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# KITCHENER LOCATION

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January 31, 2024

Habitat for Humanity Guelph Wellington Suite 100B – 104 Dawson Road Guelph, ON, N1H 1A6

Attn: Brett Daw – Director, Build

# Re: Functional Servicing Report Proposed Residential Development 303, 309 & 317 Speedvale Avenue East, Guelph, Ontario

# 1. INTRODUCTION

This Functional Servicing Report (Report) has been prepared by Strik, Baldinelli, and Moniz Ltd. (SBM) to address the requirements of the City of Guelph (City) and of the Region of Waterloo and Area Municipalities for the OPA/ZBA submission for the proposed residential development located at 303, 309 & 317 Speedvale Avenue in the City of Guelph, Ontario.

The existing approximately 0.26 ha site is bordered by the Manhattan Court Right-of-Way (ROW) to the northeast, residential lands to the southeast and southwest, and the Speedvale Avenue East ROW to the northwest.

It is SBM's understanding that the proposed development is to consist of a 6-storey apartment building with a parking garage, containing 48 total residential units (11 one-bedroom units, 17 two-bedroom units, and 20 three-bedroom units). Please refer to the attached Speedvale Affordable Housing drawings by Newton Group Ltd for Habitat for Humanity Guelph Wellington, dated December 19, 2023, and the Site Plan by SBM, provided separately.

Design requirements have been based on the City of Guelph Development Engineering Manual (DEM) dated October 2023, the region of Waterloo and Area Municipalities Design Guidelines and Supplemental Specifications for Municipal Services (DGSSMS) dated February 2023, the Ministry of Environment Conservation and Parks, Design Guidelines for Drinking-Water Systems (DGDWS), 2022, the MECP Stormwater Management Planning and Design Manual (SWMPDM), and the current edition of the Ontario Building Code (OBC).

# 2. WATER SERVICING

Based on the City of Guelph As-Recorded Drawing No. M-737A, dated May 2008, provided in Appendix A, there is an existing municipal 150 mm watermain adjacent to the subject site located within the Manhattan Court ROW. It is proposed to service the subject site via a 150 mm service which is to be connected to the existing 150 mm watermain in the Manhattan Court ROW.

# 2.1 Domestic Water Supply

As per the Speedvale Affordable Housing drawings by Newton Group Ltd, provided in Appendix A, the proposed multi-residential building consists of 48 units with 105 total bedrooms. The occupancy was calculated for two cases; using 2 people per bedroom as per OBC 3.1.17.1(b) and using 1.86 people per unit as per the City of Guelph's DEM. The OBC occupancy was taken to be conservative, for a total estimated population of 210 people. Maximum hour



SBM-23-1518

domestic demand (calculated as per MECP DGDWS) for the total occupancy load of 210 people is 148 L/min (2.46 L/s). Please refer to the Domestic Water Demand, Velocity, and Turnover calculations, attached in Appendix B.

# 2.2 Water Supply for Fire Protection

As per the Region's DGSSMS, Section B.2 requires the minimal residual pressure during Maximum Day plus Fire scenario to be not less than 140 kPa (20 psi) at any location in the water distribution system.

A fire hydrant flow test was performed at Speedvale Avenue East on December 8, 2023, with results in included in Appendix B. The flow test results show that the static pressure of the water distribution system is 60 psi (413.69 kPa) and the residual pressures are 59 psi (406.79 kPa) and 58 psi (399.90 kPa) at the test flow rates of 4,402 L/min (1,163 USGPM) and 7,188 L/min (1,899 USGPM), respectively.

A sprinkler system is required for the proposed development, and therefore the fire-fighting demand is determined as per NFPA-13 (relevant information included in Appendix B). As the proposed building will have 'Light Hazard Occupancy' (for residential occupancy) and 'Ordinary Hazard Occupancy – Group 1 (for the parking structure), the proposed building is conservatively determined to have the 'Ordinary Hazard Occupancy – Group 1' (refer to Annex A - Section A.5.3.1 of the NFPA-13). Section B.2.3.4 of the Region's DGSSMS requires that the maximum velocity shall not exceed 5.0 m/s under all flow conditions. Under fire-flow + maximum day demand of 1,991 L/min with a 150 mm diameter water service, the anticipated velocity was calculated to be 1.88 m/s, which adheres to the design standards. Please refer to the Fire Flow (NFPA-13) calculations and pressure loss calculations, provided in Appendix B.

As per the NFPA-13 and the OBC Part 3 requirements, the fire hydrant(s) shall be located 45m from the building's Siamese connection. As there is an existing hydrant within 45 m from the 'Fire Department Connection' on Speedvale Avenue E, and the fire flow and pressure loss calculations show that the proposed water distribution system can provide the calculated minimum required water supply flow rate, adequate fire protection is available for the proposed development.

# 2.3 Capacity Review

As shown in the Fire Flow calculations provided in Appendix B, the water pressure in the Speedvale Ave ROW at the required flow of 1,991 L/min (fire flow + maximum day demand), including losses (refer to Hazen Williams Pressure Loss Calculations attached to this Study) will be approximately 431.88 kPa (62.64 psi). The final pressure in the sprinkler system will be calculated by the sprinkler system designer, upon sprinkler system layout completion (Mechanical scope of work). Additionally, the sprinkler system designer is to confirm if a 150 mm water service is sufficient to provide the required final pressure in the sprinkler system, upon sprinkler system layout completion.

The water pressure under the fire fighting condition is approximately 62.64 psi, which is larger than 20 psi and less than 80 psi, and therefore meets the requirements as per the DGSSMS.

The fire flow calculations demonstrate that the proposed water distribution system can provide the minimum required water supply flow rate under the fire flow plus maximum day demand scenario, therefore there is adequate water supply available for the proposed development. These calculations are to be confirmed at the time of detailed design.

# 3. SANITARY SERVICING

Based on the City of Guelph As-Recorded Drawing No. M-737A, dated May 2008, provided in Appendix A, there is an existing 300mm diameter municipal sanitary sewer at 3.5% located within the Speedvale Avenue E ROW. It is proposed that a new 200 mm sanitary service at 2.0% will convey sanitary flows from the proposed residential building to the existing 300mm sanitary sewer located on the Speedvale Avenue East ROW.

3.1 Design Flows per OBC

As per the attached Speedvale Affordable Housing drawings by Newton Group Ltd, the proposed multi-residential building consists of 48 units with 105 total bedrooms, for a total population of 210 people as calculated in section 2.1 of this report. This is multiplied by the average usage of 300 L/day/capita or 0.00347 L/s/capita and the Harmon

peaking factor "F" of 4.14. Adding the infiltration allowance of 0.06 L/sec yields a peak design flow for the building of 2.98 L/s, which can be conveyed by the proposed 200 mm pipe at 2.0% which has a capacity of 46.36 L/s, as shown in calculations provided in Appendix C. Therefore, the proposed sanitary connection has sufficient capacity to service the proposed development.

# 4. STORMWATER MANAGEMENT AND STORM SERVICING

# 4.1 Rainfall Intensity Duration Frequency (IDF) Storm Parameters

Rainfall intensity duration frequency (IDF) storm parameters for the City of Guelph were obtained from the City's Development Engineering Manual (October 2023) from Table 5-2.

# 4.2 Pre-development Conditions

Pre-development conditions were obtained from the Plan of Survey Showing Topographic Features by J.D. Barnes Ltd., dated June 22, 2023. Under pre-development conditions, the approximately 0.26 ha site located at 303, 309 and 317 Speedvale Avenue E consists of one commercial property, two single-family dwellings, and a garage, with associated parking areas and landscaping. As per SWM calculations in Appendix D, the pre-development site has a calculated C-value of 0.64.

From the topographic survey, grading conveys flows on the subject site into the Speedvale ROW. A smaller portion of flows are directed south into the Manhattan Court ROW, where flows are ultimately directed back into the existing 1500mm storm sewer in the Speedvale ROW, as shown in City Drawing No. 2-A-50 (provided in Appendix A). As such, the subject site has been taken as a single pre-development catchment area that is ultimately tributary to the existing 1500 mm diameter storm sewer in the Speedvale ROW.

# 4.3 Post-development Conditions

Post-development conditions were obtained from the Site Plan by SBM, provided separately. Under postdevelopment conditions, the entire site will be comprised of a 6-storey residential apartment building, and associated drive aisles, amenity space, and landscaping, for a post-development C-value for the entire site of 0.80. As per the City's DEM, post-development flows are to be attenuated to pre-development levels.

# 4.4 Storm Servicing

Based on the City of Guelph As-Recorded Drawing No. M-737A, dated May 2008, provided in Appendix A, there is an existing 1500 mm diameter municipal storm sewer at 0.86% located within the Speedvale Avenue E ROW. The subject site is proposed to be serviced via a 250 mm service at 0.69%. Flows are to be restricted by flow-controlled roof drains on top of the building, and by a raised-outlet at CBMH2, which will allow flows to infiltrate via the proposed linear infiltration gallery, in order to meet City infiltration targets, as detailed in the sections below.

No additional surface flows are to be introduced into the City ROW, and as such, any excess storm flows produced by the subject site are to be stored on-site and released at pre-development levels, mimicking existing conditions.

# 4.5 Stormwater Management – Quantity Control

As shown in the attached stormwater management (SWM) calculations, due to the increase in impervious cover, increased stormwater runoff from the site is anticipated and formal SWM quantity controls are proposed to be implemented. These controls are to attenuate post-development flows of the 2 to 100-year to the pre-development levels and to allow infiltration for the runoff that is generated from 5 mm of rainfall, as per Guelph's Development Engineering Manual. SWM quality controls will be implemented to provide Enhanced Level treatment levels as per the MECP SWM Planning and Design Manual. SWM quantity and quality controls demonstrating compliance with the SWM criteria and environmental targets identified will be addressed at the time of detailed design.

As per Guelph's Stormwater Control Criteria Map, the subject site falls within the City-Wide Policy Area #13. The infiltration targets for this area require 5 mm to be infiltrated on site. Based on the total site area of 0.26 ha, the above requirement results in an infiltration volume of 13.01 m<sup>3</sup>. It is proposed to install a 48 m long linear infiltration trench between CBMH2 and CBMH3, which is sufficient to infiltrate the required volume, as shown in the SWM

calculations provided in Appendix D. The exact infiltration rate is to be confirmed prior to detailed design via a geotechnical engineer, and the proposed infiltration methodology is to be revised if required at the time of detailed design to ensure the City's infiltration targets are met.

The site has been designed for a C-value equal to 0.640. as per the pre-development conditions, which translates to a maximum allowable release rate of 67.46 L/s for the 2-year event and 141.21 L/s for the 100-year event.

Catchment U201 (484.67 m<sup>2</sup>) is comprised of the north side of the proposed development, which is mostly landscaped area. Flows from this small uncontrolled catchment area (7.55 L/s and 15.81 L/s for the 2-year and 100-year event respectively) are directed into the Speedvale Avenue E ROW, and these minimal uncontrolled flows are not anticipated to significantly impact the subject site nor the surrounding properties, as it matches the pre-existing site condition.

As shown in the attached SWM calculations in Appendix D, the resulting restricted post-development flow rates were calculated by subtracting the uncontrolled flows from the allowable flow rate. This results in maximum allowable restricted flow rates of 59.91 L/s and 125.40 L/s for the 2-year and 100-year events respectively.

Catchment A201 (853.84 m<sup>2</sup>) is comprised of the building rooftop, resulting in a C-value of 0.90. Flows within this catchment are to be restricted via 3 flow-controlled roof drains, which are to be coordinated with the mechanical design team. Each drain is proposed to release a peak flow of 1.5 L/s, for a total peak release of 4.5 L/s for the entire catchment. The rooftop storage volume was conservatively calculated by multiplying the area of the roof by the maximum water depth of 0.15 m and dividing by three. This results in an estimated storage volume of 42.69 m<sup>3</sup>, of which 12.70 m<sup>3</sup> and 24.55 m<sup>3</sup> are required to store the 2-year and 100-year storm events respectively. The restricted flows from this catchment are to be directed through the building and into area A202 underground via the proposed 250 mm connection from the building to the linear infiltration gallery.

Catchment A202 (1,263.31 m<sup>2</sup>) is comprised of the at-grade parking area. The small portion of landscaped area in this catchment has been conservatively ignored, and as such, the C-value was taken to be 0.90. The proposed parking lot is graded to direct flows into either CBMH2 or CBMH3, where flows will enter the proposed infiltration gallery. A raised outlet in CBMH2 is provided, as detailed on Engineering Drawing C3, to keep flows within the infiltration gallery until it is full. This allows for retention and infiltration onsite for 5 mm of rainfall, as per City of Guelph Development Engineering Manual (DEM) October 2023, Appendix G, while still allowing any overflow to drain towards the municipal sewer system. Based on the total site area of 0.26 ha, the above requirement results in an infiltration volume of 13.01 m<sup>3</sup> that is to be stored and infiltrated on-site. The exact infiltration rate of the soil is unknown and was estimated using the borehole results of the Geotechnical Investigation by CMT Engineering, dated August 3, 2023, provided separately. Detailed calculations and design of the infiltration gallery is to be completed at the time of detailed design for site plan approval when the exact infiltration rate of the soil onsite is known.

As shown in the SWM calculations provided in Appendix D, the volume of infiltrated water exceeds the required 13.01 m<sup>3</sup>, and there is sufficient storage within the proposed on-site storm system to attenuate the flows to a peak flow rate of 47.70 L/s for the 2-year to 100-year storm events, which is below the allowable rates of 59.91 L/s and 125.40 L/s for the 2-year and 100-year events respectively.

# 4.6 Stormwater Management – Quality Control

SWM quality controls will be implemented to provide Enhanced Level treatment levels (80% removal) as per the MECP SWM Planning and Design Manual. SWM quantity and quality controls demonstrating compliance with the SWM criteria and environmental targets identified will be addressed at the time of detailed design for Site Plan Approval.

An oil-grit separator (OGS) is proposed for the subject site to meet the above targets. Therefore, an FD-4HC OGS unit (or approved equivalent) is proposed to provide 80% TSS removal for quality control for flows that exit the site via the overflow pipe, and is ETV certified as required per Guelph's DEM. Please see Appendix D for details.

Post-development stormwater flows will be restricted to the pre-development levels during the 2 to 100-year design storm events. Major Overland Flows from the 100-year storm event will be safely conveyed overland northeast to the Manhattan Court ROW, generally matching pre-development conditions. A Preliminary Grading Plan prepared by

SBM has been provided to demonstrate the grading feasibility and intent for the subject site. Detailed SWM calculations, infiltration design, and grading plans will be prepared at the time of detailed design for Site Plan Approval.

# 5. LIMITATIONS

This report was prepared by SBM for the City of Guelph and Habitat for Humanity Guelph Wellington. Use of this report by any third party, or any reliance upon its findings, is solely the responsibility of that party. SBM accepts no responsibility for damages, if any, suffered by a third party as a result of decisions made or actions undertaken as a result of this study. Third party use of this study, without the express written consent of the Consultant, denies any claims, whether in contract, tort, and/or any other cause of action in law, against the Consultant.

All findings and conclusions presented in this report are based on site conditions as they appeared during the period of the investigation. This report is not intended to be exhaustive in scope, or to imply a risk-free facility. It should be recognized that the passage of time may alter the opinions, conclusions, and recommendations provided herein.

The design was limited to the documents referenced herein and on the SBM drawings provided separately. SBM accepts no responsibility for the accuracy of the information provided by others. All designs and recommendations presented in this study are based on the information available at the time of the review.

This document is deemed to be the intellectual property of SBM in accordance with Canadian copyright law.

# 6. CLOSURE

We trust this report meets your satisfaction. Should you have any questions or require further information, please do not hesitate to contact us.

Respectfully submitted,

# Strik, Baldinelli, Moniz Ltd.

Planning • Civil • Structural • Mechanical • Electrical

Hasan Ahmad, M. Eng., P. Eng. Civil Eng III

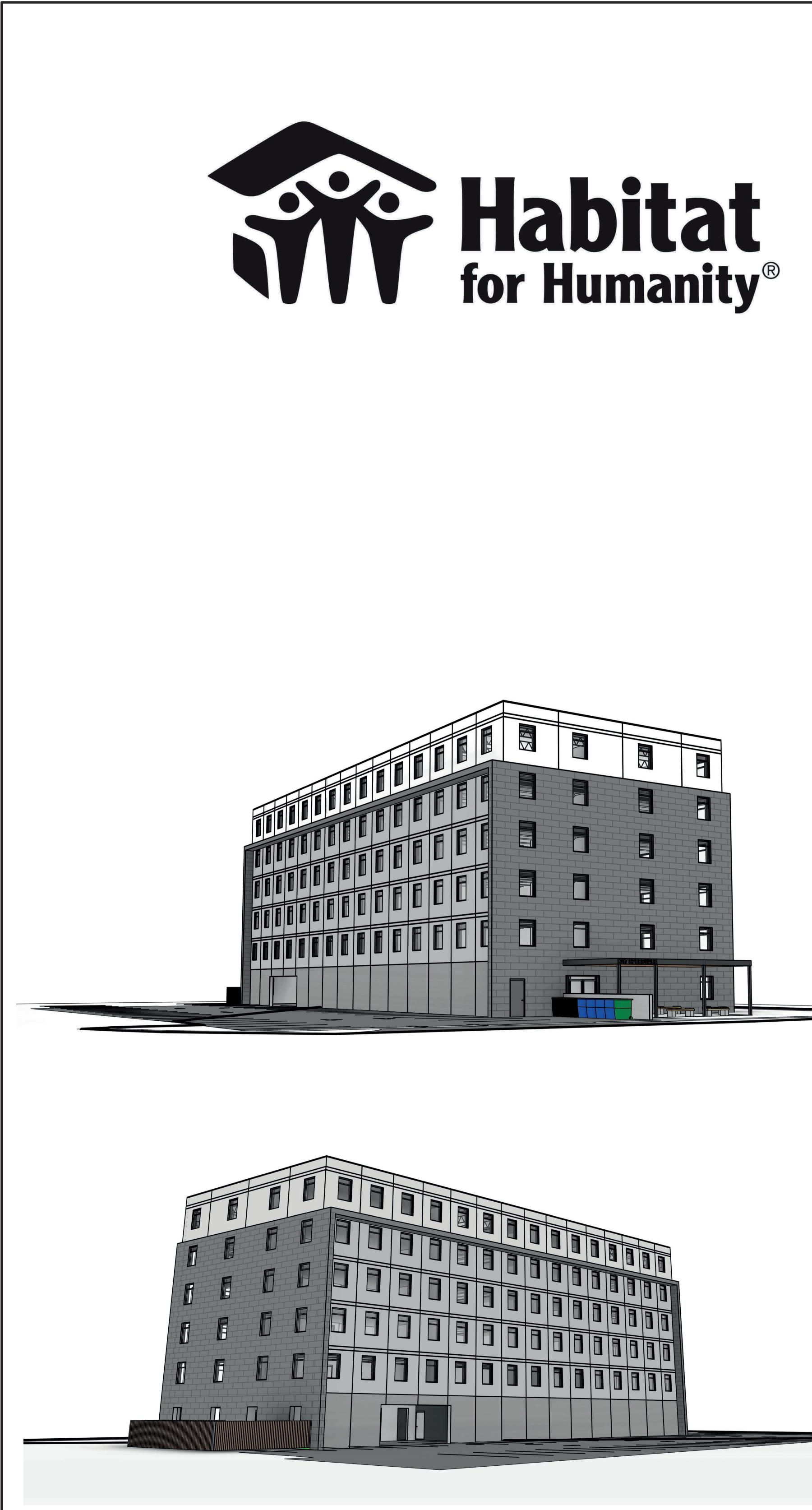
Tara Morton-Bernas Civil Project Lead, Tech V

