 0.00 56.24 -----Segment Leq : 56.24 dBA ♠ Results segment # 2: Harvard Rd (night) -----Source height = 1.05 m ROAD (0.00 + 51.22 + 0.00) = 51.22 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.00 51.22 0.00 0.00 0.00 0.00 0.00 0.00 51.22 _____ Segment Leq : 51.22 dBA Total Leq All Segments: 57.43 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 63.96 (NIGHT): 57.43

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STAMSON 5.0 NORMAL REPORT Date: 18-11-2021 13:13:24 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: eastf1.te Time Period: Day/Night 16/8 hours Description: East Facade Floor 1 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0% Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:12.00Heavy Truck % of Total Volume:3.11Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 No of house rows : 0 / 0 Surface : 2 (No woods.) 0 , 2 / 15 : (Reflective ground surface) Surface Receiver source distance : 15.00 / 15.00 m Receiver height : 2.00 / 2.00 m : 1 Topography (Flat/gentle slope; no barrier) : 0.00 Reference angle ♠ Results segment # 1: Gordon St (day) Source height = 1.20 mROAD (0.00 + 70.03 + 0.00) = 70.03 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 90 0.00 70.03 0.00 0.00 0.00 0.00 0.00 70.03 -----

Segment Leq : 70.03 dBA

Total Leq All Segments: 70.03 dBA ♠ Results segment # 1: Gordon St (night) -----Source height = 1.20 m ROAD (0.00 + 63.51 + 0.00) = 63.51 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -----_ _ _ _ _ _ _ -90 90 0.00 63.51 0.00 0.00 0.00 0.00 0.00 0.00 63.51 _____ Segment Leq : 63.51 dBA Total Leq All Segments: 63.51 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 70.03

(NIGHT): 63.51

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STAMSON 5.0 NORMAL REPORT Date: 18-11-2021 13:13:43 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: southf1.te Time Period: Day/Night 16/8 hours Description: South Facade Floor 1 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0% Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:12.00Heavy Truck % of Total Volume:3.11Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : -90.00 deg 0.00 deg . - JU. UU deg
wuuu depth : 0
No of house rows : 0 / 0
Surface : (No woods.) 0, 2 (25 (Reflective ground surface) Receiver source distance : 25.00 / 25.00 m Receiver height : 2.00 / 2.00 m : 1 Topography (Flat/gentle slope; no barrier) : 0.00 Reference angle Results segment # 1: Gordon St (day) Source height = 1.20 mROAD (0.00 + 64.80 + 0.00) = 64.80 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 70.03 0.00 -2.22 -3.01 0.00 0.00 0.00 64.80 -----

Segment Leq : 64.80 dBA

Total Leq All Segments: 64.80 dBA ♠ Results segment # 1: Gordon St (night) -----Source height = 1.20 m ROAD (0.00 + 58.28 + 0.00) = 58.28 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ _ -----90 0 0.00 63.51 0.00 -2.22 -3.01 0.00 0.00 0.00 58.28 -----Segment Leq : 58.28 dBA Total Leq All Segments: 58.28 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 64.80

. (NIGHT): 58.28

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STAMSON 5.0 NORMAL REPORT Date: 23-11-2021 11:27:43 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: westf1.te Time Period: Day/Night 16/8 hours Description: West Facade Floor 1 Road data, segment # 1: Harvard Rd (day/night) -----Car traffic volume : 2838/315 veh/TimePeriod * Medium truck volume : 55/6 veh/TimePeriod * Heavy truck volume : 36/4 veh/TimePeriod * Posted speed limit : 50 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 2420 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:1.87Heavy Truck % of Total Volume:1.24Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Harvard Rd (day/night) _____ Angle1Angle2: -90.00 deg0.00 degWood depth: 0(No woodsNo of house rows: 0 / 0Surface: 2(Reflection) (No woods.) 0 , 2 / 15 (Reflective ground surface) Receiver source distance : 15.00 / 15.00 m Receiver height : 2.00 / 2.00 m : Topography 1 (Flat/gentle slope; no barrier) Reference angle : 0.00 Results segment # 1: Harvard Rd (day) -----Source height = 1.05 m $ROAD (0.00 + 54.76 + 0.00) = 54.76 \, dBA$ Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 57.77 0.00 0.00 -3.01 0.00 0.00 0.00 54.76 -----

