

Stantec Consulting Ltd. 100-300 Hagey Boulevard, Waterloo ON N2L 0A4

February 7, 2024

Project: 161413338

Mr. Michael Witmer

Development Engineering Division Department of Engineering and Transportation Services City of Guelph 1 Carden Street Guelph ON N1H 3A1

Dear Michael,

Reference: Infiltration Testing Results in Response to Second Submission Comments and in Support of Third Draft Plan Submission - 220 Arkell Road, City of Guelph, Ontario

Stantec Consulting Limited (Stantec) prepared a Hydrogeological Assessment report (Stantec, 2019¹) on behalf of Rockpoint Properties Inc. for the lands located at 220 Arkell Road in the City of Guelph, Ontario (the Site) in support of a Draft Plan Application. As a part of the hydrogeological assessment, a pre- and post-development water balance was completed for the Site, with this water balance in turn being updated to respond to first submission comments issued by the City of Guelph (City) (Stantec, 2023a²). As provided in the City of Guelph's second submission comments memo dated September 11, 2023, and titled 2nd Submission Engineering Comments, 220 Arkell Road, Comment No. 23 stated the following:

<u>Comment No. 23</u> – In-situ infiltration is required, as per the Development Engineering Manual (DEM). Infiltration rates cannot be determined based on laboratory or particle size distribution results. Please perform in-situ testing as per the DEM and update the findings accordingly. This must be completed during the draft plan stage to ensure water balance targets can be met without the need to revise plans and re-size infiltration galleries.

Based on their review, the Grand River Conservation Authority (GRCA) made a similar request in their letter dated September 7, 2023, and titled OZS19-017 – Second Submission of Draft Plan of Subdivision and Zoning By-law Amendment, 220 Arkell Road, City of Guelph:

Comment No. 11 – It is noted in the Revised Water Balance Calculations memo that in-situ infiltration tests will be conducted during detailed design to confirm that the soils are sufficiently permeable as well as determine hydraulic conductivities of the site soils. Please comment on whether the assumptions made in the water balance calculations with respect to infiltration capacity of the site soils, in the absence of in-situ testing, are conservative and whether there will be sufficient space available on the proposed lots to accommodate the required mitigation measures if the hydraulic conductivities obtained indicate that the site soils are less conducive to infiltration.

¹ Stantec Consulting Ltd. 2019. Hydrogeological Assessment, 220 Arkell Road, Guelph, ON. May 28, 2019.

² Stantec Consulting Ltd. 2023a. Revised Water Balance Calculations in Response to First Submission Comments Draft Plan Application – 220 Arkell Road, City of Guelph, Ontario. Technical Memorandum issued to City of Guelph dated March 29, 2023.

To address these previously mentioned comments, Stantec coordinated and implemented a field program to evaluate the infiltration capacity of on-Site soils in those areas of the property where low impact development (LID) infiltration infrastructure is proposed.

Figure 1 shows the location of the Site, with details on the field work performed and the subsequent results of this work being presented in the sections below. Figures and tables referenced in this report are presented in Attachments 1 and 2, respectively, with borehole logs provided in Attachment 3.

Methods

From November 13 to 16, 2023, Moser Landscape Group (MLG) excavated 14 test pits (TP01-23 to TP14-23; Figure 1) in the footprints of proposed LID infiltration infrastructure (i.e., infiltration galleries).

Under the observation of Stantec, MLG excavated the previously mentioned test pits to depths ranging from 0.6 m and 2.8 m below ground surface (BGS), representing the projected base elevation of the future infiltration galleries. At those locations where an infiltration gallery base would occur at an elevation higher than the existing grade, MLG only removed the topsoil layer to expose the underlying native soil deposits (i.e., TP01-23 to TP03-23, TP06-23, TP09-23, TP12-23, and TP14-23). Stantec determined the test pit excavation depths / elevations by following the protocols outlined in Appendix C of the Credit Valley Conservation (CVC) and Toronto and Region Conservation (TRCA) (2010³) *Low Impact Stormwater Management Planning and Design Guideline,* which requires that the excavations extend to the projected base elevation of a given infiltration gallery for the performing of in-situ soil infiltration testing.

Stantec classified the soils targeted for infiltration testing using the ASTM guideline for visual-manual description and identification of soils (ASTM D2488-00). Once each test pit was no longer required, MLG backfilled the excavations to the existing grade.

Assessment of the infiltration potential for the on-Site soils involved the use of a Guelph Permeameter (a constant head permeameter designed to measure in-situ vertical hydraulic conductivities of a given substrate). At the base of each test pit, Stantec personnel used a hand auger to drill three 50 mm diameter cylindrical holes into the native soil to be tested, with the depths of these holes ranging from 0.2 m to 0.3 m BGS. The Guelph Permeameter was then filled with water, inserted into the hole while making a concerted effort to avoid knocking debris into the hole, and then stabilized against the substrate. Once set-up, Stantec proceeded to record the eventual steady-state rate of water recharge into the soil. The infiltration rate for each soil tested was converted from the measured vertical hydraulic conductivity to an infiltration rate using the established relationship between vertical hydraulic conductivity and infiltration rate presented by the CVC/TRCA (2010). Stantec performed two successful infiltration tests in each test pit, except for TP03-23, TP07-23 and TP12-23 where one of the tests failed. Table 1 summarizes the results of the soil infiltration testing.