I anderse

Lauren Andersen Civil Engineering Trainee I

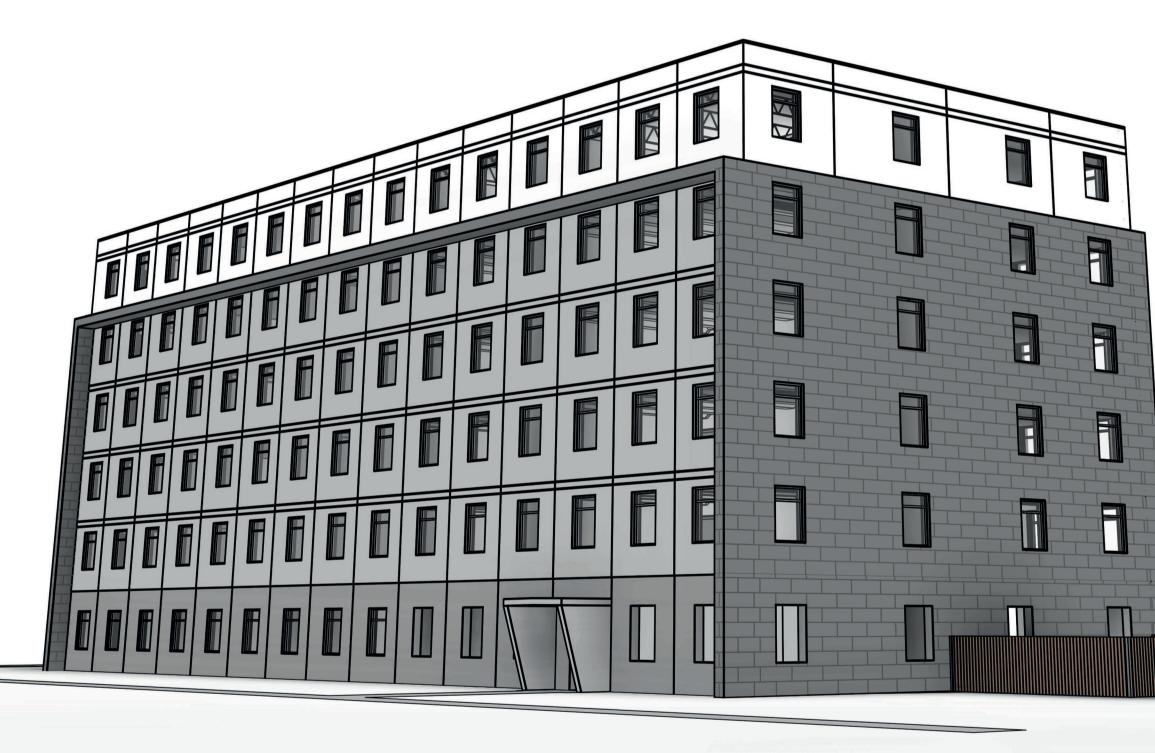
# APPENDIX A

Speedvale Affordable Housing Drawings by Newton Group Ltd., dated December 19, 2023 Plan of Survey Showing Topographic Features by J.D. Barnes Ltd., dated June 22, 2023 City of Guelph As-Recorded Drawing No. M-737A, dated May 2008 City of Guelph Drawing No. 2-A-50



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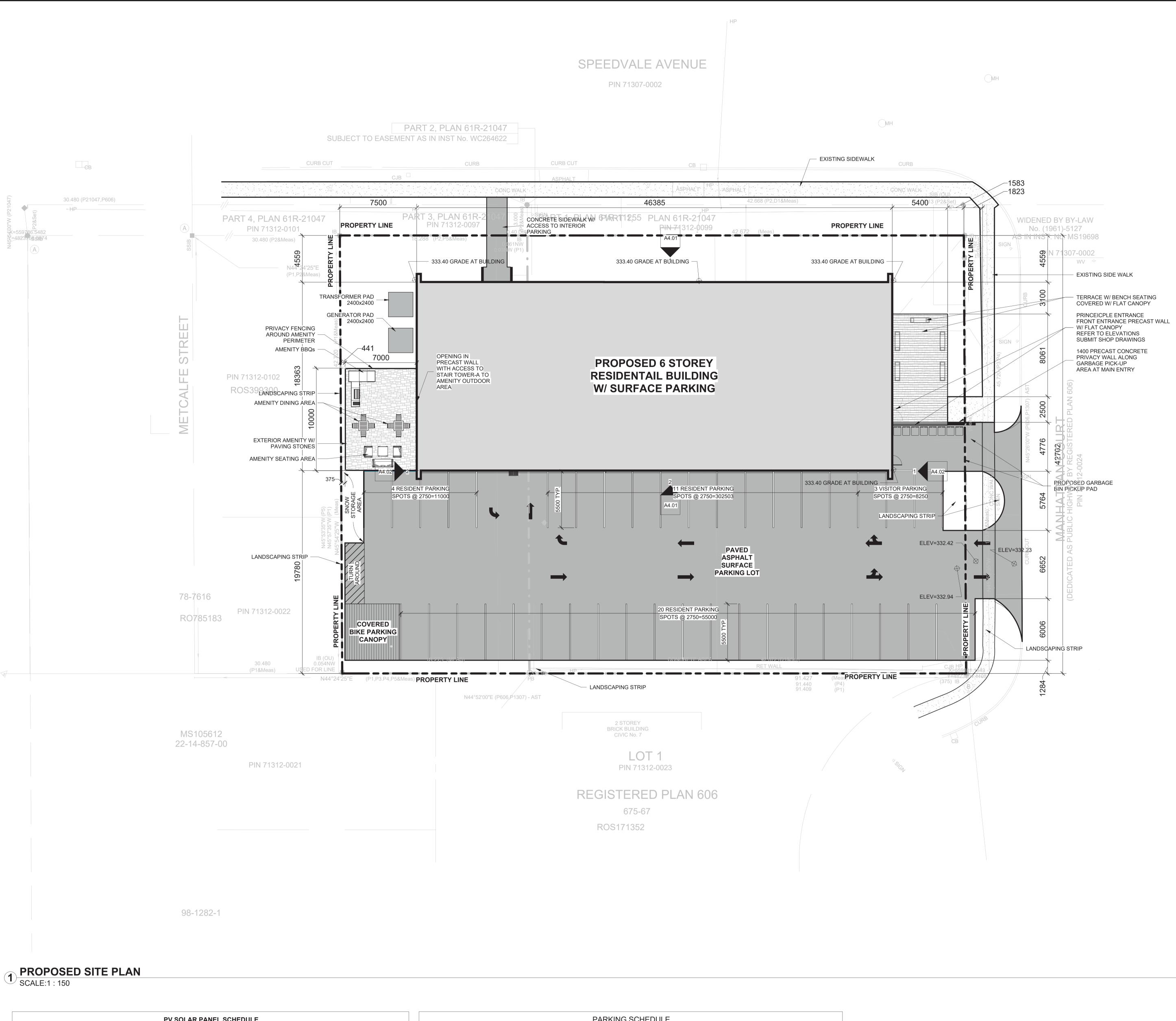


# ARCHITECTURAL DRAWING SHEET LISTSHEET NAMESHEET ISSUED DATEREV. #

| A1.00 | SITE PLAN                       | 23/08/25 | E |
|-------|---------------------------------|----------|---|
| A0.00 | COVER PAGE                      | 23/08/25 | E |
| A2.01 | BASEMENT MAIN LEVEL & LEVEL 1.0 | 23/08/25 | E |
| A2.03 | LEVEL 2.0 AND 3.0 FLOOR PLAN    | 23/08/25 | E |
| A3.01 | BUILDING SECTIONS               | 23/08/25 | E |
| A4.01 | BUILDING ELEVATIONS             | 23/08/25 | E |
| A4.02 | BUILDING ELEVATIONS             | 23/08/25 | E |
| A2.04 | LEVEL 4.0 AND 5.0 FLOOR PLAN    | 03/01/22 | E |
| A2.05 | ROOF LEVEL                      | 23/08/25 | E |
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SHEET NUMBER

|  | Ar Massey RD.<br>GUELPH, ON<br>N1H 7M6<br>TEL: (519)822-5281<br>FAX: (519)823-6332<br>www.kiwinewton.com  |
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| 23-12-19<br>23-12-19<br>23-12-19<br>23-12-19<br>23-12-19<br>23-12-19<br>23-12-19 | PROJECT<br>SPEEDVALE AFFORDABLE<br>HOUSING<br>MANHATTAN COURT & SPEEDVALE AVE E<br>GUELPH, ON<br>POSTAL CODE [TBD]<br>DRAWING   |
| 23-12-19<br>23-12-19   | COVER PAGE PROJECT NO.: 23136 PROJECT DATE: 2023-07-20 DRAWN BY: CVL  |
|  | CHECKED BY:<br>CK/PH<br>SCALE:<br>AS NOTED<br>DRAWING NO.   |



| PV SOLAR PANEL SCHEDULE             |             |                |       |             |                |                   |
|-------------------------------------|-------------|----------------|-------|-------------|----------------|-------------------|
| PANEL TYPE                          | Level       | LEVEL COMMENTS | Count | PANEL ANGLE | COMMENTS       |                   |
| PV_SOLAR PANEL 1000 x 2000 (ANGLED) | U/S OF DECK | APARTMENT ROOF | 224   | FLUSH MOUNT | BALLAST SYSTEM | TYP. STALL VISITO |
| TOTAL PANELS=: 224                  |             |                | 224   |             |                | TYP. ACC. STALL-A |



ROOM NAI

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| PARKING SCHEDULE           |                         |           |  |  |  |  |
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| STALL TYPE                 | PARKING LEVEL REFERENCE | STALL QTY | COMMENTS   |  |  |  |
|                            |                         | ·         |  |  |  |  |
| TORS CoG-2.75m x 5.5m      | EXTERIOR PARKING        | 2         | SPOTS NOT ACCESSIBLE DURING GARBAGE PICK-UP TIME |  |  |  |
| L-A CoG-3.4m x 5.50m       | INTERIOR PARKING        | 1         |  |  |  |  |
| L-B CoG-2.75m x 5.50m      | INTERIOR PARKING        | 1         |  |  |  |  |
| SIDENT CoG-2.75m x 5.5m    | INTERIOR PARKING        | 38        |  |  |  |  |
| L CoG-2.65x5.5m            | INTERIOR PARKING W/ EV  | 1         |  |  |  |  |
| SIDENT CoG-2.75m x 5.5m    | INTERIOR PARKING W/ EV  | 3         |  |  |  |  |
| SIDENT EV CoG-2.75m x 5.5m | INTERIOR PARKING W/ EV  | 2         |  |  |  |  |
| :                          |                         | 48        |  |  |  |  |
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| AMENITY AREA SCHEDULE |             |           |                     |          |  |
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| IAME                  | ROOM NUMBER | AREA (m2) | AREA (ft2)          | LOCATION |  |
|                       |             |           |                     |          |  |
| <u> </u>              | 107         | 55 m²     | 594 ft <sup>2</sup> | INTERIOR |  |
| AREA                  | N/A         | 70 m²     | 753 ft <sup>2</sup> | EXTERIOR |  |
| ITY AREA              | N/A         | 57 m²     | 614 ft²             | EXTERIOR |  |
|                       |             |           |                     |          |  |

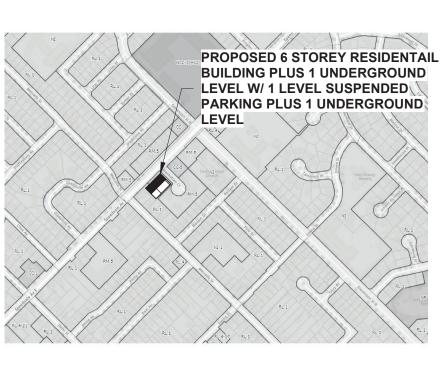
| BUILDING   |                   |                   |
|--|-------------------|-------------------|
| ROOM NAME  | ROOM<br>#         | OCCUPANCY<br>TYPE |
|  |                   |                   |
| Not Placed<br>M&E SHAFT  | 112               |                   |
| M&E SHAFT  | 113               |                   |
| Not Placed: 2  | 110               |                   |
| BASEMENT   |                   |                   |
| VESTIBULE  | 101               |                   |
| OFFICE   | 102               |                   |
| 2 BEDROOM UNIT   | 104               |                   |
| 1 BEDROOM+DEN UNIT   | 105               |                   |
| 2 BEDROOM UNIT AMENITY SPACE   | 106               |                   |
| MECHANICAL AND ELECTRICAL ROOM   | 107               |                   |
| STORAGE LOCKERS  | 100               |                   |
| GARBAGE/RECYCLE ROOM   | 110               |                   |
| COORDOR  | 111               |                   |
| STAIR TOWER-B  | 314               |                   |
| TERRACE AMENITY AREA   | N/A               |                   |
| DINING AMENITY AREA  | N/A               |                   |
| STAIR TOWER-A  | TBD               |                   |
| ELEVATOR SHAFT<br>BASEMENT: 15   | TBD               |                   |
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| LEVEL 1.0<br>2 BEDROOM UNIT  | 101               |                   |
| 3 BEDROOM UNIT   | 101               |                   |
| 1 BEDROOM+DEN UNIT   | 103               |                   |
| 2 BEDROOM UNIT   | 104               |                   |
| 1 BEDROOM UNIT   | 105               |                   |
| 3 BEDROOM UNIT   | 106               |                   |
| 2 BEDROOM UNIT   | 107               |                   |
| 3 BEDROOM UNIT   | 108               |                   |
| 3 BEDROOM UNIT<br>LEVEL 1.0: 9   | 109               |                   |
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| LEVEL 2.0<br>2 BEDROOM UNIT  | 201               |                   |
| 3 BEDROOM UNIT   | 201               |                   |
| 1 BEDROOM+DEN UNIT   | 203               |                   |
| 2 BEDROOM UNIT   | 204               |                   |
| 1 BEDROOM UNIT   | 205               |                   |
| 3 BEDROOM UNIT   | 206               |                   |
| 2 BEDROOM UNIT   | 207               |                   |
| 3 BEDROOM UNIT<br>3 BEDROOM UNIT   | 208               |                   |
| LEVEL 2.0: 9   | 209               |                   |
| LEVEL 3.0  |                   |                   |
| 2 BEDROOM UNIT   | 301               |                   |
| 3 BEDROOM UNIT   | 302               |                   |
| 1 BEDROOM+DEN UNIT   | 303               |                   |
| 2 BEDROOM UNIT   | 304               |                   |
| 1 BEDROOM UNIT   | 305               |                   |
| 3 BEDROOM UNIT   | 306               |                   |
| 2 BEDROOM UNIT<br>3 BEDROOM UNIT   | 307<br>308        |                   |
| 3 BEDROOM UNIT   | 309               |                   |
| LEVEL 3.0: 9   | 000               |                   |
| LEVEL 4.0  |                   |                   |
| 2 BEDROOM UNIT   | 401               |                   |
| 3 BEDROOM UNIT   | 402               |                   |
| 1 BEDROOM+DEN UNIT   | 403               |                   |
| 2 BEDROOM UNIT<br>1 BEDROOM UNIT   | 404               |                   |
| 3 BEDROOM UNIT   | 405               |                   |
| 2 BEDROOM UNIT   | 407               |                   |
| 3 BEDROOM UNIT   | 408               |                   |
| 3 BEDROOM UNIT   | 409               |                   |
| LEVEL 4.0: 9   |                   |                   |
| LEVEL 5.0  |                   |                   |
| 2 BEDROOM UNIT   | 501               |                   |
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| 1 BEDROOM+DEN UNIT   | 504               |                   |
| 2 BEDROOM UNIT   |                   |                   |
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| 2 BEDROOM UNIT<br>1 BEDROOM UNIT<br>3 BEDROOM UNIT<br>2 BEDROOM UNIT<br>3 BEDROOM UNIT | 506<br>507<br>508 |                   |
| 2 BEDROOM UNIT<br>1 BEDROOM UNIT   | 506<br>507        |                   |

685 m²

4022 m²

 LEVEL 5.0
 88 m²

 LEVEL 5.0
 97 m²



1 BEDROOM UNIT 1 BEDROOM+DEN UNIT

2 BEDROOM UNIT

**3 BEDROOM UNIT** 

TOTAL UNITS: 48

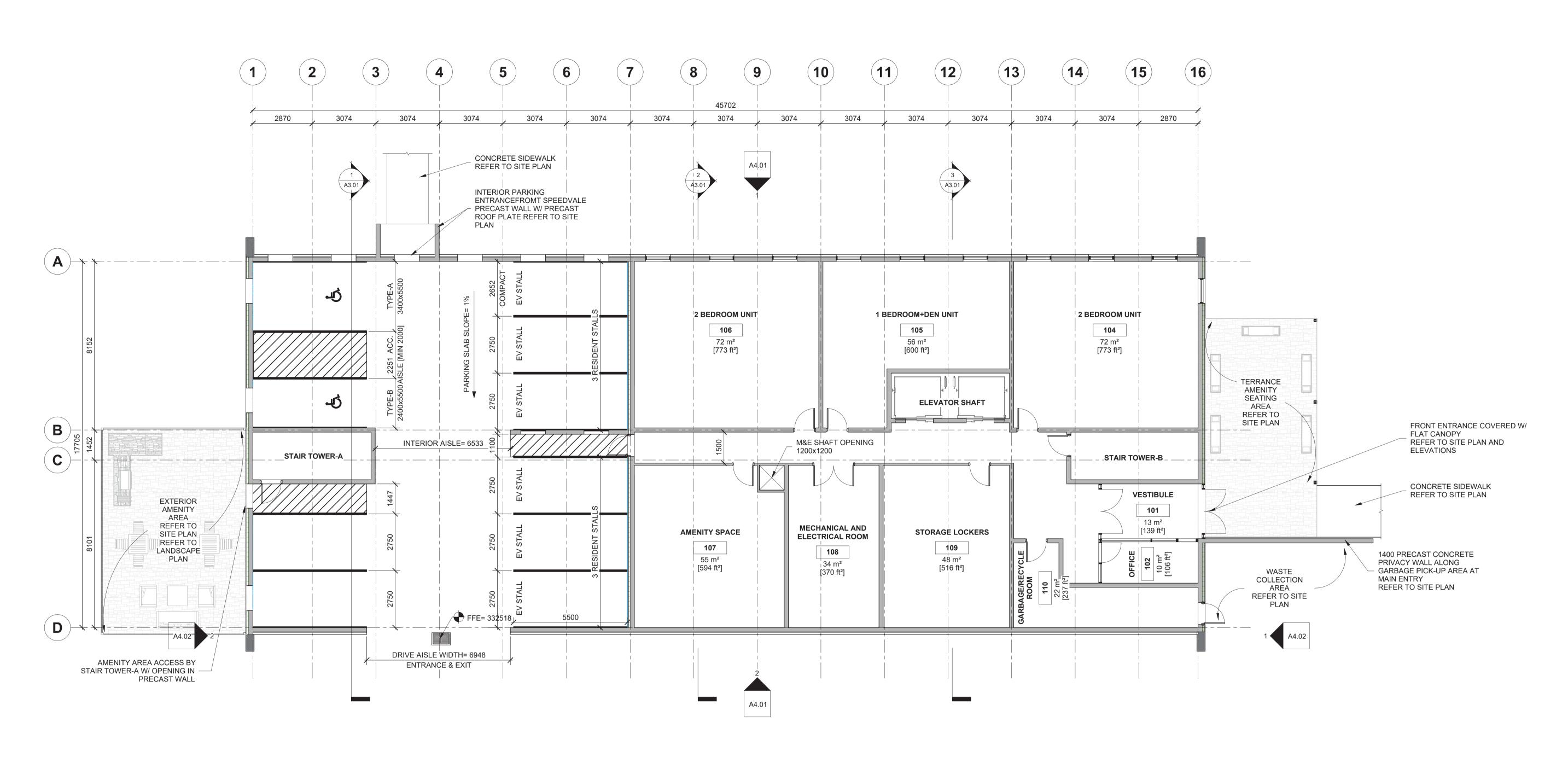
SITE KEY PLAN SCALE: 1 : 50

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|------------------|------------------|----------|--|
| ROOM NAM         | 5<br>JNIT 6<br>1 |          |  |
| DROOM UNIT       | 2                | <u>ر</u> |  |
| G BASE<br>FINISH | WALL<br>FINISH   | COMMENTS |  |
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|                  |                  |          | B       23-12-19       REISSUED FOR SPA PRE-CONSULTATION         A       23-08-25       ISSUED FOR SPA PRE-CONSULTATION         #       DATE       DESCRIPTION |
|                  |                  |          |  |
|                  |                  |          | PROJECT<br>SPEEDVALE AFFORDABI   |
|                  |                  |          | HOUSING<br>MANHATTAN COURT & SPEEDVALE AVE E<br>GUELPH, ON<br>POSTAL CODE [TBD]  |
|                  |                  |          | DRAWING<br>SITE PLAN   |

