

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
REVISED: June 22, 2017**

**GAMSBY AND MANNEROW LIMITED
PEOPLE ENGINEERING ENVIRONMENTS
GUELPH – OWEN SOUND – LISTOWEL – KITCHENER – EXETER**

Revised: June 2017
Our File: 105-172

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1.0 INTRODUCTION

In support of the Draft Plan of Subdivision Application for Part of Lot 4, Concession 3, Division 'C' (Geographic Township of Guelph) and Part of Lots 30, 32 & 33 and all of Lot 34, Registered Plan 53 (Division 'C' – Geographic Township of Guelph), in the City of Guelph herein after referred to as Cityview Ridge Subdivision, Gamsby and Mannerow Limited has prepared this revised report to address the preliminary servicing and stormwater management requirements for the site and to address the comments provided by the City of Guelph (dated September 18, 2015 and December 9, 2015).

The servicing and stormwater management techniques for the Cityview Ridge Subdivision were derived from the recommendations presented in the following reports:

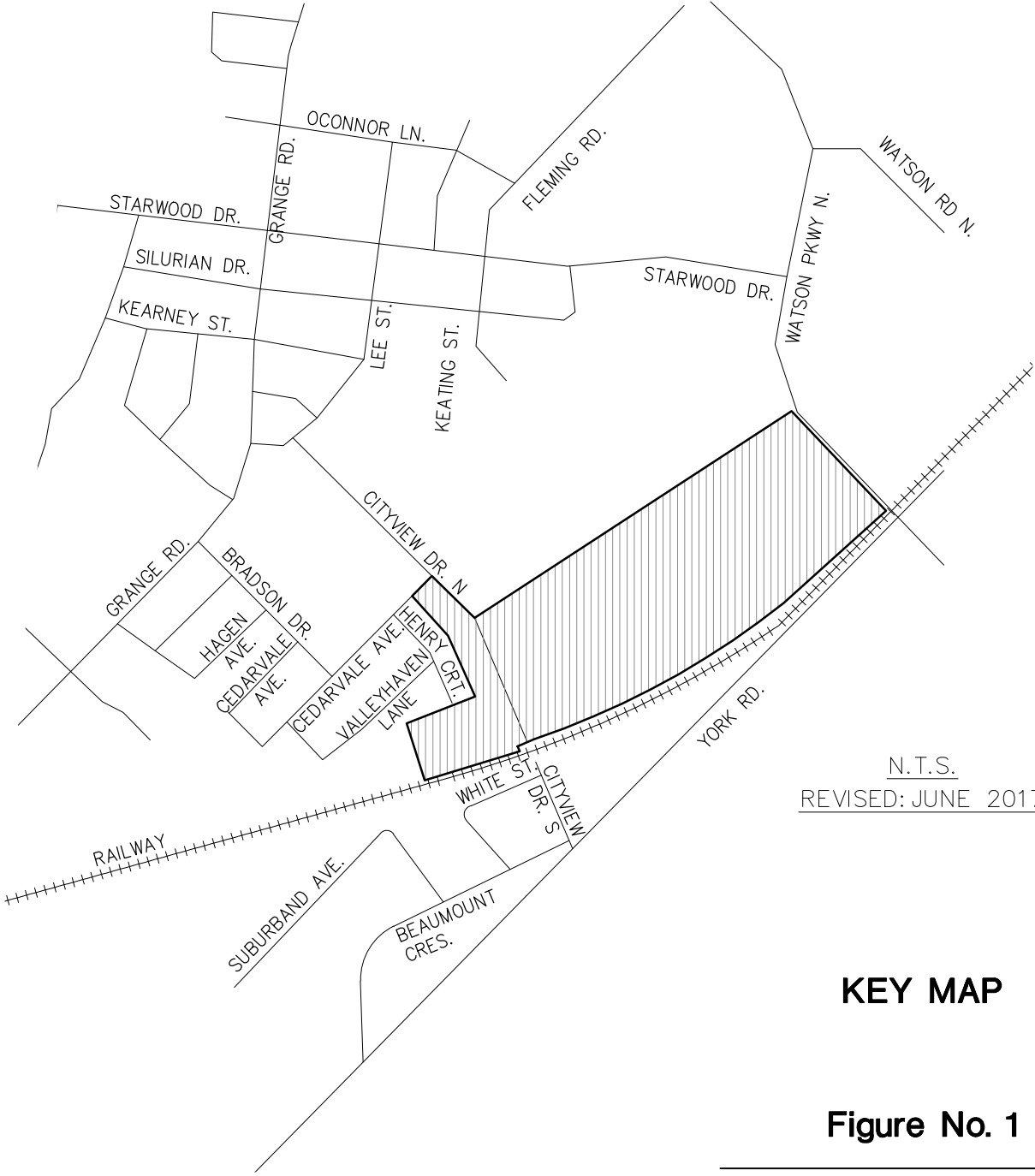
- Final Stormwater Management Design Report for the Southern Hadati Creek Watershed prepared by Schaeffus Consulting Engineers (May 1997).
- Stormwater Management Design Report Draft Plan 23T-96501 and 23T-99501 Martini/Valeriotte Subdivision prepared by Gamsby and Mannerow Limited (March 2004).
- Clythe Creek Subwatershed Overview prepared by Ecologistics Limited (January 1998).
- Eastview Secondary Plan and Addendum prepared by Cosburn Patterson Wardman Limited (1991 and 1992).
- Environmental Impact Study prepared by North-South Environmental Inc. (February 2012).
- Hydrogeological Investigation prepared by Banks Groundwater Engineering Limited (February 2012).
- Geotechnical Investigation prepared by Naylor Engineering Associates Limited (February 2012)

Together, these reports form the overview for the development of these lands.

2.0 LOCATION

Figure 1 shows the location of the Cityview Ridge Subdivision and the surrounding area. The site is bound by future development lands to the north, Watson Parkway to the east, CN Railway lands to the south and existing residential development (Valleyhaven Subdivision Phase 3) to the west.

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KEY MAP

Figure No. 1



3.0 EXISTING CONDITIONS

3.1 LAND USE

The existing land use on the site is vacant field and existing residential. Previously a portion of the site (east of Cityview Drive) was utilized as a Christmas tree farm with the remaining Christmas trees being harvested in 2006. The site has also been used as a borrow site for fill material in the past.

The lands to the north are currently vacant fields and are expected to be developed for residential purposes in the future. The lands to the east including Watson Parkway, are zoned to permit future commercial development. The lands to the south of the CN Railway lands have been developed for residential/commercial/industrial use. The lands to the west have been developed for residential use and include the Valleyhaven Subdivision Phase 3.

3.2 TOPOGRAPHY

The westerly portion of the site, west of Cityview Drive, generally drains in an east to west direction towards Hadati Creek. The average gradient across the westerly portion of the site ranges from 3.0% to 12.0%. The central portion of the site, east of Cityview Drive, generally drains in a west to southeast direction towards the low lying area and Clythe Creek. The average gradient across the central portion of the site, which includes the slope of the drumlin, ranges from 3.0% to 20.0%. The eastern portion of the site, adjacent to Watson Parkway, generally drains in an east to southwest direction towards the low lying area and Clythe Creek. The average gradient across this portion of the site ranges from 2.0% to 12.0%.

Under existing conditions there are two recognized historical drainage patterns through the site. The first is a former watercourse in the east of the site which runs north to south. This feature is identified in Figure 2 of Addendum #3 to the 2012 EIS by North-South Environmental Inc. During inspection of the watercourse in October 2016 by North-South Environmental Inc., there was evidence of surface runoff in the downstream end of the watercourse. This is not currently a recognized watercourse by the GRCA.

The historical drainage pattern is a drainage swale which runs through the middle of the site from the northwest to the southeast. During the preparation of the 2012 EIS by North-South Environmental Inc., this was not a recognized drainage pattern and no flows had ever been recorded in this area. Upon site inspection by North-South Environmental Inc., there was no evidence of a eroded channel in the area, until exiting the site area. Outside of the site, erosion has taken place and formed a channel which eventually discharges to Clythe Creek.

There currently exists a roadside ditch along Cityview drive which under existing conveys flows from the road, just to the north of the site, and the southwest corner of the site. This drainage ditch ultimately discharges to Clythe Creek via a culvert under the railroad tracks and a sewer which conveys flows under York Road. Under existing conditions a silt fence has been installed in the southwest corner of the site to discourage sediments from entering the drainage ditch and ultimately Clythe Creek. Currently flows are directed to a low point along the silt fence, where the silt fence has broken and sediment laden flows are free flowing into the roadside ditch.

3.3 SOILS

The predominant surface soil type on the site is Guelph Loam (Soil Survey of Wellington County Report No. 35). Guelph Loam has a hydrologic soil classification of BC and generally has good drainage characteristics.

The Geotechnical Investigation by Naylor Engineering Associates Limited (February 2012) established the characteristics of the underlying soils for the lands on the east side of Cityview Drive. The boreholes identified the underlying soils as topsoil overlying silt tills for the majority of the property and as topsoil overlying sand and gravel for the low lying easterly portions of the site. The results of the geotechnical investigation are included in Appendix 'A'.

As part of the Geotechnical Investigation, groundwater observation wells were installed. Groundwater measurements have been collected from 2006 to the present to establish seasonably high groundwater elevations. From the groundwater measurements and the Geotechnical Investigation, the seasonably high groundwater level is estimated to range from 0.10 metres to 6.70 metres below ground surface.

Therefore, based on the underlying soils, the practical opportunities for recharge will be limited after the development has been built. The results of the groundwater measurements are attached in Appendix 'C'.

4.0 PROPOSED DEVELOPMENT

The Draft Plan of Subdivision prepared by Black Shoemaker Robinson & Donaldson Limited (November 6, 2014) (Figure 2) illustrates the proposed lot fabric and road network. Cityview Drive will serve as the main connection and access point for this development. Access to the apartment block on the easterly half of the development will be provided by Watson Parkway.

4.1 SITE GRADING

The site layout and internal roads are shown on the Preliminary Grading and Drainage Plans (Gamsby and Mannerow Limited Drawing No. 1, 2 and 3). The grade and elevation of the streets are controlled by the elevation of Cityview Drive and the major overland flow route to the existing municipal stormwater management facility and proposed stormwater management facility.

The site has been graded to match the existing elevations along the property limits of the future development lands to the north and the CN Railway lands to the south. A portion of the site adjacent to Watson Parkway has been graded to allow for future development as an apartment block.

Under post-development conditions the former watercourse in the east of the site which runs north to south is to remain unchanged. This surface drainage feature is within the identified Natural Heritage System and is not within 100m of the closest lot line.

Under post-development conditions, the drainage swale which runs through the middle of the site from the northwest to the southeast will be removed. Surface runoff which may have discharged to this drainage swale will be routed to the stormwater management system, via the on-site storm sewers, ultimately discharging to the proposed energy dissipation structure prior to discharging to Clythe Creek.

Prior to construction, it is our recommendation that a hickenbottom be constructed at the culvert under the railroad tracks. The silt fence which is currently installed at the southwest corner of the site has failed and allows sediments to flow freely into the roadside ditch. Along with sediments from the site, sediments from the road are not stopped from flowing into Clythe Creek. A hickenbottom installed at the north end of the culvert under the railroad tracks will not disrupt the flows in the roadside ditch generated by the road and the southwest portion of the site, and will stop the flows of sediments from the road and site from discharging into Clythe Creek.

4.2 STREETS

All streets will be constructed with a minimum slope of 0.5% to a maximum slope of 6.0%. An urban road cross-section with concrete curb and gutter will be used along all streets.

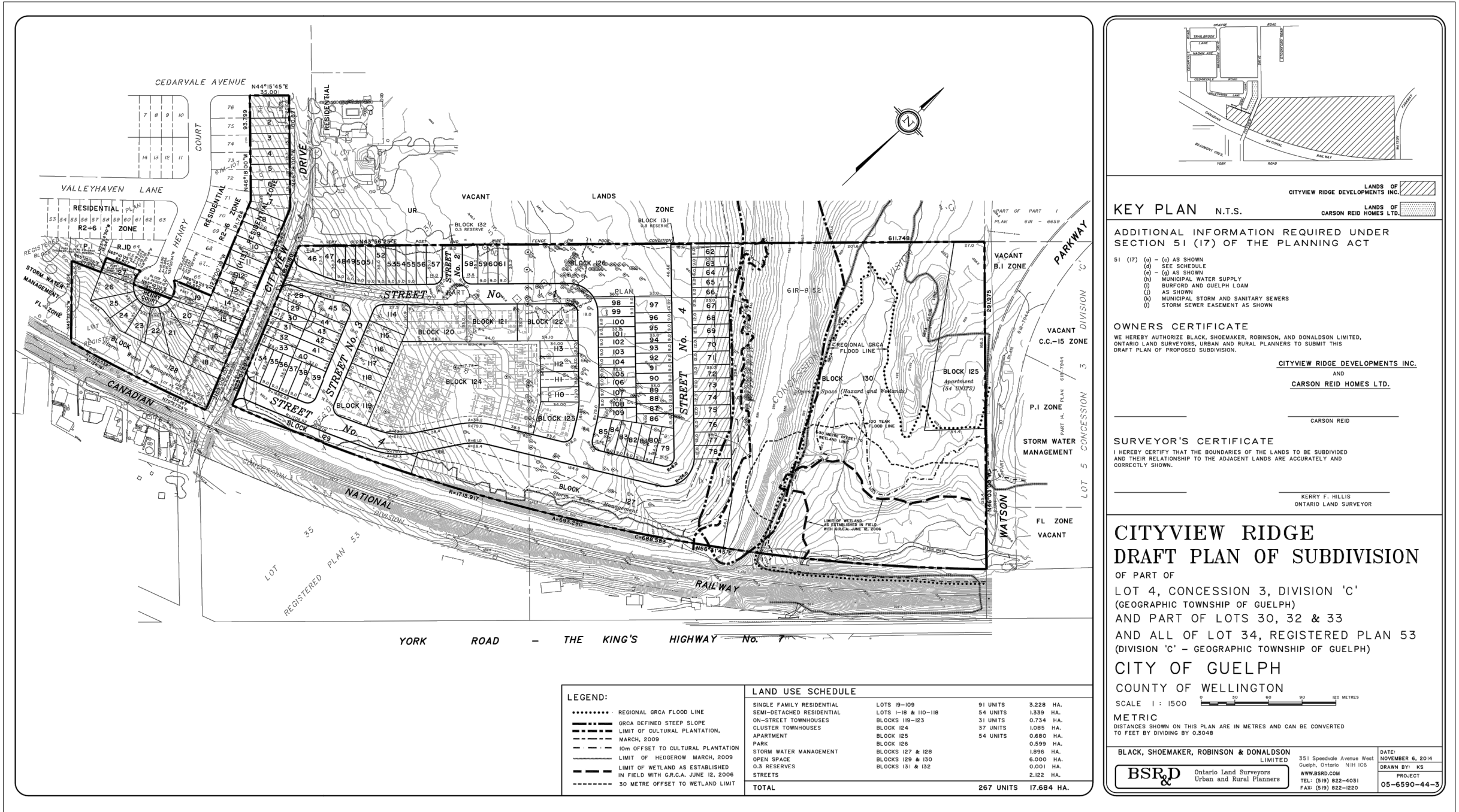
Street Nos. 1, 2, 3, and 4 have an 18.0 metre right-of-way width.

Cityview Drive has a 20.0 metre right-of-way.

The extension of the cul-de-sac on Henry Court has an 18.5 metre radius.

Concrete sidewalks, with a width of 1.5 metres, will be constructed along both sides of each street.

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DRAFT PLAN OF
SUBDIVISION

Figure No. 2



4.3 WATER SUPPLY

As part of the municipal servicing of the Valleyhaven Subdivision Phase 3, a 150 mm diameter watermain was terminated at the current limits of Henry Court and a 150 mm diameter watermain stub was extended from the 200 mm diameter watermain which crosses the CN Railway lands and terminated within the limits of the existing municipal stormwater management facility. A 200 mm diameter watermain was also terminated at the intersection of Cedarvale Avenue and Cityview Drive as part of these works.

The extension of the existing 150 mm diameter watermain on Henry Court will provide water service to the residential lots fronting on to Henry Court.

The extension of the 200 mm diameter watermain southerly on Cityview Drive from the intersection of Cedarvale Avenue and Cityview Drive will provide water supply to the residential lots fronting onto Cityview Drive.

The extension of the 150 mm diameter watermain from the existing municipal stormwater management facility, parallel to the CN Railway lands to the Cityview Drive right-of-way, along with the extension of the 200 mm diameter watermain southerly on Cityview Drive, will provide a looped watermain connection to service the Cityview Ridge Subdivision lands located on the east side of Cityview Drive. Upon development of the lands located to the north of the Cityview Ridge Subdivision, additional looping of the watermain can be achieved with future connections at Street Nos. 2 and 4.

Water supply for the apartment block located along Watson Parkway will be provided by a connection to the existing 300 mm diameter watermain on Watson Parkway.

4.4 SANITARY SEWER

As part of the municipal servicing of the Valleyhaven Subdivision Phase 3, a 200 mm diameter sanitary sewer was terminated at the current limits of Henry Court and a 200 mm diameter sanitary sewer stub was extended across the CN Railway lands and terminated within the limits of the existing municipal stormwater management facility.

The extension of the existing 200 mm diameter sanitary sewer on Henry Court will provide sanitary service to the residential lots fronting on to Henry Court.

Sanitary service for the lots fronting on to Cityview Drive and the remainder of the Cityview Ridge Subdivision (east of Cityview Drive) will be provided by the extension of a 200 mm diameter sanitary sewer from the existing 200 mm diameter sanitary sewer stub located in the existing municipal stormwater management facility, along the CN Railway lands to Cityview Drive.

Sanitary service for the apartment block on the west side of Watson Parkway will be provided by connection to the existing 525 mm diameter sanitary sewer on Watson Parkway.

4.5 STORM SEWER

All storm sewers within the Cityview Ridge Subdivision will be sized to accommodate the 5-year design storm event.

The storm sewers on Henry Court will discharge to existing municipal storm sewers, ultimately discharging to the existing municipal stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3. Storm sewers on the northerly reach of Street No.1, Streets No. 2 and 3, and the westerly reach of Street No. 4 and Cityview Drive will outlet to a stormwater conveyance channel, ultimately discharging to the existing municipal stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3. The existing municipal stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3 was designed, approved and constructed to accommodate drainage from the Cityview Ridge Subdivision. The storm sewers along the remainder of Street No. 4 will outlet to the proposed stormwater management facility.

Major storm runoff generated from the extension of Henry Court will be conveyed via the municipal right-of-way, ultimately discharging to the existing municipal stormwater management facility. Major storm runoff from Cityview Drive and the central portion of the site (lands located to the east of Cityview Drive) will be conveyed through the street right-of-ways to the stormwater conveyance channel, ultimately discharging to the existing municipal stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3. Major storm runoff from the remainder of the development will be conveyed through the street right-of-ways to the proposed stormwater management facility.

The topography of the site will generally allow for sufficient cover on the storm sewer to connect house foundation drains. Where a storm service connection is not possible, foundation drainage will be provided by sump pumps discharging to the grassed side and rear yard surfaces.

4.6 STORMWATER MANAGEMENT

Details of the stormwater management plan for the Cityview Ridge Subdivision are discussed in detail in Section 5.0.

4.7 SALT MANAGEMENT PLAN

As per the requirements of the City of Guelph, the following Salt management Plan has been developed for the Cityview Ridge Subdivision. Although not in the Region of Waterloo, this plan has been developed using the Region of Waterloo's Curb The Salt and Smart About Salt Program, as these are well respected programs and guidelines for reducing salt usage and minimizing the concentration of salt in infiltration and runoff. A two-stage salt management plan is recommended as per the Region of Waterloo Curb The Salt and Smart About Salt Program. Stage I of the salt management plan will address the ploughing of snow and the application of salt/sand within the limits of the right-of-way by municipal forces. Stage II of the salt management plan will include snow removal and placing of salt on private property by the homeowner.

The recommended best management practices for the removal of snow and application of salt/sand within the limits of the municipal right-of-way (Stage I) include the following:

- Ploughing of snow as required following snowfall events or as directed by the municipality to ensure safe passage for motorists.
- Application of salt/sand immediately following ploughing if required or as directed by the municipality. The application of salt/sand is not mandatory after each snow clearing operation.
- Monitor and document the application of salt/sand on municipal right-of-ways (i.e. frequency, concentration, etc.).
- Storage of all ploughed snow in an area appropriately designated for snow storage to minimize the impact of salt/sand on environmental features and to ensure that surface drainage is maintained. As part of the detailed engineering design, an appropriate snow storage area will be confirmed with the City.

Stage II of the salt management plan, which includes the removal and stockpiling of snow and application of salt/sand on private property, the recommended best management practices are as follows:

- Ploughing or shovelling snow on driveways and sidewalks immediately following a snowfall event to ensure the safe passage of motorists and pedestrians.
- Application of salt/sand immediately following ploughing or shovelling only as required (sand is recommended). The application of salt/sand is not mandatory after each snow clearing operation.
- Storage of all ploughed or shovelled snow in the front yards and boulevard areas (i.e. grassed areas) to a height which will not block the view of motorists and pedestrians and will not impede surface drainage.

As part of the two stage Salt Management Plan, an annual review of the plan shall be conducted by the Owner as a way to incorporate some adaptive strategies for continual improvement and reduction of salt concentrations in runoff and infiltration.

4.8 WATER BUDGET

Based on the Canadian Climate Normals for the Guelph Arboretum from 1971-2000, the average annual precipitation, for the area in which the site is located is estimated to be 923.3 mm. The potential for evapotranspiration for this area is estimated to be 555 mm for the drumlin and 495 mm for the low lying easterly portion of the site. Therefore, 368 mm and 428 mm remain available for infiltration and runoff from the drumlin and low lying areas, respectively.

From the Geotechnical Investigation (Naylor Engineering Associated Limited, February 2012), the surficial deposits across the majority of the site are described as silt tills, with sand and gravel across the low lying easterly portion of the site. A copy of the Geotechnical Investigation has been included in Appendix 'A'. Typically infiltration and runoff in areas mapped as tills is estimated to be 180 mm and 190 mm, respectively. For the low lying easterly portion of the site, the average infiltration and runoff were estimated to be 380 mm and 50 mm, respectively. A copy of the Hydrogeological Investigation prepared by Banks Groundwater Engineering Limited has been included in Appendix 'D'.

Therefore, based on the annual infiltration rates, as shown on the Monthly Water Balance calculations attached in Appendix 'G', the existing annual average groundwater recharge occurring within the 18.28-hectare site is estimated to be 41,003 m³. Under post-development conditions, the annual natural groundwater recharge occurring on-site is estimated to be 23,573 m³. Due to the high silt content in the native soils and the seasonably high groundwater level, infiltration structures cannot be constructed and still achieve the MOECC's recommended 24 hour draindown and 1 metre separation from the seasonably high groundwater levels.

Under existing conditions the annual average runoff from the site is estimated to be 31,518 m³. As a result of the proposed development the impervious area (rooftop and paved surfaces) of the site increases, the annual potential evapotranspiration for impervious surfaces decreases to 200 mm and the runoff from the site increases. The runoff from the site under post-development conditions is estimated to be 59,944 m³ per year.

Enhanced infiltration can be provided in Block 125 to reduce the difference between existing and post-development condition infiltration volumes. An additional water balance has been provided where existing runoff volumes to the wetland are matched, and the remaining portion of the site which is not needed to discharge to the wetland is infiltrated. This results in an additional 2,161 m³ in runoff volume, bringing the post-development total to 25,734 m³.

The estimated existing and post-development recharge and runoff volumes for the Cityview Ridge Subdivision are detailed in Table 1. The estimations take into account the surficial geology, which is comprised of silt tills in the westerly portion of the site and sand and gravel in the easterly portion. The net recharge values are for the uppermost overburden aquifer.

In summary, the estimated recharge and runoff volume for the Cityview Ridge Subdivision are as follows:

Table No. 1: Summary of Recharge and Runoff Volume

	Existing Condition	Post-Development Condition	Percent Change
Total Estimated Recharge	41,003 m ³	25,734 m ³	-37%
Total Estimated Runoff	31,518 m ³	59,944 m ³	90%

To minimize the impact of development on the adjacent lands, the stormwater management system has been designed to provide enhanced water quality treatment and to attenuate the post-development flows to the pre-development level. In addition, discharge from the proposed stormwater management facility will be dispersed over a large broad surface, ultimately sheetflowing overland towards Clyde Creek.

5.0 STORMWATER MANAGEMENT PLAN

In line with current practices and guidelines, the stormwater management plan for the Cityview Ridge Subdivision is a “treatment train” to attenuate post-development flows and to remove sediments prior to discharge to both Clythe Creek and Hadati Creek. Enhanced (80% total suspended solids removal) water quality control will be provided by the stormwater management system. Post-development runoff generated from the site will be attenuated to the existing condition level. The “treatment train” will include a combination of lot level, conveyance and end-of-pipe best management practices.

Lot level controls will simply consist of directing roof leaders to grassed rear lot areas and grassed rear lot and side yard swales. Lot level infiltration systems are not feasible due to the high groundwater levels and have not been incorporated into the stormwater management system for the development.

Conveyance controls will include the use a stormwater conveyance channel and oil/grit separator structure to provide quality control treatment for a portion of the runoff discharging from the site, prior to discharge to both Clythe Creek and Hadati Creek.

End-of-pipe controls will be provided by an existing stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3 (Stormwater Quality Facility No. 2 and Stormwater Quantity Control Facility) and a proposed stormwater management facility.

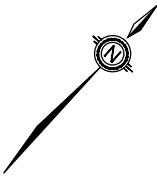
As part of the overall stormwater management analysis and design for the Valleyhaven Subdivision Phase 3, a stormwater management system consisting of both quality and quantity control facilities was designed, approved and constructed along Hadati Creek upstream of the CN Railway Tracks.

The existing Stormwater Quality Facility No. 2 was designed to provide Basic (MOE, 2003) (Formerly Level 3) quality control treatment for a maximum drainage area of 29.6-hectares (based on a maximum imperviousness coverage of 42%).