³ Credit Valley Conservation - Toronto and Region Conservation Authority (CVC-TRCA), 2010. Low Impact Development Stormwater Management Planning and Design Guide – Version 1.0.

Although recommended in CVC/TRCA (2010), the test pits were not extended an extra 1.5 m below their initial depth for additional infiltration testing given that the subsurface soil profile near the testing locations is relatively uniform in structure and often characterized by an elevated groundwater table. As shown in boreholes drilled near the infiltration testing locations, the soil profile largely consists of silty sand to sandy silt (ranging from diamicton to glaciofluvial sediments) up to 3.8 m below the base elevations of the proposed infiltration galleries (Figure 1; Attachment 3).

Results

Vertical hydraulic conductivities for the native silty sand to sandy silt deposits exposed at the base of the test pits and measured using the Guelph Permeameter ranged from 1.0×10^{-5} m/s to 2.8×10^{-7} m/s, equating to infiltration rates ranging from 33 mm/hour to 87 mm/hour (Table 1).

In the absence of testing the soil layer at a depth of 1.5 m below the proposed base elevation of the infiltration galleries, as an alternative Stantec took the high and low infiltration rate estimated from the two in-situ tests completed in each test pit to calculate a ratio and assign a subsequent safety correction factor (from Table C2 of CVC/TRCA (2010)) to apply to the geometric mean infiltration rate calculated for the test pit. As shown in Table 2, a maximum safety correction factor of 3.5 is applicable to most of the test pit locations, resulting in design infiltration rates ranging from 10 mm/hour to 28 mm/hour across the Site. This range of infiltration rates exceeds the minimum value of 4.8 mm/hour previously used by Stantec to size the on-Site infiltration galleries (Stantec, 2023b⁴).

To conclude, the investigation confirms that the on-Site soils can support the updated post-development infiltration strategy proposed in Stantec (2024a⁵) and, subsequently, that water balance targets can be achieved for the Site as presented in Stantec (2024b⁶).

⁴ Stantec Consulting Limited. 2023b. 220 Arkell Road, Guelph – Revised Preliminary Servicing, Grading and Stormwater Management Report. April 2023.

⁵ Stantec Consulting Limited. 2024a. 220 Arkell Road, Guelph, Revised Preliminary Servicing, Grading and Stormwater Management Report, Addendum No.1 – Section 5.0 Stormwater Management. February 2024.

⁶ Stantec Consulting Limited. 2024b. Revised Water Balance Calculations in Response to First and Second Submission Comments Draft Plan Application - 220 Arkell Road, City of Guelph, Ontario (Third Submission). February 2024.

Closure

We trust that the above information meets your current requirements. Please contact the undersigned if you need additional information.

Regards,

Stantec Consulting Ltd.

Grant Whitehead, MES, P.Geo. (Limited) Senior Hydrogeologist Phone: 519 585 7400 Cell: (519) 502-8933 grant.whitehead@stantec.com

Attachments:	Attachment 1:	Figure 1 – Site Location
	Attachment 2:	Table 1 – Infiltration Test Results
		Table 2 – Design Infiltration Rate Calculations
	Attachment 3	Borehole Logs

Attachment 1 Figure 1 – Tet Pit / Infiltration Testing Locations





Attachment 2 Table 1 – Infiltration Test Results Table 2 – Design Infiltration Rate Calculations