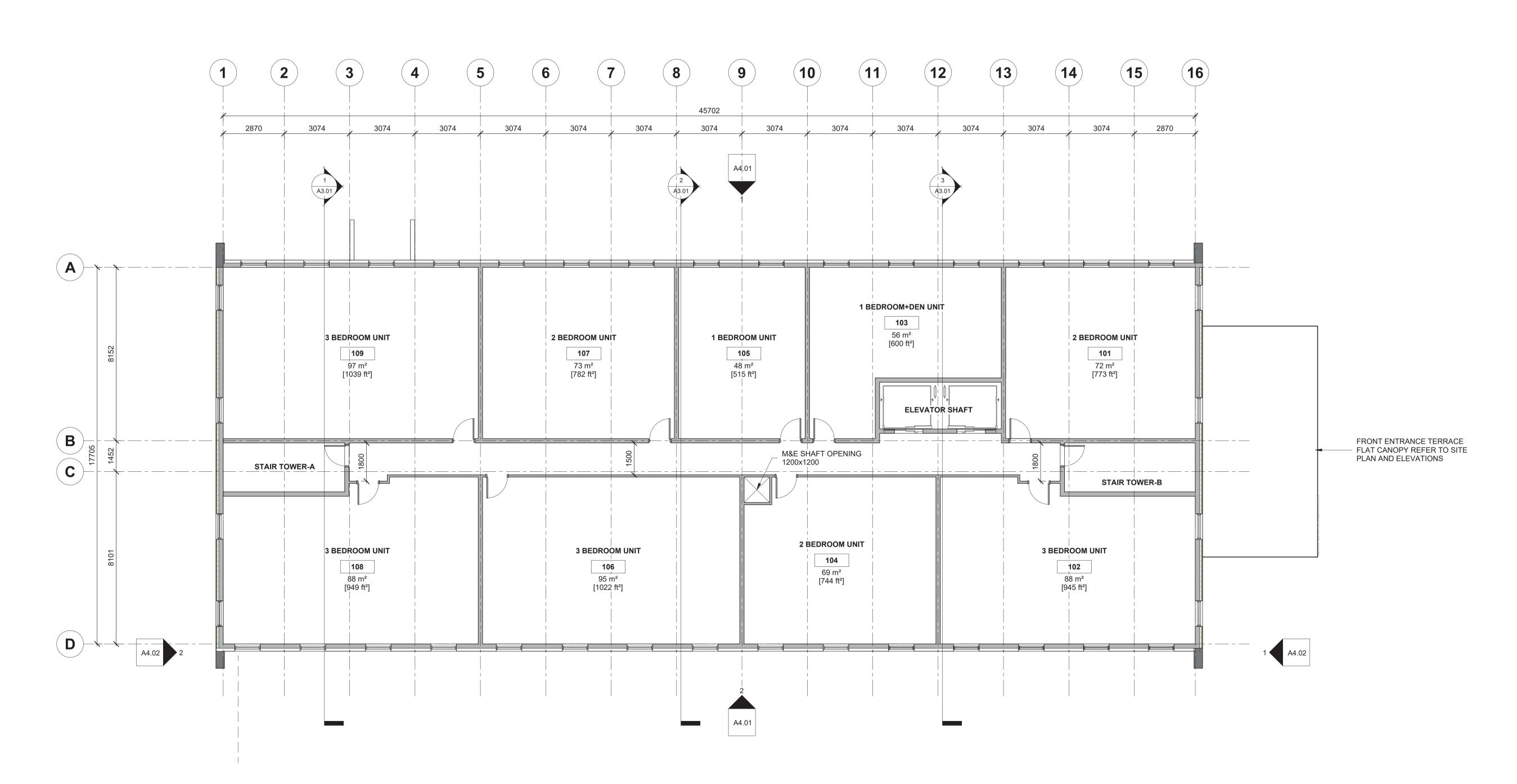
| CCUPANCY | LEVEL                  | ROOM                                    | CEILING | BASE   | WALL   | COMMENTS |
|----------|------------------------|---|---------|--------|--------|----------|
| TYPE     | REFERENCE              | AREA                                    | FINISH  | FINISH | FINISH |          |
|          |                        |   |         |        |        |          |
|          | Not Placed             | Not Placed                              |         |        |        |          |
|          | Not Placed             | Not Placed                              |         |        |        |          |
|          |                        | 0 m-                                    |         |        |        |          |
|          |                        |   |         |        |        |          |
|          | BASEMENT               | 13 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT<br>BASEMENT   | 10 m <sup>2</sup><br>72 m <sup>2</sup>  |         |        |        |          |
|          | BASEMENT               | 56 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT               | 72 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT               | 55 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT<br>BASEMENT   | 34 m <sup>2</sup><br>48 m <sup>2</sup>  |         |        |        |          |
|          | BASEMENT               | 22 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT               | 51 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT               | 14 m²                                   |         |        |        |          |
|          | BASEMENT<br>BASEMENT   | 57 m <sup>2</sup><br>70 m <sup>2</sup>  |         |        |        |          |
|          | BASEMENT               | 13 m <sup>2</sup>                       |         |        |        |          |
|          | BASEMENT               | 13 m <sup>2</sup>                       |         |        |        |          |
|          |                        | 600 m²                                  |         |        |        |          |
|          |                        |   |         |        |        |          |
|          | LEVEL 1.0              | 72 m²                                   |         |        |        |          |
|          | LEVEL 1.0              | 88 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 1.0              | 56 m²                                   |         |        |        |          |
|          | LEVEL 1.0              | 69 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 1.0<br>LEVEL 1.0 | 48 m <sup>2</sup><br>95 m <sup>2</sup>  |         |        |        |          |
|          | LEVEL 1.0              | 73 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 1.0              | 88 m²                                   |         |        |        |          |
|          | LEVEL 1.0              | 97 m²                                   |         |        |        |          |
|          |                        | 685 m²                                  |         |        |        |          |
|          |                        |   |         |        |        |          |
|          | LEVEL 2.0              | 72 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 2.0              | 88 m²                                   |         |        |        |          |
|          | LEVEL 2.0              | 56 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 2.0<br>LEVEL 2.0 | 69 m <sup>2</sup><br>48 m <sup>2</sup>  |         |        |        |          |
|          | LEVEL 2.0              | 95 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 2.0              | 73 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 2.0              | 88 m²                                   |         |        |        |          |
|          | LEVEL 2.0              | 97 m <sup>2</sup>                       |         |        |        |          |
|          |                        | 685 m²                                  |         |        |        |          |
|          | LEVEL 3.0              | 72 m²                                   |         |        |        |          |
|          | LEVEL 3.0              | 88 m²                                   |         |        |        |          |
|          | LEVEL 3.0              | 56 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 3.0<br>LEVEL 3.0 | 69 m <sup>2</sup><br>48 m <sup>2</sup>  |         |        |        |          |
|          | LEVEL 3.0              | 95 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 3.0              | 73 m²                                   |         |        |        |          |
|          | LEVEL 3.0              | 88 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 3.0              | 97 m <sup>2</sup><br>685 m <sup>2</sup> |         |        |        |          |
|          |                        | 000 111                                 |         |        |        |          |
|          |                        |   |         |        |        |          |
|          | LEVEL 4.0              | 72 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 4.0<br>LEVEL 4.0 | 88 m <sup>2</sup><br>56 m <sup>2</sup>  |         |        |        |          |
|          | LEVEL 4.0              | 69 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 4.0              | 48 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 4.0              | 95 m²                                   |         |        |        |          |
|          | LEVEL 4.0              | 73 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 4.0<br>LEVEL 4.0 | 88 m <sup>2</sup><br>97 m <sup>2</sup>  |         |        |        |          |
|          |                        | 685 m <sup>2</sup>                      |         |        |        |          |
|          |                        |   |         |        |        |          |
|          | LEVEL 5.0              | 72 m²                                   |         |        |        |          |
|          | LEVEL 5.0              | 88 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 5.0              | 56 m²                                   |         |        |        |          |
|          | LEVEL 5.0              | 69 m <sup>2</sup>                       |         |        |        |          |
|          | LEVEL 5.0<br>LEVEL 5.0 | 48 m <sup>2</sup><br>95 m <sup>2</sup>  |         |        |        |          |
|          | LEVEL 5.0              | 73 m <sup>2</sup>                       |         |        |        |          |

PROJECT NO.: 23136 PROJECT DATE: 2023-07-20 DRAWN BY: CHECKED BY: As indicated ...  $\overline{\mathbf{A}}$ 