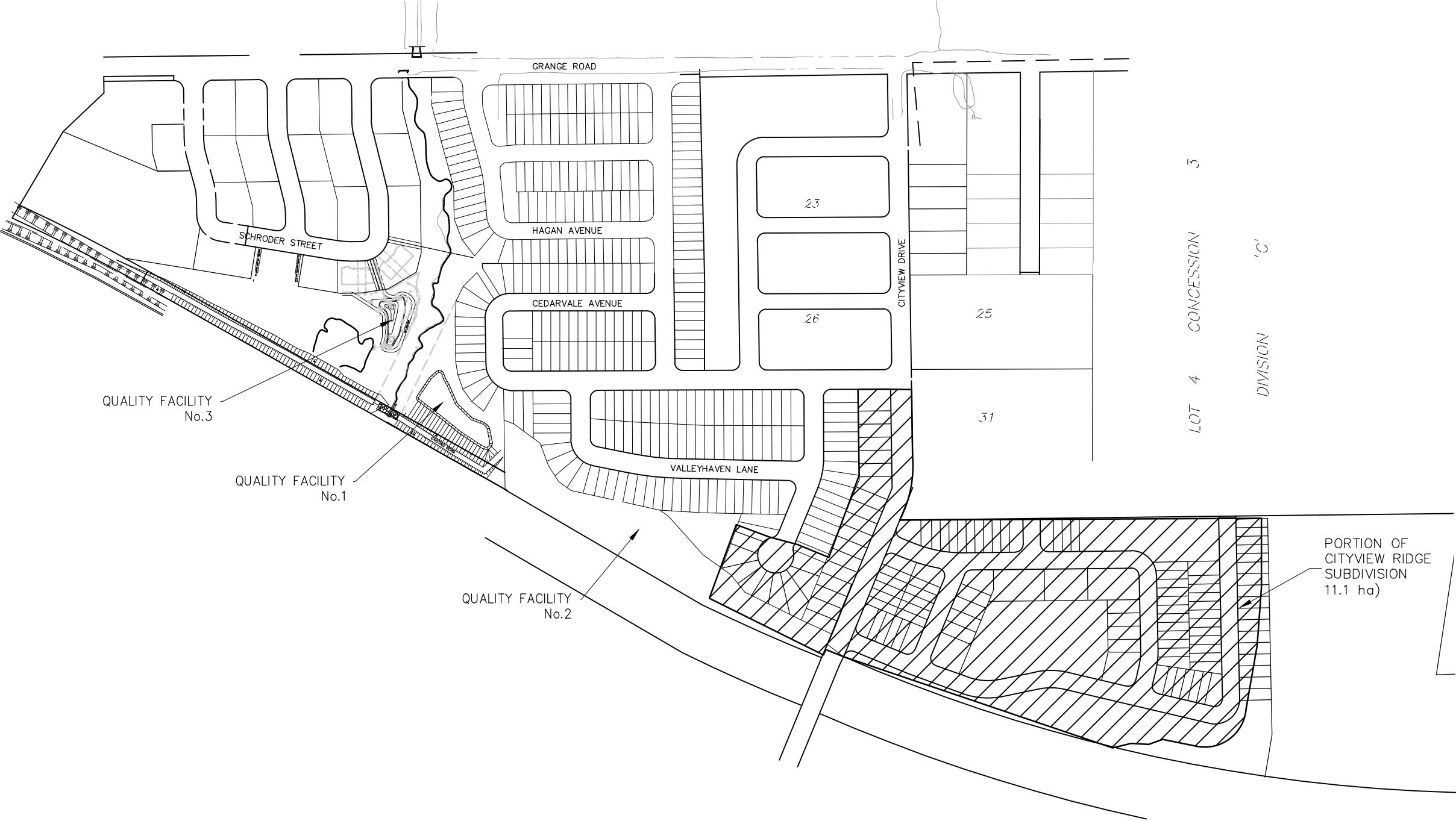
The existing Stormwater Quantity Control Facility, consisting of a detention pond located on-line with Hadati Creek, a quantity control berm and an outlet structure connected to the existing CN culvert, was designed to attenuate peak flows from a Catchment area of 72.7-hectares to the release rates recommended in the Eastview Secondary Plan.

Of the 29.6-hectare and 72.7-hectare catchment areas for the existing stormwater management facilities, 11.1-hectares represent the westerly portion of the Cityview Ridge Subdivision. Therefore, quality and quantity control treatment of runoff generated from 11.1-hectares of the Cityview Ridge Subdivision has been accounted for in the design, approval and construction of the existing Quality Facility No. 2 and the existing Quantity Control Facility. The drainage catchments utilized in the design of the existing quality and quantity control facilities are shown on Figure 3.

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OVERALL
DRAINAGE AREAS

Figure No. 3



Gamsby and Mannerow
ENGINEERS

To provide quality and quantity control for the runoff generated from the Cityview Ridge Subdivision, while also maintaining the existing drainage patterns discharging to both Hadati Creek and Clythe Creek, runoff generated from the westerly portion of the development (approximately 7.62-hectares), which includes Henry Court and Cityview Drive, will be directed to the existing stormwater management Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3.

Runoff generated from the central portion of the development will be directed to the proposed stormwater management facility. The proposed stormwater management facility will attenuate stormwater runoff to the existing condition level prior to discharge to Clythe Creek.

Quality and quantity control for runoff generated from the easterly section of the site, which includes the future apartment block, will be provided by privately owned and operated on-site stormwater management controls. The on-site stormwater management controls will be designed, reviewed and approved as part of the site plan approval process for the development block.

This combination of lot-level, conveyance and end-of-pipe controls will control the release of the runoff from the site.

5.1 STORMWATER MANAGEMENT CRITERIA

The studies, policies and guidelines used to develop the stormwater management plan for this development were as follows:

- 1) Stormwater Management Planning and Design Manual, 2003
- 2) Design Principles for Stormwater Management Facilities, 1996
- 3) Eastview Secondary Plan and Addendum, 1991 and 1992
- 4) The Interim Stormwater Quality Control Guidelines, 1991
- 5) The Stormwater Quality Best Management Practices Manual, 1991
- 6) The MTO Drainage Management Technical Guidelines, 1989
- 7) The Ontario Urban Design Guidelines, 1987

The objectives of the stormwater management plan are as follows:

- a) Provide enhanced (80% TSS) quality control by pre-treating the runoff prior to discharge to the receiving outlet.
- b) Provide quantity control for a range of design storms.
- c) Route the major storm to minimize flood damage to public and private lands.
- d) In order to minimize sediment discharge to the wetland and/or lands adjacent to the working area, erosion and sediment control measures shall be incorporated for the entire duration of the contract.
- e) Complete a Water Balance Analysis in order to evaluate total system water loss and identify measures to reduce those losses.

The method used to evaluate and design the stormwater management plan was as follows:

The City of Guelph design parameters were used to generate the mass rainfall data required to model the 2, 5, 25 and 100-year design storm events. The Regional Storm has also been modelled. The Chicago parameters and the total depth of rainfall for each storm are as follows:

Table No. 2: Chicago Rainfall Parameters

	2 Year	5 Year	25 Year	100 Year
a =	743.00	1,593.00	3,158.00	4,688.00
b =	6.000	11.000	15.000	17.000
c =	0.799	0.879	0.936	0.962
r =	0.400	0.400	0.400	0.400
td =	170.00	170.00	210.00	210.00
Rainfall depth (mm)	33.816	46.775	69.476	88.830

The Horton Infiltration method was used in the post-development runoff calculations. The parameters used in the MIDUSS modelling are given in Table No. 3.

Table No. 3: Horton Infiltration Parameters

	Impervious Areas	Pervious Areas
Maximum Infiltration	0.0 mm/hr	75.0 mm/hr
Minimum Infiltration	0.0 mm/hr	12.5 mm/hr
Lag Constant	0.05 mm/hr	0.25 mm/hr
Depression Storage	1.5 mm	5.00 mm

5.2 STORMWATER MANAGEMENT DESIGN

As part of the stormwater management system, a “treatment train” to remove sediments and thereby any absorbed contaminants prior to discharging to Hadati Creek and Clythe Creek will be provided. The “treatment train” will include lot level, conveyance and end-of-pipe management practices.

The best management practices (BMP's) in the Stormwater Management Planning and Design Manual (2003) were screened. Those found to be applicable to this development are discussed in the following sections.

5.2.1 LOT LEVEL CONTROLS

Stormwater management practices recommended to provide lot level control on this site are as follows:

a) Roof Drainage to Ground Surface

The driveways and front yards will drain to the street. The roof and rear yard will generally drain to the rear of the lot.

The roof runoff will be filtered across the grassed surface and some will infiltrate. The runoff for any event large enough to generate flow to the swale system will be adequately filtered by the grass enroute.

b) Rear Yard Swales

The lots will be graded to current City of Guelph Standards. Where practical, the length of the rear lot swales between catch basins will be increased to extend the contact time with the grassed surfaces.

To promote infiltration on the lots and in the swales, it is recommended that the average depth of graded topsoil be 300 mm.

c) Lot Level Infiltration Systems

The Stormwater Management Practices and Planning Manual (2003), recommends that infiltration structures be installed in soils having a hydraulic conductivity greater than or equal to 15 mm/hour (4.2×10^{-4} cm/s) and where a 1 metre minimum separation from the seasonally high groundwater level can be provided.

The soils on the site have high silt content and thus a low hydraulic conductivity, estimated to be in the order of 1×10^{-4} cm/s. Seasonally high groundwater levels on the site range from 0.10 metres to 6.70 metres below the ground surface, therefore making the 1 metre separation from high groundwater level difficult to achieve.

For example, the rear yard and rooftop catchment area of Lot 93 is approximately 0.03 hectares in size and will have an average imperviousness of 55%. Under a “first flush” (25-mm) design storm, this lot would generate approximately 5.54 m^3 of runoff.

An infiltration trench, 6 metres long by 3 metre wide by 1 metre deep, constructed in this lot would have an effective contact area of 18 m^2 . Based a hydraulic conductivity of 1.0×10^{-4} cm/s, the estimated rate of recharge is $1.8 \times 10^{-5} \text{ m}^3/\text{s}$.

Therefore, the estimated “drain down” time for a rear lot infiltration structure would be approximately 85 hours. The Stormwater Management Planning and Design Manual (2003) recommend that infiltration structures drain within 24 hours.

As the soils on the westerly portion of the site have a high silt content, Naylor Engineering Associates Ltd. has identified that they are unsuitable for at-source drywell infiltration.

Therefore, based on the estimated “drain down” time of 85 hours and the high groundwater levels, it is our opinion that infiltration systems are **not** feasible and should **not** be incorporated as part of the development.

5.2.2 CONVEYANCE CONTROLS

The storm conveyance system for the development will consist of a stormwater conveyance channel and storm sewers. Conveyance controls will be achieved through the regular maintenance of the grassed channels and storm sewers as part of the City’s annual maintenance program. Maintenance requirements will include the annual cleanout of the manholes, catch basins, to remove sediment, oil and debris deposited during rainfall events.

The stormwater conveyance channel will have the capacity to convey the 100-year design storm event flows from both the Cityview Ridge Subdivision and the proposed development lands to the north. The channel will be constructed along the northern limits of the CN Railway lands, to provide a link between the Cityview Ridge Subdivision and the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3.

5.2.3 END-OF-PIPE CONTROLS

a) Existing Conditions

Under existing conditions, the site consists of two (2) existing buildings and various other buildings, with the remainder of the site being open space. For hydrologic modelling purposes, the site was modelled as three (3) catchments. These catchments, which include the Cityview Drive right-of-way, are shown on the Existing Conditions Drainage Area Plan (Figure 4).

Catchment 10 (7.02 hectares, 8% impervious) represents the westerly portion of the development including the existing buildings, Cityview Drive and open space area.

Runoff generated from Catchment 10 currently sheetflows overland in an east to west direction, ultimately discharging to the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3.

Catchment 20 (4.78 hectares, 0% impervious) represents the central portion of the site.

Runoff generated from Catchment 20 currently sheetflows overland to the east, ultimately discharging to the low lying area and Clythe Creek.

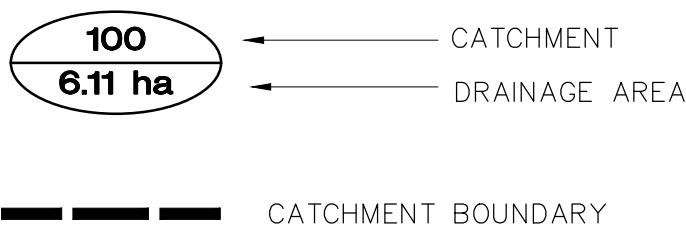
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EXISTING CONDITIONS
DRAINAGE AREA

Figure No. 4



Catchment 30 (6.48 hectares, 0% impervious) represents the remainder of the site (easterly portion).

Runoff generated from Catchment 30 currently sheetflows overland, ultimately discharging to the low lying area and Clythe Creek.

Table No. 4 summarizes the existing condition flow rates and runoff volumes from the site for the full range of design storm events.

Table No. 4: Existing Condition Flow Rates and Runoff Volumes

	CATCHMENTS					
	10	Total to Ex. SWM Pond	20	30	Total to Clythe Creek	Total from Site
2 year						
Flow Rate (m ³ /s)	0.130	0.130	0.054	0.073	0.127	0.220
Runoff Volume (m ³)	314.3	314.3	100.7	136.6	237.3	551.6
5 year						
Flow Rate (m ³ /s)	0.492	0.492	0.328	0.444	0.772	1.265
Runoff Volume (m ³)	951.8	951.8	519.7	704.5	1,224.2	2,176.0
25 year						
Flow Rate (m ³ /s)	1.344	1.344	0.931	1.261	2.192	3.536
Runoff Volume (m ³)	2,226.3	2,226.3	1,369.3	1,856.3	3,595.6	5,451.9
100 year						
Flow Rate (m ³ /s)	2.160	2.160	1.454	1.971	3.425	5.585
Runoff Volume (m ³)	3,420.5	3,420.5	2,173.5	2,946.5	5,119.9	8,540.4
Regional Storm						
Flow Rate (m ³ /s)	0.587	0.587	0.397	0.538	0.936	1.522
Runoff Volume (m ³)	6,423.1	6,423.1	3,728.8	5,054.9	8,783.7	15,206.8

b) Allowable Release Rates

The existing stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3 (Stormwater Quality Facility No. 2) was designed, approved and constructed to accommodate stormwater runoff generated from a total contributing drainage area of 29.6-hectares (42% imperviousness), of which 11.1-hectares represents the westerly portion of the Cityview Ridge Subdivision. Therefore, the allowable release rates from the Cityview Ridge Subdivision to the existing stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3 (Stormwater Quality Facility No. 2) are outlined in Table No. 5.

Table No. 5: Allowable Release Rates from the Cityview Ridge Subdivision to the Existing Stormwater Management Facility (Stormwater Quality Facility No. 2)

	Allowable Release Rate
2 Year	0.294 m ³ /s
5 Year	0.929 m ³ /s
25 Year	1.689 m ³ /s
100 Year	2.246 m ³ /s

The allowable release rate for the stormwater runoff discharging from the site to Clythe Creek was determined by calculating the existing condition flow rates discharging to Clythe Creek.

Therefore, the allowable release rates from the Cityview Ridge Subdivision to Clythe Creek are outlined in Table No. 6.

Table No. 6: Allowable Release Rates from the Cityview Ridge Subdivision to Clythe Creek

	Allowable Release Rate
2 Year	0.127 m ³ /s
5 Year	0.772 m ³ /s
25 Year	2.192 m ³ /s
100 Year	3.425 m ³ /s

c) Post-Development Conditions

Under post-development conditions, runoff generated from the westerly and central portions of the development will be directed towards either the existing stormwater management facility constructed as part of the Valleyhaven Subdivision Phase 3 (Stormwater Quality Facility No. 2) or the proposed municipal stormwater management facility.

Runoff generated from the easterly portion of the site will be attenuated through the use of privately owned and operated on-site stormwater management controls, prior to discharge to Clythe Creek. The on-site stormwater management controls will be designed, reviewed and approved as part of the site plan approval process.

For hydrologic modelling, two (2) separate hydrological models were prepared. One model was prepared for the western portion and one model was prepared for the eastern portion of the Cityview Ridge Subdivision.

The hydrologic model for the western portion of the subdivision has been adapted from the hydrological modelling created for the Valleyhaven Subdivision, Phase 3 as detailed in the Stormwater Management Design Report Draft Plan 23T-96501 and 23T-99501 for the Martini/Valeriotte Subdivision (Gamsby and Mannerow Limited, March 2004). The analysis includes the watershed discharging to the southern reach of Hadati Creek, including the external areas, existing and future development areas (including the western portion of the Cityview Ridge Subdivision) and the lands downstream of the CN Railway. The stormwater management catchments for this model are shown on Figure 5 and described below. A schematic of this model has been appended.

Catchment B2a (11.38 hectares, 42% impervious) represents the future development area north of the Cityview Ridge Subdivision and East of Cityview Drive. Stormwater runoff generated from Catchment B2a discharges to the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3 via a conveyance channel located in the southwest corner of the Cityview Ridge Subdivision.

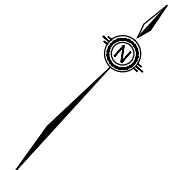
Catchment B2b (5.97 hectares, 42% impervious) represents the existing Valleyhaven Subdivision Phase 3. Stormwater runoff generated from Catchment B2b discharges to the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3.

Catchment B2c (7.55 hectares, 46% impervious) represents the western portion of the Cityview Ridge Subdivision. Stormwater runoff generated from Catchment B2c discharges to the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3 via a conveyance channel located in the southwest corner of the Cityview Ridge Subdivision.

The existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3, was designed to provide Basic (MOE, 2003) (Formerly Level 3) quality control treatment for Catchments B2a, B2b and B2c.

In order to provide enhanced water quality treatment (80% total suspended solids removal) for stormwater runoff generated from the Cityview Ridge Subdivision and discharging to the existing Stormwater Quality Facility No. 2 constructed as part of the Valleyhaven Subdivision Phase 3, an oil/grit separator structure (Stormceptor STC 14000 or approved equivalent along with a settling basin/forebay has been designed to provide additional quality control treatment

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LEGEND

B2a 21.8 ha ← CATCHMENT

← DRAINAGE AREA

--- CATCHMENT BOUNDARY

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POST-DEVELOPMENT
DRAINAGE AREAS
WESTERN PORTION OF
SUBDIVISION
Figure No. 5

for stormwater runoff generated from Catchments B2c and B2a, respectively. The settling basin/forebay has been sized to promote the settlement of particles at the inlet to the existing pond. The settling basin/forebay has been designed to meet the requirements for forebay depth, length-to-width ratio, dispersion length and flow velocity as specified in the Stormwater Management Planning and Design Manual (2003). Details of the settling basin/forebay sizing can be found in Appendix “D”.

The existing Stormwater Quantity Control Facility, consisting of a detention pond located on-line with Hadati Creek, a quantity control berm and an outlet structure connected to the existing CN culvert, will continue to provide quantity control for runoff generated from Catchments B2a, B2b and B2c.

For the eastern portion of the Cityview Ridge Subdivision, the site was modelled as three (3) catchments. These catchments are shown on Figure 6.

Catchment 201 (3.35 hectares, 65% impervious, $c=0.65$) represents the central portion of the proposed development.

Runoff generated from Catchment 201 will be directed towards the proposed stormwater management facility prior to discharging to Clythe Creek. Quantity control for Catchment 201 will be provided by the proposed stormwater management facility. A multi-stage outlet structure consisting of a 90 mm diameter knockout, a 375 mm diameter outlet pipe and a 10.0 metre wide overflow weir will attenuate runoff generated from Catchment 201 prior to discharge to the energy dissipation/dispersion structure.

Quality control for Catchment 201 will be provided by a sediment forebay. The forebay of the Stormwater Management Facility will have a length of 42.0 m, top width of 7.0 m, bottom width of 1.0 m and a depth of 1.0 m. The forebay will have a required settling length of 41.5 m and a dispersion length of 10.6 m. The average flow velocity for the 5 year design storm event is 0.17 m/s through the forebay which is less than the allowable velocity of 0.5 m/s. The sediment forebay has been designed to meet the requirements for forebay depth, length-to-width ratio, dispersion length and flow velocity as specified in the Stormwater Management Planning and Design Manual (MOE, 2003).

Details of the sediment forebay sizing can be found in Appendix “E”.

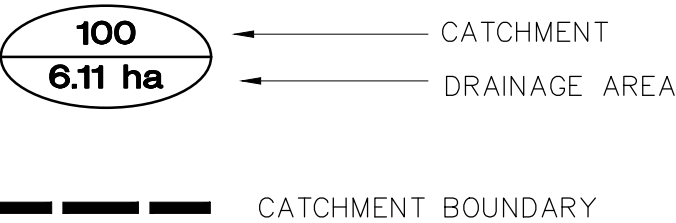
The energy dissipation/dispersion structure (65 m long by 2.0 m wide by 1.0 m deep), consisting of 19 mm diameter clear stone and perforated storm sewer, will dissipate the energy from the runoff and disperse the flows over a large area. The perforated storm sewer located in the clear stone will disperse the flows throughout the length of the structure. Runoff will then percolate through the stone, ultimately discharging out the top of the stone. Discharge from the structure will then sheetflow along the entire length of the structure (65 m) overland towards Clythe Creek.

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LEGEND



POST-DEVELOPMENT
DRAINAGE AREAS
EASTERN PORTION OF
SUBDIVISION

Figure No. 6



The energy dissipation/dispersion structure will also act as a cooling trench to reduce the temperature of the stormwater runoff discharging to Clythe Creek. Details of the energy dissipation/dispersion and cooling structure are provided in Appendix “D”.

During the detailed design stage of the Subdivision, additional measures will be investigated and considered to enhance the function of the energy dissipation/dispersion structure. These measures may include the planting of shrubs and ground covering vines to reduce the direct input of solar radiation on the trench.

In addition, the proposed stormwater management facility has been designed as a wetland type facility with a 0.40 metre deep permanent pool to provide the required water quality control storage volume. The total contributing area discharging to the facility is 3.41-hectares, with an average imperviousness of 65%. From Table 3.2 of the Stormwater Management Planning and Design Manual (2003), a wetland type facility designed for enhanced treatment (80% total suspended solids removal) requires 115 m³/ha of storage volume for a contributing drainage area that is approximately 65% impervious. 40 m³/ha of the required storage volume represents the extended detention storage volume, while the remaining 75 m³/ha represents the permanent pool storage volume. Therefore, 255 m³ of permanent pool storage is required. The permanent pool has been designed with approximately 714 m³ of storage.

Catchment 202 (0.74 hectares, 25% impervious, $c=0.25$) represents a portion of the rooftops, rear yard areas and open space areas of the proposed development.

Runoff generated from a portion of Catchment 202, including the rooftops and rear yards, will be directed to the energy dissipation/dispersion and cooling structure prior to discharge to Clythe Creek. Runoff generated from the remainder of the catchment will sheetflow uncontrolled, ultimately discharging to Clythe Creek.

Quality control treatment for runoff generated from Catchment 202 will be provided by directing runoff over grassed surfaces prior to discharge to Clythe Creek.

Catchment 300 (6.48 hectares, 0% impervious) represents the remainder of development area which consists of open space area and a future apartment block along Watson Parkway.

Runoff generated from Catchment 300 will continue to sheetflow uncontrolled to Clythe Creek. At such time as development of the apartment block proceeds, privately owned and operated on-site quality and quantity control facilities will be required to attenuate stormwater runoff generated from the development block to the existing condition or pre-development level, prior to discharge to Clythe Creek.

The on-site stormwater management controls will be designed, reviewed and approved as part of the site plan approval process for the apartment block. The on-site stormwater management controls which may be utilized include, but are not limited to, stormwater management facility (i.e. SWM pond), rooftop storage, parking lot ponding (to a maximum depth of 0.3 m), below grade storage (i.e. clear stone storage, super pipe storage, etc.) and oil/grit separator structure.

Table No. 7 lists the uncontrolled post-development flow rates and runoff volumes for each catchment area shown on Figure No. 5 and Figure No. 6, for the 2, 5, 25 and 100-year design storm events and the Regional Storm.

Table No. 7: Post-Development Uncontrolled Flow Rate and Runoff Volume

	CATCHMENTS					
	B2c	Total to Ex. SWM Pond	201	202	300	Total to Clythe Creek
2 year						
Flow Rate (m ³ /s)	0.211	0.211	0.496	0.041	0.073	0.538
Runoff Volume (m ³)	563.2	563.2	730.6	70.6	136.6	937.8
5 year						
Flow Rate (m ³ /s)	0.674	0.674	0.675	0.069	0.444	0.868
Runoff Volume (m ³)	1,756.9	1,756.9	1,119.0	142.8	704.5	1,966.3
25 year						
Flow Rate (m ³ /s)	1.177	1.177	1.074	0.169	1.261	2.156
Runoff Volume (m ³)	2,791.2	2,791.2	1,829.9	283.2	1,856.3	3,969.4
100 year						
Flow Rate (m ³ /s)	1.563	1.563	1.469	0.256	1.971	3.366
Runoff Volume (m ³)	3,650.7	3,650.7	2,449.4	410.2	2,946.5	5,806.1
Regional Storm						
Flow Rate (m ³ /s)	0.928	0.928	0.376	0.067	0.538	0.911
Runoff Volume (m ³)	10,099.4	10,099.4	6,363.5	883.7	5,054.9	12,302.1

Table Nos. 8, 9 and 10 compare the routing results through the stormwater conveyance channel, proposed stormwater management facility and energy dissipation/dispersion and cooling structure against the available stage/storage discharge capacities, respectively.

Table No. 8: Catchment B2a & B2c – Stormwater Conveyance Channel Stage/Velocity/Depth of Flow

Overland Flow Swale	Available			Actual		
	Peak Flow m ³ /s	Channel Velocity m/s	Depth of Flow m	Peak Flow m ³ /s	Channel Velocity m/s	Depth of Flow m
Swale Bottom	0.000	0.000	0.000	---	---	---
2-Year	---	---	---	0.531	1.40	0.21
5-Year	---	---	---	1.605	1.88	0.35
Regional Storm	---	---	---	2.304	2.07	0.42
25-Year	---	---	---	2.856	2.18	0.46
100-Year	---	---	---	3.746	2.33	0.52
Top of Bank	16.90	3.38	1.00	---	---	---

Table No. 9: Catchment 201 – Proposed Stormwater Management Facility Available Stage/Storage/Discharge

CONTROL	Available Capacity			Actual Capacity Used		
	Peak Flow m ³ /s	Storage Volume m ³	Storage Elevation m	Peak Flow m ³ /s	Storage Volume m ³	Storage Elevation m
Pond Bottom	0.00	0.0	339.35	---	---	---
Top of Permanent Pool	0.000	0.0	339.75	---	---	---
2 year	---	---	---	0.009	661.6	340.03
5 year	---	---	---	0.010	1,030.9	340.17
CB Lip Elevation	0.011	1,263.6	340.25	---	---	---
25 year	---	---	---	0.176	1,389.4	340.29
Regional Storm	---	---	---	0.307	1,518.1	340.33
100 year	---	---	---	0.412	1,610.3	340.36
Weir	0.470	3,771.9	340.95	---	---	---
Top of Bank	1.736	4,653.3	341.15	---	---	---

Table No. 10: Catchment 201 – Energy Dissipation/Dispersion and Cooling Structure Available Stage/Storage/Discharge

CONTROL	Available Capacity			Actual Capacity Used		
	Peak Flow m ³ /s	Storage Volume m ³	Storage Elevation m	Peak Flow m ³ /s	Storage Volume m ³	Storage Elevation m
Bottom of Stone	0.00	0.0	336.00	---	---	---
Top of Stone / Weir	0.0002	50.1	337.00	---	---	---
2 year	---	---	---	0.009	50.1	337.00
5 year	---	---	---	0.010	50.1	337.00
25 year	---	---	---	0.176	50.9	337.01
Regional Storm	---	---	---	0.307	51.4	337.01
100 year	---	---	---	0.412	51.9	337.02
Overflow	2.13	59.3	337.10	---	---	---

Table No. 11 identifies the energy dissipation/dispersion and cooling structure inlet and outlet flow rates and velocities.