TABLE 1 INFILTRATION TESTING RESULTS

Test Pit	Test	Ground	Tes	t Pit	Projected	Ver	tical Hydrau	lic	Infiltration	Soil Substrate Tested
Location	No.	Surface	Excavati	on Depth	Infiltration Gallery	(Conductivity	У	Rate ⁽²⁾	
ID		Elevation ⁽¹⁾			Base Elevation			Geomean		
		(m AMSL)	(m BGS)	(m AMSL)	(m AMSL)	(cm/s)	(m/s)	(m/s)	(mm/hr)	
Guelph Perme	ameter 1	Testing								
TP01-23	1	333 75	0.95	332.80	335.00	9.7E-05	9.7E-07	14F-06	51	Fine SAND some silt
11 01 20	2	000.10	0.90	332.85	000.00	2.0E-04	2.0E-06	1.42 00	01	
TP02-23	1	334 25	0.84	333.41	335.00	4.6E-04	4.6E-06	4 2E-06	68	Silty SAND to SILT with some sand
11 02-20	2	004.20	0.75	333.50	000.00	3.9E-04	3.9E-06	4.2L-00	00	City CANE to CIET with Some Sand
TP03-23	1	334.00	1.05	332.95	334.86	3.2E-04	3.2E-06	-	63	Fine SAND
TP04-23	1	338.40	1.70	336.70	336.80	2.1E-04	2.1E-06	1 7E-06	53	SILT with some fine sand (DIAMICTON)
11 04-23	2	550.40	1.75	336.65	550.00	1.4E-04	1.4E-06	1.7 -00		
TP05-23	1	338 50	1.15	337.35	337.40	3.4E-05	3.4E-07	2 8E-07	33	Sandy SILT to Fine SAND
11 00-20	2	000.00	1.25	337.25	007.40	2.3E-05	2.3E-07	2.00-01		Gandy GIET to TINE GAND
TP06-23	1	337.20	0.98	336.22	338.00	2.2E-04	4 2.2E-06 2.9E-06		61	Sandy SILT to Silty SAND (DIAMICTON)
11 00-20	2	007.20	0.94	336.26	000.00	3.9E-04	3.9E-06	2.52-00	01	Sandy SIET to Sinty SAND (BIAMISTON)
TP07-23	1	337.50	1.50	336.00	336.30	1.7E-04	1.7E-06	-	53	Gravelly SAND, some cobbles
TP08-23	1	340.00	2.80	337.20	337 30	6.1E-04	6.1E-06	3.2E-06	63	Fine SAND, some coarse sand and cobbles
11 00-20	2	040.00	2.70	337.30	007.00	1.7E-04	1.7E-06	0.2L-00	00	The CANE, some coalse sand and cobbles
TP09-23	1	338 50	1.05	337.45	338 10	1.3E-03	1.3E-05	1.0E-05	86	Silty Fine SAND
11 00 20	2	000.00	1.05	337.45	000.10	8.4E-04	8.4E-06	1.02 00	00	
TP10-23	1	339 50	1.93	337.57	337.84	3.9E-04	3.9E-06	4 3E-06	68	SILTY SAND (DIAMICTON)
11 10-23	2	000.00	1.97	337.53	007.04	4.7E-04	4.7E-06	4.02-00	00	
TP11-23	1	340.00	2.20	337.80	337 84	2.4E-04	2.4E-06	5.8E-07	40	SILT (DIAMICTON)
11 11 20	2	040.00	2.20	337.80	001.04	1.4E-05	1.4E-07	0.02 01	40	
TP12-23	1	335.80	0.63	335.00	336.30	1.1E-03	1.1E-05	-	87	Silty Fine SAND, some coarse sand
TP13-23	1	336.30	0.99	335.31	335 50	7.2E-05	7.2E-07	2.3E-06	58	Silty CLAY to Clavey SILT
11 10-20	2	000.00	0.81	335.49	000.00	7.3E-04	7.3E-06	2.02-00	00	
TP14-23	1	338.20	0.83	337.37	338.03	1.7E-04	1.7E-06	4 3E-06	68	Sandy SILT to Silty SAND (DIAMICTON)
11 17-25	2	000.20	0.95	337.25	000.00	1.1E-03	1.1E-05	4.0∟-00	00	
					G	EOMEAN =	3.1E-06	-	62	

Notes:

(1) Ground surface elevation estimated from existing condition / pre-development topographic contour mapping prepared by J.D. Barnes Limited (January 2023).

(2) Infiltration rate calculated based on established relationship between vertical hydraulic conductivity and infiltration rate presented in *Credit Valley Conservation and Toronto and Region Conservation (2010) Low Impact Stormwater Management Planning and Design Guideline - Version 1.0.* The estimated infiltration rate for the soil substrate in each test pit is based on the geometric mean vertical hydraulic conductivity estimated for that pit.

TABLE 2 - DESIGN INFILTRATION RATE CALCULATIONS

Proposed Infiltration Facility								
Test Pit Location / ID	TP0	1-23	TP0	2-23	TP0	3-23	TP0	4-23
Base of Facility								
High Vertical K (m/s) / Infiltration Rate (mm/hr) ⁽¹⁾	2.0E-06	56	4.6E-04	70	3.2E-06	63	2.1E-06	56
Low Vertical K (m/s) / Infiltration Rate (mm/hr)	9.7E-07	46	3.9E-04	66	-	-	1.4E-06	51
Ratio ⁽²⁾		1.2		1.1		-		1.1
Safety Factor ⁽³⁾		3.5		3.5		3.5		3.5
Design Infiltration Rate		16		20		18		16

Test Pit Location / ID	TP0	5-23	TP0	6-23	TP0	7-23	TP08	3-23
Base of Facility								
High Vertical K (m/s) / Infiltration Rate (mm/hr) ⁽¹⁾	3.4E-07	35	3.9E-06	67	1.7E-06	53	6.1E-06	75
Low Vertical K (m/s) / Infiltration Rate (mm/hr)	2.3E-07	31	2.2E-06	57	-	-	1.7E-06	53
Ratio ⁽²⁾		1.1		1.2		-		1.4
Safety Factor ⁽³⁾		3.5		3.5		3.5		3.5
Design Infiltration Rate		10		19		15		21