DRAWING NO. **A1.00** 

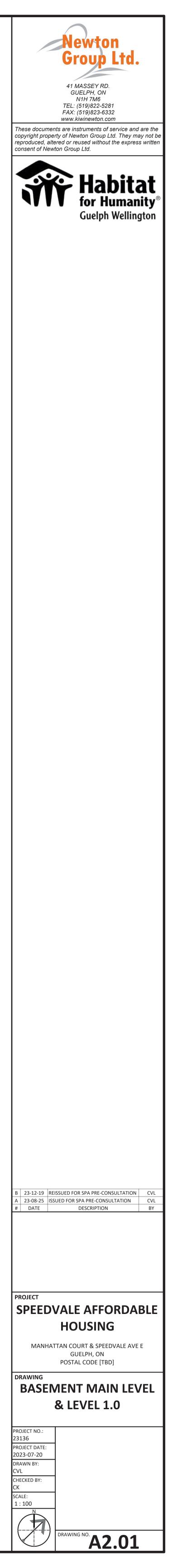


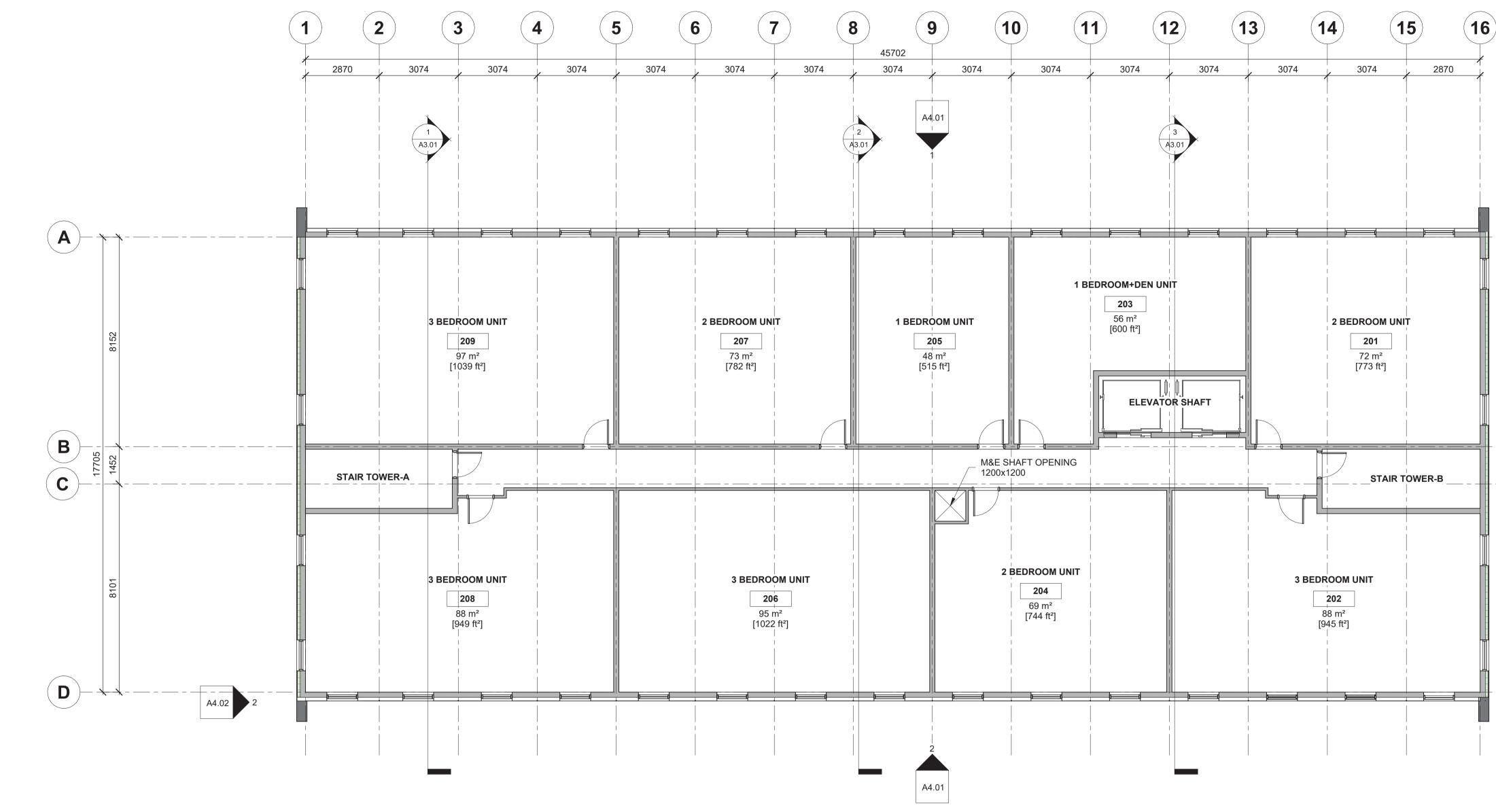




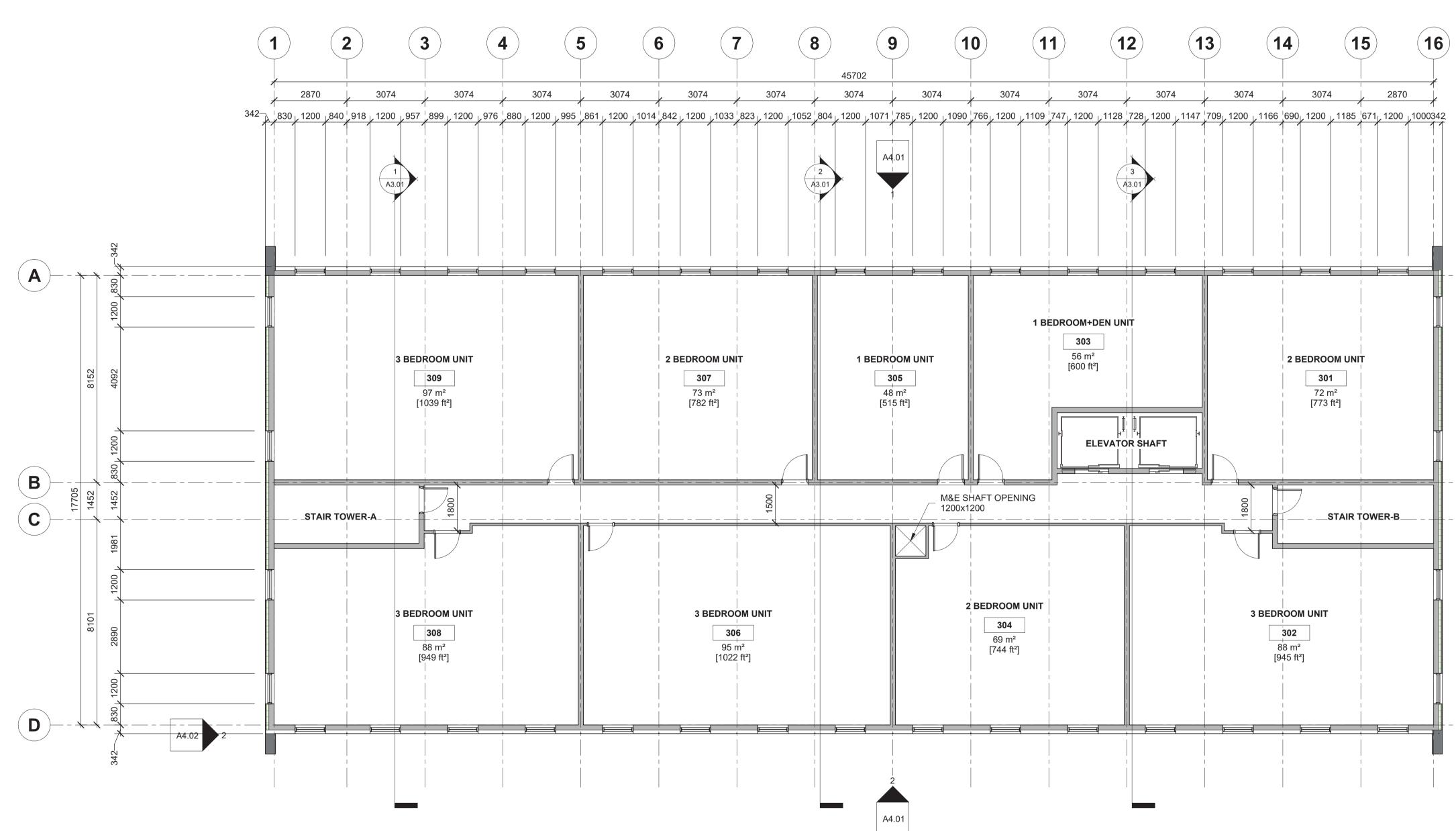


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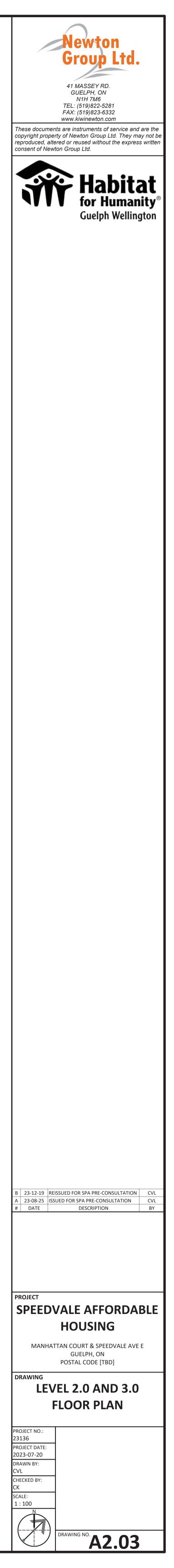
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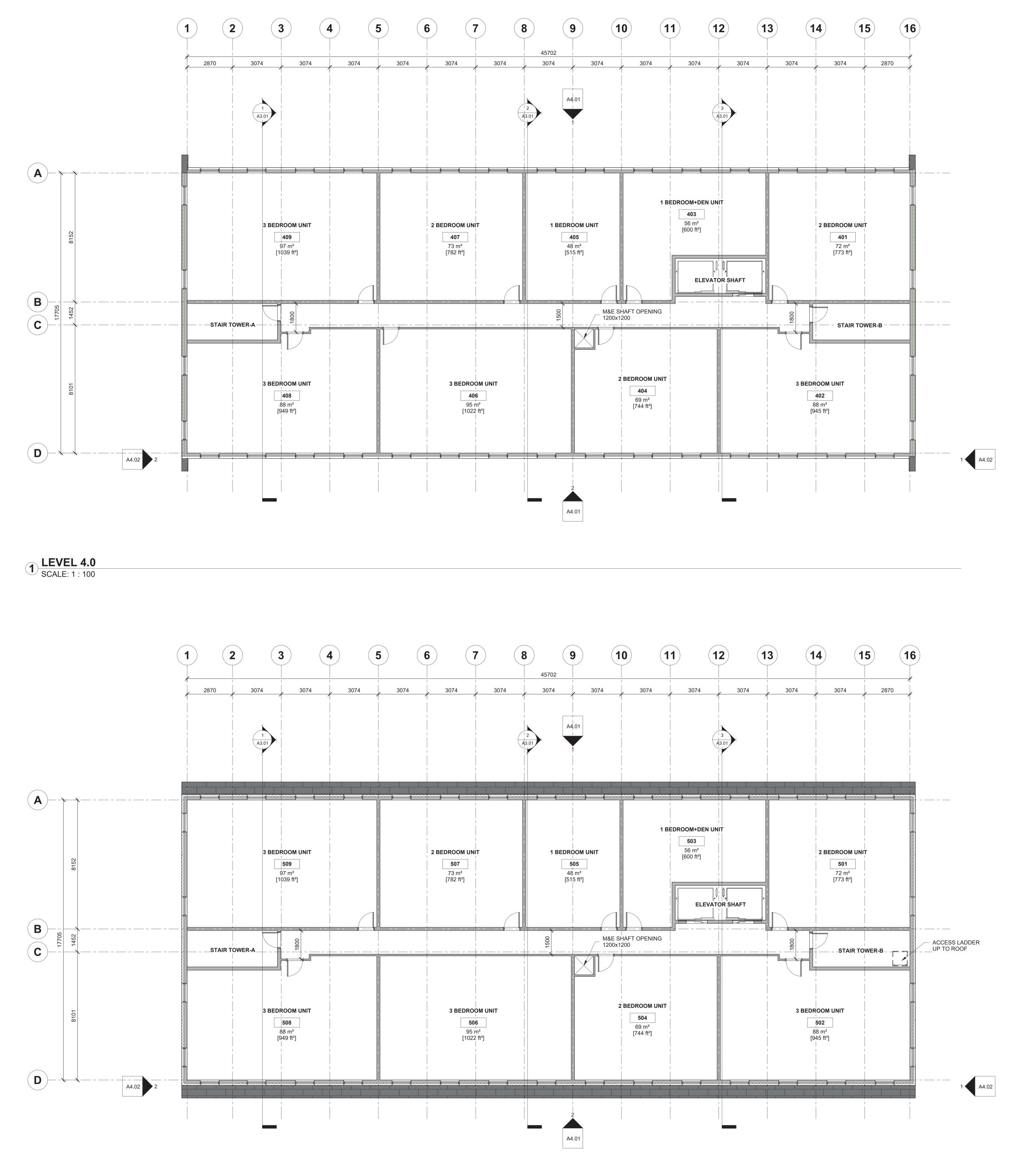
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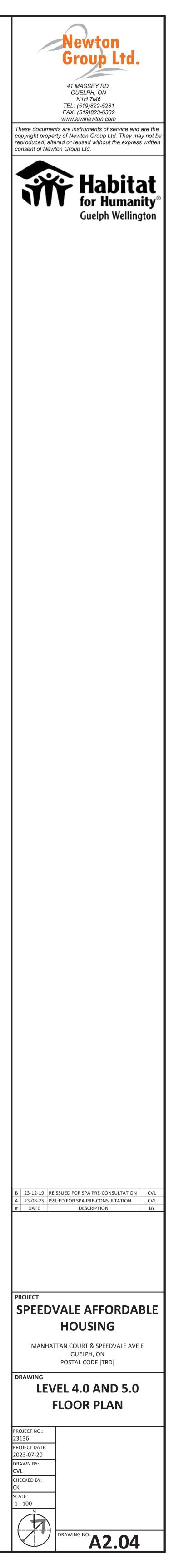
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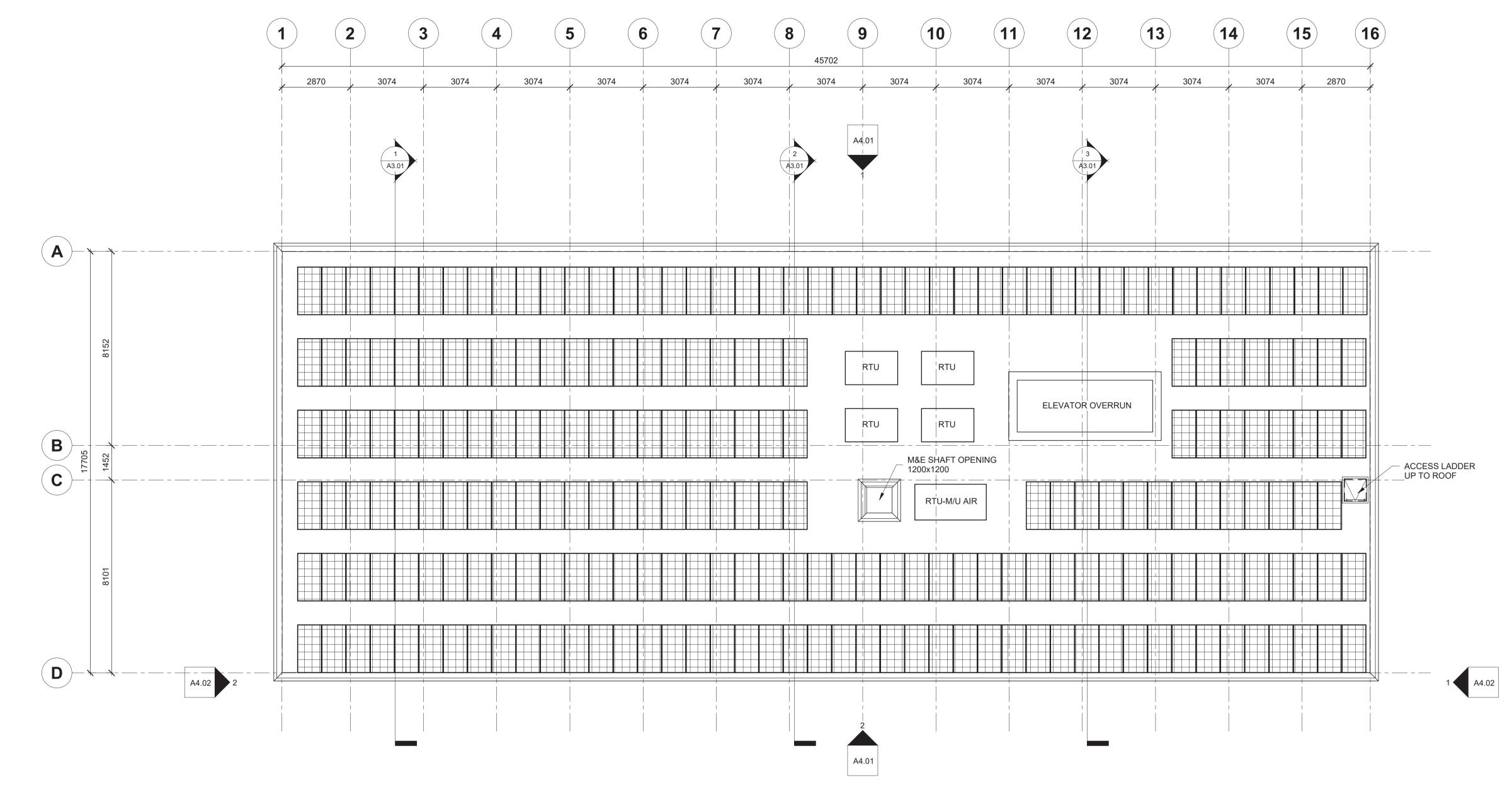




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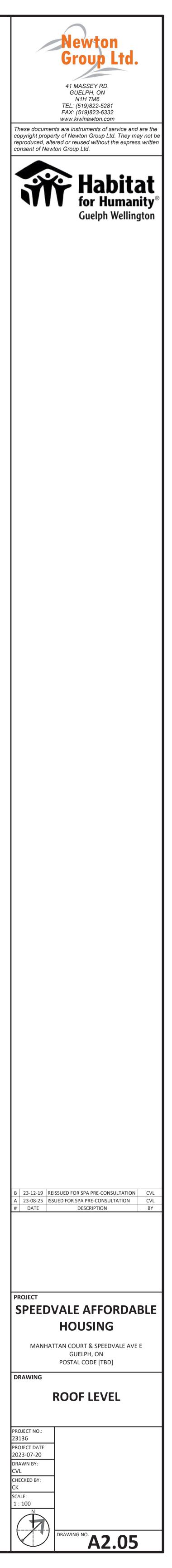
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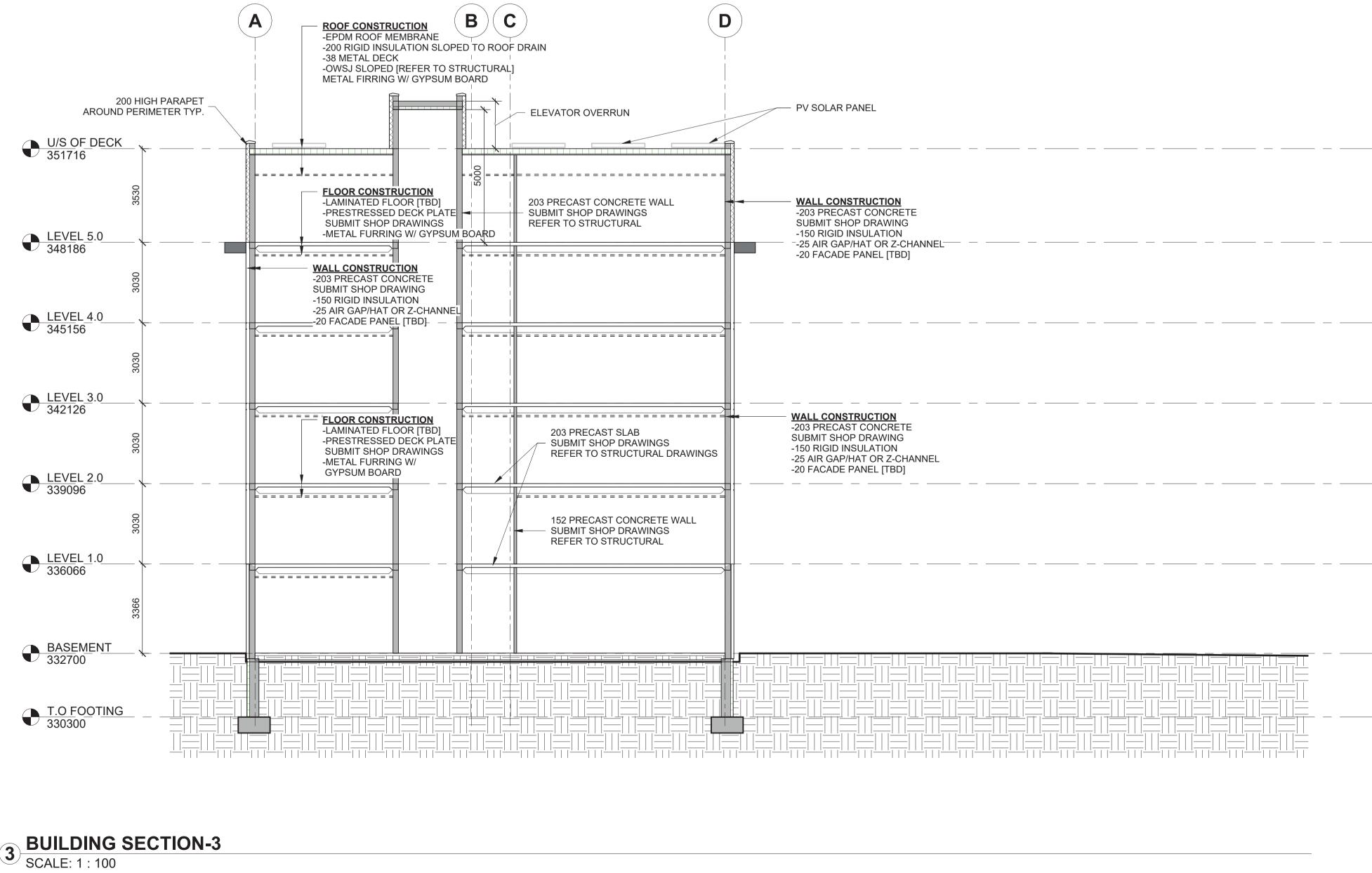




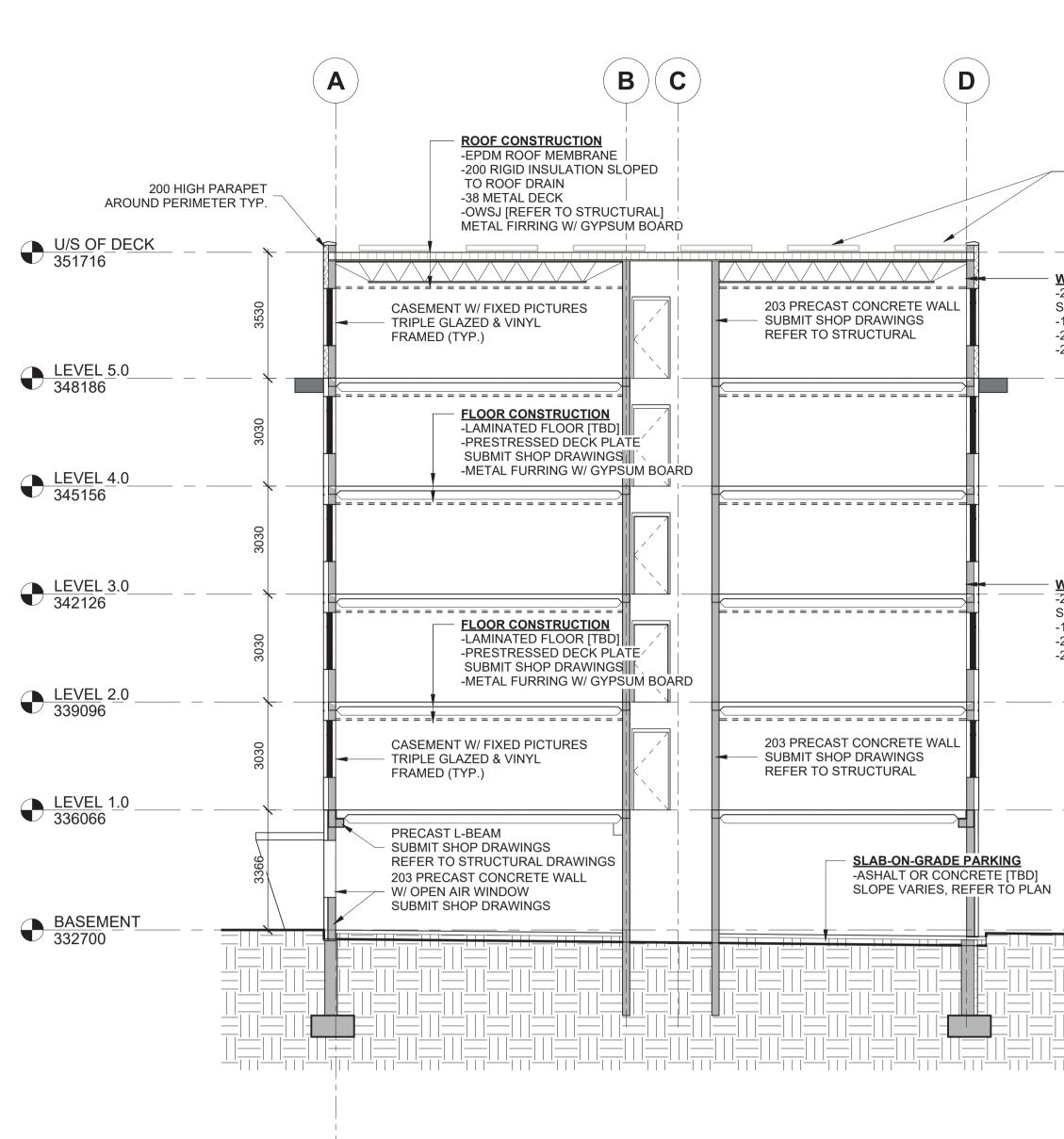
1 U/S OF DECK SCALE: 1 : 100

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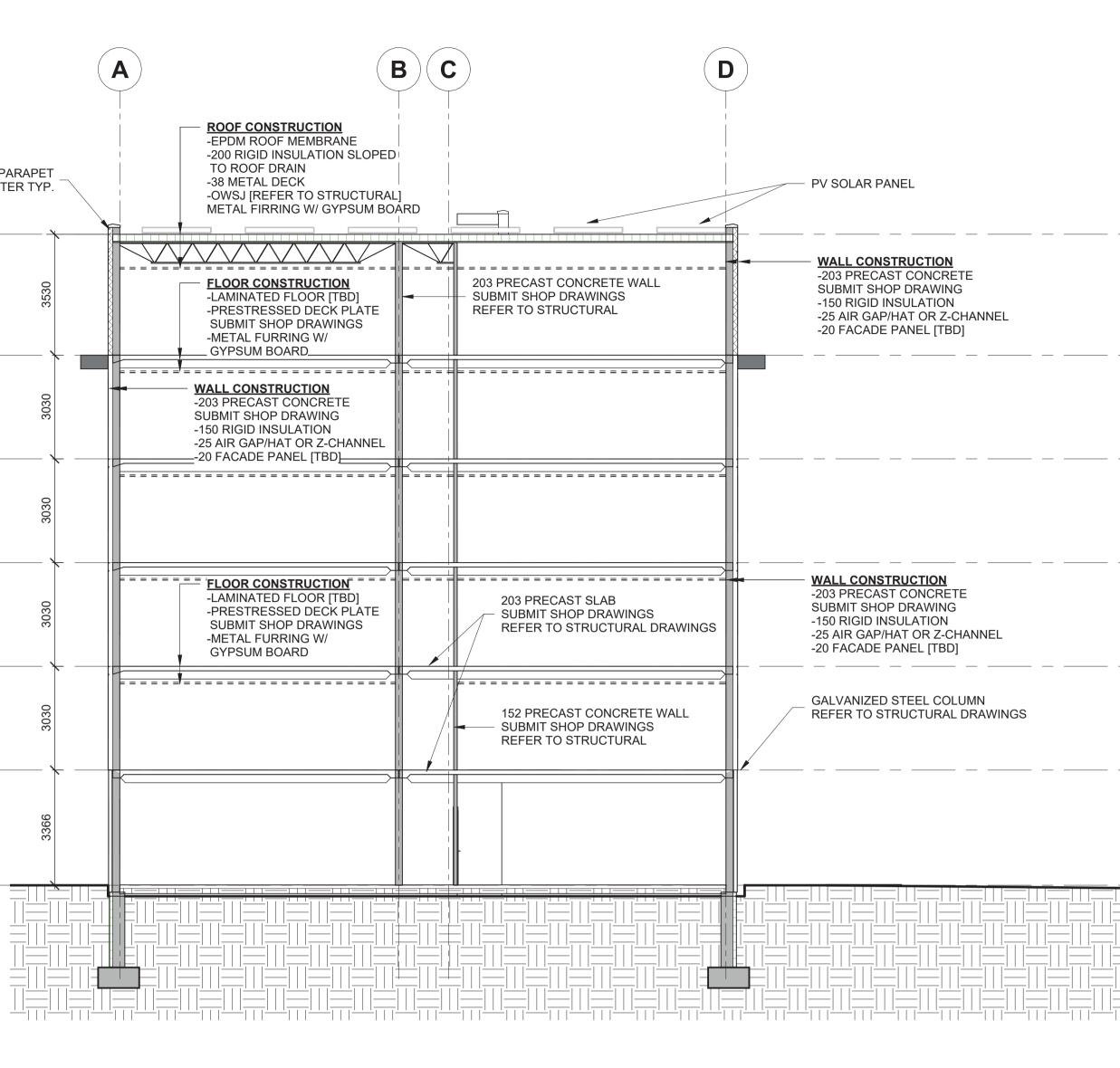