Table No. 11: Energy Dissipation/Dispersion Structure Flow Rate and Velocity

DESIGN STORM	Inlet		Outlet		% Reduction
	Flow Rate (m ³ /s)	Velocity (m/s)	Flow Rate (m ³ /s)	Velocity (m/s)	
2 year	0.009	1.492	0.009	0.088	94.1 %
5 year	0.010	1.568	0.010	0.092	94.1 %
25 year	0.176	3.629	0.176	0.290	92.0 %
Regional Storm	0.307	4.212	0.307	0.362	91.4 %
100 year	0.412	4.531	0.412	0.407	91.0 %

Table Nos. 12 and 13 compare the allowable release rates to the post-development flow rates discharging to the existing Stormwater Quality Facility No. 2 and to Clythe Creek, respectively.

**Table No. 12: Comparison of Allowable and Post-Development Conditions
Flows Discharging to Existing Stormwater Quality Facility No. 2**

DESIGN STORM	ALLOWABLE RELEASE RATES TO EXISTING SWM POND	POST-DEVELOPMENT FLOW RATES TO EXISTING SWM POND (CATCHMENT B2C)
	Flow Rate (m ³ /s)	Flow Rate (m ³ /s)
2 year	0.294	0.212
5 year	0.929	0.679
25 year	1.689	1.186
100 year	2.246	1.576

Therefore, the post-development flow rates discharging to the existing stormwater management facility (Stormwater Quality Facility No. 2) are less than the allowable release rates for the full range of design storm events.

**Table No. 13: Comparison of Allowable and Post-Development Conditions
Flows Discharging to Clythe Creek**

DESIGN STORM	ALLOWABLE RELEASE RATE TO CLYTHE CREEK	POST-DEVELOPMENT FLOW RATE TO CLYTHE CREEK (CATCHMENTS 201, 202 & 300)
	Flow Rate (m ³ /s)	Flow Rate (m ³ /s)
2 year	0.127	0.086
5 year	0.772	0.507
25 year	2.192	1.400
100 year	3.425	2.335
Regional Storm	0.936	0.906

Therefore, the post-development flow rates discharging to Clythe Creek have been attenuated to less than the allowable release rates, for the full range of design storm events.

Upon development of the apartment block (Block 125) located adjacent to Watson Parkway, privately owned and operated on-site quality and quantity stormwater management controls will be required to attenuate post-development flows to the existing condition level prior to discharge from the apartment block.

The allowable release rates (i.e. the existing condition release rates) from the Apartment block are as follows:

Table No. 14: Allowable Release Rates from the Apartment Block (Block 125)

DESIGN STORM	ALLOWABLE RELEASE RATE FROM APARTMENT BLOCK (BLOCK 125)
	Flow Rate (m ³ /s)
2 year	0.008
5 year	0.047
25 year	0.132
100 year	0.207
Regional Storm	0.056

5.2.4 MINOR / MAJOR DRAINAGE SYSTEM

Minor system drainage will be conveyed to the existing and proposed stormwater management facilities via storm sewers with the capacity to convey the 5-year design storm event.

Major design storm flows from the westerly portion of the development will be conveyed to the existing Stormwater Quality Facility No. 2 via the municipal right-of-way and the stormwater conveyance channel. Major design storm flows from the central portion of the development will be conveyed to the proposed stormwater management facility via the municipal right-of-way. Preliminary analysis indicates that the municipal right-of-ways have the capacity to convey the runoff from a major design storm event.

The major design storm drainage patterns expected for the Cityview Ridge Subdivision are shown on Figure 7.

5.2.5 FLOODPLAIN ANALYSIS

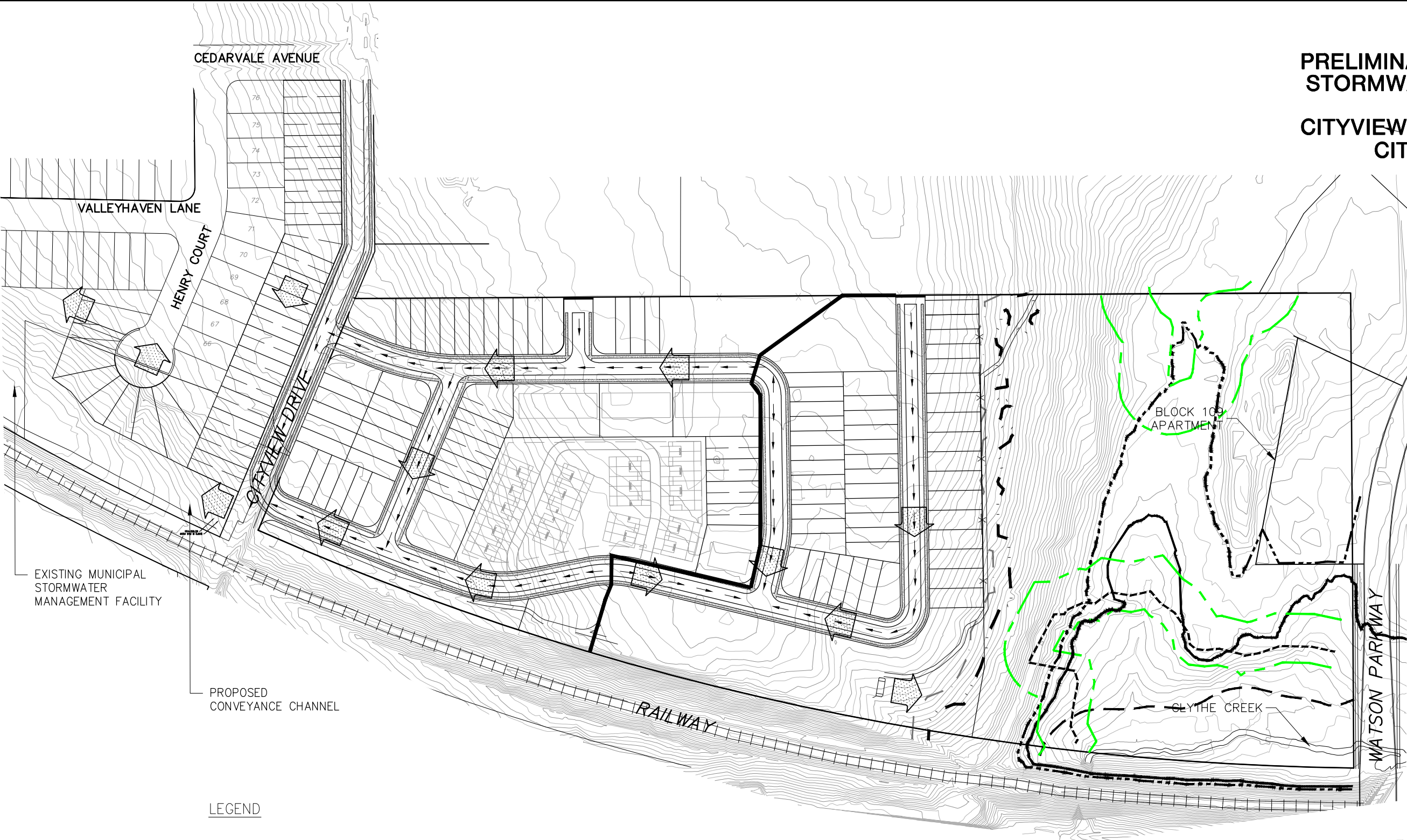
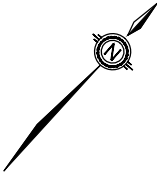
Cosburn Patterson Wardman Limited, as part of the Eastview Secondary Plan, analyzed the existing floodlines through Hadati Creek and Clythe Creek. As part of the Valleyhaven Subdivision Phase 3, the floodline analysis for Hadati Creek was updated. The floodline analysis for Clythe Creek was later revised by the Grand River Conservation Authority.

With the construction of the proposed stormwater management facility for the Cityview Ridge Subdivision, the flood storage volume for the major design storm event is being provided within the facility for the flows from the developable lands, along with the preliminary grading of the future apartment block, the floodplain storage volume has been maintained to ensure that the hazard to the public is minimized.

The HEC-RAS modelling has been edited to show the existing condition and post-development floodlines. A comparison to the pre- and post-development floodlines (flow rate, water surface elevation and flood width) through the Clythe Creek floodplain to the CN Railway lands has been included in Appendix 'E'. The post-development Regional Storm and 100-year Design Storm Event floodlines are shown on Drawing No. 2.

The HEC-RAS analysis is attached in Appendix 'F'.

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MAJOR STORM
DRAINAGE PATTERN

Figure No. 7

- LEGEND
- MAJOR OVERFLOW DISCHARGE ROUTE
 - MAJOR INTERNAL OVERFLOW ROUTE
 - DRAINAGE AREA DIVIDE
 - LIMIT OF CITYVIEW RIDGE SUBDIVISION

6.0 SEDIMENT AND EROSION CONTROL PLAN

A silt fence will be installed along the property boundary and along the environmentally sensitive areas of the site. The silt fence will minimize the opportunity for water borne sediments to be transported from the site. The ecologist and/or the Environmental Inspector will flag the location of the silt fence with the contractor. In accordance with standard City practice, an Environmental Inspector will be retained to monitor the construction activities. The silt fence location is shown on the Preliminary Grading and Drainage Plans (Drawings No. 1, 2 and 3).

Temporary rock check dams will be installed in rear yard swales after the initial grading has been completed to slow the flow rates and promote the settlement of water borne sediments before they reach the silt fences and stormwater management facilities.

Upon completion of the grading, any area not subject to active construction within 30 days will be top soiled and seeded as per OPSS 572.

The proposed stormwater management facility will be rough graded and used as a temporary sediment pond for the central portion of the site during the servicing and house building construction. The storage capacity of this pond exceeds the combined 250 m³/hectare of active and dead storage required. A heavy duty silt fence will be placed around the proposed stormwater management facility during construction.

A silt fence will be placed around the outlet structure of the existing stormwater management facility to restrict the movement of sediment. The discharge structure will restrict the release rate and provide extended detention for a minimum 24-hour period.

Once catch basins have been installed, the grates will be wrapped in filter cloth. This feature will be maintained until all building and landscaping has been completed.

Inspection and maintenance of all silt fencing and sediment and erosion controls will start after installation is complete. These features will be inspected on a weekly basis or after a rainfall event of 13 mm or greater. Maintenance will be carried out, within 48 hours, on any part of the controls found to need repair.

An Environmental Inspector will submit monthly reports on the conditions of the sediment and erosion control measures to the City of Guelph and the Grand River Conservation Authority.

Once construction and landscaping within the limits of the subdivision has been substantially completed (75% house building construction is complete), the silt fence will be removed, any accumulated sediment will be collected and the area will be restored. Upon final inspection by both the Environmental Inspector and City of Guelph, the monthly reporting on the condition of the sediment and erosion control measures will cease.

After construction of the complete development, erosion and sediment transport will be minimal.

7.0 MAINTENANCE PLAN

A two-phase maintenance plan is recommended. Phase I will address the short-term more intensive maintenance necessary during and immediately after construction. Once all landscaping has been completed, maintenance will shift to Phase II.

As outlined in the section on Sediment and Erosion Control, Phase I will include weekly inspection of all sediment control devices plus “as needed” inspection after any significant rainfall, with all immediate repair of any damaged works and collection of captured sediment. This work will be carried out by the Consultant and/or the Environmental Inspector during the construction of the works. A monthly status report will be prepared and distributed to the City of Guelph and the Grand River Conservation Authority.

Phase II will be the maintenance carried out by the City of Guelph after all construction has been completed. This work will involve a yearly visual inspection of the stormwater management facilities to determine the amount of sediment accumulation. Sediment should be removed as required and the recommended vegetation replanted.

8.0 CONCLUSIONS

From the foregoing analysis, the following conclusions are drawn:

1. Water supply for the proposed Cityview Ridge Subdivision will be provided by:
 - a. the extension of the existing 150 mm diameter watermain on Henry Court,
 - b. the extension of the existing 200 mm diameter watermain southerly on Cityview Drive,
 - c. the extension of the existing 150 mm diameter watermain from the existing municipal stormwater management facility to the Cityview Drive right-of-way, and
 - d. via a connection to the existing 300 mm diameter watermain on Watson Parkway.
2. Sanitary service for the Cityview Ridge Subdivision will be provided by:
 - a. the extension of the existing 200 mm diameter sanitary sewer on Henry Court,
 - b. the extension of a 200 mm diameter sanitary sewer from the 200 mm diameter sanitary sewer stub in the existing municipal stormwater management facility to the Cityview Drive right-of-way, and
 - c. via a connection to the existing 525 mm diameter sanitary sewer on Watson Parkway.
3. All storm sewers within the Cityview Ridge Subdivision will be sized to accommodate the 5-year design storm event.
4. The topography of the site will generally allow for sufficient cover on the storm sewer to connect house foundation drains. Where a storm service connection is not possible, foundation drainage will be provided by sump pumps discharging to the grassed side and rear yard surfaces.
5. Quality and quantity control for runoff generated from the westerly portion of the development will be provided by the existing Stormwater Quality Facility No. 2 and the existing Stormwater Quantity Control Facility, constructed as part of the Valleyhaven Subdivision Phase 3.

Quality and quantity control for runoff generated from the central portion of the development will be provided by a sediment forebay before entering the proposed stormwater management facility, prior to discharge to Clyde Creek.

Quality and quantity control for runoff generated from the easterly section of the site which includes a future development apartment block will be provided by privately owned and operated on-site stormwater management controls, which will be designed, reviewed and approved as part of the site plan approval process for the development.

6. Installation of infiltration systems in the rear yard areas is not feasible due to the low hydraulic conductivity of the native underlying silty tills and the presence of high groundwater levels.
7. The floodplain storage volume has been maintained under post-development conditions to ensure that the hazard to the public is minimized.
8. The stormwater management systems meet the current Provincial and Municipal guidelines.
9. During the construction phase, the proposed stormwater management facility will be used as part of the erosion and sediment control plan. This in conjunction, with the other erosion control measures, will minimize the transport of sediment off-site during the construction period.

All of which is respectfully submitted.

GAMSBY AND MANNEROW LIMITED

Per:



Angela Kroetsch, P.Eng.

AK/pg

Encl.



W:\Guelph\105-2005\105172\Documents\Reports, Manuals, Contracts\105172 SWM Design Report_ Revised June 2017.doc

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX "A"

**Geotechnical Investigation
Naylor Engineering Associates Ltd.
(February 2012)**

**GEOTECHNICAL INVESTIGATION
P.T. VALERIOTE SUBDIVISION
CITYVIEW DRIVE
GUELPH, ONTARIO
for
CARSON REID HOMES LTD.**

0353G4.R01_Rev.
February 2012

DISTRIBUTION:
1ec: Client
1ec: Gamsby & Mannerow Limited
1cc: File

February 17, 2012

Carson Reid Homes Ltd.
183 Dufferin Street
Guelph, Ontario
N1H 4B3

Attention: Mr. Carson Reid

Dear Sir:

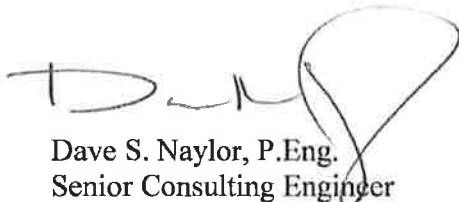
**Re: Geotechnical Investigation
P.T. Valeriote Subdivision
Cityview Drive
Guelph, Ontario**

Naylor Engineering Associates Ltd. is pleased to submit this *revised* report for the geotechnical investigation recently completed for the above-referenced development site.

This report outlines the investigation procedures and provides a summary of the subsurface conditions encountered. Geotechnical comments and recommendations are provided for slope stability assessment, site grading, site servicing, pavement design, house foundations, industrial/commercial building foundations, stormwater infiltration, and stormwater management ponds design.

We trust that this report is suitable for your present requirements and we thank Carson Reid Homes Ltd. and Gamsby & Mannerow Limited for this opportunity to have been of service. If you have any questions or require any further geotechnical consultation, please do not hesitate to contact our office.

Yours very truly,



Dave S. Naylor, P.Eng.
Senior Consulting Engineer

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List of Abbreviations

Figure 1 – Particle Size Distribution Curves

Figures 2 and 3 – Standard Proctor Moisture-Density Test Results

Borehole Logs – Boreholes 101 through 110

Drawing 1 – Location Plan

Drawing 2 – Site Plan

Drawing 3 – Slope Stability A-A'

Drawing 4 – Typical Structural Fill Pad Detail

Drawing 5 – Typical Pavement Subdrain Detail

1. Introduction

Naylor Engineering Associates Ltd. was retained by Carson Reid Homes Ltd. to carry out a geotechnical investigation for a proposed residential subdivision on Cityview Drive in Guelph, Ontario, as shown on the appended Location Plan, Drawing 1. This work was authorized by Mr. Carson Reid of Carson Reid Homes Ltd. on July 13, 2006, following submission of a detailed proposal.

The project involves the residential development of a 17.682 ha property. The proposed residential subdivision will contain about 150 lots with full municipal services. An apartment block is proposed for the northeast corner of the property. A stormwater management pond is proposed at the south central area of the property.

The purpose of this investigation was to determine the subsurface soil and groundwater conditions and, based on that information, prepare this engineering report with geotechnical recommendations pertaining to slope stability, site grading, site servicing, pavement design, house foundations, industrial/commercial foundation design, stormwater infiltration and stormwater management pond design. The report does not address site environmental or hydrogeological issues.

2. Investigation Procedure

2.1 Field Program

The fieldwork for this investigation was carried out between July 31 and August 2, 2006 and involved the drilling of ten boreholes (Boreholes 101 through 110) to depths of 5.6 to 11.1 m at the locations shown on the appended Site Plan, Drawing 2. Twenty topsoil thickness holes were dug to measure the topsoil thickness. Approximate topsoil thickness hole locations are also shown on Drawing 2.

The boreholes were advanced with a CME-75 track-mounted drillrig equipped with continuous flight solid stem augers, supplied and operated by a specialist drilling contractor. Soil samples were recovered from the boreholes at regular 0.75 and 1.50 m depth intervals using a 50 mm O.D. split spoon sampler in accordance with the Standard Penetration Test (SPT) procedure. The SPT N-values recorded are plotted on the appended borehole logs.

Monitoring wells were installed in all of the boreholes to allow measurement of the stabilized groundwater levels. These installations comprised 50 mm diameter PVC pipes with slotted filters, as well as bentonite seals. At Boreholes 103, 104, 105, 106, and 107, a shallow 19 mm diameter CPVC pipe was also installed to determine the vertical hydraulic gradient. Groundwater levels were measured in the standpipes and monitoring wells on August 8, 2006 by Naylor Engineering Associates Ltd. Details of installations and groundwater measurements are provided on the appended borehole logs.

All standpipes and monitoring wells were installed by licensed well technicians in accordance with Ontario Regulation 903. A well tag was attached to the standpipe at Borehole 011. The standpipes must be properly decommissioned by a licensed well technician within six months of last use, and certainly before construction begins.

The fieldwork was supervised throughout by a member of our engineering staff who directed the drilling and sampling procedures; conducted SPT testing; documented the soil stratigraphies, and cared for the recovered soil samples.

The borehole locations and ground surface elevations were surveyed by Gamsby & Mannerow Limited and the data was supplied to us in AutoCAD format. It is understood that the elevations are related to a geodetic datum.

2.2 Laboratory Testing

All soil samples secured during this investigation were returned to our laboratory for moisture content tests; the results of which are plotted on the borehole logs. Geotechnical laboratory tests carried out on selected samples of the major subsurface soils from the investigation comprised three particle size distribution test with results presented on Figure 1, and two standard Proctor moisture-density tests with results plotted on Figures 2 and 3.

The soil samples will be stored for a period of four months (December 2006) from the date of sampling. After this time, they will be discarded unless prior arrangements have been made for longer storage.

3. Site Conditions

3.1 Site Description

The subject development is approximately 17.682 ha and is located in the northeast area of Guelph, Ontario. For the purpose of this report it was assumed Watson Parkway runs north-south adjacent to the east side of the property. The property is bordered on the north by a vacant field, on the south by a Canadian National Railway Line, on the east by Watson Parkway, and on the west by existing residential development.

The property is split in two pieces: with the proposed residential development on the west side of the property and a proposed apartment block on the east side. From the low-lying lands in the east part of the property area, the grade slopes up about 20 m to the higher lands in the west section.

The residential property is moderately sloped. A hill runs north-south and divides the residential property into east and west sloping sides. The residential property is vegetated with mostly tall grass and some medium sized deciduous trees.

The proposed apartment block is relatively level and is at the northeast corner of the property. The apartment block is densely vegetated with spruce trees. The topographic relief for this part of the property is less than 1 m.

3.2 Subsurface Soil Conditions

We refer to the appended borehole logs for detailed soil descriptions and stratigraphies, SPT N-values, moisture content profiles, details of standpipe installations, and groundwater observations and measurements.

The subsurface stratigraphy at the site generally comprises topsoil overlying silt till in the proposed residential area. At the proposed apartment block at the northeast corner of the property, the subsurface stratigraphy generally comprises topsoil overlying sand and gravel. Descriptions of the various soil deposits and the groundwater conditions encountered are provided in the following subsections.

3.2.1 Topsoil

Topsoil was contacted surficially throughout the property. The topsoil is typically 200 to 350 mm thick in the proposed residential area, and 400 mm thick in the low lying land. The topsoil generally comprises dark brown silt. The average topsoil thickness in the residential lands and commercial lands are 250 mm and 300 mm, respectively.

3.2.2 Sand and Gravel

Sand and gravel was encountered in the low lying area at the northeast corner of the site (Boreholes 109 and 110). The sand and gravel continues below the termination depths of the boreholes. This deposit consists of sand and gravel with some silt; and there were frequent cobbles and boulders in the soil matrix. A particle size distribution analysis performed on one sample of the sand and gravel indicated the sample contained 44% gravel, 41% sand, and 15% silt (see Figure 1).

Typically, the sand and gravel is very dense based on SPT N-values of greater than 50 blows per 300 mm penetration of the split-spoon sampler. The moisture content of the sand and gravel is typically about 5% above the water table, and between 8 and 12% in saturated conditions.

3.2.3 Silt Till

Silt till was encountered in all boreholes located in the proposed residential area. The silt till continues below the termination depths of the boreholes in which it was encountered. In Boreholes 102 and 105, possible weathered bedrock was encountered at borehole termination depth. This deposit ranges in composition from sandy silt with some gravel and cobbles, to silt with some clay sand and gravel. Particle size distribution analyses performed on two samples of the silt till indicated the samples contained 5% to 11% gravel, 41% sand, 36 to 44% silt, and 10 to 11% clay (see Figure 1).

Typically, within 2 m of the ground surface, the silt till is loose to compact based on SPT N-values of 5 to 25 blows per 300 mm. Below this upper portion, the silt till is dense to very dense based on SPT N-values from 30 to greater than 50 blows per 300 mm.

The moisture content of the silt till is typically between 8 and 12%. Two standard Proctor moisture-density tests performed on samples of the silt till from Boreholes 105 and 106 indicated maximum dry densities of 2.065 t/m³ and 2.185 t/m³ and optimum moistures of 9.0% and 8.7% (see Figures 2 and 3).

3.3 Groundwater

Groundwater was encountered in saturated seams within the silt till, and under water table (unconfined) conditions in the sand and gravel deposit. The stabilized levels were between Elevation 321.0 m (Borehole 110) to 344.5 m (Borehole 107).

Within the apartment block at the northeast corner, the horizontal gradient of the groundwater in the sand and gravel is from north to south towards Clythe Creek. Within the remainder of the residential area, the variable groundwater levels in seams within the silt till generally follow the topography.

4. Discussion and Recommendations

The project involves the residential development of an approximately 17.682 ha property. The proposed subdivision will be provided with full municipal services. It is assumed that on-site stormwater management controls will be required for the apartment block abutting Watson Parkway North. A portion of the lands on the west half of the site will drain to an existing stormwater management facility located to the west of Cityview Drive.

The subsurface stratigraphy at the site generally comprises topsoil overlying silt till in the proposed residential area, and topsoil overlying sand and gravel in the apartment block. Groundwater is contained in thin seams within the silt till at variable depths, and in the sand and gravel at about 3 to 4 m depth.

The following sections of this report provide geotechnical recommendations for the construction of the subdivision including slope stability assessment, site grading, site servicing, pavement design, house foundations, apartment building foundations, stormwater infiltration and stormwater management pond design.

4.1 Site Grading

At the time of the report preparation, grading plans were not available for review; however, we would anticipate area grading of the property to prepare the land for construction of the proposed residential subdivision. In general, material may be cut from the high areas to raise grades in lower areas of the site.

Prior to carrying out any area grading of the site, the surficial topsoil should be removed from cuts and critical fill areas. In calculating the approximate quantity of topsoil to be stripped, we note that the average thickness of topsoil contacted in the boreholes is about 300 mm for the residential lands and 300 mm for the commercial/industrial lands. We recommend that the topsoil thickness be increased by 50 mm for volume calculations to account for variations, and some stripping of the mineral soil below. The topsoil material could be used for landscaping fill to raise grades in the rear yards of the house lots or in park areas.

Following stripping of topsoil, the exposed subgrade should be inspected by Naylor Engineering Associates Ltd. Fill should be placed in maximum 300 mm thick lifts and compacted to the following minimum percentages of standard Proctor maximum dry density (SPMDD):

Fill Use	Minimum Compaction Required
Structural fill to support residential houses	98% SPMDD
Structural fill to support commercial/industrial buildings	100% SPMDD
Subgrade fill beneath streets	95% SPMDD
Bulk fill in landscaped areas	90% SPMDD

The major soil likely to be generated from the cut areas of the residential lands is silt till. The moisture content of the silt till generally ranges between 8 and 12%, and the optimum moisture for compaction is about 9% (see Figures 2 and 3). The silt till will have to be allowed to dry before it can be used as structural fill, and therefore we recommend that any structural filling be carried out in the drier summer months.

The structural fill should extend at least 1.0 m beyond the footing edge of any building and down to the subgrade level at a slope of 45° to the horizontal. A typical detail for structural fill placement beneath house foundations is shown on Drawing 5, appended.

The major soil likely to be generated from the apartment block side of the site is sand and gravel and this material will be well-suited for compaction.

Full-time inspection by experienced geotechnical personnel should be carried out during fill placement and compaction to examine and approve potential sources of fill material, and to carefully monitor the placement and verify the compaction by insitu density testing.

4.2 Site Servicing

Following the site grading operations, the property will be serviced to provide the individual lots and blocks with full municipal services. It is anticipated that the invert levels for the watermain and sewers will be at conventional depths, some 2 to 4 m below finished grade.

Temporary excavations to conventional depths for installation of underground pipes at this site should comply with Regulation 213/91 (Construction Projects) under the Ontario Occupational Health and Safety Act. The predominant soils encountered in the test holes would be classified as Type 2 soils, and temporary side slopes should be cut near vertical in the bottom 1.2 m and then trimmed back to an inclination of maximum 1 horizontal to 1 vertical.

No major groundwater problems are envisaged for excavations at this site. In general, low to moderate rates of seepage are to be expected from the silt till. It is expected that the groundwater inflow can be handled using conventional sump pumping techniques.

The subgrade soils beneath the watermain and sewer pipes will comprise native mineral soils or compacted fill placed during the site grading operations. No bearing problems are anticipated for flexible or rigid pipes founded in the native deposits or compacted on-site soils. The bedding should be placed in accordance with Ontario Provincial Standard Drawings (OPSD 802.030 and 802.033).