Test Pit Location / ID	TP0	9-23	TP1)-23	TP1 ⁴	1-23	TP1	2-23
Base of Facility								
High Vertical K (m/s) / Infiltration Rate (mm/hr) ⁽¹⁾	1.3E-05	92	4.7E-06	70	2.4E-06	58	1.1E-05	88
Low Vertical K (m/s) / Infiltration Rate (mm/hr)	8.4E-06	82	3.9E-06	67	1.4E-07	27	-	-
Ratio ⁽²⁾		1.1		1.0		2.1		-
Safety Factor ⁽³⁾		3.5		2.5		3.5		3.5
Design Infiltration Rate		26		28		17		25

Test Pit Location / ID	TP1	3-23	TP14-23				
Base of Facility							
High Vertical K (m/s) / Infiltration Rate (mm/hr) ⁽¹⁾	7.3E-06	79	1.1E-05	88			
Low Vertical K (m/s) / Infiltration Rate (mm/hr)	7.2E-07	42	1.7E-06	53			
Ratio ⁽²⁾		1.9		1.7			
Safety Factor ⁽³⁾		3.5		3.5			
Design Infiltration Rate		23		25			

Notes:

- (1) Infiltration rate calculated based on established relationship between vertical hydraulic conductivity and infiltration rate presented in *Credit* Valley Conservation and Toronto and Region Conservation (2010) Low Impact Stormwater Management Planning and Design Guideline Version 1.0.
- (2) Given the structural consistency of the geological deposits / soils present beneath the Site together with the presence of an elevated groundwater table, Stantec did not complete additional infiltration testing of soils situated 1.5 m below the base of the proposed LID infiltration galleries. As an alternative, Stantec calculated the ratio and subsequent Safety Factor using the high and low vertical hydraulic conductivity results estimated for the soil at the projected base elevation of each gallery.
- (3) Table C2 provided on Page C8 (Appendix C) of the CVC/TRCA (2010) Low Impact Stormwater Management Planning and Design Guideline Version 1.0.

Low Impact Development Stormwater Management Planning and Design Guide

Table C2: Safety correction factors for calculating design inflitration f	Table C2: Safe	v correction fa	actors for	calculating	design	infiltration	rates
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Ratio of Mean Measured Infiltration Rates ¹	Safety Correction Factor ²
≤1	2.5
1.1 to 4.0	3.5
4.1 to 8.0	4.5
8.1 to 16.0	6.5
16.1 or greater	8.5

Source: Wisconsin Department of Natural Resources. 2004. Conservation Practice Standards. Site Evaluation for Stormwater Infiltration (1002). Madison, WI.

Notes:

- Ratio is determined by dividing the geometric mean measured infiltration rate at the proposed bottom elevation of the BMP by the geometric mean measured infiltration rate of the least permeable soil horizon within 1.5 metres below the proposed bottom elevation of the BMP.
- 2. The design infiltration rate is calculated by dividing the geometric mean measured infiltration rate at the proposed bottom elevation of the BMP by the safety correction factor.

Attachment 3 Borehole Logs

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		- moist to saturated			10-	ss	5	300	26			•							23 28 41 8				
1					12-			610															
4					13- 14-																		
					15-	<u> </u>		420											-				
5	329.1				16-	∦ss	6	<u>430</u> 610	28			::: :							-				
1		END OF BOREHOLE at approximately 5.2 m below existing			18-														-				
6		grade.			19-																		
1.1		Water level measured at 2.4 m			20																		
7		below grade on completion of drilling	ŝ		22 -													Ē					
(i			8		23-																		
		Monitoring well installed with 50 mm screen from approximately 1.5			25-														•				
8-		m to 4.6 m below grade.			26-														-				
					28-													-	-				
9					29 - 30 -														-				
1					31-													Ē	-				
10					32-														-				
					34-													E					
					35-													E					
					37-																		
38-																			1				
12-	14 2 2 11				1 39 -						Fie	liiii ld Van	e Test,	kPa	: [: : : :		1::::	:::: <u>}</u>					
											Rei	moulde sket Pe	ed Van	e Test, heter Ta	kPa est. ku	Pa							