**BUILDING SECTION-1** SCALE: 1 : 100



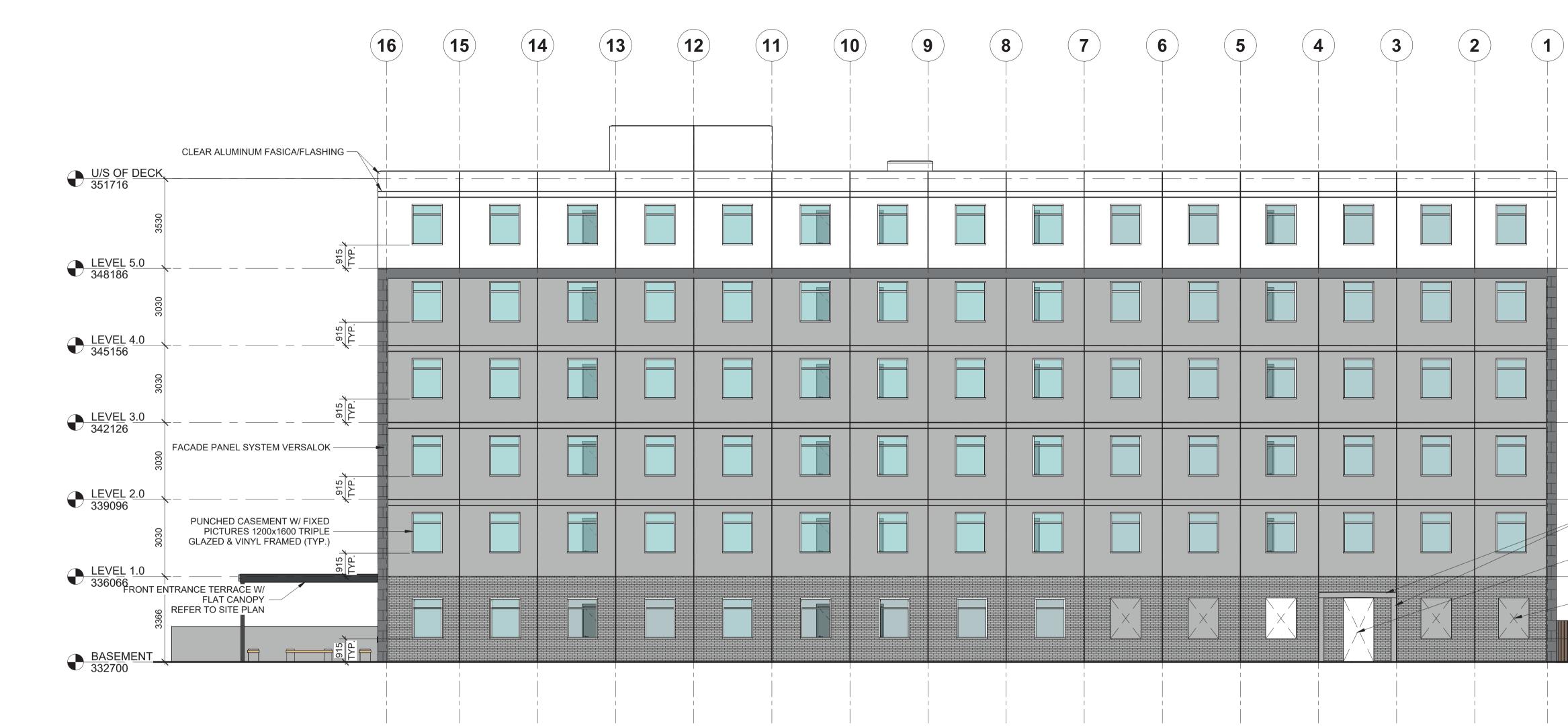
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| — SOLAR PV PANEL  | 200 HIGH PAR<br>AROUND PERIMETER   |
|---|------------------------------------|
| WALL CONSTRUCTION         -203 PRECAST CONCRETE         SUBMIT SHOP DRAWING         -150 RIGID INSULATION   | U/S OF DECK<br>351716              |
| -25 AIR GAP/HAT OR Z-CHANNEL<br>-20 FACADE PANEL [TBD]<br>  | <u>LEVEL 5.0</u><br>348186         |
|   | <u>LEVEL 4.0</u><br>345156         |
| WALL CONSTRUCTION         -203 PRECAST CONCRETE         SUBMIT SHOP DRAWING         -150 RIGID INSULATION         -25 AIR GAP/HAT OR Z-CHANNEL         -20 FACADE PANEL [TBD] | • <u>LEVEL 3.0</u><br>342126       |
|   | <u>LEVEL 2.0</u><br>339096         |
|   | <u>LEVEL 1.0</u><br>336066         |
|   | BASEMENT<br>332700                 |
|   |                                    |
|   | 2 BUILDING SECTI<br>SCALE: 1 : 100 |
|   |                                    |
|   |                                    |
|   |                                    |
|   |                                    |
| - PV SOLAR PANEL  |                                    |
| - WALL CONSTRUCTION<br>-203 PRECAST CONCRETE<br>SUBMIT SHOP DRAWING<br>-150 RIGID INSULATION<br>-25 AIR GAP/HAT OR Z-CHANNEL  |                                    |
|   |                                    |
| WALL CONSTRUCTION         -203 PRECAST CONCRETE         SUBMIT SHOP DRAWING         -150 RIGID INSULATION         -25 AIR GAP/HAT OR Z-CHANNEL         -20 FACADE PANEL [TBD] |                                    |

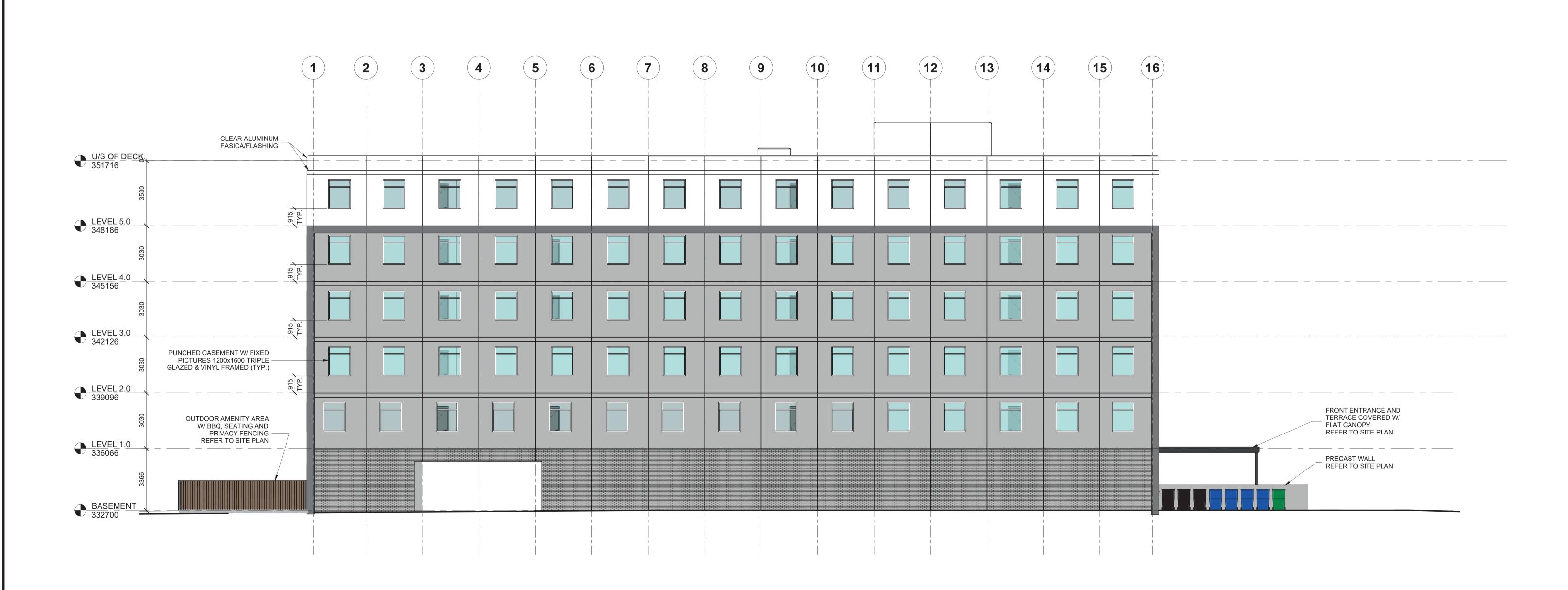


TION-2

| At MASSEY RD.<br>GUELPH, ON<br>N1H 7M6<br>TEL: (519)822-5281<br>FAX: (519)823-6332<br>www.kiwinewton.com<br>These documents are instruments of service and are the<br>copyright property of Newton Group Ltd. They may not be<br>reproduced, altered or reused without the express written<br>consent of Newton Group Ltd. |
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| PROJECT<br>SPEEDVALE AFFORDABLE  |
| HOUSING<br>MANHATTAN COURT & SPEEDVALE AVE E<br>GUELPH, ON<br>POSTAL CODE [TBD]<br>DRAWING<br>BUILDING SECTIONS<br>PROJECT NO.:<br>23136   |
| PROJECT DATE:<br>2023-07-20<br>DRAWN BY:<br>CVL<br>CHECKED BY:<br>CK<br>SCALE:<br>1:100<br>DRAWING NO.<br>A3.01  |



NORTH BUILDING ELEVATION SCALE: 1 : 100

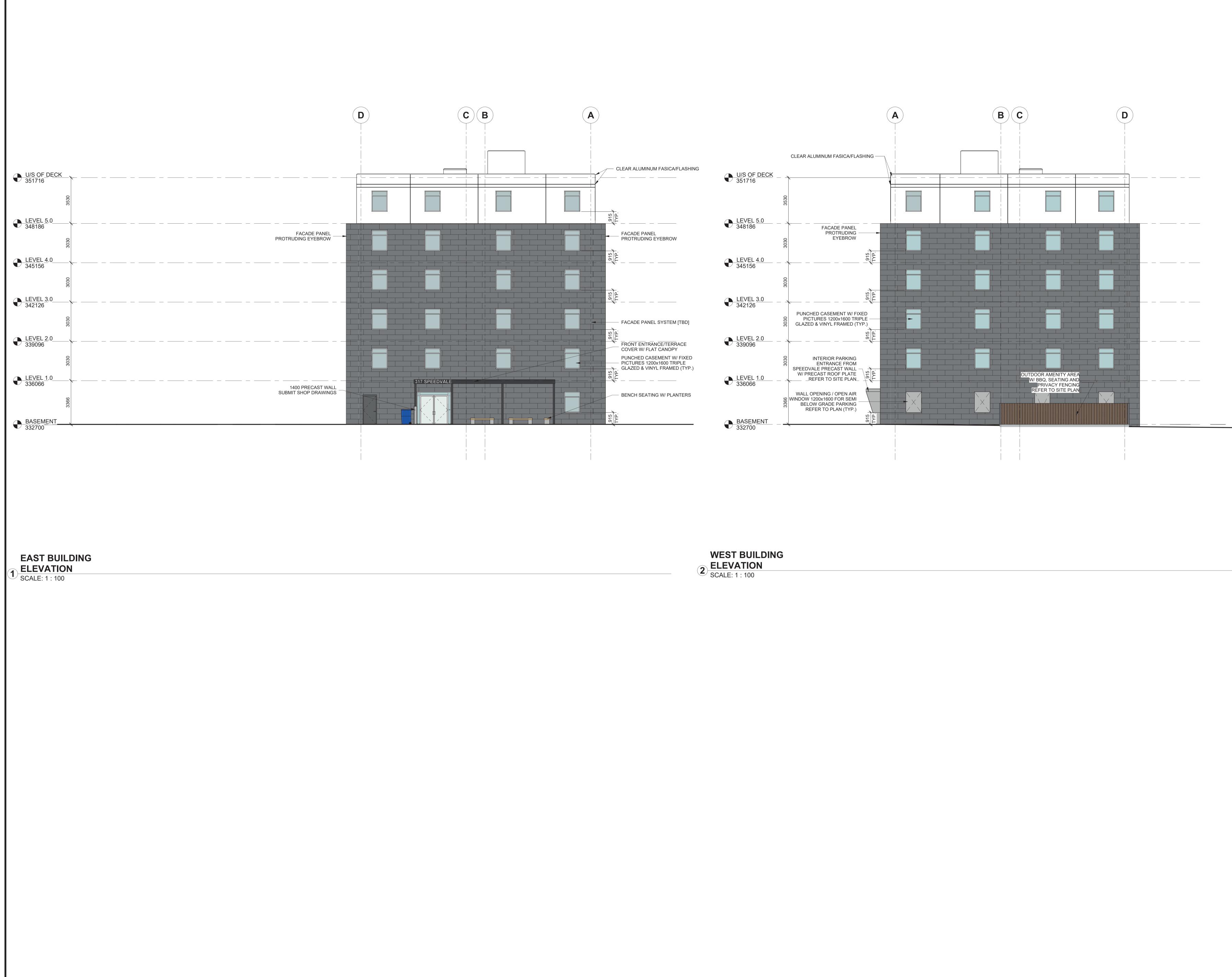


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# INTERIOR PARKING ENTRANCE FROM SPEEDVALE PRECAST WALL W/ PRECAST ROOF PLATE REFER TO SITE PLAN WALL OPENING FOR ACCESS TO INTERIOR PARKING WALL OPENING FOR ACCESS TO INTERIOR PARKING WALL OPENING / OPEN AIR WINDOW 1200x1600 REFER TO PLAN (TYP.)

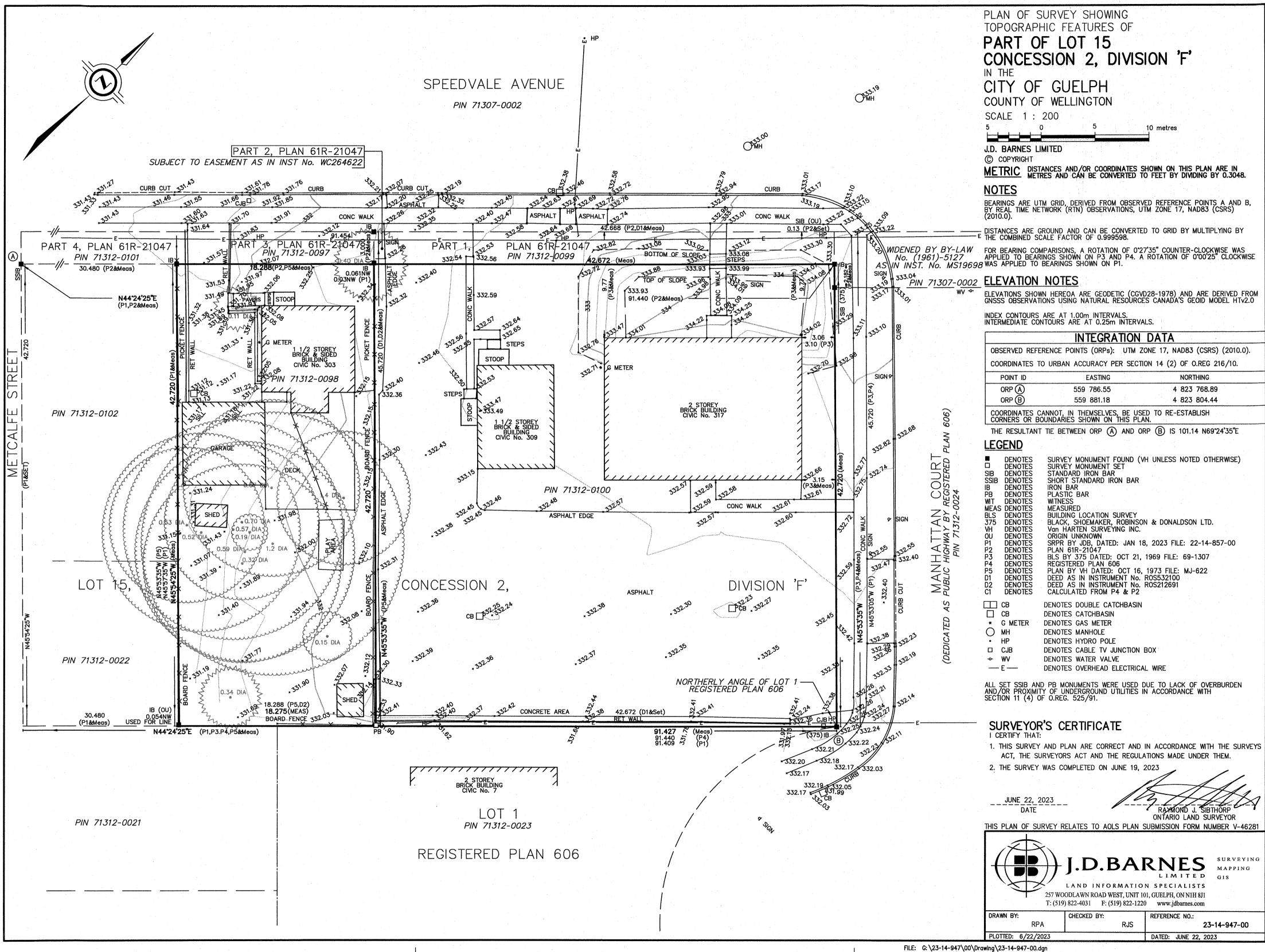
|   | Newton  |   |
|---|---|---|
|   | Group Ltd.<br>41 MASSEY RD.<br>GUELPH, ON   |   |
|   | N1H 7M6<br>TEL: (519)822-5281<br>FAX: (519)823-6332<br>www.kiwinewton.com<br>s are instruments of service and are the |   |
| copyright propert                                   | ty of Newton Group Ltd. They may not b<br>red or reused without the express writter                                   | е |
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|   | TAN COURT & SPEEDVALE AVE E<br>GUELPH, ON<br>POSTAL CODE [TBD]  |   |
| drawing<br>BUILD                                    | ING ELEVATIONS  |   |
| PROJECT NO.:<br>23136<br>PROJECT DATE:              |   | _ |
| 2023-07-20<br>DRAWN BY:<br>CVL<br>CHECKED BY:<br>CK |   |   |
| SCALE:<br>1:100                                     |   |   |
|   | DRAWING NO. A4.01   | - |