Pipe bedding for water and sewer services should be conventional Class 'B' pipe bedding comprising a minimum 150 mm thick layer of OPSS Granular 'A' aggregate below the pipe invert. The bedding course may be thickened if portions of the subgrade become unduly wet during excavation. Granular 'A' type aggregate should be provided around the pipe to at least 300 mm above the pipe. The bedding aggregate should be compacted to a minimum 98% SPMDD.

The trenches above the specified pipe bedding should be backfilled with inorganic on-site soils placed in 300 mm thick lifts and compacted to at least 95% SPMDD. Based on the results of insitu moisture content and standard Proctor moisture-density tests carried out on the native overburden deposits, the majority of the on-site excavated materials will be compactable to the required 95% SPMDD. The silt till soil may require some drying prior to re-use as trench backfill.

To minimize potential problems, backfilling operations should follow closely after excavation so that only a minimal length of trench is exposed. Care should be taken to protect side slopes of excavations by diverting surface run-off away from the excavations. If construction extends into the winter, then the backfilling operations should be planned so that exposure of the backfill material to frost is kept to a minimum and to ensure that frozen material is not used as backfill.

Excavations for the installation of sewers across the apartment block may extend into saturated sand and gravel deposits. The hydraulic conductivity of the granular soil is estimated to be in the order of 10^{-5} m/s based on the gradation analysis. Moderate to significant groundwater inflow through the granular soil is expected where the excavations extend below an elevation of 320.4 m. It is believed that the groundwater inflow can be controlled with high capacity pumps and perimeter interceptor ditches. In order to facilitate sewer installation more than 0.6 m below the stabilized groundwater table, a dewatering system installed by a specialist dewatering contractor may be required to lower groundwater level prior to excavation.

Frequent inspection and compaction testing by experienced geotechnical personnel should be carried out to examine and approve backfill materials, and to verify that the specified degree of compaction has been achieved.

4.3 Pavement Design

A number of local residential streets are planned for the residential subdivision. Following site grading and installation of services, the pavement subgrade will comprise predominantly recompacted excavated silt tilt soils. The following pavement component thicknesses are recommended based on the proposed pavement usage, and the frost-susceptibility and strength of the subgrade soils:

Pavement Component	Local Streets
Asphaltic Concrete	90 mm
Granular 'A' Base Course	150 mm
Granular 'B' Subbase Course	450 mm

The pavement subgrade materials should be thoroughly proof-rolled under supervision of a geotechnical engineer prior to placement of the Granular 'B' subbase course. If any unstable areas are noted, then the Granular 'B' thickness may need to be increased to support pavement construction traffic. This should be left as a field decision at the time of construction, but it is recommended that these materials be carried as a provisional item under the construction contract.

Samples of both the Granular 'A' and Granular 'B' aggregates should be checked for conformance to OPSS 1010 prior to utilization on site and during construction. The Granular 'B' subbase and Granular 'A' base courses must be compacted to 100% SPMDD, as verified by insitu density testing.

The asphaltic concrete should comprise a binder layer of HL4 and a surface layer of HL3. It is recommended that the compacted thickness be 55 mm of HL4 binder and 35 mm of HL3 surface for the local streets. The purpose of the thicker HL4 layer is to support construction traffic during the time period before the HL3 is placed.

The asphaltic concrete paving materials should conform to the requirements of OPSS 1150. The asphalt should be placed in accordance with OPSS 310 and compacted to within the range of 92.0 to 97.5% of the plant produced Maximum Relative Density (MRD) value. The Performance Graded Asphalt Cement designation for the asphaltic concrete is 58-28.

The silt till subgrade soils has poor natural drainage and therefore continuous pavement subdrains are recommended. A typical detail of a pavement subdrain is provided in Drawing 4, appended.

The concrete for sidewalks, and curb and gutter should be proportioned, mixed, placed, and cured in accordance with the requirements of OPSS 351, 353, and 1350, and shall meet the following specific requirements:

- minimum 28-day compressive strength = 32 MPa
- slump = maximum 80 mm
- air entrainment = $6.5\% \pm 1.5\%$

During cold weather, the freshly placed concrete must be covered with insulating blankets to protect against freezing. Three cylinders from each day's pour should be taken for compressive strength testing. Air entrainment, temperature, and slump tests should be made from the same batch of concrete from which test cylinders are made.

The subgrade for the sidewalks should comprise undisturbed native mineral soil or well-compacted fill. A minimum 150 mm thick layer of compacted Granular 'A' type aggregate should be placed beneath the sidewalk slabs.

4.4 House Foundations

The undisturbed native mineral soil deposits underlying this site are considered suitable to support residential house foundations. Where the footing levels will be above the existing native mineral soil grade, structural fill will be utilized. The native soil or properly compacted structural fill will be suitable to support house footings proportioned to the minimum sizes provided in Part 9 of the Ontario Building Code.

All founding surfaces for residential dwellings on structural fill or native soils should be inspected by Naylor Engineering Associates Ltd. personnel prior to placing concrete. The purpose of the inspection is to ensure that the subgrade soils are capable of supporting the house foundations, and to confirm that the house envelope does not extend beyond the limits of the structural fill pad.

The subgrade soils are considered to be frost susceptible and must be protected from freezing at all times including during construction. The exterior footings, or footings in unheated areas, should be provided with a minimum 1.20 m of earth cover upon final grading for frost protection.

House basements at this site must be provided with perimeter weeping tile systems as per the Ontario Building Code. The drain tile or pipe should be laid on undisturbed or well-compacted soil so that the top of the tile or pipe is below the bottom of the basement floor slab. The weeping tile must drain to a suitable frost-free outlet or sump as per City of Guelph requirements. We recommend that the bedding for the tiles comprise concrete sand.

4.5 Stormwater Management

At the time of the report preparation, no design details of the SWM pond were available for review. In general, the silty soils at the site will not allow stormwater infiltration; however, the SWM pond will be suitable for storage and siltation control. The sand and gravel deposit on the east side of the property would allow stormwater infiltration.

It is anticipated that berms will be required to create the SWM pond. The berms should be constructed using the on-site silt till. The berm fill should be placed in thin lifts and compacted to at least 95% SPMDD.

The SWM pond berms should be sloped at 3 horizontal to 1 vertical, or flatter, and should be re-topsoiled and vegetated as soon as possible.

It is anticipated at-source dry well infiltration may be considered for the subdivision. The soils in the proposed residential area have a high silt content and are not suitable for at-source drywell infiltration. In the proposed apartment block, the sand and gravel deposits may be used for at-source infiltration. Based on particle size distribution analyses, we estimate that the hydraulic conductivity of the native sand and gravel is in the order of 10^{-5} m/s. We recommend that an infiltration rate of 15 mm/hr be assumed for sizing the dry wells. All drywell subgrades should be inspected by Naylor Engineering Associates Ltd. to confirm the conditions are suitable for infiltration.

4.6 Apartment Buildings

At the time of the report preparation, no building locations for the apartment blocks were available. We recommend further investigation when this information is available to determine subsurface condition details for foundations and services.

All organics and other deleterious materials should be removed from beneath the footprint of the proposed building(s) and new pavement areas.

Following removal of unsuitable material, the exposed subgrade should be inspected by a geotechnical engineer. Any soft or unstable areas should be subexcavated. The native subgrade soil will comprise sand and gravel and will be contacted below the topsoil.

The undisturbed native mineral soils are considered suitable to support conventional building foundations. If the footing levels will be above the existing native mineral soils, then structural fill should be placed as noted in Section 4.1. Building foundations constructed on the native mineral soil or approved structural fill may be proportioned for a nominal net allowable bearing pressure of 200 kPa.

All founding surfaces for buildings on structural fill or native soils should be inspected by Naylor Engineering Associates Ltd. personnel prior to placing concrete. The purpose of the inspection is to ensure that the subgrade soils are capable of supporting the foundations, and to confirm that the building envelope does not extend beyond the limits of the structural fill pad.

The subgrade soils are considered to be frost susceptible and must be protected from freezing at all times including during construction. The exterior footings or footings in unheated areas should be provided with a minimum 1.20 m of earth cover upon final grading for frost protection.

4.7 Slope Stability Assessment

In order to analyze the stability of the existing slope, Boreholes 104 to 106 were advanced near the top of slope. A slope profile at the steepest location is shown on Drawing 2. The information was then used for computer analyses of the slope stability using the Slope/W Program (Morgenstern-Price Method). The results of the analyses are shown on Drawing 3.

The soil parameters used in the analyses have been estimated based on the results of the field and laboratory testing and are as follows:

Soil Material	Unit Weight (kN/m ³)	Angle of Internal Friction	Cohesion (kPa)
Silt Till	22	32°	20

The slope stability analyses were carried out for a number of potential failure types. The various failures analyzed included shallow slumping type failure of the slope surface, medium depth rotational failures in the silt till, and deep rotational failures through the entire height of the slope.

In order to determine an appropriate development setback from the top of slope, a minimum factor of safety of 1.50 was used as per Grand River Conservation Authority policy. The steepest slope profile was used for the analyses to determine the setback required to achieve this factor of safety. The setback is typically determined based on the point at which the failure slipcircle (for factor of safety of 1.50) intersects the tableland of the crest of the slope; however, the analyses revealed that the slope has a factor of safety of greater than 1.50. The analysis reveals that the slope has a factor of safety of 2.75 which is well above the Grand River Conservation Authority minimum slope factor of safety.

Toe erosion at the wetland at the bottom of the slope is expected to be minor. A nominal 100 year erosion setback of 1 m is recommended.

A 6 m erosion access allowance is recommended for slopes by the Ministry of Natural Resources. The erosion access allowance is the setback needed to ensure enough space is available for workers and vehicles to access the area.

In conclusion, the primary causes of potential instability for the slope embankment would be development and loading directly at the crest, and general surface erosion caused by run-off from the site. To ensure no loading at the crest (from buildings, pools, fill, etc.) and to compensate for possible long-term erosion, the following setbacks from the top of slope are recommended:

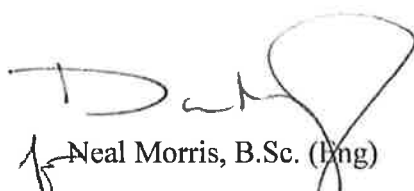
Cross-Section	Stability Setback for Factor of Safety of 1.50 (m)	100 year Erosion Setback (m)	Erosion Access Allowance Setback (m)	Total Development Setback from Top of Slope (m)
A-A'	0	1	6	7

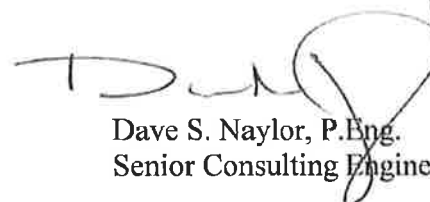
The estimated top of slope and 'total development setback' lines are shown on Drawing 2, appended.


Surface run-off must be directed away from the slope crest if possible. No fill should be placed at the crest of the slope or over the face of the existing slope unless the fill placement is engineered. No excavation work should be carried out on the slope or at the bottom of the slope.

This investigation was conducted to determine geotechnical parameters for the construction of the proposed residential subdivision and apartment block on Cityview Drive in Guelph, Ontario. The recommendations in this report are based on subsurface conditions encountered at specific borehole locations, and conditions between the boreholes will vary. Should conditions be encountered which differ materially from those at the borehole locations, we ask that we be notified immediately in order to assess the additional information and its effects on our conclusions.

Respectfully submitted,


Neal Morris, B.Sc. (Eng)
jb/jmp


Dave S. Naylor, P.Eng.
Senior Consulting Engineer



LIST OF ABBREVIATIONS

The abbreviations commonly employed on the borehole logs, on the figures, and in the text of the report, are as follows:

Sample Types		Soil Tests and Properties	
AS	auger sample	SPT	Standard Penetration Test
CS	chunk sample	UC	unconfined compression
RC	rock core	FV	field vane test
SS	split spoon	ϕ	angle of internal friction
TW	thin-walled, open	γ	unit weight
WS	wash sample	w_p	plastic limit
		w	water content
		w_l	liquid limit
		I_L	liquidity index
		I_p	plasticity index
		PP	pocket penetrometer

Penetration Resistances

Dynamic Penetration Resistance	The number of blows by a 63.5 kg (140 lb.) hammer dropped 0.76 m (30 in.) required to drive a 50 mm (2 in.) diameter 60 ° cone a distance 0.30 m (12 in.). The cone is attached to 'A' size drill rods and casing is not used.
Standard Penetration Resistance, N (ASTM D1586)	The number of blows by a 63.5 kg (140 lb.) hammer dropped 0.76 m (30 in.) required to drive a standard split spoon sampler 0.30 m (12 in.)
WH	sampler advanced by static weight of hammer
PH	sampler advanced by hydraulic pressure
PM	sampler advanced by manual pressure

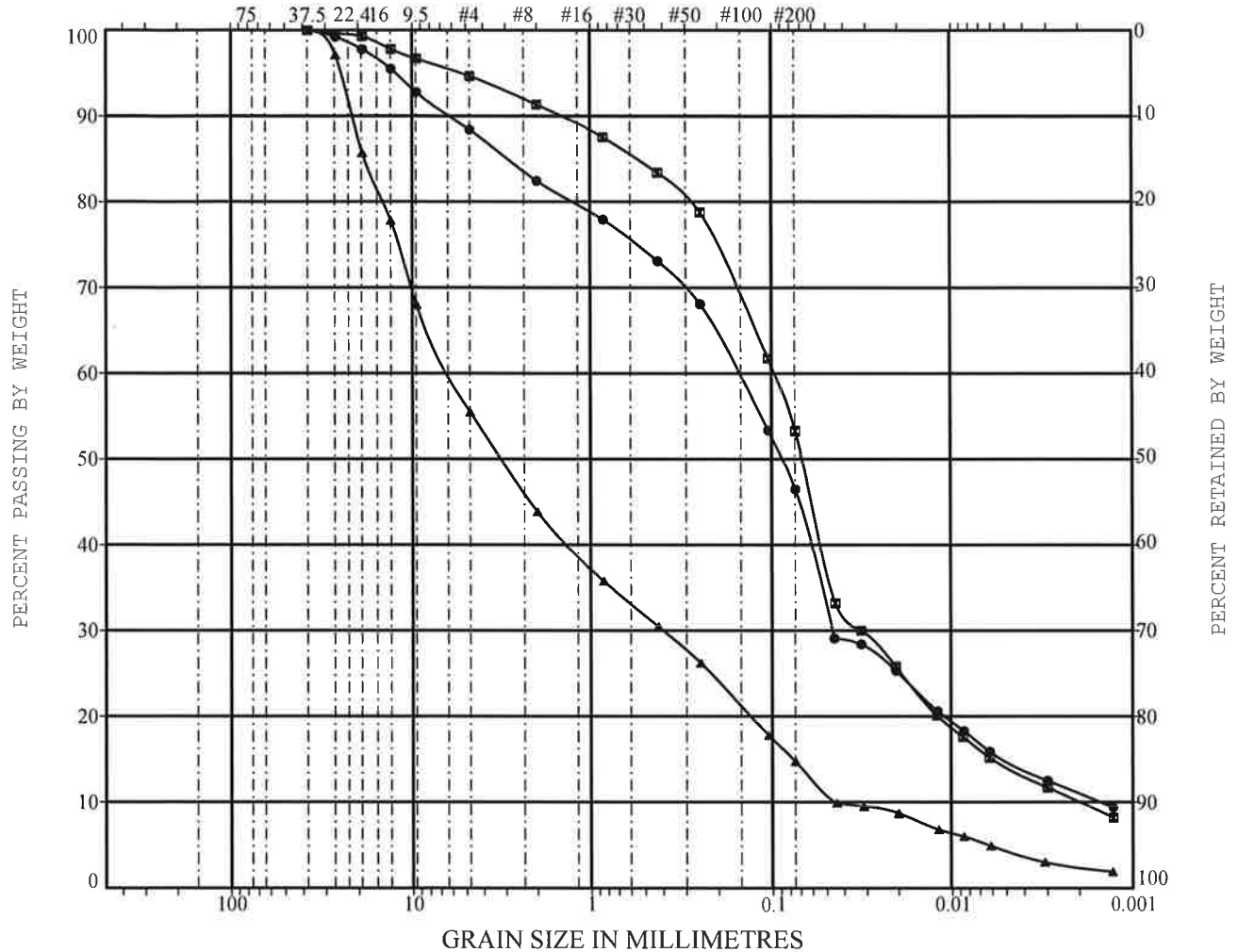
Soil Description

Cohesionless Soils	SPT 'N' Value	D_r (%)
Relative Density (D_r)	(blows per 0.30 m)	
Very Loose	0 to 4	0 to 20
Loose	4 to 10	20 to 40
Compact	10 to 30	40 to 60
Dense	30 to 50	60 to 80
Very Dense	over 50	80 to 100
Cohesive Soils	Undrained Shear Strength (C_u)	
Consistency	kPa	psf
Very Soft	less than 12	less than 250
Soft	12 to 25	250 to 500
Firm	25 to 50	500 to 1000
Stiff	50 to 100	1000 to 2000
Very Stiff	100 to 200	2000 to 4000
Hard	over 200	over 4000
DTPL	Drier than plastic limit	
APL	About plastic limit	
WTPL	Wetter than plastic limit	

Naylor Engineering Associates Ltd.

UNIFIED SOIL CLASSIFICATION

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	
U.S. SIEVE SIZE IN MILLIMETRES			U.S. STANDARD SIEVE No.			HYDROMETER



PROJECT P.T. Valeriotte Subdivision

LOCATION Cityview Drive, Guelph, Ontario

JOB NO. 0353G4

CURVE BOREHOLE/ SAMPLE DEPTH

ID TEST PIT NO. (m) SOIL DESCRIPTION

- BH101 BS 1.85-3.05 SILT TILL: SILT and SAND, some Gravel, trace Clay
- BH105 BS 1.22-2.13 SILT TILL: SAND and SILT, trace Gravel and Clay
- ▲ BH110 Sa2 5.00-6.50 SAND AND GRAVEL, some Silt

REMARKS



Naylor Engineering Associates Ltd.
CONSULTING ENGINEERS

Figure No. 1



Naylor
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Associates
CONSULTING ENGINEERS

LABORATORY PROCTOR MOISTURE-DENSITY TEST

PROJECT P.T. Valeriot Subdivision

LOCATION Cityview Drive, Guelph, Ontario

JOB NO. 0353G4

BOREHOLE NO. BH105

DATE TESTED August 21, 2006

SAMPLE DEPTH 1.22 - 2.13

TESTED BY WF

SOIL TYPE SILT TILL

MOISTURE CONTENT 14.9%

REMARKS _____

STANDARD PROCTOR - ASTM D698-91

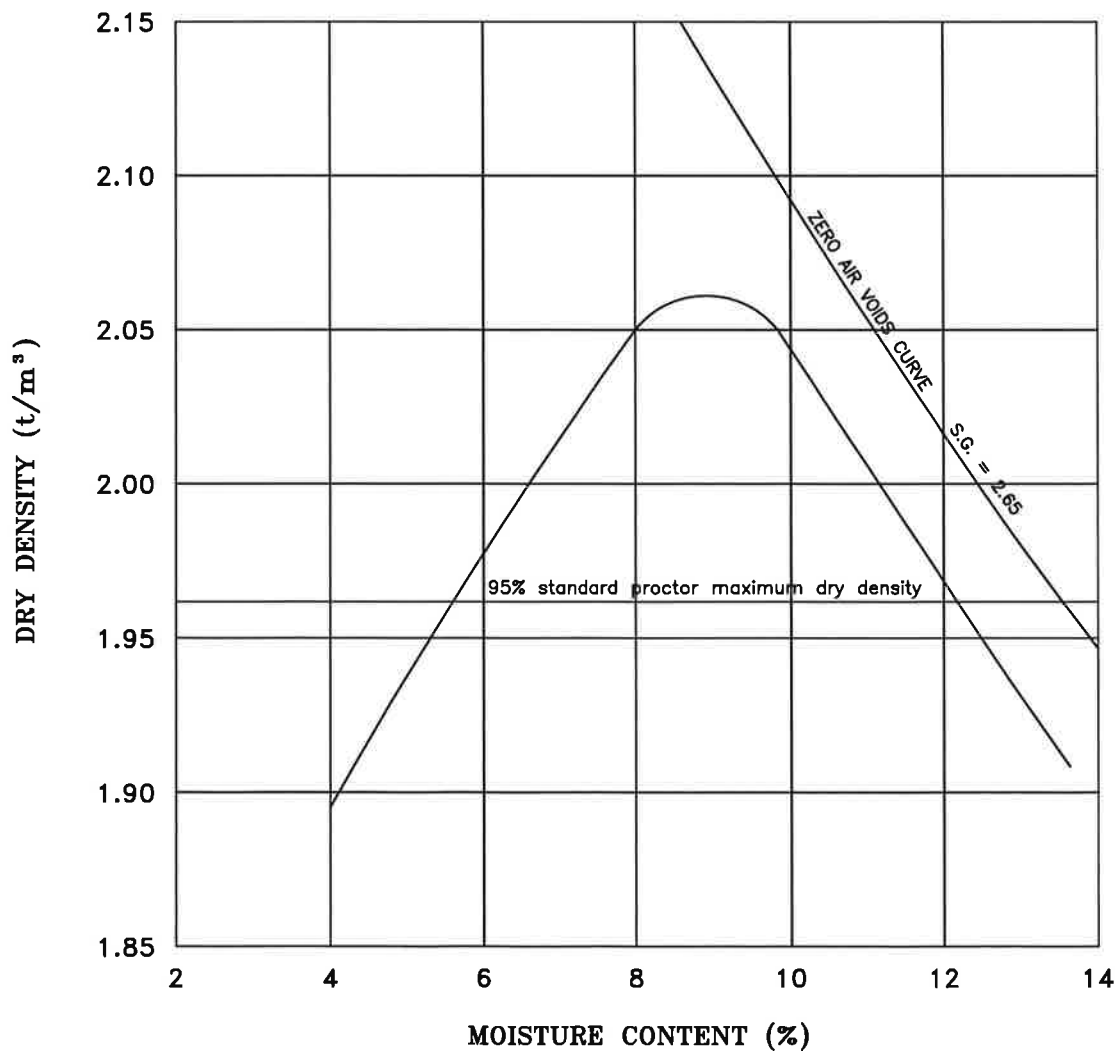
METHOD - A ☒ B ☐ C ☐ D ☐

MODIFIED PROCTOR - ASTM D1557-91

METHOD - A ☐ B ☐ C ☐ D ☐

MAXIMUM DRY DENSITY 2.065 t/m³

OPTIMUM MOISTURE 9.0%





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LABORATORY PROCTOR MOISTURE-DENSITY TEST

PROJECT P.T. Valeriot Subdivision

LOCATION Cityview Drive, Guelph, Ontario

JOB NO. 0353G4

BOREHOLE NO. BH106

DATE TESTED August 21, 2006

SAMPLE DEPTH 1.52 - 3.05m

TESTED BY KJ

SOIL TYPE SILT TILL

MOISTURE CONTENT 8.7%

REMARKS _____

STANDARD PROCTOR - ASTM D698-91

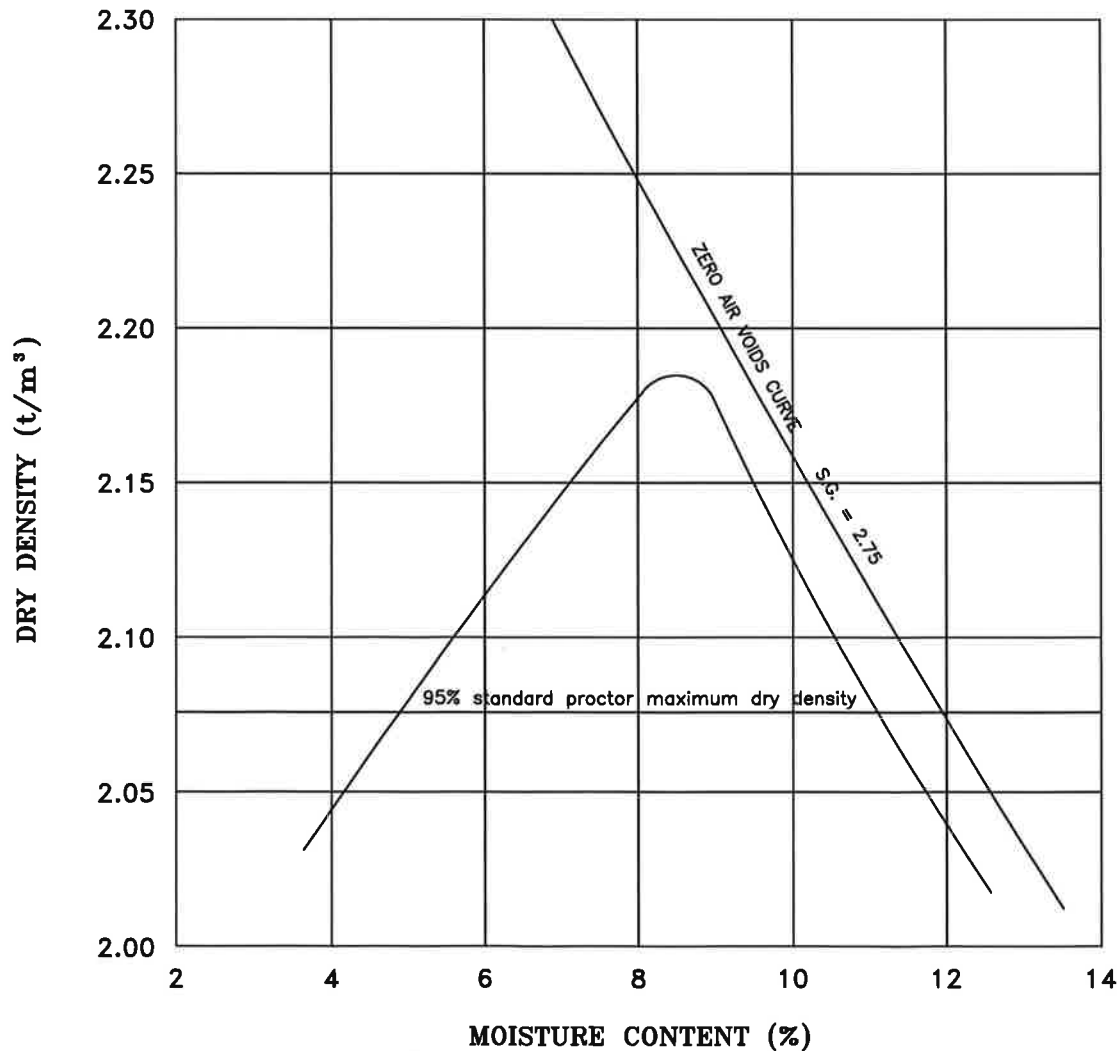
METHOD - A ☐ B ☐ C ☒ D ☐

MODIFIED PROCTOR - ASTM D1557-91

METHOD - A ☐ B ☐ C ☐ D ☐

MAXIMUM DRY DENSITY 2.185 t/m³

OPTIMUM MOISTURE 8.7%





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Borehole Number: 101

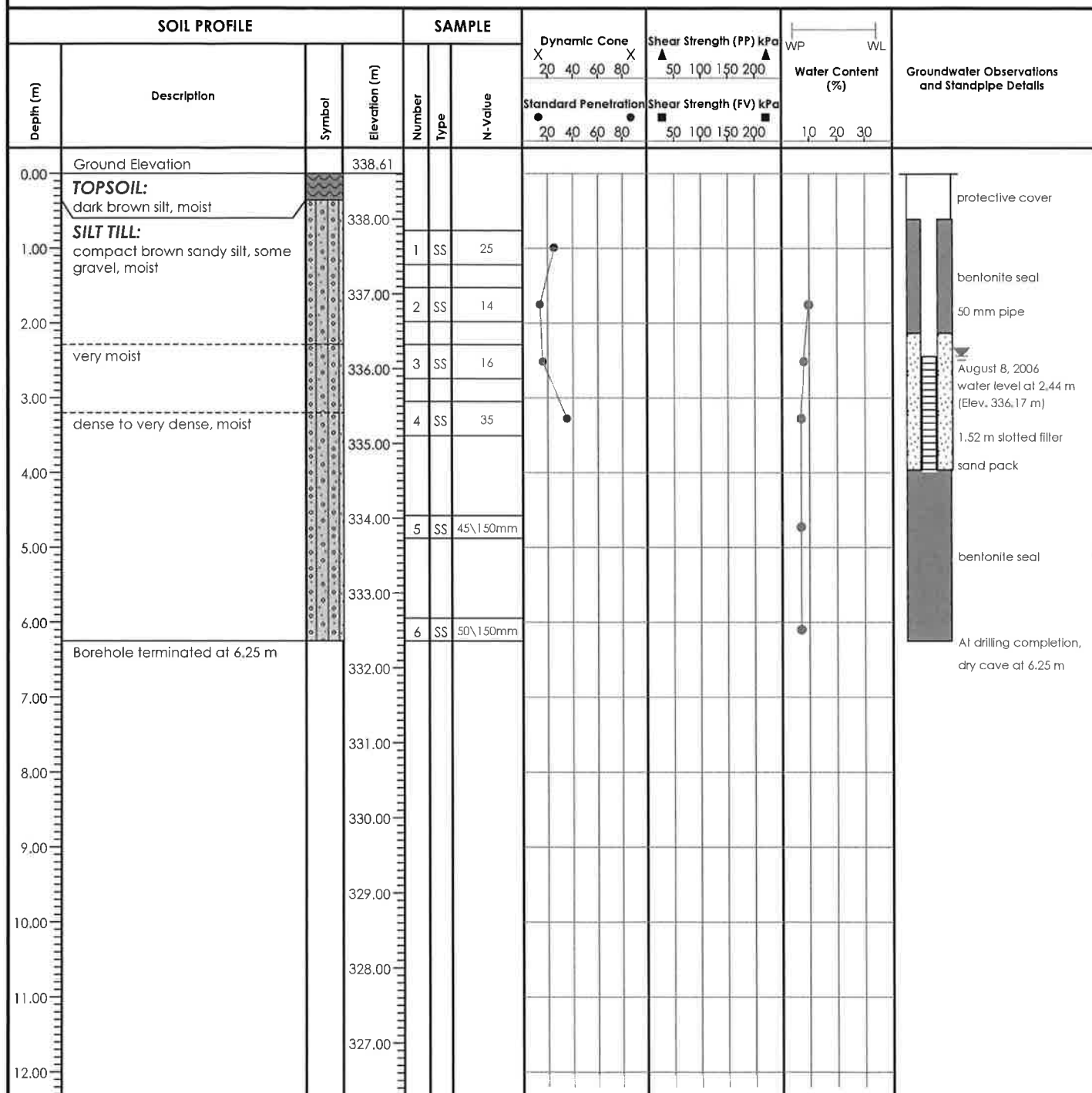
Ground Elevation: 338.61 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 2, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: Bulk sample taken from 1.83 to 3.05 m.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates INC.
(INCORPORATED 1986)