	S	tantec	B		EH N: 48	[OI 319 1	.E 11 F	REC 2: 565	C OR 287	D					BI	H04	4-1	7	ş	Sheet	1 of 1
C		Carson Reid Homes Ltd.	N											_	PRO	JECI	Г No	• .	1	<u>6141</u>	<u>3338</u>
	ATES: F	ORING April 5, 2017	1			WAT	ER I	EVEL							DA1 TPC	UM	– Vат	ION		<u>- Gec</u> 34	40.86
							SAN			U	NDF	RAIN	ED S	— HEA	RS.	TRE	NGT		a)		
TH (m)	ATION (m)	STRATA DESCRIPTION	A PLOT	S LEVE	TH (ft)		2	(mm) (%)	≡ %)		-	50		10	0		150	W _P	20 w	00 	
DEP			STRAI	WATEI	DEP	ТҮРЕ	NUMBER	COVERY R(%)/SC	N-VALUI DR RQD('	WAT DYN STA	ier C Iamic Ndaf	CONTE CONI RD PEI	E PEN	ATTER ETRATION	RBER(TION T TEST	G LIMI TEST, ', BLO'	TS BLOV WS/0.:	₩ ¥\$/0.3r 3m	−Ö n ▼		EMARKS & RAIN SIZE
0 -	340.0	Grass Field			0	_		RE(TC		10	0 2	0 3	0 4	0 5	0 6	i0 7	70 8	80 9	0 1	00 _{GR}	(%) SA SI CL
	<u>339.7</u> 339.3	280 mm TOPSOIL Loose, brown, SAND (SM)	<u> </u>		1 - 2 -	ss	1	<u>230</u> 610	8	•	o		100								
1-		- some gravel, trace silt - wet			- 3 - 4 -	ss	2	<u>460</u> 610	11	C.					2005			1455			
2		Sand with Gravel (SM) TILL - moist			5 - 6 -	ss	3	<u>430</u> 610	26	o											
					7 - 8 -	ss	4	460	67	0						•				- 18	36 37 9
3 -					9- 10-			610												Ē	
					11 - 12 -	ss	5	<u>460</u> 610	87	Ø											
4		2			13- 14-																17
					15-	X ss	6	250	50/	0									.>>	27	32 32 9
5-					16- 17-			250												-	
					18- 19-																
0-		- wet		I	20-	×ss	7	<u>130</u> 130	- <u>50/</u> -130	С									>>		
×					22-															E	
					23- 24-													****		Ē	
					25-	M ee		460	04	X											
8-	331.8				20-27	1 22	0	610	- 04												
		approximately 8.2 m below existing			28-																
9 -		grade.			29- 30-								****	1111						Ē	18
		Water level measured at 6.4 m			31-		:														
10	2	drilling.			32-															- -	
		Monitoring well installed with 50			34-															E	
11-		mm screen from approximately 4.6 m to 7.6 m below grade.			36-															E - -	
					37- 38-								100000							E E F	
12-		· · · · · · · · · · · · · · · · · · ·			39-						Fiel	d Ve	ne To	et La) Da					FI	
											Rer	nould	led V	ane T	a 'est, k	cPa					
										Δ	Poc	ket P	enetr	omete	er Te	st, kP	'a				

Monitoring Well: MW101-22

Project: 220 Arkell Road Client: Carson Reid Homes Ltd. Guelph ON Location: 161413338 Number: Field investigator: J. Hale Contractor: Aardvark Drilling Inc.

Method: CME 850/Hollow Stem Auger/Split Spoon Date started/completed: 10-Mar-2022 Ground surface elevation: 338.22 m AMSL Top of casing elevation: 339.08 m AMSL 4819147 Easting: Northing: 565227

				SUBSURFACE PROF	FILE		SAMPLE DETAILS			ILS	INSTALLATION DETAILS	
(1	Depth Gra		phic og	Stratigraphic Descri	ption	Elevation (m AMSL) Depth (m BGS) 339.08	Sample Number	Sample Type	Recovery	N Value	Diagram	Description
0	- - 0 0 0		Ground Surface			338.22 0.00				— Above Ground Casing 0.86 m stick-up		
	-	<u>//</u> . <u>\ (</u>	<u>,,,,</u> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Some clay, trace sand, organics, very dark greyish be	rown, moist, very loose	337.46	1	SS	8" 33%	3		
5				Trace organics, dark brown, moist, loose		336.70	2	SS	6" 25%	7		Water level 1.19 m BGS 31-Mar-2022
	- 2 -			SANDY SILI (TILL) Brown, very moist, loose		1.52	3	SS	6" 25%	6		 Holeplug 0 to 4.18 m BGS
10				Trace cobbles and gravel from 2.44 to 3.05 m, very s	tiff		4	SS	8" 33%	26		
S	-			Hard		334.41	5	SS	16" 67%	78		 203 mm Borenole Diameter 0 to 7.62 m BGS
21/23 SHULICHINS	4 			SILTY SAND (TILL) Some gravel, brown, moist, hard		3.81	6	SS	10" 42%	50		
MPLAIE.GUI 12/							7	SS	8" 33%	50		
NIEC-DAIA	6					332.12	8	SS	8" 33%	50		
	-			SILT (TILL) Trace sand, gravel and cobbles, grey, moist, hard		6.10 331.36	9	SS	10" 42%	50		No. 10 Slot Schedule 40 PVC Screen 4.48 to 7.53 m BGS
AKKELL_RUAU	+			No soil sample collected		6.86						
25 25				End of Borehole		7.62		·	I	I	1	
BOREHOLE AND WEL	Scree Sand Well S	en Interv Pack Ir Seal Int	val: nterva erval	4.48 - 7.53 m BGS Not al: 4.48 - 7.53 m BGS m / : 0.00 - 4.18 m BGS m E SS n/a	tes: AMSL - metres above mean sea level 3GS - metres below ground surface - split-spoon sample - not available		AGS -	Above (Ground	Surface		
STANIECI	Drawn By/Checked By: SH/ Sheet 1 of 1											