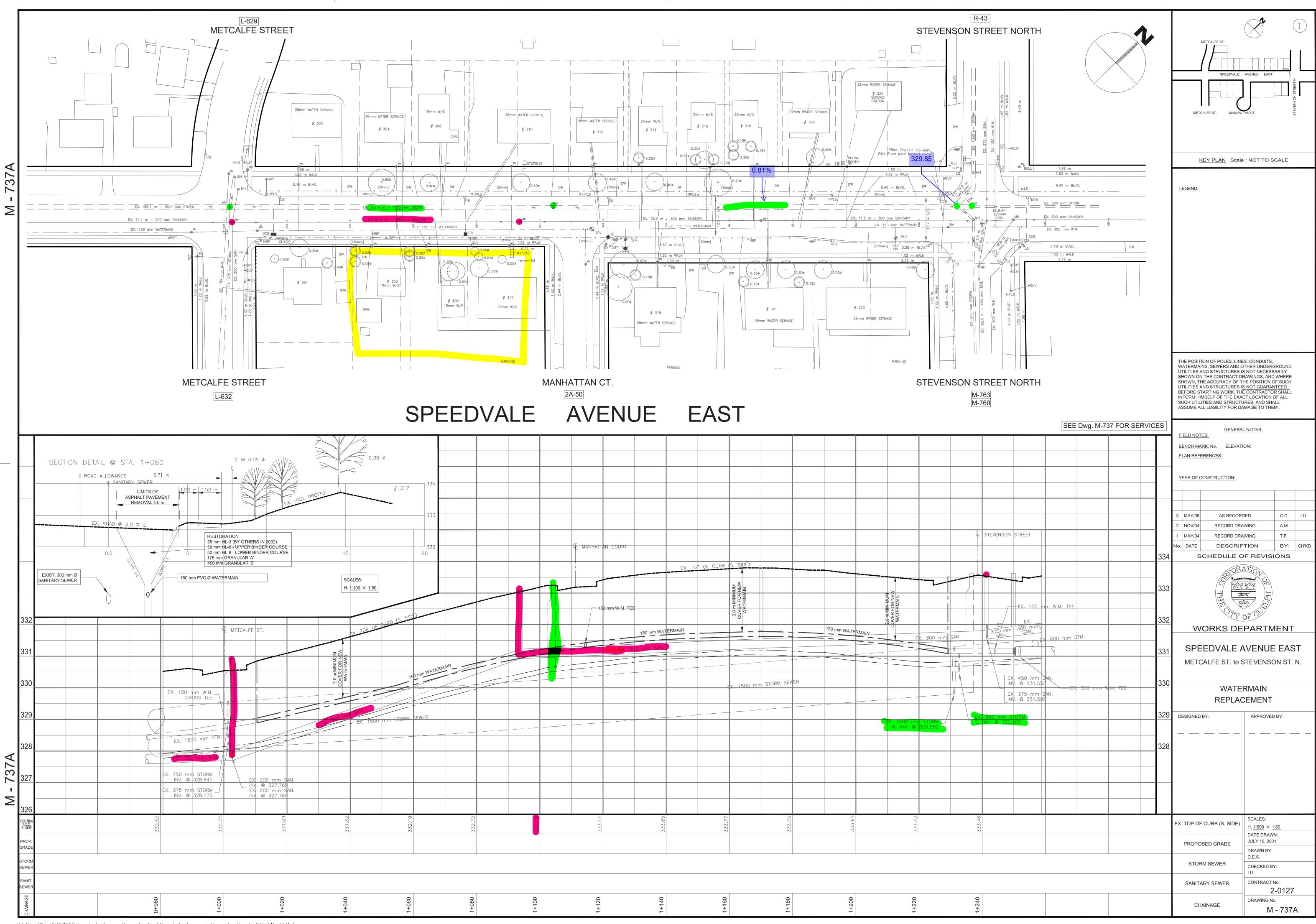
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| Newton<br>Group Ltd.   |
|--|
| 41 MASSEY RD.<br>GUELPH, ON<br>N1H 7M6<br>TEL: (519)822-5281<br>FAX: (519)823-6332   |
| www.kiwinewton.com<br>These documents are instruments of service and are the<br>copyright property of Newton Group Ltd. They may not be<br>reproduced, altered or reused without the express written<br>consent of Newton Group Ltd. |
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| SPEEDVALE AFFORDABLE<br>HOUSING<br>MANHATTAN COURT & SPEEDVALE AVE E   |
| GUELPH, ON<br>POSTAL CODE [TBD]<br>DRAWING   |
| PROJECT NO.:<br>23136  |
| PROJECT DATE:<br>2023-07-20<br>DRAWN BY:<br>CVL<br>CHECKED BY:   |
| CK<br>SCALE:<br>1:100  |
| DRAWING NO. <b>A4.02</b>   |

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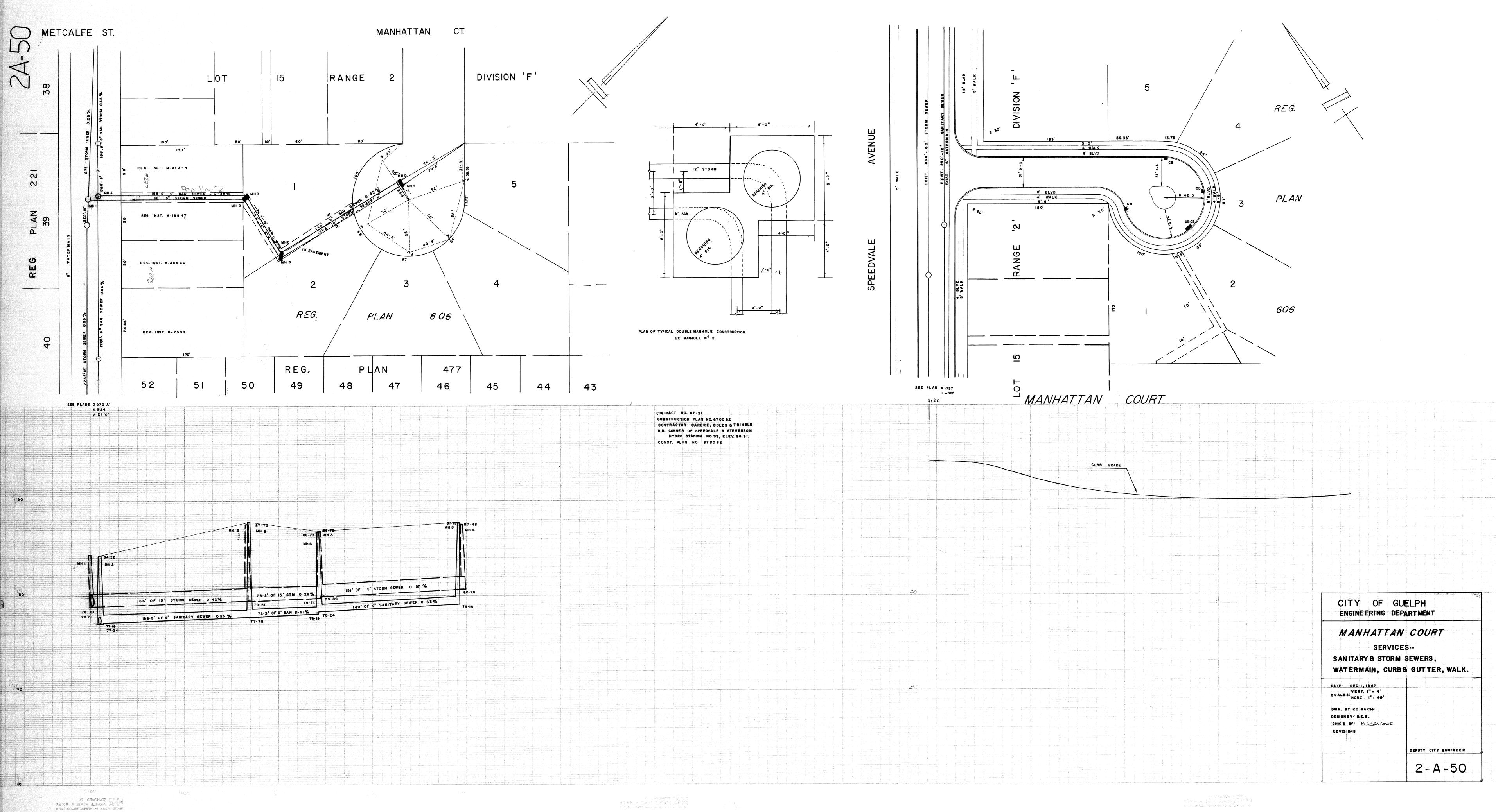


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| 1+080 | 1+100 | 1+120 | 1+140 | 1+160 | 1+180 | 1+200 | 1+220 |  |
|-------|-------|-------|-------|-------|-------|-------|-------|--|
|       |       |       |       |       |       |       |       |  |



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## APPENDIX B

Flow Test Report, Project No. 2023-NSD-130, dated December 8, 2023 Domestic Water and Fire Water Calculations Fire Flow Calculations Hazen-Williams Pressure Loss Calculations Relevant NFPA Information Sheets



# FLOW TEST REPORT

Form SD-003A RevDate: Dec 01, 2021

| PROJECT INFORMATION |                                  |                   |              |  |  |
|---------------------|----------------------------------|-------------------|--------------|--|--|
| Project Name:       | 317 Speedvale Ave East Flow Test | Design Project #: | 2023-NSD-130 |  |  |
| eite Address:       | 317 Speedvale Ave East Guelph ON | Const. Project #: | NA           |  |  |
| City Contact:       | Josh Baker                       | Phone #:          | 519-826-1655 |  |  |
| Flow Tester:        | Rob Smith                        | Phone #:          | 226-376-3053 |  |  |
| Technical Contact:  | Andy Coghlin                     | Phone #:          | 519-476-0761 |  |  |



# Page 1 of 2





Form SD-003A RevDate: Dec 01, 2021

| 2378                                    |                 |           |            | TEST IN             | FORMA                                  | TION           |                        |            |
|---|-----------------|-----------|------------|---------------------|--|----------------|------------------------|------------|
| Minimu                                  | m Required f    | Flow:     | NA         |                     |  |                | Min Ports:             | 2          |
| Pers                                    | onnel Preser    | nt: I     | Robert Si  | mith                |  |                | Test Date:             | 2023-12-08 |
| City / External Company: City of Guelph |                 |           | Test Time: | 11:00am             |  |                |                        |            |
|   | TEST EQUIPMENT  |           |            |                     |  |                |                        |            |
| 🗌 Hose                                  | Monsters w      | ith built | in Pitot   |                     | Hose                                   | e length use   | d:                     |            |
| 🗌 Hand                                  | l held pitot ga | auge      |            |                     | □ F                                    | ollard diffuse | er elbow with built in | Pitot      |
| Othe                                    | r:              |           |            |                     |  |                |                        |            |
|   |                 |           |            | TEST                | RESUL                                  | тѕ             |                        |            |
| Number<br>of Ports                      |                 |           |            | Total Flow<br>(GPM) | Static / Residual<br>Pressure<br>(PSI) |                |                        |            |
| 0 Ports                                 | 0 Ports 60      |           |            |                     |  |                |                        | 60         |
| 1 Port                                  | 2.5             | 0.9       |            |                     | 48                                     |                | 1,163                  | 59         |
| 2 Ports                                 | 2.5             | 0.9       |            | 32                  |  | 32             | 1,899                  | 58         |
| 3 Ports                                 | 2.5             | 0.9       |            |                     |  |                | 0                      |            |
| 4 Ports                                 | 2.5             | 0.9       |            |                     |  |                | 0                      |            |
| 0 Ports                                 |                 |           |            | STATIC RE           | -CHECK                                 | 1              | 5. · · · ·             | 60         |
|   |                 |           |            | TES                 | T NOTE                                 | S              |                        |            |
|   |                 |           |            |                     |  |                |                        |            |
|   |                 | HYDR      | AULIC      | ADJUSTME            | NTS (FC                                | OR OFFICE      | USE ONLY)              |            |
|   |                 | AD        | JUSTME     | ENTS FOR HY         | DRAUL                                  | C GRADE L      | .INE (HGL)             | 1          |
|   | Reservoir HO    | GL (m):   |            |                     |  | Site Ele       | vation (m):            |            |
| Theo                                    | retical Static  | Head (I   | PSI):      | 0                   | PSI                                    | to subtract f  | rom test pressures:    | 0          |

# OTHER HYDRAULIC ADJUSTMENTS

Other adjustment as required by the City / AHJ:

Page 2 of 2

1599 Adelaide St. N., Unit 301 London, ON N5X 4E8 P: 519-471-6667

# KITCHENER LOCATION

132 Queen St. S. Unit 4 Kitchener, ON N2G 1V9 P: 519-725-8093

sbm@sbmltd.ca

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# DOMESTIC WATER DEMAND, VELOCITY, AND TURNOVER CALCULATION

DATE: JOB NO.: January 24, 2024 SBM-23-1518

Client:Habitat for Humanity Guelph WellingtonProject:Proposed Residential DevelopmentLocation:303, 309 & 317 Speedvale Avenue E, Guelph

# DEMAND CALCULATION

| Avg. Day Demand =          | 225         | L/day/cap | DGSSMS B.2.2.2   |
|----------------------------|-------------|-----------|------------------|
| Avg. Day Demand =          | 0.002604167 | L/s/cap   |                  |
| Max. Day Peaking Factor =  | 3           |           | (Table 3-3)      |
| Max. Hour Peaking Factor = | 4.5         |           | (Table 3-3)      |
| Occupancy =                | 2           | p/bedroom | OBC 3.1.17.1 (b) |
|                            |             |           |                  |

|                                  | No. Bedrooms | Population | Avg. Day (L/s) | Max. Hour (L/s) | Max. Day (L/s) |
|----------------------------------|--------------|------------|----------------|-----------------|----------------|
| Occupany Load - OBC 3.1.17.1 (b) | 105          | 210        | 0.55           | 2.46            | 1.64           |
| Total                            |              |            | 0.55           | 2.46            | 1.64           |

(148 L/min) (98 L/min)

# VELOCITY CALCULATION

| Diameter (mm) | Demand (L/s) | Velocity (m/s) |
|---------------|--------------|----------------|
| 150           | 2.46         | 0.139          |

Maximum allowable velocity of 5.0 m/s as per Section B.2.3.4 Maximum Velocity of the Region of Waterloo and Area Municipalities - Design Guidelines and Supplemental Specifications for Municipal Services (DGSSMS February 2023)

# **VOLUME CALCULATION**

| Diameter (mm) | Length from Municipal Watermain<br>to Building (m) | Volume (Litres) |
|---------------|--|-----------------|
| 150           | 19.89  | 351.49          |
|               | Total  | 351.49          |

# **TURNOVER CALCULATIONS**

| Average Day Demand (L/s) | Volume (L) | Hours | Days |
|--------------------------|------------|-------|------|
| 0.55                     | 351.49     | 0.18  | 0.01 |





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# KITCHENER LOCATION

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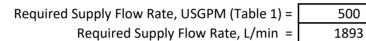
# **Fire-Fighting Flow NFPA#13**

| Client: | Habitat for Humanity Guelph Wellington |
|---------|--|
| Job No: | SBM-23-1518                            |
| Date:   | January 28, 2024                       |
|         | Calculated, not for data entry         |
|         | For data entry                         |

| Client:   | Habitat for Humanity Gueiph Weilington    |
|-----------|---|
| Project:  | Proposed Residential Development          |
| Location: | 303, 309 & 317 Speedvale Avenue E, Guelph |
|           |   |

# Table 1. NFPA#13 Flow Demand Requirements

| Hazard     | Sprinkler Flow<br>(USGPM) | Hydrant Allowance<br>(USGPM) | Total Flow<br>(USGPM) |
|------------|---------------------------|------------------------------|-----------------------|
| Light      | 175                       | 100                          | 275                   |
| Ordinary 1 | 250                       | 250                          | 500                   |
| Ordinary 2 | 350                       | 250                          | 600                   |
| Extra 1    | 750                       | 500                          | 1250                  |
| Extra 2    | 1000                      | 500                          | 1500                  |



Maximum Day Demand, L/min =

Required Supply Fire Flow + Maximum Day Demand, L/min = 1991

Incorporate Hazen-Williams and Bernoulli's Principles:

$$P_{\text{residual}} = P_{\text{static}} - (Q_{\text{required}}/Q_{\text{test}})^{1.85} \times (P_{\text{static}} - P_{\text{test}})$$

1.64 98.4

|                                | 60.00 | *psi (413.69 kPa) = | 0.00 L/min (0 USGPM)              |
|--------------------------------|-------|---------------------|-----------------------------------|
| Provided Supply Flow Rate @    | 59.00 | *psi (406.79 kPa) = | 4402.00 L/min (1163 USGPM)        |
|                                | 58.00 | *psi (399.9 kPa) =  | <b>7188.00</b> L/min (1899 USGPM) |
| Residual pressure at hydrant = | 59.52 | psi (410.38 kPa) =  | <b>1991.40</b> L/min (526 USGPM)  |
|                                |       |                     |                                   |

L/min

\* Refer to Hydrant Flow Test by Northern Sprinkler Design - 317 Speedvale Ave East, Guelph

kPa)

L/s (Refer to attached Domestic Water Demand calculation)

# **Table 1. Water Velocity Calculation**

| Diameter (mm) | Demand (L/min) | Velocity (m/s) |
|---------------|----------------|----------------|
| 150           | 1991           | 1.878          |

Maximum allowable velocity of 3.0 m/s as per Table 3-6 from the MOE Design Guidelines for Drinking-Water Systems

| Approximate Elevation of Tested Hydrant =                    | 334.10 | m                                    |
|--|--------|--------------------------------------|
| Approximate Elevation of Proposed Fire-Fighting Connection = | 331.30 | m                                    |
| Change in pressure due to elevation change =                 | 2.80   | m head (3.98 psi <i>,</i> 27.45 kPa) |
| Change in pressure due to elevation change =                 | 3.98   | psi                                  |
|  |        |                                      |

Water supply pressure at the proposed property under fire flow conditions (not

| - | - | - | - |                          |       |             |
|---|---|---|---|--------------------------|-------|-------------|
|   |   |   |   | accounting for losses) = | 63.50 | psi (437.82 |

Calculated Pressure Loss in Pipes = 0.86 psi (Refer to attached Pressure Loss in Pipes calculation)

Water Pressure at Proposed Fire FightingConnection Under Firefighting Conditions Including Losses =62.64psi (431.89 kPa)

Therefore, water supply pressure at the proposed building under fire flow conditions accounting for losses = 62.64 psi (431.89 kPa) which is greater than the 140 kPa (20 psi) required per the MOE Guidelines for Drinking Water Systems



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# KITCHENER LOCATION

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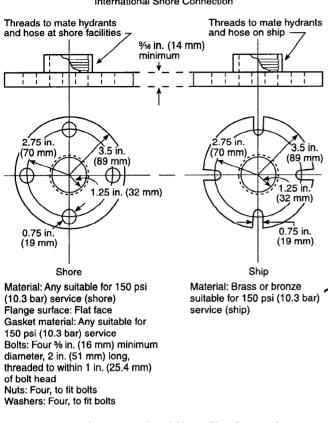
www.sbmltd.ca sbm@sbmltd.ca PLANNING · CIVIL · STRUCTURAL · MECHANICAL · ELECTRICAL Pressure Loss in Pipes (Hazen-Williams ) Calculations January 28, 2024 DATE: SBM-23-1518 JOB NO .: Habitat for Humanity Guelph Wellington Client: **Proposed Residential Development** Project: Location: 303, 309 & 317 Speedvale Avenue E, Guelph For data entry Calculated, not for data entry Pressure in Main Starting Pressure Head at Building Connection without pressure loss 437.82 kPa \*Refer to attached fire hydrant flow test and Fire Flow Calculation Pressure Loss in 150mm Service Friction Losses Through Pipe Fitting in Terms of Equivalent Length of Pipe: 2.78 \*\*Refer to NFPA 1142, Table I.1 (c) \*\*Valve (2x4.56 ft) m \*\*TEE (1x30.10 ft) 9.17 m Length of pipe (m) [refer to drawing C3] 19.89 m I = total length of pipe, including additional length due to loss in fittings 31.84 m \*\*\*c = Hazen-Williams roughness constant 150 \*\*Refer to NFPA 1142, Table I.1 (d) \*\*\*\* Refer to Fire-Fighting Flow NFPA#13 Calculation q = volume flow (L/s) [refer to fire-fighting demand calculations ] 33.2 d = inside or hydraulic diameter (mm) [refer to drawing C3] 150 **Calculated Pressure Loss** f = friction head loss in mm of water per 100 m of pipe (mm  $H_20$  per 100 m pipe) -1901.99 f = friction head loss in kPa per 100 m of pipe (kPa per 100 m pipe) -18.66 -605.59 Head loss (mm H20) Head loss (kPa) -5.94 or -0.86 psi **Calculated Flow Velocity** 1.88 \*\*\*\*\*Less than 3.0 m/s as per MOE Design Guidelines for Drinking Water v = flow velocity (m/s) Systems Final Pressure at the proposed building for sprinklers accounting for pressure loss (kPa) 431.88 62.64 psi or

## NFPA # 13 FLOW DEMAND REQUIREMENTS

| HAZARD      | SPRINKLER FLOW          | HYDRANT ALLOWANCE             | TOTAL FLOW |
|-------------|-------------------------|-------------------------------|------------|
| Light       | 175 GPM                 | 100 GPM                       | 275 GPM    |
| Ordinary 1  | 250 GPM                 | 250 GPM                       | 500 GPM    |
| Ordinary 2  | 350 GPM                 | 250 GPM                       | 600 GPM    |
| Extra 1     | 750 GPM                 | 500 GPM                       | 1250 GPM   |
| Extra 2     | 1000 GPM                | 500 GPM                       | 1500 GPM   |
| Warehousing | Varies too much to come | e up with a generic water dem | and        |

The pressures range on each of these flows and would be generally be 35 PSI - 80 PSI Requirments, but this information can't truly be given until final layouts and calculations are complete

ANNEX A



### International Shore Connection

### FIGURE A.3.10.7 International Shore Fire Connection.

A.5.1 Occupancy examples in the listings as shown in the various hazard classifications are intended to represent the norm for those occupancy types. Unusual or abnormal fuel loadings or combustible characteristics and susceptibility for changes in these characteristics, for a particular occupancy, are considerations that should be weighed in the selection and classification.