Segment Leq : 54.76 dBA

Total Leq All Segments: 54.76 dBA ♠ Results segment # 1: Harvard Rd (night) -----Source height = 1.05 m ROAD (0.00 + 48.21 + 0.00) = 48.21 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 51.22 0.00 0.00 -3.01 0.00 0.00 0.00 48.21 _____ Segment Leq : 48.21 dBA Total Leq All Segments: 48.21 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 54.76

(NIGHT): 48.21

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STAMSON 5.0 NORMAL REPORT Date: 21-03-2022 16:18:41 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: ola1.te Time Period: Day/Night 16/8 hours Description: Outdoor Living Area #1 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0% Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:12.00Heavy Truck % of Total Volume:3.11Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 No of house rows : 0 / 0 Surface (No woods.) : 2 (Reflective ground surface) Surface Receiver source distance : 165.00 / 165.00 m Receiver height : 2.00 / 2.00 m : 1 Topography (Flat/gentle slope; no barrier) Reference angle : 0.00 ♠ Results segment # 1: Gordon St (day) Source height = 1.20 mROAD (0.00 + 56.61 + 0.00) = 56.61 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 70.03 0.00 -10.41 -3.01 0.00 0.00 0.00 56.61 -----

Segment Leq : 56.61 dBA

Total Leq All Segments: 56.61 dBA ♠ Results segment # 1: Gordon St (night) -----Source height = 1.20 m ROAD (0.00 + 50.09 + 0.00) = 50.09 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 63.51 0.00 -10.41 -3.01 0.00 0.00 0.00 50.09 _____ Segment Leq : 50.09 dBA Total Leq All Segments: 50.09 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 56.61

(NIGHT): 50.09

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STAMSON 5.0 NORMAL REPORT Date: 21-03-2022 16:18:58 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: ola2.te Time Period: Day/Night 16/8 hours Description: Outdoor Living Area #2 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0% Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:12.00Heavy Truck % of Total Volume:3.11Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 No of house rows : 0 / 0 (No woods.) : 2 (Reflective ground surface) Surface Receiver source distance : 110.00 / 110.00 m Receiver height : 2.00 / 2.00 m : 1 Topography (Flat/gentle slope; no barrier) Reference angle : 0.00 ♠ Results segment # 1: Gordon St (day) Source height = 1.20 mROAD (0.00 + 58.37 + 0.00) = 58.37 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 70.03 0.00 -8.65 -3.01 0.00 0.00 0.00 58.37 -----

Segment Leq : 58.37 dBA

Total Leq All Segments: 58.37 dBA ♠ Results segment # 1: Gordon St (night) -----Source height = 1.20 m ROAD (0.00 + 51.85 + 0.00) = 51.85 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 63.51 0.00 -8.65 -3.01 0.00 0.00 0.00 51.85 _____ Segment Leq : 51.85 dBA Total Leq All Segments: 51.85 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 58.37

. (NIGHT): 51.85

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STAMSON 5.0 NORMAL REPORT Date: 21-03-2022 16:19:11 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: ola3.te Time Period: Day/Night 16/8 hours Description: Outdoor Living Area #3 Road data, segment # 1: Gordon St (day/night) -----Car traffic volume : 23623/2625 veh/TimePeriod * Medium truck volume : 775/86 veh/TimePeriod * Heavy truck volume : 518/58 veh/TimePeriod * Posted speed limit : 60 km/h Road gradient : 0% Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20585 Percentage of Annual Growth : 2.50 Number of Years of Growth : 12.00 Medium Truck % of Total Volume:12.00Heavy Truck % of Total Volume:3.11Day (16 hrs) % of Total Volume:90.00 Data for Segment # 1: Gordon St (day/night) _____ Angle1 Angle2 : -90.00 deg 0.00 deg Wood depth : 0 No of house rows : 0 / 0 Surface : 2 (No woods.) 0, . 2 / 55 : (Reflective ground surface) Surface Receiver source distance : 55.00 / 55.00 m Receiver height : 2.00 / 2.00 m : 1 Topography (Flat/gentle slope; no barrier) : 0.00 Reference angle Results segment # 1: Gordon St (day) Source height = 1.20 mROAD (0.00 + 61.38 + 0.00) = 61.38 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 70.03 0.00 -5.64 -3.01 0.00 0.00 0.00 61.38 -----