Monitoring Well: MW102-22

Project: 220 Arkell Road Client: Carson Reid Homes Ltd. Guelph ON Location: 161413338 Number: Field investigator: J. Hale Aardvark Drilling Inc. Contractor:

Method: Date started/completed: 10-Mar-2022 Ground surface elevation: 340.06 m AMSL Top of casing elevation: 340.89 m AMSL Easting: 4819086 Northing: 565229

CME 850/Hollow Stem Auger/Split Spoon

SUBSURFACE		SUBSURFACE PRO	OFILE		:	SAMPLE	DETA	ILS	INSTALLATION DETAILS		
De	pth	Graphic Log	Stratigraphic Desc	ription	Elevation (m AMSL) Depth (m BGS)	Sample Number	Sample Type	Recovery	N Value	Diagram	Description
(ft)	(m)				340.89						
- - 0 —		<u>- 1/2</u> , <u>1/2</u> 	Ground Surface TOPSOIL Organics, silt, some clay and sand, trace silt, dark	brown, moist, loose	<u>340.06</u> 0.00	1	SS	20"	6		← Above Ground Casin 0.83 m stick-up
-	-	<u></u>	SAND		339.30 0.76			83%			
-			Trace silt, and trace gravel, moist, loose		000 54	2	SS	12" 50%	7		
5 —	- 2		SILTY SAND Some coarse gravel, moist, dense		1.52	3	SS	14" 58%	31		← Holeplug
-	-		SAND Some gravel, trace silt, light brown, moist, dense		337.77 2.29	4	SS	20" 83%	34		0 to 4.16 m BGS
10 — -			SILT (TILL) Some sand and gravel, light brown, moist, hard		3.05	5	SS	20" 83%	50		 203 mm Borehole Diameter 0 to 7.62 m BGS Water Level 3.09 m BGS
-	- 4					6	SS	12" 50%	50		21-Mar-2022
-	-					7	SS	8" 33%	50		
-	- 6					8	SS	24" 100%	66		No.2 Silica Sand 4.16 to 7.51 m BGS
-	-		No gravel, trace sand, wet			9	SS	18" 75%	86		No. 10 Slot Schedule 40 PVC Screen 4.46 to 7.51 m BGS
-	-		Some gravel, trace sand, light brown-grey, wet		222.44	10	SS	3" 13%	n/a		
25 —	8		End of Borehole		7.62		I]	
	Screen I Sand Pa Well Se	Interval: ack Interv al Interva	4.57 - 7.51 m BGS N al: 4.57 - 7.51 m BGS m l: 0.00 - 4.16 m BGS s n	lotes: n AMSL - metres above mean sea level n BCS - metres below ground surface S - split-spoon sample /a - not available		AGS -	Above G	Ground	Surface		
(St	antec	Drawn By/Checked By: SH/							Sheet 1 of 1



Monitoring Well: MW103-22

Project:	220 Arkell Road	Method:	CME 850/Hollow Stem Auger/Split Spoon
Client:	Carson Reid Homes Ltd.	Date started/completed:	10-Mar-2022
Location:	Guelph ON	Ground surface elevation:	: 335.01 m AMSL
Number:	161413338	Top of casing elevation:	335.85 m AMSL
Field investigator:	J. Hale	Easting:	4819009
Contractor:	Aardvark Drilling Inc.	Northing:	565182

			SUBSURFACE I	E PROFILE			SAMPLE DETAILS				INSTALLATION DETAILS	
De (ft)	pth (m)	Graphic Log	Stratigraphic D	escription	Elevation (m AMSL) Depth (m BGS) 335.85	Sample Number	Sample Type	Recovery	N Value	Diagram	Description	
(ff) (ff) (f) (f) (f) (f) (f) (f)	(m) 		Ground Surface TOPSOIL Sandy silt, trace organics, moist, loose No Recovery - cobble in tip of split spoon. SAND Trace silt and gravel, brown, moist, compact SILT (TILL) Trace sand and gravel, brown, moist, very stiff		335.85 335.01 0.00 334.25 0.76 333.49 1.52 331.96 3.05	1 2 3 4 5	SS SS SS SS SS SS	16" 67% 0" 0% 	9 22 25 28 24		 Above Ground Casing 0.84 m stick-up Water Level 0.7 m BGS 31-Mar-2022 Holepiug 0 to 2.52 m BGS 203 mm Borehole Diameter 0 to 6.10 m BGS 	
- - 15 — -	4 		SILTY SAND (TIFF) Trace gravel, brown, wet, very stiff		331.20 3.81	6	ss ss	10" 42% 12" 50%	22		 No.2 Silica Sand 2.52 to 5.87 m BGS No. 10 Slot Schedule 40 PVC Screen 2.82 to 5.87 m BGS 	
20	- 6		Hard End of Borehole		328.91 6.10	8	SS	8" 33%	50			
25	- 8 Screen I Sand P <i>a</i> Well Se	nterval: ick Interva	2.82 - 5.87 m BGS al: 2.82 - 5.87 m BGS l: 0.00 - 2.52 m BGS	Notes: m AMSL - metres above mean sea level m BGS - metres below ground surface SS - split-spoon sample n/a - ont available		AGS -	Above C	Ground	Surface			
(Stantec Drawn By/Checked By: SH/ Sheet 1 of 1											