Borehole Number: 102

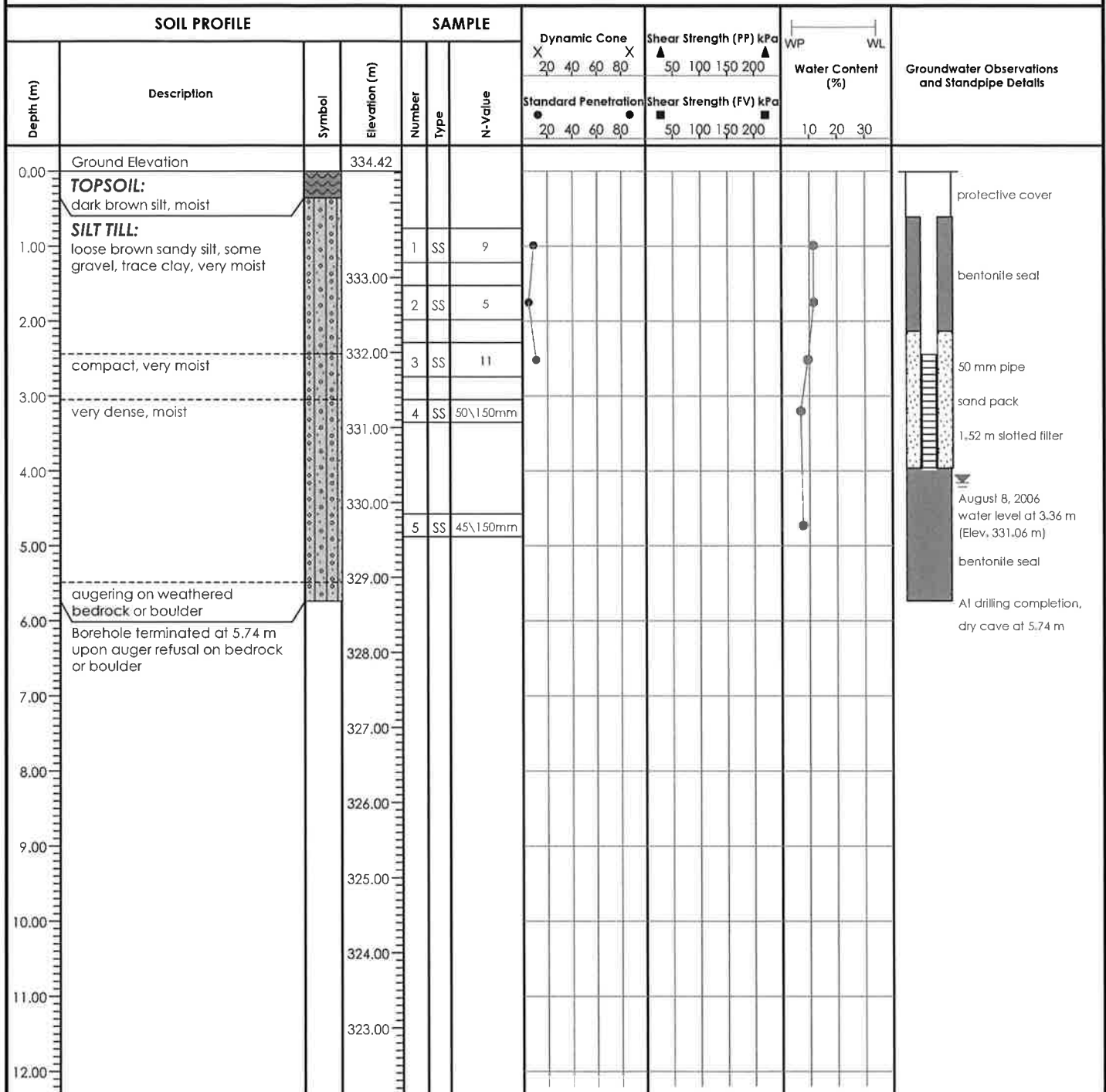
Ground Elevation: 334.42 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 2, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes:

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates Inc.
GEOTECHNICAL ENGINEERS

Borehole Number: 103

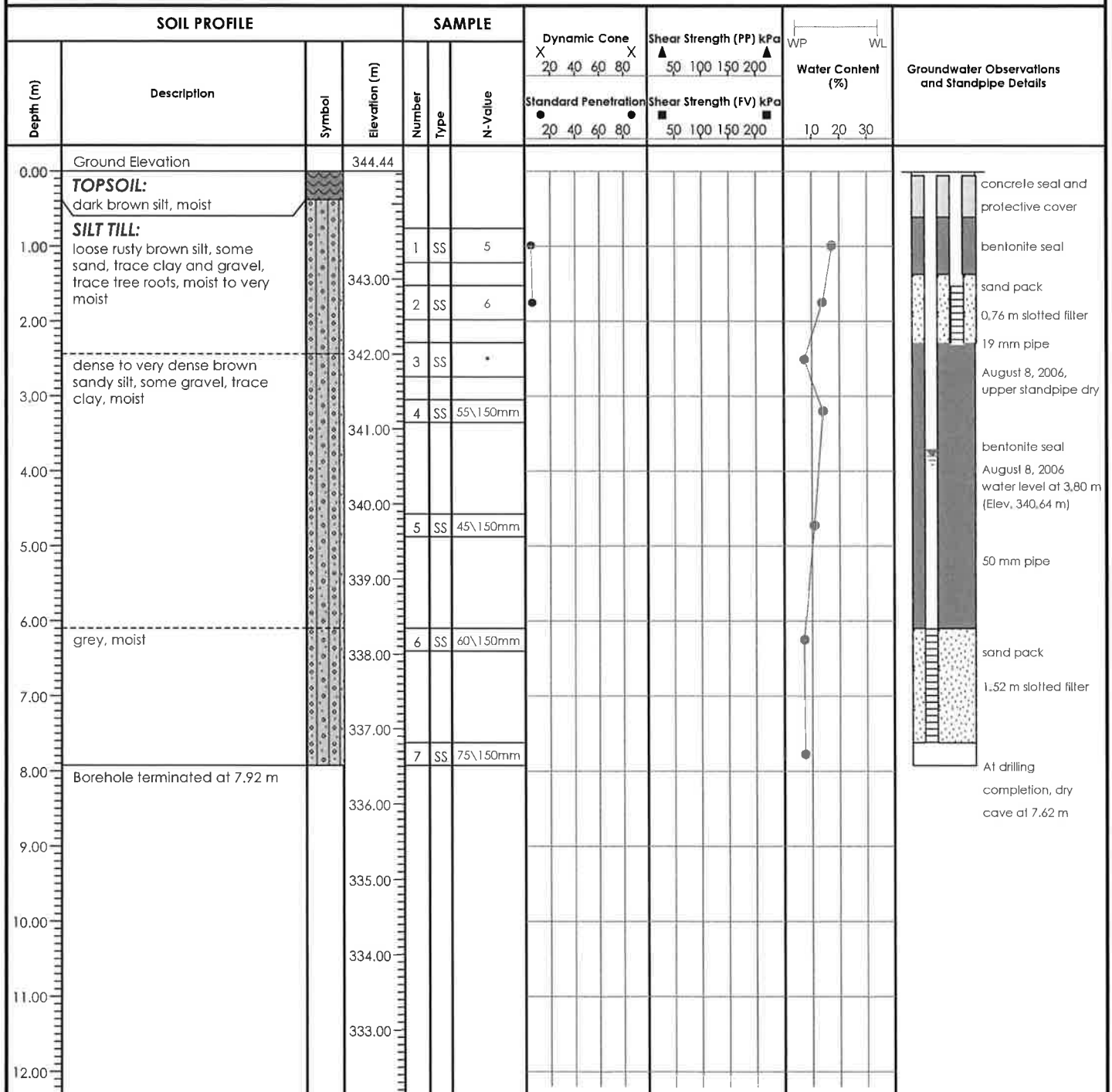
Ground Elevation: 344.44 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN

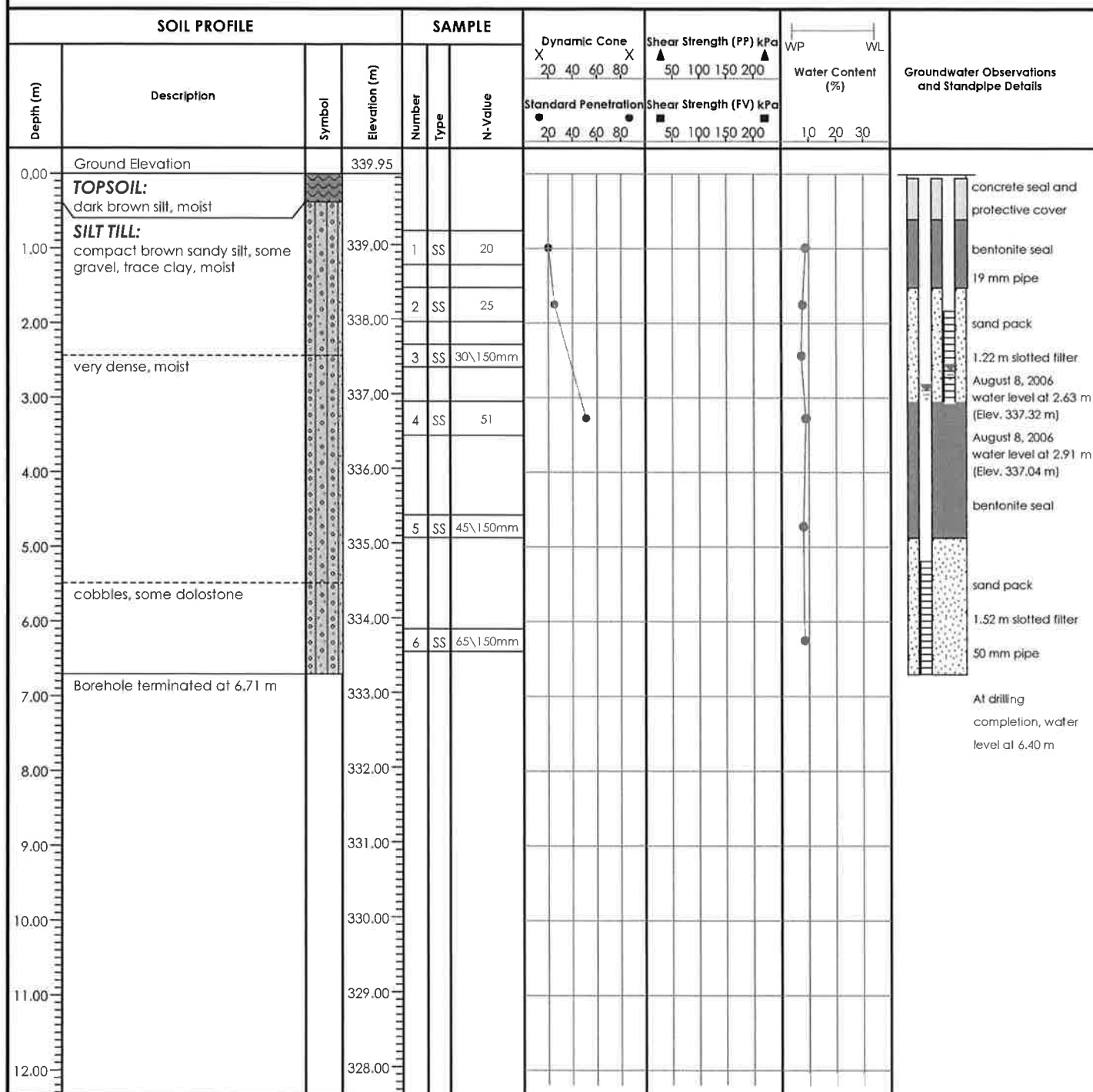
Drill Method: Solid Stem Auger

Notes: * Sampler driving on gravel.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes:

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates Ltd.
CONSULTING ENGINEERS

Borehole Number: 105

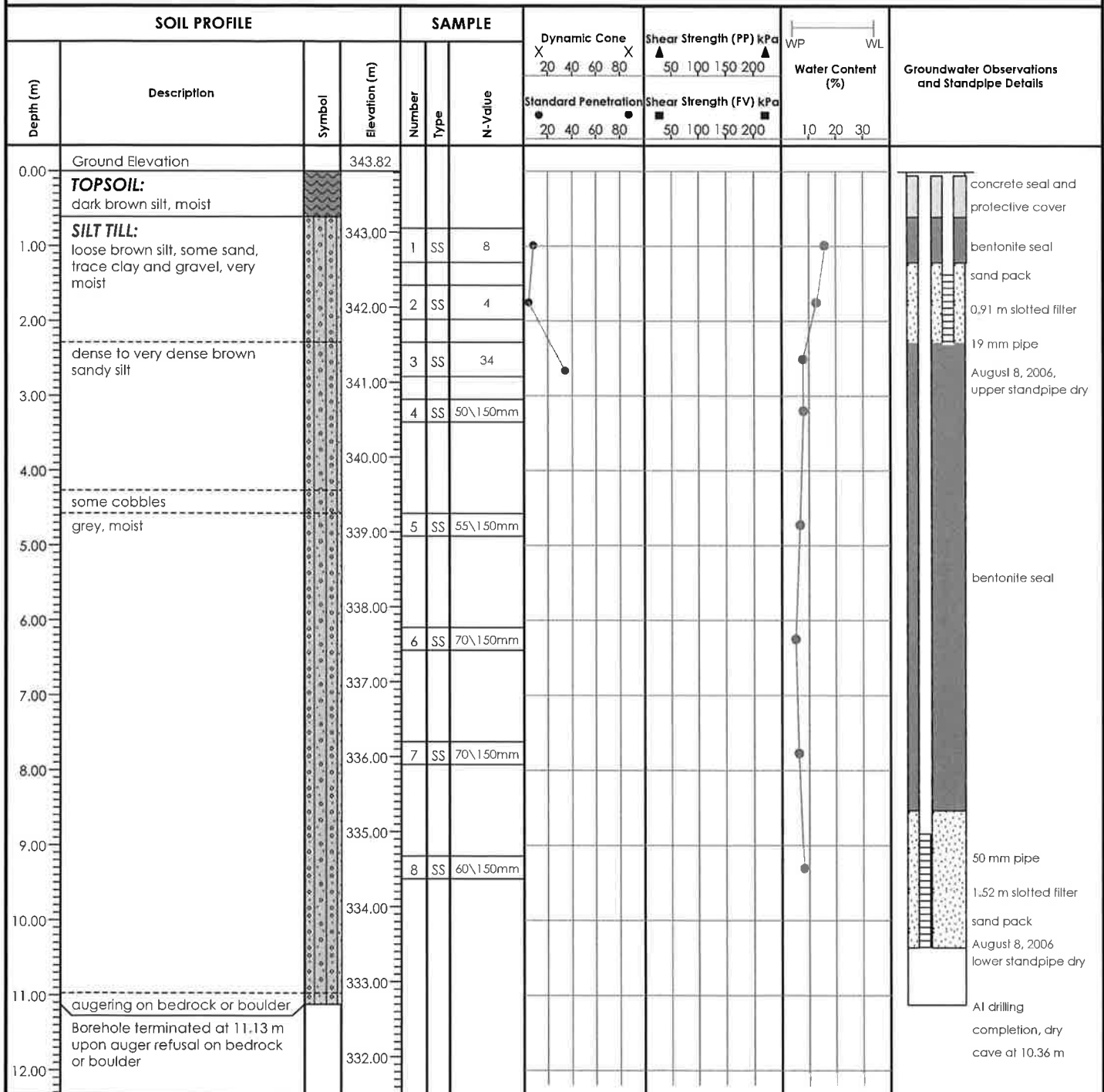
Ground Elevation: 343.82 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: Bulk sample taken from 1.22 to 2.13 m.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates
CONSULTING ENGINEERS

Borehole Number: 106

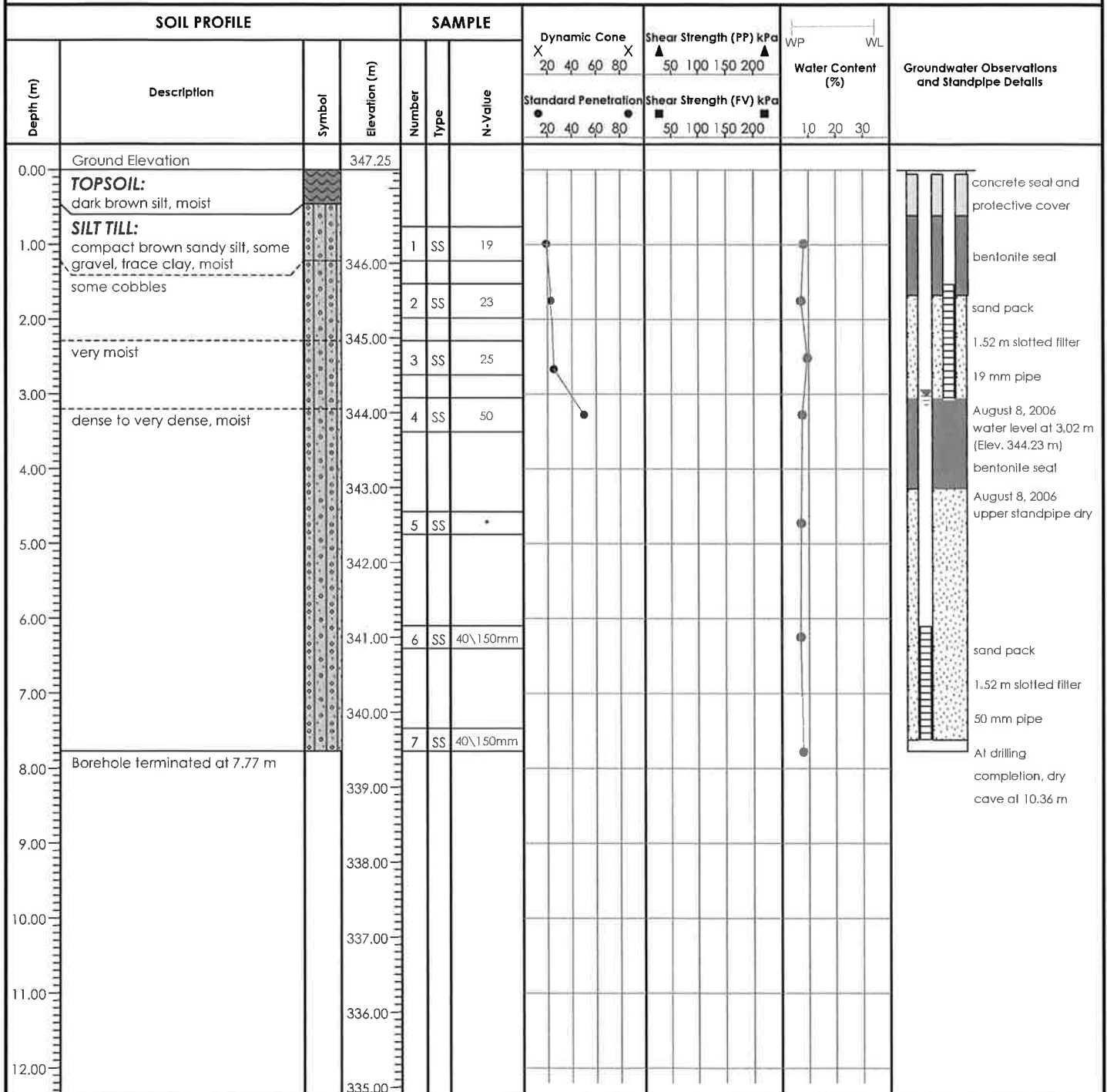
Ground Elevation: 347.25 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 2, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: Bulk sample taken from 1.52 to 3.05 m. *Sampler bouncing on gravel.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates
CONSULTING ENGINEERS

Borehole Number: 107

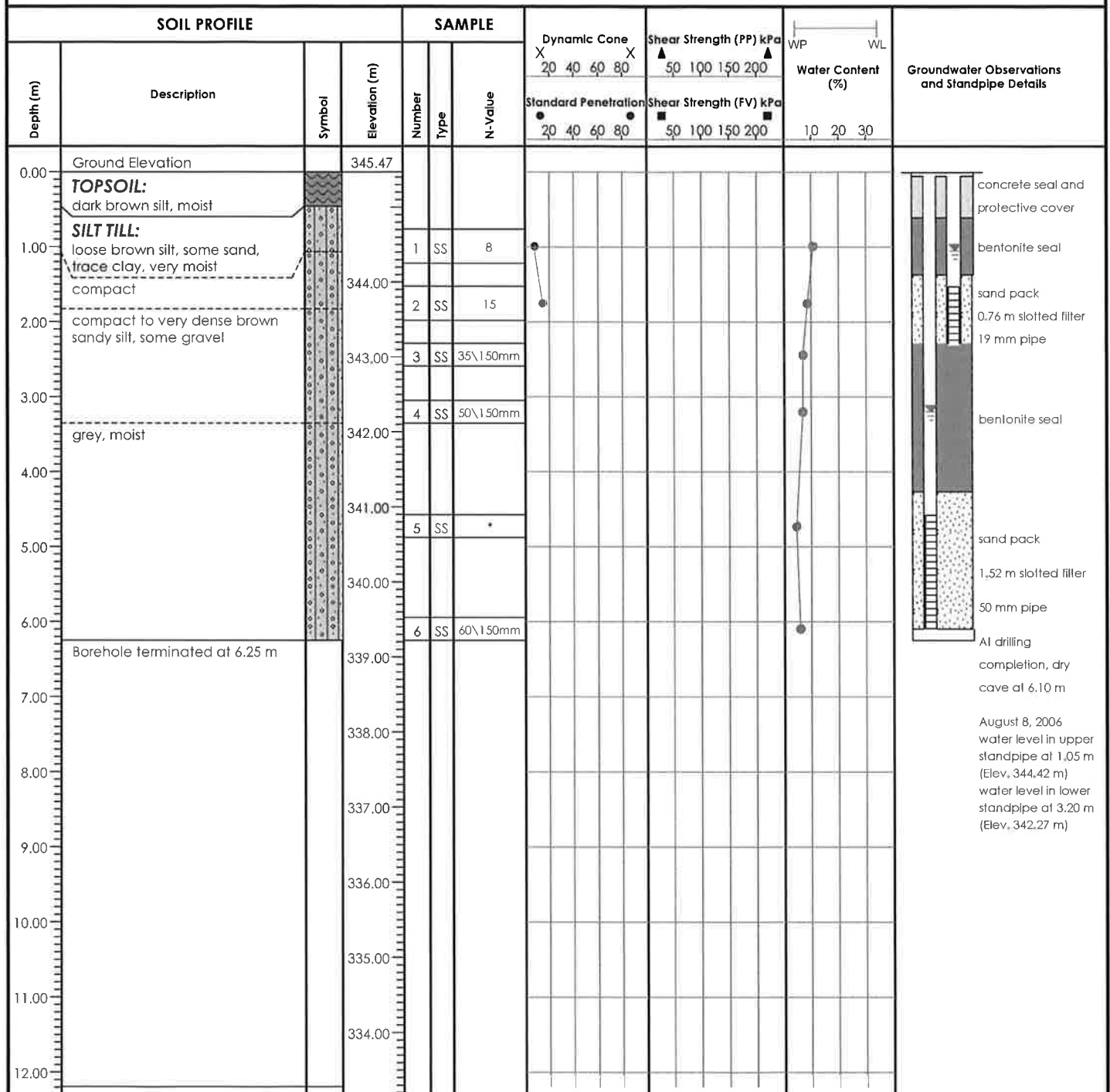
Ground Elevation: 345.47 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: * Sampler bouncing on gravel.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