The light hazard classification is intended to encompass residential occupancies; however, this is not intended to preclude the use of listed residential sprinklers in residential occupancies or residential portions of other occupancies.

A.5.2 Light hazard occupancies include occupancies having uses and conditions similar to the following: Animal shelters Churches Clubs Eaves and overhangs, if of combustible construction with no combustibles beneath Educational Hospitals, including animal hospitals and veterinary facilities Institutional Kennels Libraries, except large stack rooms Museums Nursing or convalescent homes

Offices, including data processing

Residential

Restaurant seating areas

Theaters and auditoriums, excluding stages and prosceniums Unused attics

Note that it is not the committee's intent to automatically equate library bookshelves with ordinary hazard occupancies or with library stacks. Typical library bookshelves of approximately 8 ft (2.4 m) in height, containing books stored vertically on end, held in place in close association with each other, with aisles wider than 30 in. (762 mm) can be considered to be light hazard occupancies. Similarly, library stack areas, which are more akin to shelf storage or record storage, as defined in NFPA 232, Standard for the Protection of Records, should be considered to be ordinary hazard occupancies.

A.5.3 For purposes of these definitions, Class I, Class II, Class III, and Class IV commodities would be considered to have moderate rates of heat release, while Group A plastics would be considered to have high rates of heat release. Stockpiles are considered to include display merchandise (mercantile) and arrangements of combustibles ancillary to operations within the occupancy as opposed to dedicated storage areas where the fire loading is generally more severe.

A.5.3.1 Ordinary hazard occupancies (Group 1) include occupancies having uses and conditions similar to the following:

Automobile parking and showrooms

**Bakeries** 

Beverage manufacturing

Canneries

×.

Dairy products manufacturing and processing

**Electronic plants** 

Glass and glass products manufacturing

Laundries

Restaurant service areas

A.5.3.2 Ordinary hazard occupancies (Group 2) include occupancies having uses and conditions similar to the following:

Agricultural facilities Barns and stables Cereal mills Chemical plants - ordinary **Confectionery products** Distilleries Dry cleaners Exterior loading docks

Note that exterior loading docks only used for loading and unloading of ordinary combustibles should be classified as OH2. For the handling of flammable and combustible liquids, hazardous materials, or where utilized for storage, exterior loading docks and all interior loading docks should be protected based upon the actual occupancy and the materials handled on the dock, as if the materials were actually stored in that configuration.

Feed mills Horse stables Leather goods manufacturing Libraries - large stack room areas Machine shops Metal working Mercantile Paper and pulp mills Paper process plants Piers and wharves

# APPENDIX C

Sanitary Design Sheet

| 303, 309 & 317 Spe                                    | eedvale Avenue E, G                         | uelph              |  |                 |                |                     |              |  |                              |          |                                | Desig    | ın Param               | neters                        |                         |                   |        |                        |                  |                          |             |              |              |                          |                    |
|---|---|--------------------|--|-----------------|----------------|---------------------|--------------|--|------------------------------|----------|--------------------------------|----------|------------------------|-------------------------------|-------------------------|-------------------|--------|------------------------|------------------|--------------------------|-------------|--------------|--------------|--------------------------|--------------------|
| CITY OF<br>GUELPH, ON                                 |   |                    | SANITARY SEWER I   | DESIGN          | SHEE           | Т                   |              | <u>Average Daily Flo</u><br>*Residential = |                              | L/cap/da | y                              |          | Mannings<br>Min. Veloo |                               | 0.0130<br>0.6 m/        | /sec              |        |                        | Harmon Pe        | aking Factor             | Equation: M | in. PF = 2 N | /lax. PF = 4 |                          |                    |
|   |   |                    | ENGINEERING AND F  | <b>PUBLIC W</b> | <b>ORKS</b>    |                     |              | =  | 0.00347                      | L/cap/s  | -                              |          | Max. Velo              | ocity                         | 3.0 m                   | /sec              |        |                        |                  | 1 /                      |             |              |              |                          |                    |
| Project Number:<br>Date:<br>Design By:<br>Checked By: | SBM-23-1518<br>January 28, 2024<br>H. Ahmad |                    | Drainage Area Plan No: NA  |                 |                |                     |              |  |                              |          |                                |          |                        | al Harmon P<br>al Areas Infil | -                       | . ,               | L/s/ha |                        | $\mathbf{F} = 1$ | $+\frac{14}{4+\sqrt{R}}$ | = (P = Po)  | pulatio      | on' 1,000)   |                          |                    |
| File:   | S:\2023 Jobs\SBM-23-1518 Habitat            | GW - 303-317 Speed | vale Ave - Guelph\04 dDocs\03 Civil\Calculations\FSR\SAN\SBM-23-1518 | HFH - 317 Speed | vale Ave., Gue | elph - Sanitary Sew | er Design Sl |  |                              |          |                                |          |                        |                               |                         |                   |        |                        |                  |                          |             |              |              |                          |                    |
|   | LOCATION                                    |                    | RESIDENTIAL AREAS a  | nd POPUL        | ATION          |                     |              | SCHC<br>INSTITU                            |                              | C        | OMMERC                         | IAL      | INI                    | DUSTRIAL                      | L                       |                   | INFI   | TRATION                |                  |                          |             | DESIGN       |              |                          |                    |
|   | MANHOLE                                     |                    | HECTARES OF EACH DENSITY   |                 |                |                     | PEAK         |  |                              | RES AND  |                                | EACH ZON | IING                   |                               |                         |                   |        |                        | TOTAL            |                          |             |              |              | FULL                     |                    |
| STREET  | AREA MANHOLE<br>NO. FROM<br>MH              | TO<br>MH           | 0 0 0 0 0 0  |                 |                |                     | RES.<br>FLOW | AREA CUMUL<br>AREA AREA                    | 5 <i>L/s/ha</i><br>PEAK FLOW | AREA     | 0.50 <i>L</i><br>CUMUL<br>AREA |          |                        |                               | /s/ha T<br>PEAK<br>FLOW | OTALS-C-I<br>FLOW | AREA   | CUMUL INFI<br>AREA FLO |                  | LENGTI                   | H SLOPE P   | IPE SIZE     |              | FULL<br>FLOW<br>VELOCITY | ACTUAL<br>VELOCITY |
|   |   |                    | 0.00 0.00 0.00 0.00 0.00 0.00 0.00                                   | 1000s           | 1000s          |                     | L/sec        | ha ha                                      | L/sec                        | ha       | ha                             | L/sec    | ha                     |                               | L/sec                   | L/sec             | ha     | ha L/se                | : L/sec          | т                        | %           | mm           | L/sec        | m/s                      | m/s                |
| Design Flows Per OBC                                  | Site  | EX. SAN            | 0.26   | * 0.210         | 0.210          | 4.14                | 2.92         | 0.00 0.00                                  | 0.000                        | 0.00     | 0.00                           | 0.0000   | 0.00                   | 0.00                          | 0.0000                  | 0.0000            | 0.26   | 0.00 0.06              | 50 2.9           | 98                       | 2.00        | 200          | 46.3604      | 1.476                    | 0.828              |
| Design Flows Per DEM 20                               | 023 (Apartments)                            |                    | 1  | **              |                |                     |              | 1  |                              |          |                                |          |                        |                               |                         |                   |        |                        |                  |                          |             |              |              |                          |                    |
|   | Isite                                       | EX. SAN            | 0.26   | 0.089           | 0.089          | 4.26                | 1.24         | 0.00 0.00                                  | 0.000                        | 0.00     | 0.00                           | 0.0000   | 0.00                   | 0.00                          | 0.0000                  | 0.0000            | 0.26   | 0.00 0.06              | 50 1 :           | 31                       | 2.00        | 200          | 46.3604      | 1.476                    | 0.645              |

\*The maximum building population of 210 people based on 105 bedrooms and an occupancy load of 2 people per bedroom as per the current Ontario Building Code (OBC).

\*\*The maximum building population of 89 based on 48 units and a population of 1.86 people per unit per the City of Guelph's Development Engineering Manual (DEM)

## APPENDIX D

SWM Calculations ADS OGS Sizing Summary

# STRIK BALDINELLI C PLANNING · CIVIL · STRUCTURAL · MECHANICAL · ELECTRICAL

# LONDON LOCATION

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# **KITCHENER LOCATION**

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PRE-DEVELOPMENT CONDITIONS

### Stormwater Management (SWM) Calculations:

| DATE:<br>JOB NO.: | January 30, 2024<br>58M-23-1518              |
|-------------------|--|
| Client:           | Habitat for Humanity Guelph Wellington       |
| Project:          | Proposed Residential Building                |
| Location:         | 303, 309 & 317 Speedvale Avenue East, Guelph |

| Return Period                      | 2-year | 5-year | 10-year | 25-year | 50-year | 100-year |
|------------------------------------|--------|--------|---------|---------|---------|----------|
| A                                  | 475.61 | 632.75 | 721.92  | 822.74  | 893.8   | 953.29   |
| В                                  | -0.738 | -0.741 | -0.736  | -0.725  | -0.719  | -0.711   |
| *Intensity, I = A(tc) <sup>B</sup> |        |        |         |         |         |          |

\*Refer to Section 5.5.1.1 of the City of Guelph Development Engineering Manual (DEM) October 2023.

Γ

|                                     | Area (m <sup>2</sup> )      | C               | A*C      | 2-Year Pre-Development Flows:                       |        |      |
|-------------------------------------|-----------------------------|-----------------|----------|---|--------|------|
| Fotal Site Area:                    | 2,601.82                    |                 |          | C =   | 0.64   |      |
| Building Area:                      | 401.50                      | 0.9             | 361.35   | Time of concentration t <sub>c</sub> =              | 5.0    | min  |
| Concrete/Asphalt:                   | 1,245.50                    | 0.9             | 1120.95  | Intensity, i (@ t <sub>c</sub> ) =                  | 145.01 | mm/h |
| Gravel                              | 0.00                        | 0.7             | 0        | Pre-Development Flow, Q <sub>r</sub> = 2.78*C*i*A = | 67.46  | l/s  |
| andscaped/Open:                     | 954.82                      | 0.2             | 190.964  |   |        |      |
| otals:                              | 2,601.82                    |                 | 1673.264 | 100-Year Pre-Development Flows:                     |        |      |
| eq = Sum(A*C)/Sum(A) =              | 0.64                        |                 |          | C =   | 0.64   |      |
|                                     |                             |                 |          | Time of concentration t <sub>c</sub> =              | 5.0    | min  |
| ime of Concentration of 5 min per I | Development Engineering Man | ual Section 5.5 |          | Intensity, i (@ t <sub>c</sub> ) =                  | 303.57 | mm/h |
|                                     |                             |                 |          | Pre-Development Flow, Q, = 2,78*C*i*A =             | 141.21 | 1/5  |



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A\*C

0 1136.979

0 1136.979 

|                                     |                            |          |          | POST-DEVELOPMENT CONDITIONS  |                        |                                    |
|-------------------------------------|----------------------------|----------|----------|------------------------------|------------------------|------------------------------------|
| POST-DEVELOPMENT OVERALL SIT        | ε.                         |          |          |                              |                        |                                    |
| POST-DEVELOPMENT OVERALE ST         | Area (m <sup>2</sup> )     | с        | A*C      |                              |                        |                                    |
| Total Site Area:                    | 2,601.82                   | c        | Ac       |                              |                        |                                    |
| Building Area:                      | 853.84                     | 0.9      | 768.456  |                              |                        |                                    |
| Concrete/Asphalt:                   | 1,392.39                   | 0.9      | 1253.151 |                              |                        |                                    |
| Gravel                              | 0.00                       | 0.7      | 0        |                              |                        |                                    |
| andscaped/Open:                     | 355.59                     | 0.2      | 71.118   |                              |                        |                                    |
| Totals:                             | 2,601.82                   |          | 2092.725 |                              |                        |                                    |
| C <sub>eq</sub> = Sum(A*C)/Sum(A) = | 0.80                       |          |          |                              |                        |                                    |
| POST-DEVELOPMENT CONTROLLED         | CATCHMENT (A201 - ROOFTOP) | <u>.</u> |          | POST-DEVELOPMENT CONTR       | OLLED CATCHMENT        | (A202 - PARKING):                  |
|                                     | Area (m <sup>2</sup> )     | с        | A*C      |                              | Area (m <sup>2</sup> ) | с                                  |
| Total Site Area:                    | 853.84                     |          |          | Total Site Area:             | 1,263.31               |                                    |
| Building Area:                      | 853.84                     | 0.9      | 768.456  | Building Area:               | 0.00                   | 0.9                                |
| Concrete/Asphalt:                   | 0.00                       | 0.9      | 0        | Concrete/Asphalt:            | 1,263.31               | 0.9                                |
| Gravel                              | 0.00                       | 0.7      | 0        | Gravel                       | 0.00                   | 0.7                                |
| Landscaped/Open:                    | 0.00                       | 0.2      | 0        | Landscaped/Open:             | 0.00                   | 0.2                                |
| Totals:                             | 853.84                     |          | 768.456  | Totals:                      | 1,263.31               | _                                  |
| C <sub>eq</sub> = Sum(A*C)/Sum(A) = | 0.90                       |          |          | $C_{eq} = Sum(A*C)/Sum(A) =$ | 0.90                   |                                    |
| POST-DEVELOPMENT UNCONTROL          | LED CATCHMENT (U201):      |          |          |                              |                        |                                    |
|                                     | Area (m <sup>2</sup> )     | с        | A*C      | 2                            | -Year Post-Develop     | ment Flows (U201)                  |
| Total Site Area:                    | 484.67                     |          |          |                              |                        | C =                                |
| Building Area:                      | 0.00                       | 0.9      | 0        |                              | Time of                | f concentration t <sub>c</sub> =   |
| Concrete/Asphalt:                   | 129.08                     | 0.9      | 116.172  |                              |                        | Intensity, i (@ t <sub>r</sub> ) = |
| Gravel                              | 0.00                       | 0.7      | 0        | Pre                          | e-Development Flow     | , Q, = 2.78*C*i*A =                |
| Landscaped/Open:                    | 355.59                     | 0.2      | 71.118   |                              |                        |                                    |
| Totals:                             | 484.67                     |          | 187.29   | 100                          | -Year Post-Develop     | ment Flows (U201)                  |
| C <sub>eq</sub> = Sum(A*C)/Sum(A) = | 0.39                       |          |          |                              |                        | C =                                |
|                                     |                            |          |          |                              | Time of                | f concentration t <sub>r</sub> =   |
|                                     |                            |          |          |                              |                        | Intensity, i (@ t.) =              |
|                                     |                            |          |          | Pro                          |                        | 0.= 2.78*C*i*A =                   |

| 2-Year Post-Development Flows (U201)                |        |       |
|---|--------|-------|
| C =   | 0.39   |       |
| Time of concentration t <sub>c</sub> =              | 5.0    | min   |
| Intensity, i (@ t <sub>c</sub> ) =                  | 145.01 | mm/hr |
| Pre-Development Flow, Q <sub>r</sub> = 2.78*C*i*A = | 7.55   | l/s   |
| 100-Year Post-Development Flows (U201)              |        |       |
| C =   | 0.39   |       |
| Time of concentration t <sub>c</sub> =              | 5.0    | min   |
| Intensity, i (@ t <sub>c</sub> ) =                  | 303.57 | mm/hr |
| Pre-Development Flow, $Q_r = 2.78 * C^*i * A =$     | 15.81  | I/s   |

| RETURN PERIOD | ALLOWABLE PRE-<br>DEVELOPMENT FLOWS<br>[A101] (L/S) | UNCONTROLLED POST-<br>DEVELOPMENT FLOWS<br>[U201+U202] (L/s) | ALLOWABLE POST-<br>DEVELOPMENT RELEASE<br>FROM SITE (L/s) | ALLOWABLE SURFACE<br>OUTFLOWS (L/s) |
|---------------|---|--|---|-------------------------------------|
| 2-year        | 67.46   | 7.55   | 59.91   | 0                                   |
| 100-year      | 141.21  | 15.81  | 125.40  | 65.50                               |



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### CATCHMENT A201 STORAGE CALCULATIONS - A201 (BUILDING ROOF)

FLOW RESTRICTION ROOF DRAINS: Restricted Flow Rate = 4.50 L/s

Note: Number and location of roof drains to be confirmed by roof designer and mechanical engineer

RAINFALL DATA: Rainfall Data - Guelph Rainfall Intensity Duration

| STORAGE | CALCULATIONS: |  |
|---------|---------------|--|

| 2 Yr Stm E                              | vent          |                        |                   |                         |                            |                    |                             |                   |
|---|---------------|------------------------|-------------------|-------------------------|----------------------------|--------------------|-----------------------------|-------------------|
|   |               |                        |                   | Orifice/Flow Restrictor |                            |                    |                             |                   |
|   |               | Inflow, Q <sub>i</sub> | Volume In (¥      | Outflow                 | Surface Outflow (Scuppers) | Total Outflow      | Volume Out (¥ <sub>o)</sub> | Difference/       |
| Duration                                | Intensity "i" | 2.78*C*i*A             | Q*t*60/1000       | Q <sub>orifice</sub>    | Q <sub>surface</sub>       | Q <sub>total</sub> | Q <sub>o</sub> *t*60/1000   | Storage           |
| (min.)                                  | (mm/hr)       | (l/s)                  | (m <sup>3</sup> ) | (l/s)                   | (l/s)                      | (l/s)              | (m <sup>3</sup> )           | (m <sup>3</sup> ) |
| 5                                       | 145.01        | 45.84                  | 13.75             | 4.50                    | 0.00                       | 4.50               | 1.35                        | 12.40             |
| 10                                      | 86.95         | 18.57                  | 11.14             | 4.50                    | 0.00                       | 4.50               | 2.70                        | 8.44              |
| 20                                      | 52.13         | 11.14                  | 13.36             | 4.50                    | 0.00                       | 4.50               | 5.40                        | 7.96              |
| 30                                      | 38.65         | 8.26                   | 14.86             | 4.50                    | 0.00                       | 4.50               | 8.10                        | 6.76              |
| 60                                      | 23.17         | 4.95                   | 17.82             | 4.50                    | 0.00                       | 4.50               | 16.20                       | 1.62              |
| 120                                     | 13.89         | 2.97                   | 21.37             | 2.97                    | 0.00                       | 2.97               | 21.37                       | 0.00              |
| 180                                     | 10.30         | 2.20                   | 23.77             | 2.20                    | 0.00                       | 2.20               | 23.77                       | 0.00              |
| Max. Storage Volume (m <sup>3</sup> ) = |               |                        |                   |                         |                            | 12.40              |                             |                   |