Monitoring Well: MW104-22

Project:	220 Arkell Road	Method:	CME 850/Hollow Stem Auger/Split Spoon
Client:	Carson Reid Homes Ltd.	Date started/completed:	11-Mar-2022
Location:	Guelph ON	Ground surface elevation:	: 337.97 m AMSL
Number:	161413338	Top of casing elevation:	339.01 m AMSL
Field investigator:	A.Singh	Easting:	4819065
Contractor:	Aardvark Drilling Inc.	Northing:	565136

		SUBSURFACE PROFILE		SAMPLE DETAILS			MLS	INSTALLATION DETAILS	
Depth	Graphic Log	Stratigraphic Description	Elevation (m AMSL) Depth (m BGS)	Sample Number	Sample Type	Recovery	N Value	Diagram	Description
(ft) (m)			339.01						
	<u>x1 /2</u> . x1 1/1 - <u>24 - 1/2</u> - <u>24 - 6</u> - <u>24</u>	Ground Surface TOPSOIL Dark brown, loose	<u>337.97</u> 0.00	1	SS	12" 50%	1-1-2-3 (3)		Above Ground Casing 1.04 m stick-up
		SANDY SILT Dark brown, soft	0.76	2	SS	9" 38%	1-1-3-2 (4)		Holeplug 0 to 2.47 m BGS
5		SILTY SAND Brown, moist. compact Grey	1.52	3	SS	16" 67%	2-4-20-12 (24)		< ── 203 mm Borehole
		No recovery	2.29	4	SS	0" 0%	7-9-30-19 (39)		Diameter 0 to 6.10 m BGS
	\bigcirc	SILTY SAND Trace gravel, brown, dense	334.92	5	SS	16" 67%	6-20-14-40 (34)		2.88 m BGS 31-Mar-2022
4 		GRAVEL & COBBLES Trace sand, very dense	3.81	6	SS	4" 17%	21-50 (71)		No.2 Silica Sand 2.47 to 5.82 m BGS
15 — 		SILTY SAND Brown, wet, dense	4.57	7	SS	2" 8%	25-16-24-31 (40)		No. 10 Slot Schedule 40 PVC Screen 2.77 to 5.82 m BGS
		CLAYEY SILT Brown, hard	332.33 5.64 331.87	8	SS	16" 67%	2-2-12-50 (14)		
		End of Borehole	6.10	I		<u> </u>	I]	
Screen Sand Pa Well Se	Interval: ack Interv al Interva	2.77 - 5.82 m BGS Notes: ral: 2.77 - 5.82 m BGS m AMSL - metres above mean sea level il: 0.00 - 2.47 m BGS m BGS - metres below ground surface		AGS -	Above (Ground	Surface		

STANTEC BOREHOLE AND WELL V2 161413338_ARKELL_ROAD_LOGS.GPJ STANTEC - DATA TEMPLATE.GDT 12/21/23 SHUTCHINSON

m BGS - metres below ground surface SS - split-spoon sample n/a - not available

Monitoring Well: MW105-22

Project:	220 Arkell Road	Method:	CME 850/Hollow Stem Auger/Split Spoon
Client:	Carson Reid Homes Ltd.	Date started/completed:	11-Mar-2022
Location:	Guelph ON	Ground surface elevation	: 338.42 m AMSL
Number:	161413338	Top of casing elevation:	339.41 m AMSL
Field investigator:	A.Singh	Easting:	4819101
Contractor:	Aardvark Drilling Inc.	Northing:	565078