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Borehole Number: 108

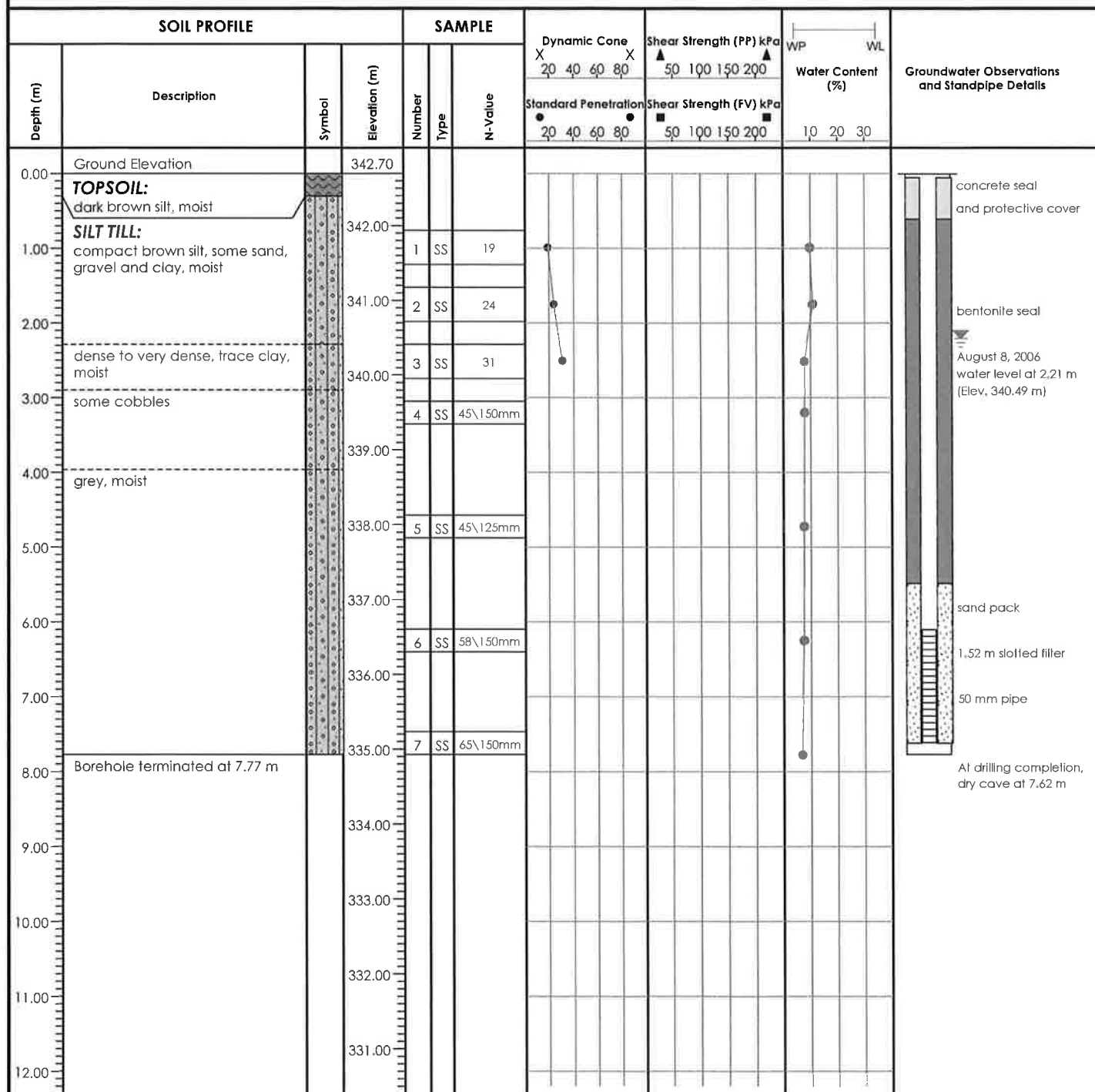
Ground Elevation: 342.70 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: Bulk sample taken from 1.52 to 3.05 m.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



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Borehole Number: 109

Ground Elevation: 326.19 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 1, 2006

SOIL PROFILE			SAMPLE			Dynamic Cone	Shear Strength (PP) kPa	Water Content (%)	Groundwater Observations and Standpipe Details
Depth (m)	Description	Symbol	Elevation (m)	Number	Type	N-Value	X 20 40 60 80	50 100 150 200	
							Standard Penetration	Shear Strength (FV) kPa	
							20 40 60 80	50 100 150 200	
0.00	Ground Elevation		326.19						<p>concrete seal and protective cover</p> <p>bentonite seal</p> <p>50 mm pipe</p> <p>sand pack</p> <p>1.52 m slotted filter</p> <p>August 8, 2006 water level at 4.44 m (Elev. 321.75 m)</p> <p>At drilling completion, wet cave at 3.96 m</p>
	TOPSOIL: dark brown silt, moist								
1.00	SAND AND GRAVEL: very dense brown sand and gravel, frequent cobbles and boulders, some silt, damp			1	SS	55			
			325.00						
				2	SS	30\, 150mm			
2.00			324.00						
				3	SS	*			
3.00			323.00						
				4	SS	*			
4.00	saturated		322.00						
				5	SS	*			
5.00	augering on possible bedrock		321.00						
	Borehole terminated at 5.64 m								
6.00			320.00						
7.00			319.00						
8.00			318.00						
9.00			317.00						
10.00			316.00						
11.00			315.00						
12.00			314.00						

Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: * Sampler bouncing on gravel.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Naylor
Engineering
Associates Inc.
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Borehole Number: 110

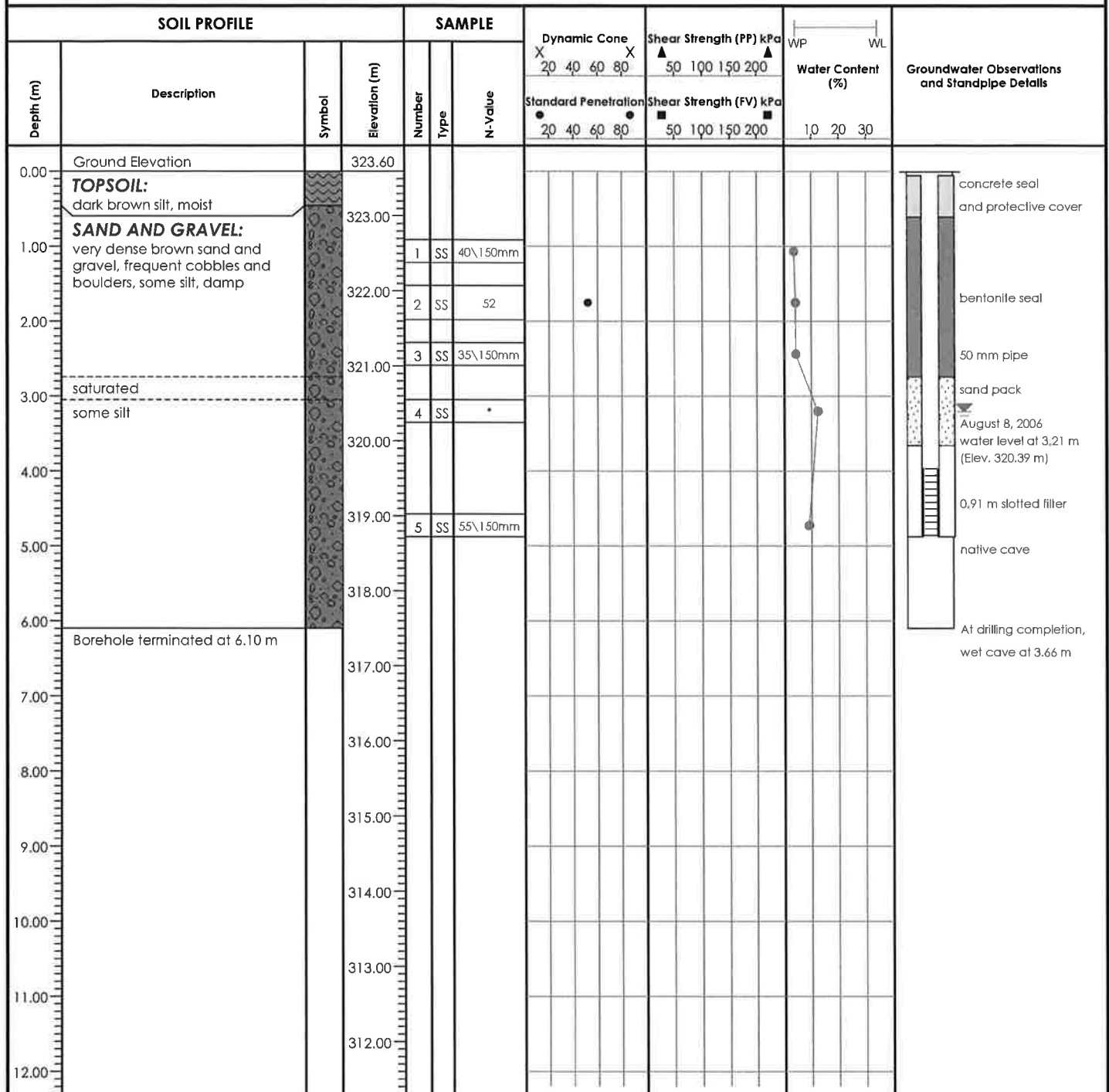
Ground Elevation: 323.60 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 1, 2006



Reviewed by: DN


Drill Method: Solid Stem Auger

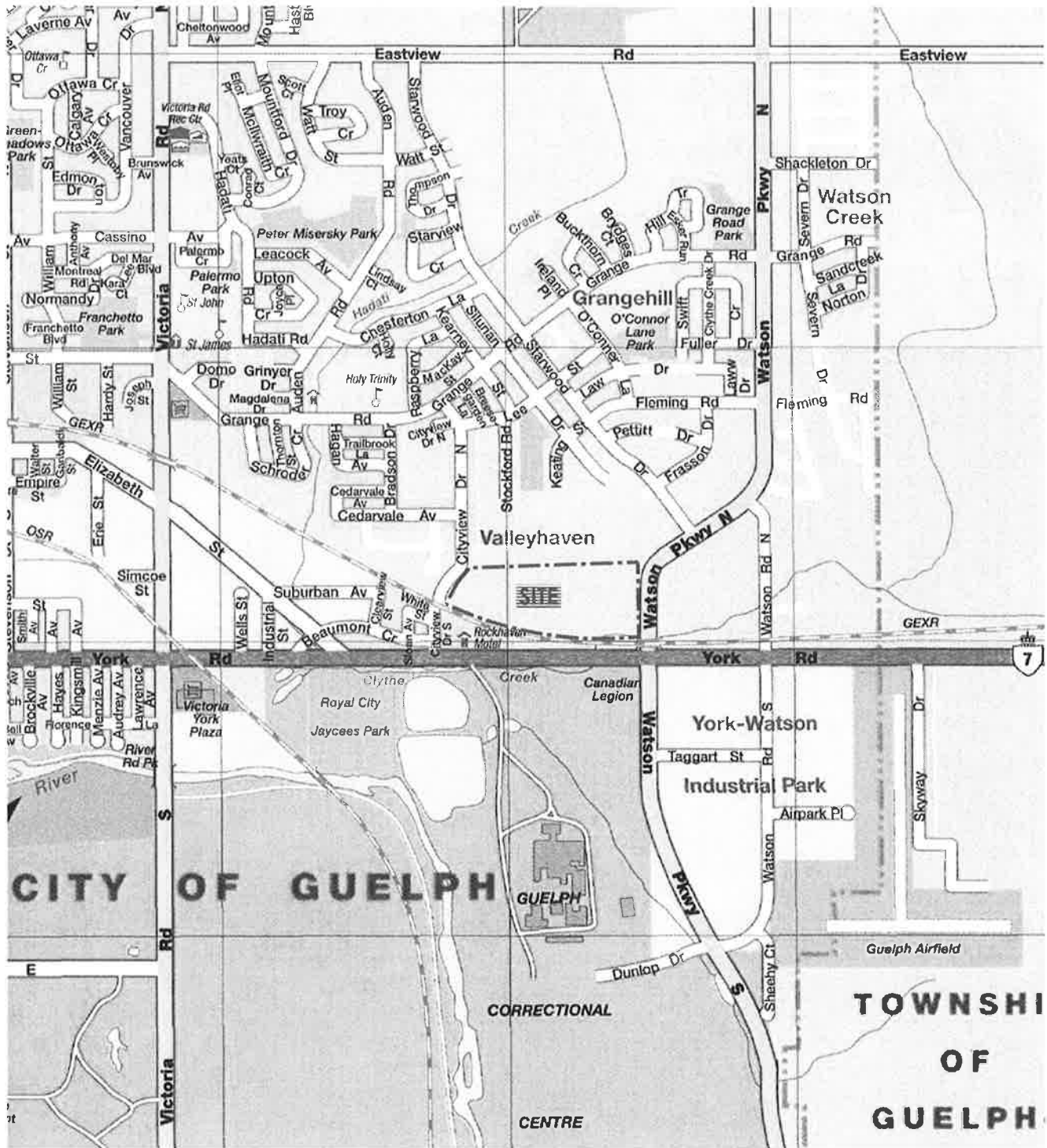
Notes: * Sampler bouncing on gravel.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)

 NORTH	No.	Revisions	Date
	0	Report Issued	Sept. 2006
	1		
	2		
	3		



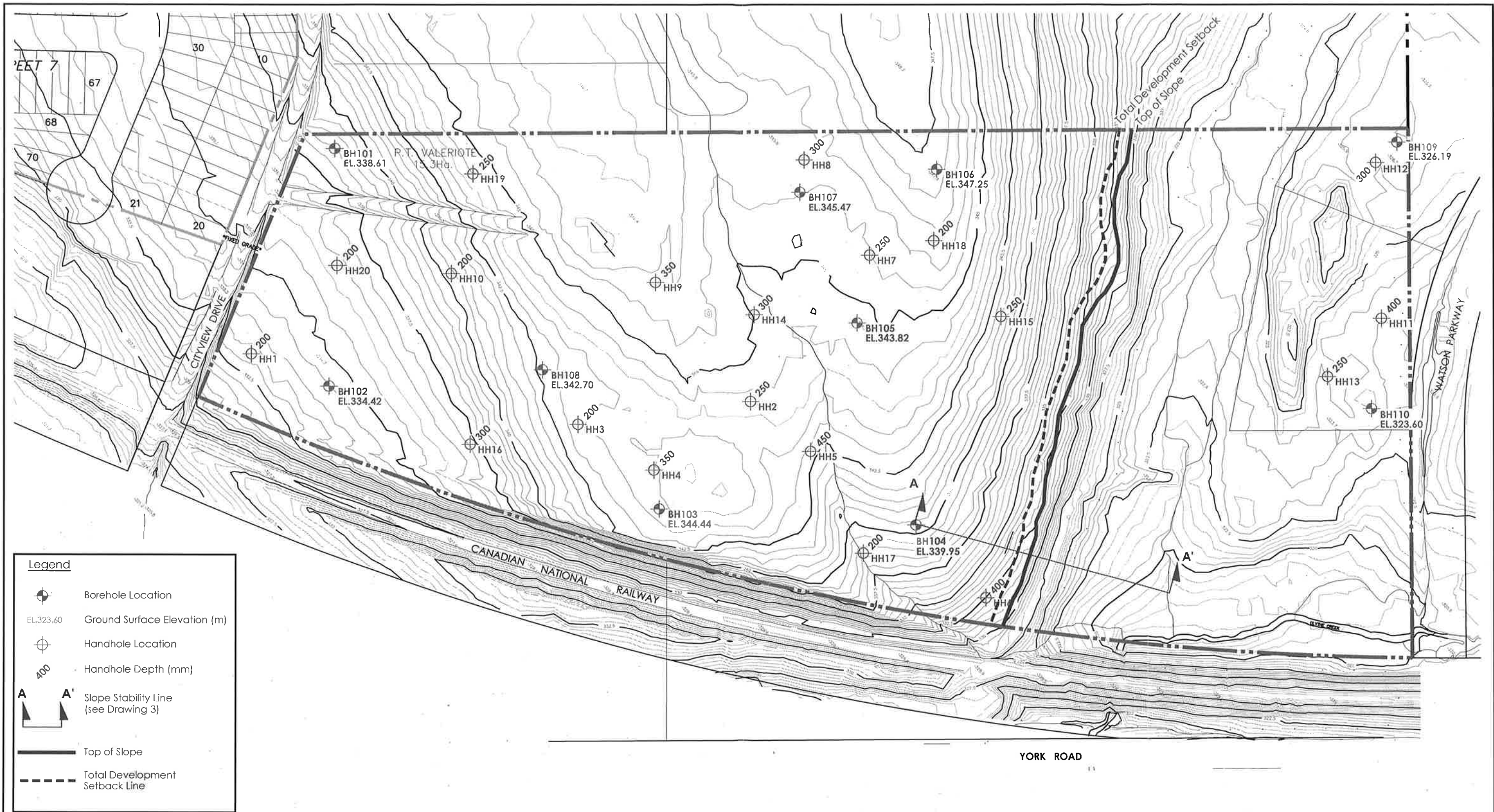
Drawing Reference: Base drawing from page G1 of MapArt's Kitchener-Waterloo Map Book (2006).

P.T. Valeriot Subdivision
Cityview Drive
Guelph, Ontario



LOCATION PLAN

Date	Scale	Job No.	Drawing No.
Sept. 2006	1:20000	0353G4	1



F:\0353\0353G4\0353G4_02.dwg
August 31, 2006 (SR)

Note:
Locations of site features in this drawing are approximate based on available information. Exact locations must be verified in the field.

No.	Revisions	Date
0	Report Issued	Sept. 2006
1	Report Revised	Jan. 2012
2		
3		



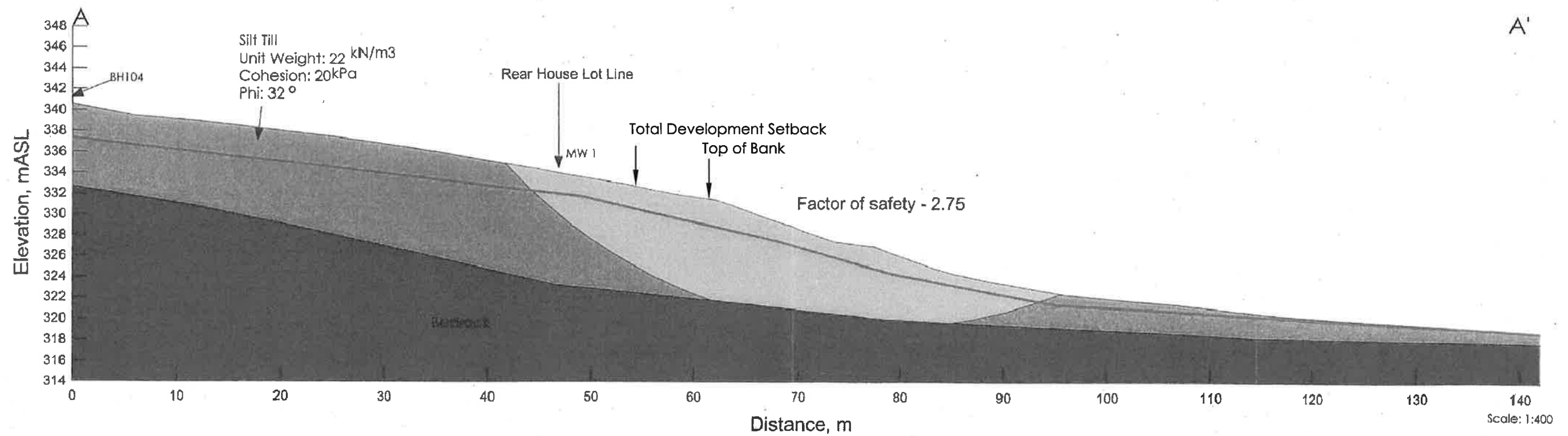
NORTH




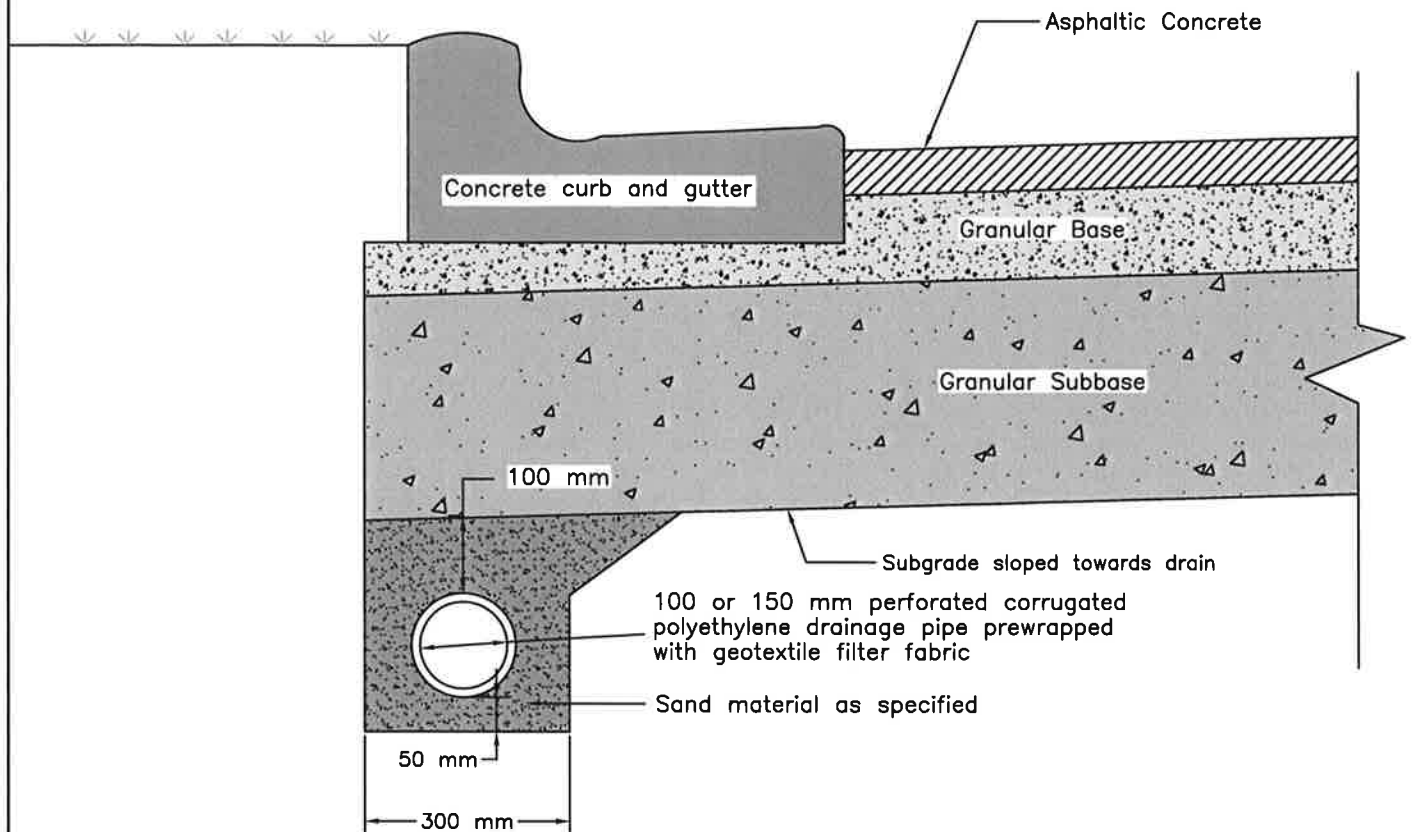
P.T. Valeriote Subdivision
Cityview Drive
Guelph, Ontario

SITE PLAN

Date	Scale	Job No.	Drawing No.
Sept. 2006	1:2000	0353G4	2



No.	Revisions	Date	 Naylor Engineering Associates Ltd. CONSULTING ENGINEERS	P.T. Valeriotte Subdivision Cityview Drive Guelph, Ontario	SLOPE STABILITY A - A'			
	Report Issued	Sept. 2006			Date	Scale	Job No.	Drawing No.
0					Sept. 2006	1:400	0353G4	3
1								
2								
3								



GENERAL REQUIREMENTS FOR PAVEMENT SUBDRAINS

1. Perforated corrugated polyethylene drainage pipe shall meet the requirements of OPSS 1840.
2. Pipe filter fabric conforming to OPSS 1860 for geotextile Class 1 with a filtration opening size of 150 to 450 microns shall be supplied on all sections of perforated pipe.
3. The open upstream ends of pipes should be capped.
4. Subdrain pipes to be set on at least 1% grade draining to a positive frost-free outlet. If the subdrains are outletted to a ditch then the last 1.5 m of the outlet pipe should consist of a corrugated galvanized steel pipe equipped with a rodent gate.
5. Bedding and backfill material shall be concrete sand meeting the gradation requirements of OPSS 1002 (Fine Aggregate for Concrete).