(3 roof drains at 1.5 L/s capacity per drain)

Drawdown Time (hr) = 0.77

| 100 Yr Stm E | vent          |                        |                   |                         |                            |                    |                             |                   |
|--------------|---------------|------------------------|-------------------|-------------------------|----------------------------|--------------------|-----------------------------|-------------------|
|              |               |                        |                   | Orifice/Flow Restrictor |                            |                    |                             |                   |
|              |               | Inflow, Q <sub>i</sub> | Volume In (¥i)    | Outflow                 | Surface Outflow (Scuppers) | Total Outflow      | Volume Out (¥ <sub>o)</sub> | Difference/       |
| Duration     | Intensity "i" | 2.78*C*i*A             | Q*t*60/1000       | Q <sub>orifice</sub>    | Q <sub>surface</sub>       | Q <sub>total</sub> | Q <sub>o</sub> *t*60/1000   | Storage           |
| (min.)       | (mm/hr)       | (l/s)                  | (m <sup>3</sup> ) | (I/s)                   | (I/s)                      | (I/s)              | (m <sup>3</sup> )           | (m <sup>3</sup> ) |
| 5            | 303.57        | 64.85                  | 19.46             | 4.50                    | 0.00                       | 4.50               | 1.35                        | 18.11             |
| 10           | 185.45        | 39.62                  | 23.77             | 4.50                    | 0.00                       | 4.50               | 2.70                        | 21.07             |
| 20           | 113.29        | 24.20                  | 29.04             | 4.50                    | 0.00                       | 4.50               | 5.40                        | 23.64             |
| 30           | 84.92         | 18.14                  | 32.65             | 4.50                    | 0.00                       | 4.50               | 8.10                        | 24.55             |
| 60           | 51.88         | 11.08                  | 39.90             | 4.50                    | 0.00                       | 4.50               | 16.20                       | 23.70             |
| 120          | 31.69         | 6.77                   | 48.74             | 4.50                    | 0.00                       | 4.50               | 32.40                       | 16.34             |
| 180          | 23.75         | 5.07                   | 54.80             | 4.50                    | 0.00                       | 4.50               | 48.60                       | 6.20              |

Max. Storage Volume (m<sup>3</sup>) = 24.55 Drawdown Time (hr) = 1.52

AVAILABLE ROOFSTOP STORAGE

 Location
 Area (m<sup>2</sup>)
 Depth (m)
 Volume (m<sup>3</sup>)
 (Refer to Site Grading Plan Sheet C4, provided separately)

 Proposed Bidg
 853.84
 0.15
 42.69
 Note: Available Roof Storage Volume conservatively calculated using V = AxD/3

 Total Storage Required for 2-year (m<sup>3</sup>) =
 12.40
 Total Storage Required for 10-year (m<sup>3</sup>) =
 24.55

Therefore, the rooftop storage of 42.69 m<sup>3</sup> is sufficient to store 2-year through 100-year storm requirements on the roof of proposed building (A201).

# STRIK BALDINELLI C PLANNING · CIVIL · STRUCTURAL · MECHANICAL · ELECTRICAL

# LONDON LOCATION

1599 Adelaide St. N., Unit 301 London, ON N5X 4E8 P: 519-471-6667

# **KITCHENER LOCATION**

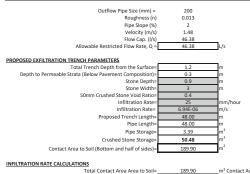
132 Queen St. S. Unit 4 Kitchener, ON N2G 1V9 P: 519-725-8093

CATCHMENT A202 STORAGE CALCULATIONS

Refer to the maximum capacity of the outflow pipe at CBMH2

Estimated as per Table 4.4 in the MECP based the infiltration rate of sandy loam

Soil type and infiltration rate estimated based on results found in the Geotechnical Investigation by CMT Engineering Inc., dated August 3, 2023. Exact infiltration rates are to be determined prior to detailed design.



| tact Area Area to Soil= 189.90 m <sup>2</sup> Contact Area to Soil |  |
|--|--|
| Infiltration Rate (I) = 25 mm/hr                                   |  |
| Infiltration Rate (I) = 6.94E-06 m/s                               |  |
| Site Infiltration = 0.001319 m <sup>3</sup> /sec                   |  |
| Site Infiltration = 4.748 m <sup>3</sup> /hr                       |  |
|  |  |
| 'A*I= 0.00132 m³/s   |  |

| VOLUME REQUIRED TO INFILTRATE 5mm OVER ENTIRE SITE     |          |                |
|--|----------|----------------|
| Site Area=   | 0.260182 | ha             |
| Site Area =  | 2601.82  | m <sup>2</sup> |
| Required Rainfall Depth to be stored over entire site= | 0.005    | m              |
| Volume Required to be Infiltrated=                     | 13.01    | m³             |
|  |          |                |

Surface Storage Drav

0.00 0.00

2-year: 100-year:

n Time (minutes)

min min

RAINFALL DATA:

Rainfall Data - Guelph Rainfall Intensity Duration

### STORAGE CALCULATIONS: 2 Yr Stm Event

|   |               |                        |                         |                             |              |                   | Overflow Pipe        |                      |                         |                             | 1                 |
|---|---------------|------------------------|-------------------------|-----------------------------|--------------|-------------------|----------------------|----------------------|-------------------------|-----------------------------|-------------------|
|   |               | Inflow, Q <sub>i</sub> | Inflow from Roof Drains | Volume In ( <del>V</del> i) | Infiltration | Infiltration      | Outflow              | Surface Outflow      | Allowable Total Outflow | Volume Out (¥ <sub>o)</sub> | Difference/       |
| Duration                                | Intensity "i" | 2.78*C*i*A             | [A201] (L/s)            | Q*t*60/1000                 | Rate         | Volume Out        | Q <sub>orifice</sub> | Q <sub>surface</sub> | Q <sub>total</sub>      | Q <sub>o</sub> *t*60/1000   | Storage           |
| (min.)                                  | (mm/hr)       | (l/s)                  |                         | (m <sup>3</sup> )           | (I/s)        | (m <sup>3</sup> ) | (I/s)                | (I/s)                | (I/s)                   | (m <sup>3</sup> )           | (m <sup>3</sup> ) |
| 5                                       | 145.01        | 45.84                  | 4.50                    | 15.10                       | 1.32         | 0.40              | 46.38                | 0.00                 | 47.70                   | 14.31                       | 0.79              |
| 10                                      | 86.95         | 27.48                  | 4.50                    | 19.19                       | 1.32         | 0.79              | 30.66                | 0.00                 | 31.98                   | 19.19                       | 0.00              |
| 20                                      | 52.13         | 16.48                  | 4.50                    | 25.17                       | 1.32         | 1.58              | 19.66                | 0.00                 | 20.98                   | 25.17                       | 0.00              |
| 30                                      | 38.65         | 12.22                  | 4.50                    | 30.09                       | 1.32         | 2.37              | 15.40                | 0.00                 | 16.72                   | 30.09                       | 0.00              |
| 60                                      | 23.17         | 7.32                   | 4.50                    | 42.57                       | 1.32         | 4.75              | 10.51                | 0.00                 | 11.82                   | 42.57                       | 0.00              |
| 120                                     | 13.89         | 4.39                   | 4.50                    | 64.02                       | 1.32         | 9.50              | 7.57                 | 0.00                 | 8.89                    | 64.02                       | 0.00              |
| 180                                     | 10.30         | 3.26                   | 2.97                    | 67.22                       | 1.32         | 14.24             | 4.91                 | 0.00                 | 6.22                    | 67.22                       | 0.00              |
| Max. Storage Volume (m <sup>3</sup> ) = |               |                        |                         |                             |              |                   | 0.79                 |                      |                         |                             |                   |
|   |               |                        |                         |                             |              |                   |                      |                      | Dra                     | wdown Time (hr) =           | 0.17              |

| 100 Yr St | m Event       | 1                      |                         |                             |              |                   |                          |                      |                         |                             |                   |
|-----------|---------------|------------------------|-------------------------|-----------------------------|--------------|-------------------|--------------------------|----------------------|-------------------------|-----------------------------|-------------------|
|           |               | Inflow, Q <sub>i</sub> | Inflow from Roof Drains | Volume In ( <del>V</del> i) | Infiltration | Infiltration      | Overflow Pipe<br>Outflow | Surface Outflow      | Allowable Total Outflow | Volume Out (¥ <sub>o)</sub> | Difference/       |
| Duration  | Intensity "i" | 2.78*C*i*A             | [A201] (L/s)            | Q*t*60/1000                 | Volume       | Volume Out        | Q <sub>orifice</sub>     | Q <sub>surface</sub> | Q <sub>total</sub>      | Q <sub>o</sub> *t*60/1000   | Storage           |
| (min.)    | (mm/hr)       | (l/s)                  |                         | (m <sup>3</sup> )           | (I/s)        | (m <sup>3</sup> ) | (l/s)                    | (I/s)                | (l/s)                   | (m <sup>3</sup> )           | (m <sup>3</sup> ) |
| 5         | 303.57        | 95.95                  | 4.50                    | 30.14                       | 1.32         | 0.40              | 46.38                    | 0.00                 | 47.70                   | 14.31                       | 15.82             |
| 10        | 185.45        | 58.62                  | 4.50                    | 37.87                       | 1.32         | 0.79              | 46.38                    | 0.00                 | 47.70                   | 28.62                       | 9.25              |
| 20        | 113.29        | 35.81                  | 4.50                    | 48.37                       | 1.32         | 1.58              | 38.99                    | 0.00                 | 40.31                   | 48.37                       | 0.00              |
| 30        | 84.92         | 26.84                  | 4.50                    | 56.41                       | 1.32         | 2.37              | 30.02                    | 0.00                 | 31.34                   | 56.41                       | 0.00              |
| 60        | 51.88         | 16.40                  | 4.50                    | 75.23                       | 1.32         | 4.75              | 19.58                    | 0.00                 | 20.90                   | 75.23                       | 0.00              |
| 120       | 31.69         | 10.02                  | 4.50                    | 104.52                      | 1.32         | 9.50              | 13.20                    | 0.00                 | 14.52                   | 104.52                      | 0.00              |
| 180       | 23.75         | 7.51                   | 4.50                    | 129.69                      | 1.32         | 14.24             | 10.69                    | 0.00                 | 12.01                   | 129.69                      | 0.00              |

Max. Storage Volume (m<sup>3</sup>) Drawdown Time (hr) 15.8

### CALCULATION FOR AVAILABLE STORAGE:

| ocation   | Area (m <sup>2</sup> ) | Depth (m)   | Volume (m <sup>3</sup> ) | (Refer to Site Servicing Plan Sheet C3, provided separately) |
|---|------------------------|---|--------------------------|--|
| CBMH2   | 1.13                   | 2.13  | 2.41                     |  |
| CBMH3   | 1.13                   | 1.71  | 1.93                     |  |
|   | Total Structur         | e Storage Available (m <sup>3</sup> ) =   | 4.34                     |  |
| vailable Storage in Pipes:                        |                        |   |                          |  |
| ocation   | Dia. (m)               | Length (m)  | Volume (m <sup>3</sup> ) | (Refer to Site Servicing Plan Sheet C3, provided separately) |
| CBMH2-CBMH3                                       | 0.3                    | 48.00   | 3.39                     |  |
|   | Total Pip              | e Storage Available (m <sup>3</sup> ) =   | 3.39                     |  |
|   |                        |   |                          |  |
| vailable Storage in Infiltration Galle<br>ocation | ry:<br>Length (m²)     | Depth (m)   | Volume (m <sup>3</sup> ) | 7  |
| Crushed Stone Storage                             | 48.00                  | 0.90  | 50.48                    | -1   |
| crusileu storie storage                           |                        | e Storage Available (m <sup>3</sup> ) =   | 50.48                    |  |
|   | TOLAT PIP              | e storage Available (III.) =  | 50.48                    |  |
|   | Total Undergroup       | d Storage Available (m <sup>3</sup> ) =   | 58.21                    | 7  |
|   | rotal ondergroun       | a storage Available (III ) =  | 30.21                    | <b>_</b>   |
| vailable Surface Storage:                         |                        |   |                          |  |
| ocation   | Area (m <sup>2</sup> ) | Depth (m)   | Volume (m <sup>3</sup> ) | (Refer to Site Grading Plan Sheet C4, provided separately)   |
| CBMH3   |                        | 0.05  | 0.20                     | Obtained from Civil3D  |
|   |                        |   |                          |  |
|   |                        |   | 0.20                     |  |
|   | Total Surfac           | e Storage Available (m³) =  | 0.20                     |  |
|   | Total Surfac           | e Storage Available (m <sup>3</sup> ) =   | 0.20                     |  |
|   |                        | e Storage Available (m <sup>3</sup> ) =<br>al Storage Available (m <sup>3</sup> ) = | 58.41                    | _<br>7   |
|   | Tot<br>Requ            |   |                          | 0 m³ of surface ponding utilized under 2-year event          |

Sufficient storage of 58.41 m<sup>3</sup> is provided to store 2vr. and 100vr storm storage requirements.

www.sbmltd.ca

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# **ADS OGS Sizing Summary**

| Project Name:        | 317 Speedvale Ave |        |                         |
|----------------------|-------------------|--------|-------------------------|
| Consulting Engineer: | SBM               |        |                         |
| Location:            | Guelph, ON        |        |                         |
| Sizing Completed By: | C. Neath          | Email: | cody.neath@ads-pipe.com |

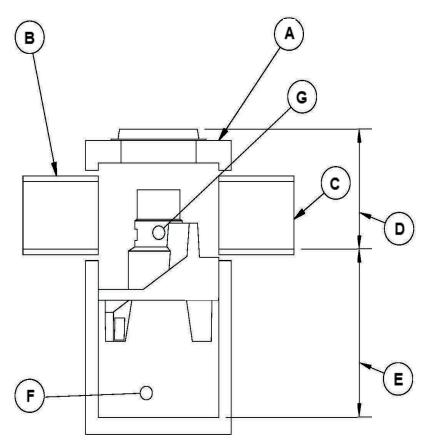
| Treatment Requirements |                |            |  |  |  |  |
|------------------------|----------------|------------|--|--|--|--|
| Treatment Goal:        | Enhanced (MOE) |            |  |  |  |  |
| Selected Parameters:   | 80% TSS        | 90% Volume |  |  |  |  |
| Selected Unit:         | F              | D-4HC      |  |  |  |  |

| Summary of Results |             |                |  |  |  |  |  |
|--------------------|-------------|----------------|--|--|--|--|--|
| Model              | TSS Removal | Volume Treated |  |  |  |  |  |
| FD-4HC             | 95.0%       | >90%           |  |  |  |  |  |
| FD-5HC             | 97.0%       | >90%           |  |  |  |  |  |
| FD-6HC             | 98.0%       | >90%           |  |  |  |  |  |
| FD-8HC             | 99.0%       | >90%           |  |  |  |  |  |
| FD-10HC            | 99.0%       | >90%           |  |  |  |  |  |

| FD-4HC Specification                        |          |  |  |  |  |  |
|---|----------|--|--|--|--|--|
| Unit Diameter (A):                          | 1,200 mm |  |  |  |  |  |
| Inlet Pipe Diameter (B):                    | 250 mm   |  |  |  |  |  |
| Outlet Pipe Diameter (C):                   | 250 mm   |  |  |  |  |  |
| Height, T/G to Outlet Invert (D):           | 840 mm   |  |  |  |  |  |
| Height, Outlet Invert to Sump (E):          | 1515 mm  |  |  |  |  |  |
| Sediment Storage Capacity (F):              | 0.78 m³  |  |  |  |  |  |
| Oil Storage Capacity (G):                   | 723 L    |  |  |  |  |  |
| Recommended Sediment Depth for Maintenance: | 440 mm   |  |  |  |  |  |
| Max. Pipe Diameter:                         | 600 mm   |  |  |  |  |  |
| Peak Flow Capacity:                         | 510 L/s  |  |  |  |  |  |

| Site Elevations:       |        |  |  |  |  |  |
|------------------------|--------|--|--|--|--|--|
| Rim Elevation:         | 330.97 |  |  |  |  |  |
| Inlet Pipe Elevation:  | 330.13 |  |  |  |  |  |
| Outlet Pipe Elevation: | 330.13 |  |  |  |  |  |

| Site Details                |                     |  |  |
|-----------------------------|---------------------|--|--|
| Site Area:                  | 0.2117 ha           |  |  |
| % Impervious:               |                     |  |  |
| Rational C:                 | 0.90                |  |  |
| Rainfall Station:           | Waterloo_Wellington |  |  |
| Particle Size Distribution: | Fine                |  |  |
| Peak Flowrate:              | 46.4 L/s            |  |  |



# Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



# Net Annual Removal Efficiency Summary: FD-4HC

| Rainfall Intensity <sup>(1)</sup>    | Fraction of<br>Rainfall <sup>(1)</sup> | FD-4HC<br>Removal<br>Efficiency <sup>(2)</sup> | Weighted Net-Annual<br>Removal Efficiency |
|--------------------------------------|--|--|---|
| mm/hr                                | %                                      | %  | %   |
| 0.50                                 | 0.3%                                   | 100.0%   | 0.3%                                      |
| 1.00                                 | 27.0%                                  | 100.0%   | 27.0%                                     |
| 1.50                                 | 3.2%                                   | 100.0%   | 3.2%                                      |
| 2.00                                 | 13.6%                                  | 100.0%   | 13.6%                                     |
| 2.50                                 | 7.2%                                   | 100.0%   | 7.2%                                      |
| 3.00                                 | 1.8%                                   | 99.6%  | 1.8%                                      |
| 3.50                                 | 6.7%                                   | 98.2%  | 6.6%                                      |
| 4.00                                 | 3.7%                                   | 97.0%  | 3.6%                                      |
| 4.50                                 | 1.5%                                   | 95.9%  | 1.4%                                      |
| 5.00                                 | 4.8%                                   | 95.0%  | 4.5%                                      |
| 6.00                                 | 3.3%                                   | 93.4%  | 3.1%                                      |
| 7.00                                 | 4.7%                                   | 92.1%  | 4.3%                                      |
| 8.00                                 | 2.8%                                   | 90.9%  | 2.5%                                      |
| 9.00                                 | 2.0%                                   | 89.9%  | 1.8%                                      |
| 10.00                                | 2.5%                                   | 89.1%  | 2.2%                                      |
| 20.00                                | 9.0%                                   | 83.5%  | 7.5%                                      |
| 30.00                                | 3.1%                                   | 80.4%  | 2.5%                                      |
| 40.00                                | 1.0%                                   | 78.3%  | 0.8%                                      |
| 50.00                                | 0.8%                                   | 76.7%  | 0.6%                                      |
| 100.00                               | 0.9%                                   | 71.9%  | 0.7%                                      |
| 150.00                               | 0.1%                                   | 69.2%  | 0.1%                                      |
| 200.00                               | 0.0%                                   | 0.0%   | 0.0%                                      |
|                                      | Total Not Amount                       |  | 05.0%                                     |
| Total Net Annual Removal Efficiency: |  | 95.3%  |   |
| Total Runoff Volume Treated:         |  |  | >90%                                      |

# Notes:

- (1) Rainfall Data: 1981:2007,HLY03 6149387, Waterloo/Wellington Airport, ON
- (2) Based on third party verified data and appoximating the removal of a PSD similar to the STC Fine distribution
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.