Segment Leq : 61.38 dBA

Total Leq All Segments: 61.38 dBA ♠ Results segment # 1: Gordon St (night) -----Source height = 1.20 m ROAD (0.00 + 54.86 + 0.00) = 54.86 dBAAngle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ -90 0 0.00 63.51 0.00 -5.64 -3.01 0.00 0.00 0.00 54.86 -----Segment Leq : 54.86 dBA Total Leq All Segments: 54.86 dBA ♠ TOTAL Leq FROM ALL SOURCES (DAY): 61.38

(NIGHT): 54.86

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ATTACHMENT C



ATTACHMENT D

Table C1 Stationary Noise Impact Source Data 785 Gordon Street, Guelph, Ontario

		Total	Data Source	Height			
		SWL	or	Absolute	Above Roof		
Noise Source Description	Cadna ID	(dBA)	Representative Data	(m)	(m)	Х	у
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562903	4819442
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562906	4819434
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562907	4819429
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562858	4819452
HVAC_2FAN	HVAC_2FAN		HVAC_2FAN	7	1.5	17562787	4819382
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562843	4819436
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	11.5	1.5	17563082	4819447
HVAC_2FAN	HVAC_2FAN		HVAC_2FAN	11.5	1.5	17563092	4819457
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	11.5	1.5	17563095	4819455
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	11.5	1.5	17563104	4819437
HVAC_2FAN	HVAC_2FAN	82.8	HVAC_2FAN	7	1.5	17562801	4819400
Rep_Chiller	Rep_Chiller	92.8	Rep_Chiller	7.5	2	17562829	4819438
Representative_MUA	Representative_MUA	80.6	Representative_MUA	11.5	1.5	17563087	4819452
Representative_MUA	Representative_MUA	80.6	Representative_MUA	11.25	1.5	17563090	4819454
Representative_MUA	Representative_MUA	80.6	Representative_MUA	6.75	1.5	17562762	4819356
Representative_MUA	Representative_MUA	80.6	Representative_MUA	6.75	1.5	17562855	4819410
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562886	4819424
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562884	4819415
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562876	4819414
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562864	4819401
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562868	4819398
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562873	4819393
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562811	4819407
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562809	4819404
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562816	4819413
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562823	4819415
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562803	4819398
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562796	4819392
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562793	4819389
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562748	4819344
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562746	4819347
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562757	4819353
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562766	4819360
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562753	4819348
Small_HVAC	Small_HVAC		Small_HVAC	6.75	1.25	17562745	4819339
Small_HVAC	Small_HVAC		Small_HVAC	6.75	1.25	17562756	4819345
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562773	4819376
Small_HVAC	Small_HVAC		Small_HVAC	6.75	1.25	17562778	4819373
Small_HVAC	Small_HVAC		Small_HVAC	6.75	1.25	17562835	4819445
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562839	4819442
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562874	4819400
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562876	4819404
Small_HVAC	Small_HVAC	81.9	Small_HVAC	9.25	1.25	17562910	4819316
Small_HVAC	Small_HVAC	81.9	Small_HVAC	9.25	1.25	17562921	4819299
Small_HVAC	Small_HVAC	81.9	Small_HVAC	9.25	1.25	17562912	4819301
Small_HVAC	Small_HVAC	81.9	Small_HVAC	9.25	1.25	17562903	4819304
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563085	4819445
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563089	4819449
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563091	4819451
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563096	4819445
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563101	4819441
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563104	4819444
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563106	4819446
Small_HVAC	Small_HVAC		Small_HVAC	11.25	1.25	17563110	4819443
Small_HVAC	Small_HVAC	81.9	Small_HVAC	6.75	1.25	17562772	4819368