			SUBSURFACE PROFILE	ROFILE			E DETA	JILS	IN	INSTALLATION DETAILS	
De (ft)	pth (m)	Graphic Log	Stratigraphic Description	Elevation (m AMSL) Depth (m BGS)	Sample Number	Sample Type	Recovery	N Value	Diagram	Description	
	() -			339.41					ĺ		
0	0	<u>x 1,</u>	Ground Surface TOPSOIL Silty sand, dark brown, loose	338.42 0.00	1	SS	14" 58%	1-2-2-1 (4)		Above Ground Casing 0.99 m stick-up	
-	-		SANDY SILT Trace gravel, brown, very stiff	337.48 0.94 336.90	2	SS	12" 50%	2-5-12-12 (17)			
5	2		SILTY SAND Dark brown, moist SAND Trace gravel, light brown SILTY SAND	$ \begin{array}{r} 1.52\\336.80\\1.62\\336.59\\1.83\end{array} $	3	SS	16" 67%	3-7-7-10 (14)			
10			\Brown, stiff CLAYEY SILT (TILL) Brown, moist, firm	2.29	4	SS	17" 71%	2-3-6-12 (9)		₩ater Level 2.69 m BGS 31-Mar-2022	
-	-		Trace graver, ury, fraiu		5	SS	13" 54%	22-42-50 (92)		Holeplug 0 to 5.60 m BGS 203 mm Borehole Diameter	
NOSNIH: 15 -	-4 -		GRAVEL	333.85 4.57	6	SS	8" 33%	30-50 (50)		0 to 9.14 m BGS	
12/21/23 SHUI	- - -		Trace sand, very dense SILTY SAND (TILL) Trace second beau band	333.09 5.33	7	SS	8" 33%	20-50 (70)			
- - 20 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02 - 02	6		No gravel from 6.10 to 6.86 m BGS, moist		8	SS	14" 58%	8-16-20-19			
	1- 1 1		CLAYEY SILT (TILL) Trace gravel, grey, wet, hard	331.56 6.86	9	SS	67%	(36)			
25 -			Irace gravel from 6.93 to 7.62 m, hard.		11	55	67%	(80) 50		No.2 Silica Sand 5.60 to 8.95 m BGS No. 10 Slot Schedule 40	
	_		No soil collected				42%	(U)		5.90 m to 8.95 m BGS	
8			End of Borehole	329.28 9.14					j::::::		
	Screen I Sand Pa Well Sea	nterval: lick Interv al Interva	5.90 - 8.95 m BGS Notes: al: 5.90 - 8.95 m BGS m AMSL - metres above mean sea level m BGS - metres below ground surface SS - split-spoon sample n/a - not available n/a - not available		AGS -	Above (Ground	Surface			
	N/a - not available Drawn By/Checked By: SH/ Sheet 1 of 1										



Monitoring Well: MW106-22

Project:	220 Arkell Road	Method:	CME 850/Hollow Stem Auger/Split Spoon
Client:	Carson Reid Homes Ltd.	Date started/completed:	11-Mar-2022
Location:	Guelph ON	Ground surface elevation	: 334.06 m AMSL
Number:	161413338	Top of casing elevation:	335.03 m AMSL
Field investigator:	A.Singh	Easting:	4819055
Contractor:	Aardvark Drilling Inc.	Northing:	565006

			SUBSURFACE	PROFILE			SAMPLE	DETA	ILS	INSTALLATION DETAILS	
De (ft)	epth (m)	Graphic Log	Stratigraphic D	escription	Elevation (m AMSL) Depth (m BGS) 335.03	Sample Number	Sample Type	Recovery	N Value	Diagram	Description
0	- - - - - - - - - - - - - - - -		Ground Surface TOPSOIL Clayey silt, dark brown, firm SILTY SAND Brown, moist, compact		334.06 0.00 333.07 0.99 332.54	2	SS	15" 63% 14" 58%	3-3-3-3 (6) 3-8-8-5 (16)		Above Ground Casing 0.97 m stick-up < <hasdata(water Level<cr>0.97 m BGS 31-Mar-2022Water Level</cr></hasdata(water
	- - - - - - - - - - -		CLAYEY SILT Dark brown, stiff, moist SILTY SAND Brown, moist, loose Wet at 2.29 m BGS		1.52 332.46∫ 1.60	3 4 5	SS SS SS	16" 67% 17" 71% 18" 75%	1-5-4-6 (9) 1-3-4-3 (7) 2-2-6-4 (8)		¹ Holeplug 0 to 2.60 m ← 203 mm Borehole Diameter 0 to 6.10 m
TEMPLATE.GDT 12/21/23 SHUTCHIN 51	4 		CLAYEY SILT (TILL) Greyish brown, wet, hard Grey, dry from 4.65 to 5.33 m BGS, hard		328.73	6	ss ss	20" 83% 20" 83%	6-19-19-18 (38) 30-34-50 (84)		No.2 Silica Sand 2.60 to 5.95 m No. 10 Slot Schedule 40 PVC Screen 2.90 to 5.95 m
18_ARKELL_ROAD_LOGS.GPU STANTEC - DATA			SILTY SAND (TILL) Trace gravel, grey, hard End of Borehole		5.33 327.96 6.10	8	SS	8" 33%	28-50 (50)		
- 52 52	Screen I Sand Pa Well Se	nterval: ack Interval al Interva	3.05 - 5.95 m BGS al: 3.05 - 5.95 m BGS l: 0.00 - 2.60 m BGS	Notes: m AMSL - metres above mean sea level m BGS - metres below ground surface SS - split-spoon sample n/a - not available		AGS -	Above (Ground	Surface		
	Stantec Drawn By/Checked By: SH/ Sheet 1 of 1									Sheet 1 of 1	