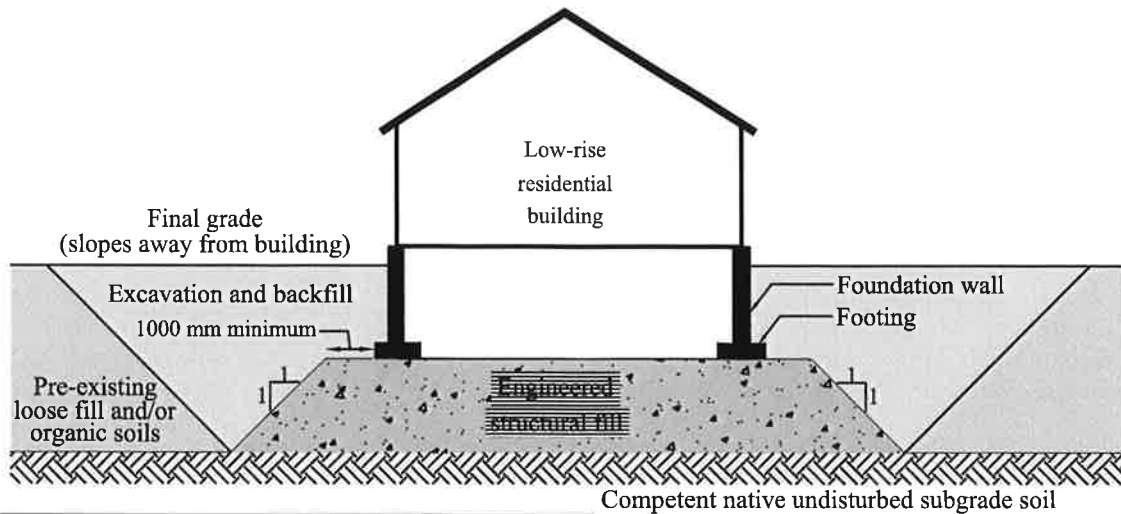


Naylor
Engineering
Associates
CONSULTING ENGINEERS

TYPICAL PAVEMENT SUBDRAIN DETAIL

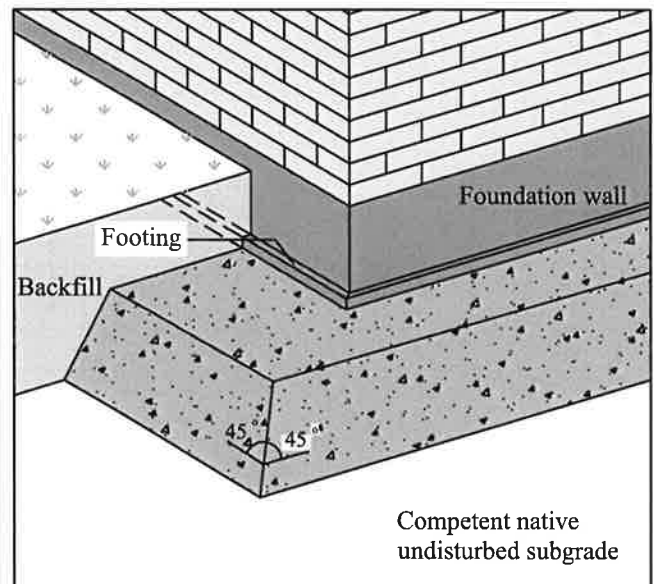
Date	Scale	Job No.	Drawing No.
Sept. 2006	NTS	0353G4	4

ENGINEERED STRUCTURAL FILL PAD



GENERAL REQUIREMENTS FOR ENGINEERED STRUCTURAL FILL

1. The area must be excavated of all pre-existing loose fill, topsoil, and/or organic soil until competent native undisturbed soil is reached.
2. The excavation should allow for the structural fill to extend 1000 mm beyond the outside edge of the building footings and down to the approved subgrade soil at a slope of 1 horizontal to 1 vertical (45°).
3. The subgrade below the engineered fill should be inspected and approved by a geotechnical engineer prior to fill construction. Fill placement and compaction operations to be carried out under full-time geotechnical supervision.
4. The structural fill should comprise sand and gravel aggregate placed in 300 mm thick lifts and compacted to at least 98% Standard Proctor Maximum Dry Density (SPMDD). The exterior backfill should consist of approved inorganic soil also placed in 300 mm thick lifts and compacted to minimum 95% SPMDD.
5. All excavations must be carried out in conformance with the current Ontario Occupational Health and Safety Act and Regulations 213/91 for construction projects.
6. Exterior footings must be provided with minimum 1.2 m of soil cover for frost protection.



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TYPICAL STRUCTURAL FILL PAD DETAIL

Date	Scale	Job No.	Drawing No.
Sept. 2006	NTS	0353G4	5

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “B”

**Slope Stability Assessment
Englobe Corp.
(February 2016)**

February 17, 2016

Cityview Ridge Developments Inc.
c/o Ms. Angela Kroetsch, P.Eng.
GM BluePlan Engineering
330 Trillium Drive, Unit D
Kitchener, Ontario N2E 3J2

Subject: Cityview Ridge Subdivision
Slope Stability Assessment – Lots 62 to 78
Guelph, Ontario
Our ref.: 160-P-0009857-0-01-100-GE-L-0001-01

Dear Ms. Kroetsch:

Englobe Corp. (Englobe) is pleased to provide this letter report for the slope stability analysis recently completed for the proposed Cityview Ridge Subdivision at the location shown on the appended Location Plan, Drawing 1. The work for this investigation was authorized by Mr. Carson Reid of Cityview Ridge Developments Inc. on February 2, 2016.

The area being investigated comprises Lots 62 to 78 along the east side of the proposed development. It is understood that the proposed development will include the placement of fill and construction of retaining walls and a walking trail along the rear of the above mentioned lots.

The purpose of this slope stability analysis is to assess the impact of the proposed structures on the stability of the existing slope at the site.

General Information

The subject site is located on Cityview Drive, Guelph Ontario and the area being investigated is located at the east side of the site, near the top of a slope. A Grand River Conservation Authority (GRCA) regulated wetland is located at the base of the subject slope.

Naylor Engineering Associates Ltd. (NEA) previously completed a geotechnical investigation and slope stability assessment at the subject site including the drilling of three boreholes near the top of the slope (Boreholes BH104 to BH106) to depths of 6.7 to 11.1 m. The findings of this investigation illustrated that the existing slope is comprised of native non-cohesive silt till. Groundwater was found to occur in saturated seams at variable depths within the silt till deposit. A slope stability analysis was carried out along the steepest portion of the slope located in the southeast portion of the site. The results of the slope stability analysis found that the slope had a factor of safety of greater than 1.5. We refer the reader to the geotechnical investigation for further information (NEA, Geotechnical Investigation, P.T. Valeriote Subdivision, Cityview Drive, Guelph, Ontario. 0353G4.R01_Rev, February 2012). The relevant borehole logs of the previous investigation and site plan (NEA – Drawing 2 – Site Plan) illustrating the borehole locations have been appended to this letter.

It is understood that proposed structures include three retaining walls, swales, houses, a walking trail, and fill placement will occur with the proposed site development, near the top of the slope. The three proposed retaining walls will traverse along the east side of Lots 72 to 78, Lot 67, and along the east side of the walking trail behind Lots 77 and 78 (Gamsby and Mannerow Engineers, Carson Reid Homes Cityview Ridge, Project Number 105-172, Preliminary Site Grading and Drainage Plan [Drawing 2] and Trail Plan and Sections [Drawing 8], Revised March 30, 2015). It is further understood that grades at the rear of Lots 75 to 78 are to be raised by up to 3.5 m with final grades near Elevation 340.5 to 341.0 m. The fill will be partially retained by the retaining walls, beyond which it is to be sloped to the east at an inclination of 3 horizontal to 1 vertical, then blends into the existing grades. The thickness of the fill decreases toward the north, and along Lots 68 to 72, the proposed elevation at the rear of the lots is close to or below the existing grades.

Slope Stability Assessment

Cross-Section B-B' was created based on topographic data provided by Gamsby and Mannerow Engineers and the location of the section is shown on our Drawing 2 – Site Plan, and is illustrated in Drawing 3 – Cross Section B-B'. The cross section was created to represent a worst case scenario, where the slope was the steepest and the proposed additional loading was greatest. Cross-Sections X-X and O-O from the provided topographic plan were also used to assess the slope stability.

The information from the boreholes and cross-sections were used for computer analyses of the slope stability using the Slope/W Program (Morgenstern-Price Method). The soil parameters used in this analysis have been estimated based on the information from the existing boreholes, laboratory testing, as well as local experience and available literature values and are provided in Table 1.

Table 1 Soil Parameters

SOIL MATERIAL	UNIT WEIGHT (kN/m ³)	ANGLE OF INTERNAL FRICTION (°)	COHESION (kPa)
Silt Till	22	32	0

The following assumptions have been made in order to assess the possible impact of the proposed structures on the slope stability at the subject site:

- ▶ Soil conditions at the site comprise native silt till deposits. Suspected bedrock was encountered but was not proven by coring during the NEA investigation. As such the soil was assumed to be continuous to Elevation 300 m.
- ▶ Foundations will be designed as per the previous geotechnical report (NEA, 0353G4.R01_Rev).
- ▶ The proposed retaining wall will be adequately designed for sliding and overturning.
- ▶ Grades of the site will be raised (where applicable) with well compacted subgrade or structural fill. The fill is placed in 300 mm thick lifts and compacted to 95% SPMDD (subgrade fill) or 98% SPMDD (structural fill for residential buildings and below retaining walls) at a minimum.
- ▶ The proposed fill and retaining wall were assumed to have a unit weight of 24 kN/m³.
- ▶ The assumed groundwater depth is 2.6 m at the top of the slope and at ground surface at the GRCA 100-year floodplain.

A slope stability analysis was carried out on the three cross sections for a number of potential failure types. The various failures analyzed included shallow slumping type failure of the slope surface, medium depth rotational failures, and deep rotational failures.

Following the GRCA policy, the design range for the factor of safety must be 1.30 to 1.50 or greater.

The results of the slope stability assessment completed for the slope sections and considering the proposed retaining walls, houses and fill indicate factors of safety in excess of 1.5 for all three of the analyzed cross sections, at which medium depth to deep rotational failures would cause the loss of the structure.

In conclusion, the findings of our slope stability assessment do not show an aggravation of existing slope instabilities or future slope instabilities due to the proposed structures. As well, there is an adequate factor of safety against rotational slope failures that could adversely affect the stability of the proposed structures.

Retaining Wall Design and Construction

The design of the retaining walls should be done by a licensed structural engineer. The retaining wall must be designed to resist the lateral earth pressures. For calculating the lateral earth pressure for walls restrained at the bottom only, an active earth pressure coefficient (K_a) of 0.36 and soil unit weight of 20 kN/m³ may be used. An appropriate safety factor should be employed (Section 24.3.3.3 Canadian Foundation Engineering Manual).

We recommend that the backfill for the wall comprise clean free-draining granular material such as OPSS Granular 'B'. The soils encountered on-site are not considered suitable for reuse as retaining wall backfill. The backfill should be placed in thin lifts and compacted to 95% standard Proctor maximum dry density (SPMDD). Over-compaction should be avoided since this may cause excessive lateral earth pressures against the retaining walls. It is recommended that backfilling operations be inspected in order to approve the backfill materials and ensure the proper degree of compaction is being achieved.

Subdrains should be installed behind the retaining wall foundations. The subdrains should comprise minimum 150 mm diameter perforated pipes with filter sock and sand bedding (OPSS Concrete Sand). The subdrains must drain by gravity to a frost free outlet.

The slope behind the retaining wall should be graded with an inclination of 3.0 horizontal to 1.0 vertical or less and the soil considered as surcharge in the retaining wall design. The finished slopes should be topsoiled and vegetated as soon as possible after construction to minimize surface erosion. The minimum topsoil thickness should be 100 mm. Some routine maintenance of the slope surfaces may be required to address minor long-term weathering and erosion.

To reduce surface runoff over the retaining wall and down the slope it is recommended that surface runoff be diverted behind the retaining wall and lead to a positive outlet.

Subject : Cityview Ridge Subdivision, Slope Stability Assessment – Lots 62 to 78
Guelph, Ontario
160-P-0009857-0-01-100-GE-L-0001-01

February 17, 2016

Englobe should be contacted if the design of the proposed structures changes (i.e. size, location, or proposed footing depths) in order to provide updated recommendations on slope stability.

We trust that this information is complete and suitable for your present requirements. If you have any questions or require further information, please do not hesitate to contact our office.

Yours very truly,



Dan Gonser EIT
Geotechnical Department



J.B. England, P.Eng.
Senior Geotechnical Engineer

alc

Encl. Drawing 1 – Site Plan
Encl. Drawing 2 – Site Plan
Encl. Drawing 3 – Cross-Section A-A'
Encl. NEA – Drawing 2 – Site Plan
Encl. NEA – Boreholes BH104 to BH106

10 cm

5

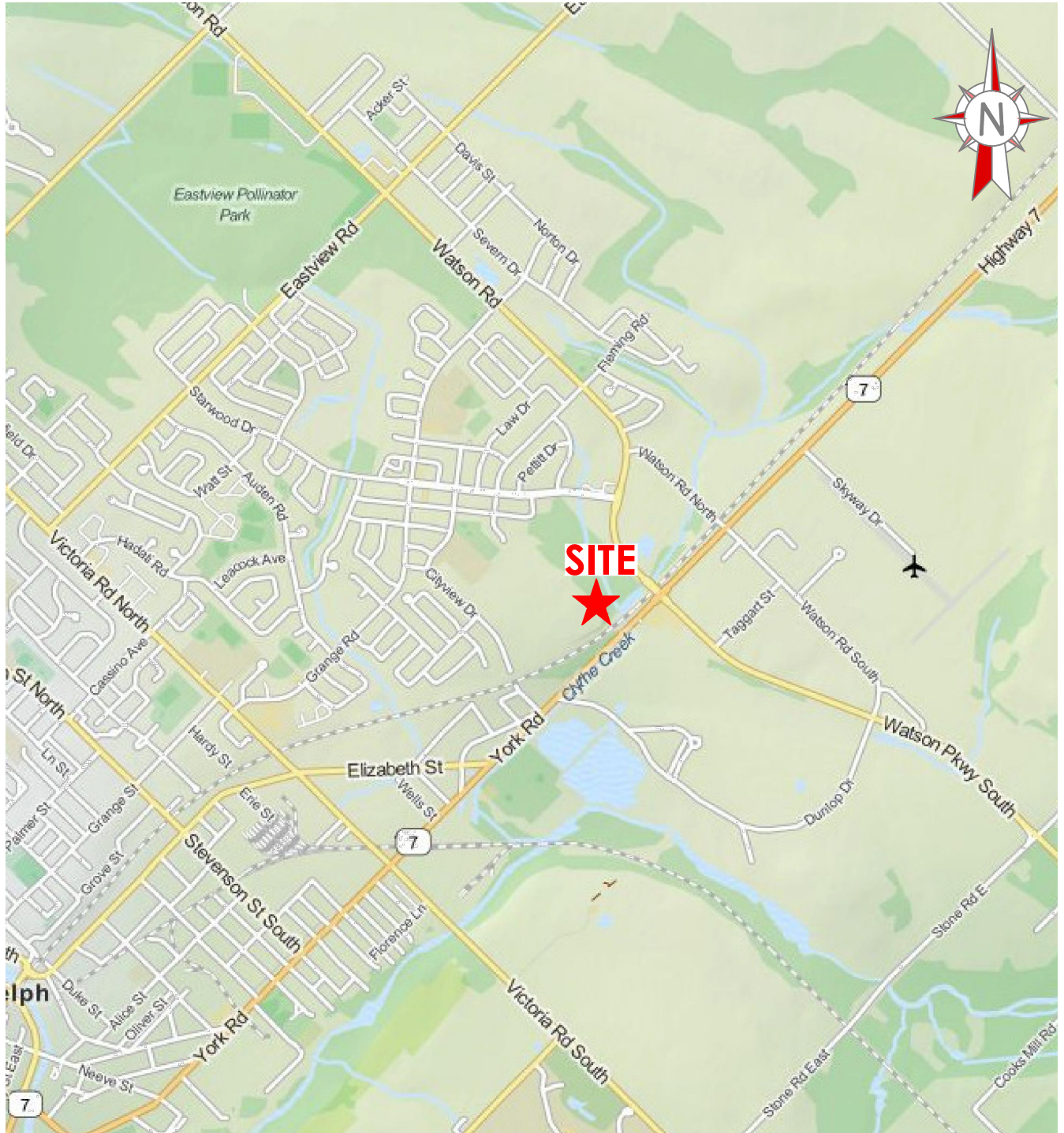
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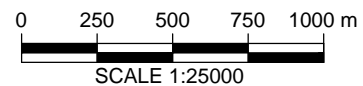
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0



NOTES :

1-REFERENCES : © OpenStreetMap contributors (2016).



Project

Cityview Ridge Subdivision Slope Stability Assessment

Guelph, Ontario

Title

LOCATION PLAN



Englobe Corp.

353, Bridge Street East
Kitchener (Ontario) N2K 2Y5
Telephone : 519.741.1313
Fax : 519.741.5422

Prepared **K. Ashe**

Drawn **K. Ashe**

Checked **D. Gonser**

Discipline **GEOTECHNICAL**

Scale **1 : 25000**

Date **2015-02-04**

Project manager

D. Gonser

Sequence no.

01 of 03

M. dept.

160

Project

P-0009857-0-01-100

Disc.

GE

Dwg no.

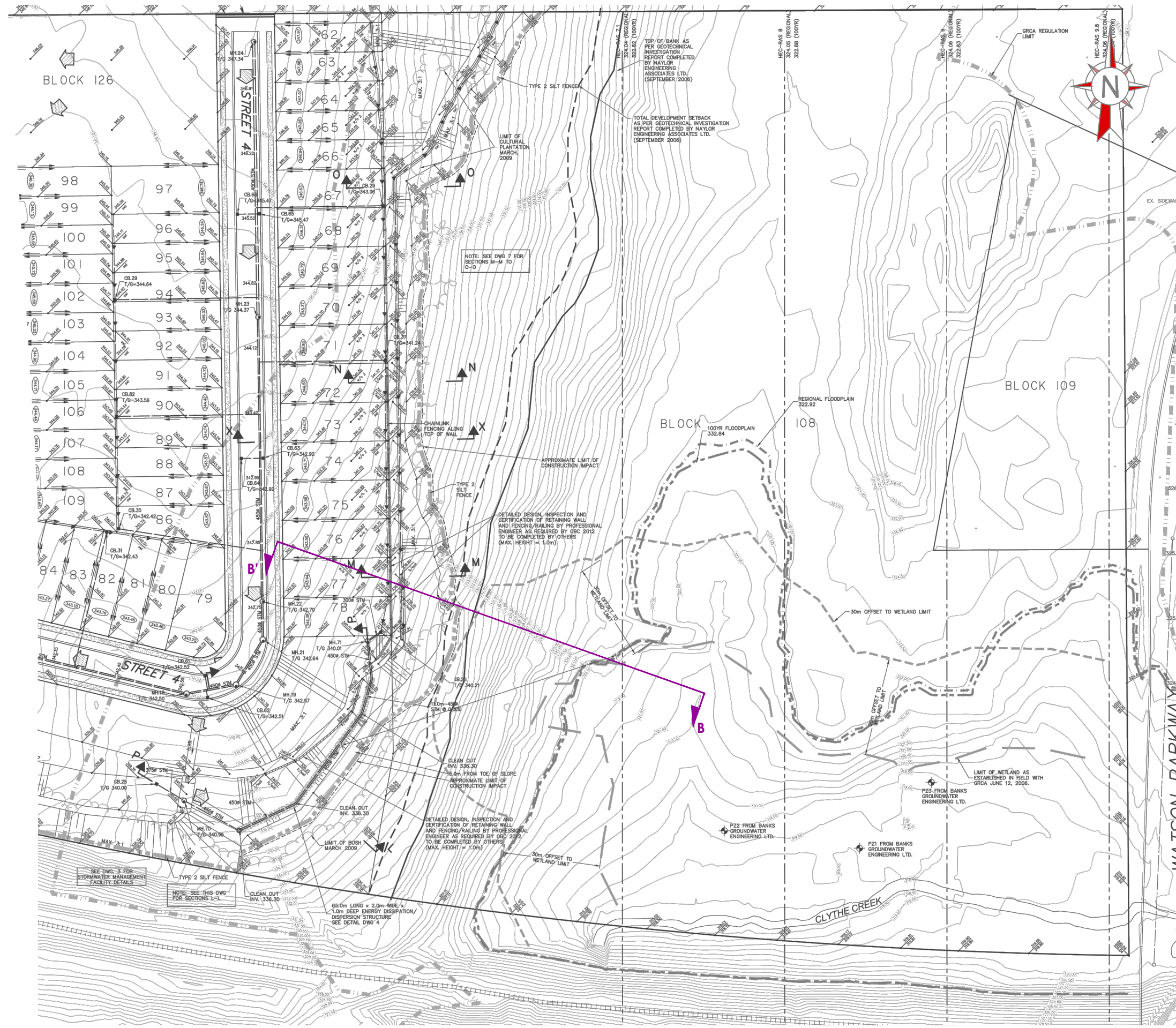
001

Rev.

00

G:\160\160009857\24_CAD\160-0009857-0-01-100_DWG001.DWG

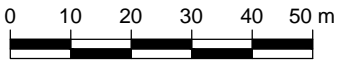
10 cm
5
4
3
2
1
0



LEGEND :



CROSS SECTION



SCALE 1:1250

NOTES :

1-REFERENCES : GAMSBY AND MANNEROW ENGINEERS, Carson Reid Homes Cityview Ridge, Preliminary Grading and Drainage Plan, Project Number 105-172, Drawing Number 2, Revised March 30, 2015.

2-Drawing scale may be distorted due to file conversion and/or copying. Measurements taken from the drawing must be verified in the field.

Project

Cityview Ridge Subdivision Slope Stability Assessment

Guelph, Ontario

Title

SITE PLAN



Englobe Corp.

353, Bridge Street East
Kitchener (Ontario) N2K 2Y5
Telephone : 519.741.1313
Fax : 519.741.3422

Prepared **K. Ashe**

Drawn **K. Ashe**

Checked **D. Gonser**

Project manager

D. Gonser

Discipline **GEOTECHNICAL**

Scale **1:1250**

Date **2016-02-04**

Sequence no.

02 of 03

M. dept.

160

Project

P-0009857-0-01-100

Disc.

GE

Dwg no.

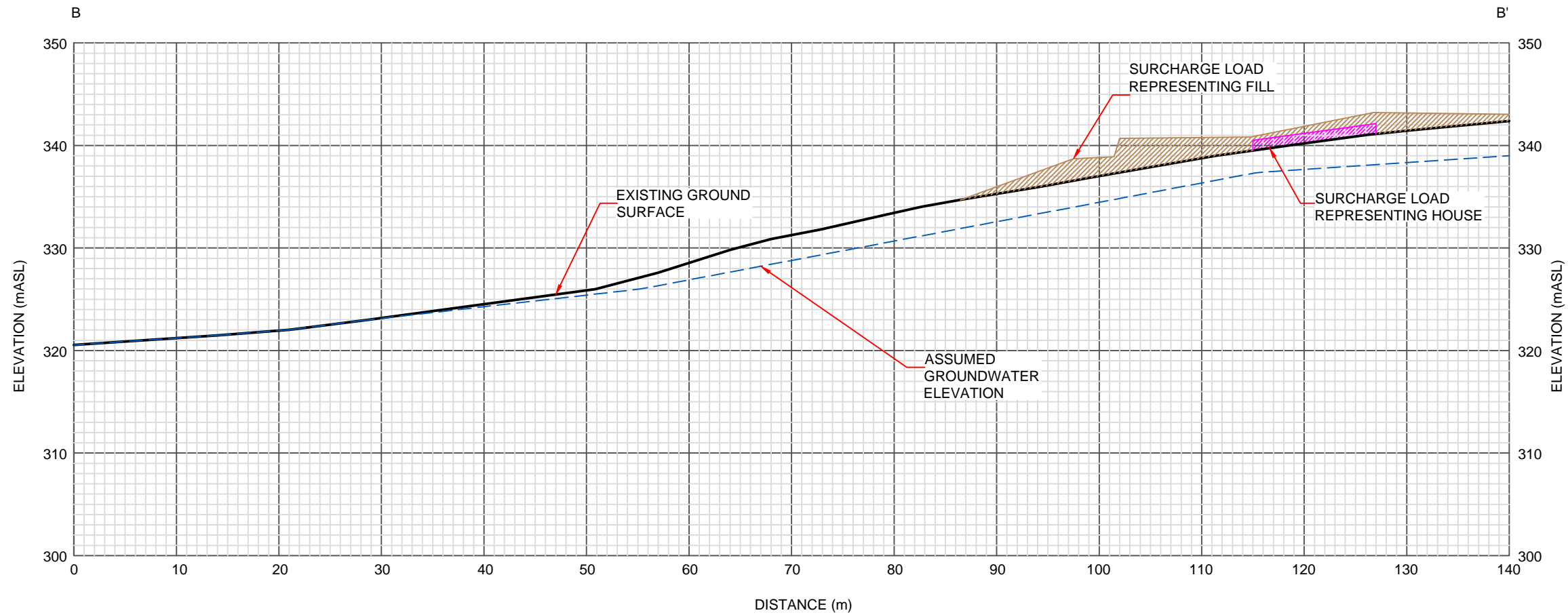
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Rev.

00

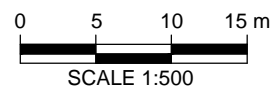
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10 cm
5
4
3
2
1
0



NOTES :

1-Drawing scale may be distorted due to file conversion and/or copying.
Measurements taken from the drawing must be verified in the field.



Project

**Cityview Ridge Subdivision
Slope Stability Assessment**

Guelph, Ontario

Title

CROSS SECTION B - B'



Englobe Corp.

353, Bridge Street East
Kitchener (Ontario) N2K 2Y5
Telephone : 519.741.1313
Fax : 519.741.5422

Prepared **K. Ashe**

Drawn **K. Ashe**

Checked **D. Gonser**

Discipline **GEOTECHNICAL**

Scale **1 : 500**

Date **2016-02-04**

Project manager

D. Gonser

Sequence no.

03 of 03

M. dept.

160

Project

P-0009857-0-01-100

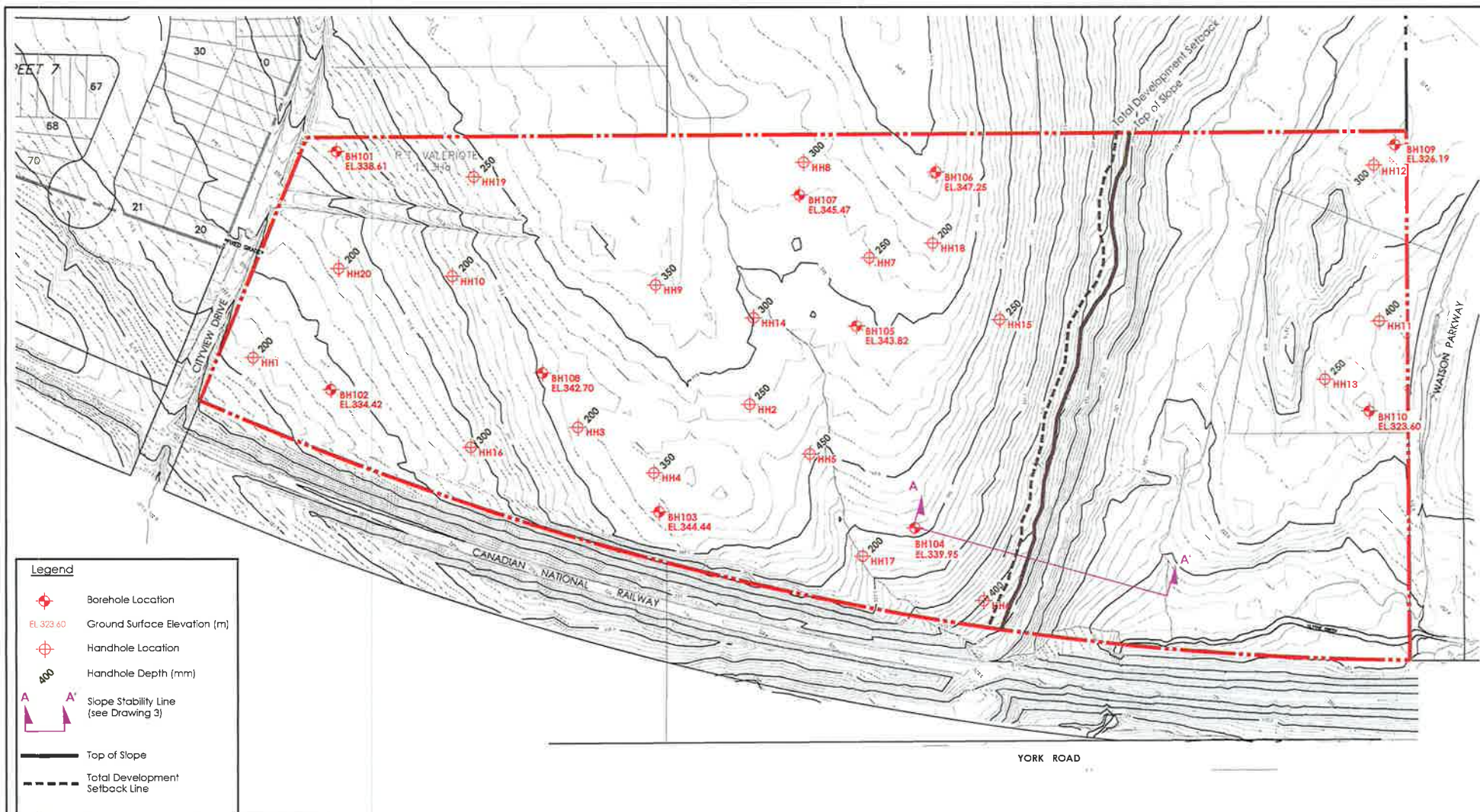
Disc.

GE

Dwg no.

003 00

Rev.



Drawing Reference: Base drawing provided by City of Guelph.

Note:
Locations of site features in this drawing are approximate based on available information. Exact locations must be verified in the field.

No.	Revisions	Date
0	Report Issued	Sept. 2006
1	Report Revised	Jan. 2012
2		
3		



NORTH



P.T. Valerlote Subdivision
Cityview Drive
Guelph, Ontario

SITE PLAN

Date	Scale	Job No.	Drawing No.
Sept. 2006	1:2000	0353G4	2



**Naylor
Engineering
Associates Ltd.**
CONSULTING ENGINEERS

Borehole Number: 104

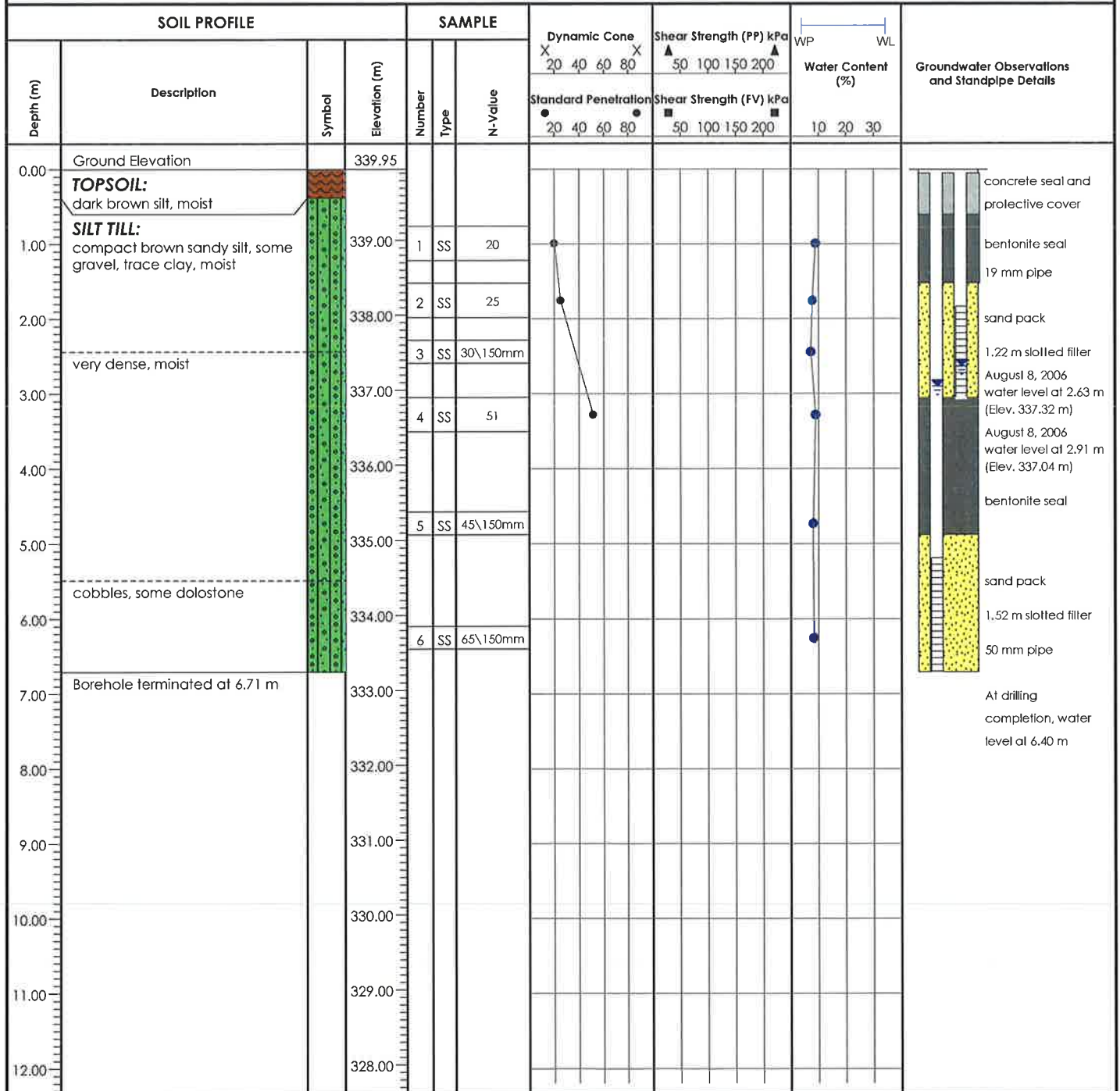
Ground Elevation: 339.95 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN
Drill Method: Solid Stem Auger
Notes:

Field Tech.: RM
Sheet: 1 of 1
Drafted by: DC(01a)

Borehole Number: 105

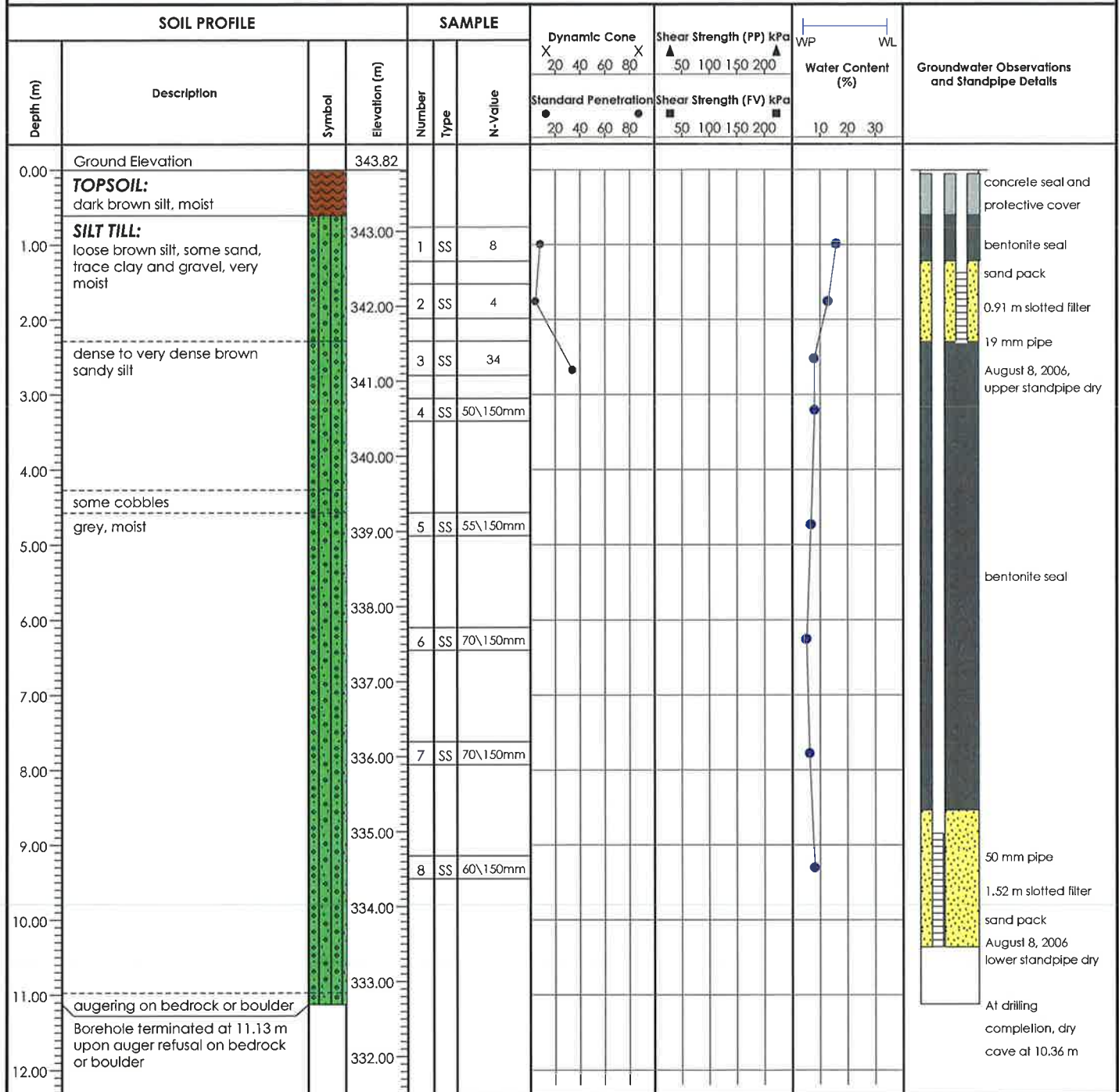
Ground Elevation: 343.82 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: July 31, 2006



Reviewed by: DN

Drill Method: Solid Stem Auger

Notes: Bulk sample taken from 1.22 to 2.13 m.

Field Tech.: RM

Sheet: 1 of 1

Drafted by: DC(01a)



Borehole Number: 106

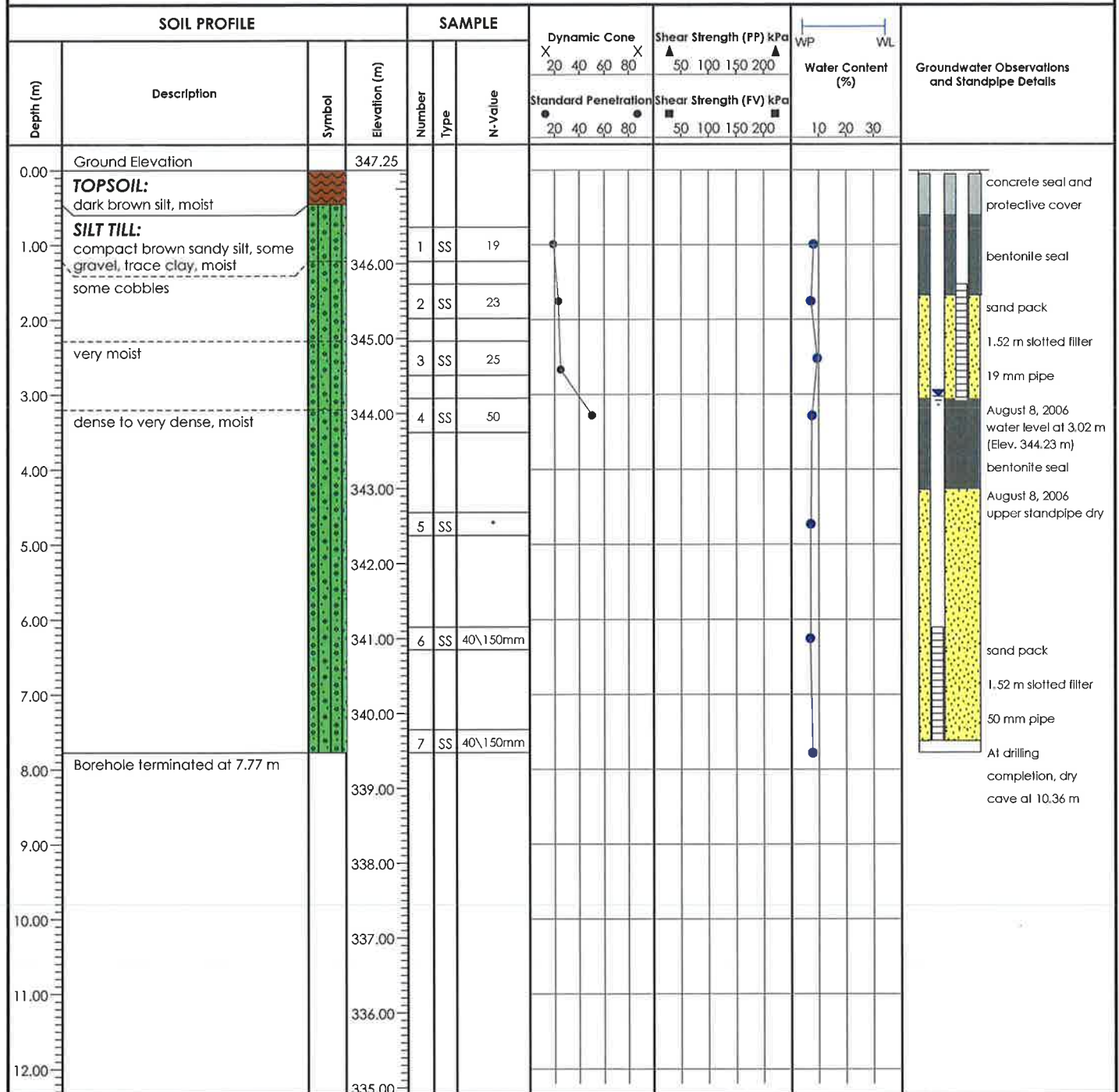
Ground Elevation: 347.25 m

Project: P.T. Valeriotte Subdivision

Job No.: 0353G4

Location: Cityview Drive, Guelph, Ontario

Drill Date: August 2, 2006



Reviewed by: DN

Field Tech.: RM

Drill Method: Solid Stem Auger

Sheet: 1 of 1

Notes: Bulk sample taken from 1.52 to 3.05 m. *Sampler bouncing on gravel.

Drafted by: DC(01a)

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “C”

GROUNDWATER ELEVATION MEASUREMENTS

**Completed by Gamsby and Mannerow Limited
(August 2006 - November 2014)**

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

GROUNDWATER ELEVATIONS (m)

INSTALLED AUGUST 2006

WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>>	AUG 8/06	AUG 17/06	OCT 3/06	JAN 22/08	APR 3/08	MAY 30/08	JUL 21/08	OCT 15/08	DEC 18/08
BH 101	338.61	339.38		336.94	336.79	336.98	337.81	338.62	337.41	337.06	337.25	338.37
BH 102	334.42	335.22		330.98	331.50	330.61	333.47	334.43	333.26	331.40	332.56	334.04
BH 103 U	344.44	345.74			342.97		344.07	344.44	343.65	342.96	343.04	344.41
BH 103 L	344.44	345.70		341.36	341.17	340.71	342.48	343.74	342.21	341.23	341.59	
BH 104 U	339.95	340.66			337.27		338.77	339.68	338.36	337.47	337.47	
BH 104 L	339.95	340.59		336.94	336.64	336.06	337.59	338.49	336.90	336.10	336.72	338.36
BH 105 U	343.82	344.49					342.54	343.72	342.41		342.16	
BH 105 L	343.82	344.41		333.66	334.53	334.85		337.34	337.39	335.88	335.84	
BH 106 U	347.25	347.98			344.27		346.12	346.92	345.25	344.48	344.60	
BH 106 L	347.25	347.92		344.27	344.20	343.88	346.09	346.85	345.21	344.30	344.53	346.26
BH 107 U	345.47	346.21		344.45	344.15	344.65	344.60		344.69	344.66	344.77	345.30
BH 107 L	345.47	346.17		342.30	344.71		345.07	345.34	344.70	344.34	344.75	345.23
BH 108	342.70	343.25		340.46	340.29	340.39	341.62	342.12	340.81	340.27	340.38	341.93
BH 109	326.19	326.83		322.39	322.34	322.42	323.01	324.20	324.13	322.58	322.45	
BH 110	323.60	324.25		321.04	320.96	321.09	321.65	322.90	320.39	321.14	321.00	

Notes:

Ground elevation represents shots on the ground beside the borehole
August 8, 2006 water level measurements taken by Naylor Engineering Associates Ltd.
May 13, 2009 water level measurements taken by Banks Groundwater Engineering

See Geotechnical Investigation (Naylor Engineering Associates Ltd., January 2012)
for existing monitoring well locations

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

INSTALLED AUGUST 2006

WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>> MAY 13/09 AUG 4/09 OCT 19/09 DEC 15/09 MAR 12/10 JUL 17/10 SEP 27/10 DEC 1/10 FEB 15/11									
BH 101	338.61	339.38	338.016	336.756	338.616	337.405	337.846	337.216	336.379	337.164	337.287	
BH 102	334.42	335.22	333.743	330.583		333.256	332.148	332.091	330.597	330.496	332.385	
BH 103 U	344.44	345.74	342.937				343.802	343.03		343.171		
BH 103 L	344.44	345.70	343.846			342.208	342.056	341.566		341.598	341.575	
BH 104 U	339.95	340.66	338.576				337.466	337.725		336.826		
BH 104 L	339.95	340.59	337.936	334.576			337.036	336.544	333.358	335.704	336.095	
BH 105 U	343.82	344.49	342.599				342.657			342.397	342.197	
BH 105 L	343.82	344.41	336.994	334.824			337.235	337.785	334.214	333.399	335.548	
BH 106 U	347.25	347.98	345.606				345.451			344.161	344.705	
BH 106 L	347.25	347.92	345.614		346.846	345.214	345.409	344.459	341.979	344.512	344.713	
BH 107 U	345.47	346.21	345.011	344.006		344.691	345.406	344.377	343.763	345.388	344.87	
BH 107 L	345.47	346.17	344.96								344.702	
BH 108	342.70	343.25	341.207	339.812	342.119	340.811	341.112	340.335	339.598	340.234	341.471	
BH 109	326.19	326.83	323.239		324.202	324.126	322.619		322.254	322.727	322.421	
BH 110	323.60	324.25	321.859		322.897	320.386	321.028		320.795	321.097	320.982	

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

INSTALLED AUGUST 2006

WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>>	MAY 13/11	JUL 22/11	SEP 28/11	DEC 16/11	FEB 16/12	APR 3/12	JUNE 8/12	AUG 24/12	OCT 10/12
BH 101	338.61	339.38		337.362	336.301	335.260	337.682	338.080	338.023	337.129	335.967	335.908
BH 102	334.42	335.22		333.084	330.959	329.784	333.321	333.677	333.506	330.915	330.626	330.614
BH 103 U	344.44	345.74		342.737			342.997	343.684	343.591			
BH 103 L	344.44	345.70		341.914	340.369	338.465	341.492	342.494	342.395	341.096	339.126	338.081
BH 104 U	339.95	340.66		337.975	336.696	336.315	338.222	338.475	338.476	337.021	337.005	336.998
BH 104 L	339.95	340.59		336.921	335.663	332.665	337.555	337.651	337.570	335.969	333.466	333.419
BH 105 U	343.82	344.49		342.092	341.215		342.162	342.708	342.675	341.884		
BH 105 L	343.82	344.41		336.422	335.393	333.709		336.390	336.352	335.437	333.666	333.279
BH 106 U	347.25	347.98		345.159	343.733	343.590	344.719		344.854	344.266	344.301	344.314
BH 106 L	347.25	347.92		345.187	343.706	341.418	344.739	344.900	344.820	344.044	341.359	340.299
BH 107 U	345.47	346.21		344.292	343.380	342.523	344.655		345.102	344.453	343.361	343.256
BH 107 L	345.47	346.17		344.369	343.426	342.334	344.573	345.088	345.040	344.330	342.484	342.494
BH 108	342.70	343.25		340.887	339.681							
BH 109	326.19	326.83		322.230	321.899	321.331	322.345	322.984	323.165	322.496	322.124	322.194
BH 110	323.60	324.25		321.200		319.823	320.872	321.539	321.772	321.052	320.682	320.766

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

INSTALLED AUGUST 2006

WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>>	DEC 13/12	FEB 6/13	APR 18/13	JUNE 4/13	AUG 8/13	OCT 29/13	DEC 9/13	FEB 19/14	APR 28/14
BH 101	338.61	339.38		338.135	338.011	338.466	337.828	337.681	337.677	338.064	337.792	338.326
BH 102	334.42	335.22		332.437	333.806	334.172	332.882	332.013	332.012	333.009	332.664	333.799
BH 103 U	344.44	345.74		343.561	344.067	344.440	343.211	343.032	343.135	343.278	343.060	344.050
BH 103 L	344.44	345.70		341.781	342.649	343.503	341.924	341.665	341.531	342.176	341.999	343.121
BH 104 U	339.95	340.66		338.031	338.723	339.294	338.202	338.175	337.576	337.986	337.784	338.645
BH 104 L	339.95	340.59		337.120	337.705	338.272	337.152	337.366	337.094	337.423	337.150	338.062
BH 105 U	343.82	344.49		342.535	343.108	343.820	342.760	342.284	342.145	342.476		343.322
BH 105 L	343.82	344.41		333.610	336.497	337.289	336.624	336.070	335.160	336.139		337.022
BH 106 U	347.25	347.98		345.266	345.304	345.992	344.686	344.413	345.008	345.004	344.660	345.418
BH 106 L	347.25	347.92		345.209	345.246	345.920	344.641	344.333	344.980	344.963	344.620	345.382
BH 107 U	345.47	346.21		345.289		345.245	345.075	344.844	345.234	345.176	345.160	345.150
BH 107 L	345.47	346.17		345.175	345.017	345.202	345.142	344.853	345.203	345.185	345.140	345.157
BH 108	342.70	343.25										
BH 109	326.19	326.83		322.675	323.184	323.721	322.994	322.757	322.683	322.716	322.694	323.278
BH 110	323.60	324.25		321.275	321.835	322.524	321.555	321.436	321.265	321.298	321.253	321.937

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

INSTALLED AUGUST 2006

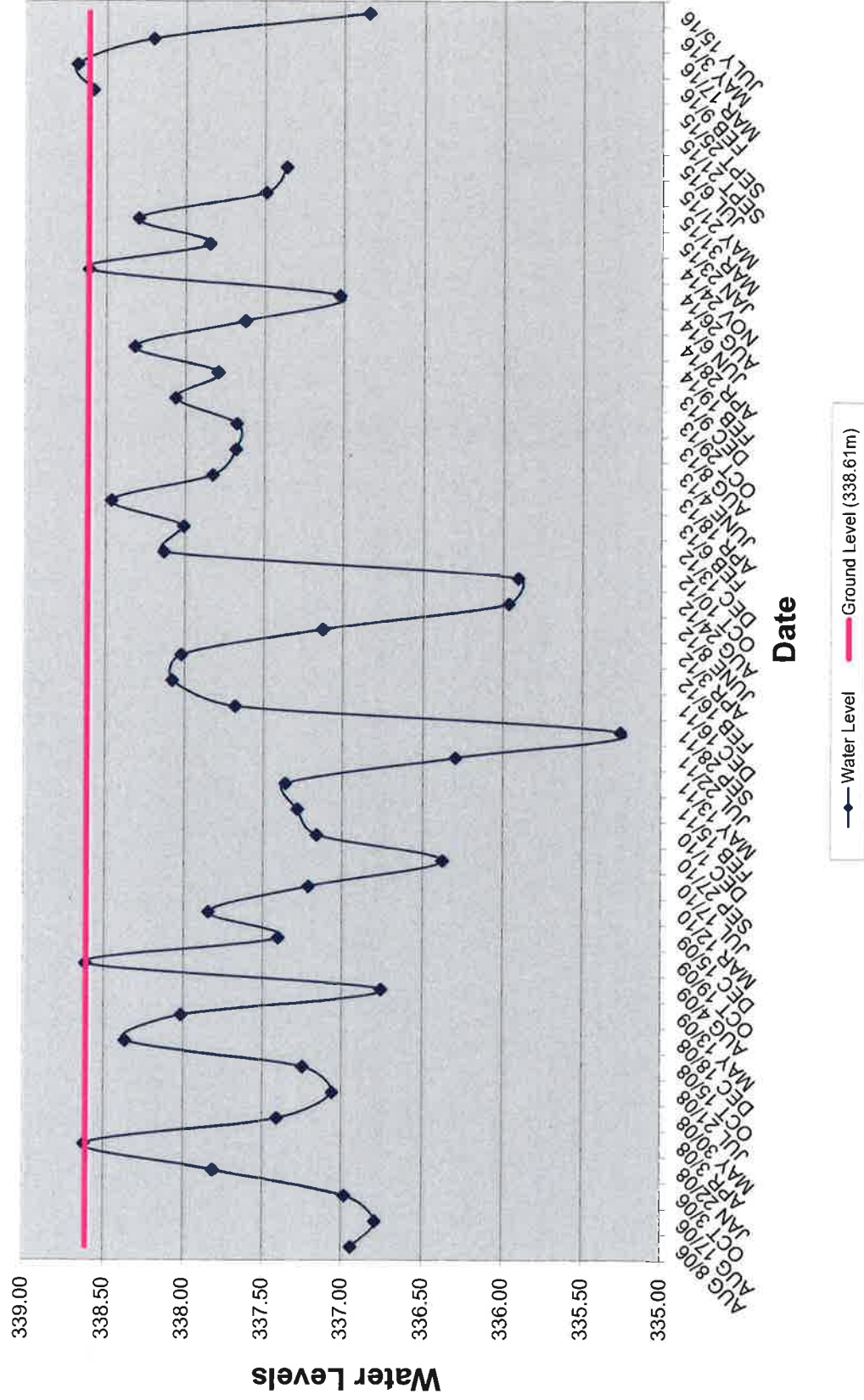
WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>>	JUN 6/14	AUG 26/14	NOV 24/14	JAN 23/15	MAR 31/15	MAY 21/15	JUL 6/15	SEPT 21/15
BH 101	338.61	339.38		337.622	337.026	338.610	337.846	338.302	337.496	337.366	
BH 102	334.42	335.22		332.640		333.183	332.687	333.400	332.443	332.369	
BH 103 U	344.44	345.74		343.252		342.978	343.070	343.595	343.112	343.027	
BH 103 L	344.44	345.70		342.362	340.666	342.046	342.204	342.662	342.194	341.744	339.666
BH 104 U	339.95	340.66		338.064		337.421	337.713	338.286	337.539	337.760	
BH 104 L	339.95	340.59		337.471	335.534	337.260	337.206	337.619	336.846	337.091	
BH 105 U	343.82	344.49		342.466		342.321	342.243	342.512	342.484	342.447	
BH 105 L	343.82	344.41		336.664	334.894	335.766	336.011	335.276	336.302	336.462	
BH 106 U	347.25	347.98		344.703		345.362	344.633	345.061	344.708		
BH 106 L	347.25	347.92		344.690	343.153	345.412	344.612	345.043	344.654	344.872	
BH 107 U	345.47	346.21		344.677	344.081	345.346	345.346		344.466	344.486	
BH 107 L	345.47	346.17		344.698	344.107	345.343	344.912	345.216	344.320	344.920	
BH 108	342.70	343.25									
BH 109	326.19	326.83		322.911	322.487	322.946	322.697	322.795	322.785	322.827	322.233
BH 110	323.60	324.25		321.573		321.261	321.307	321.302	321.389	321.555	

CITYVIEW RIDGE SUBDIVISION
PROJECT NO.: 105-172

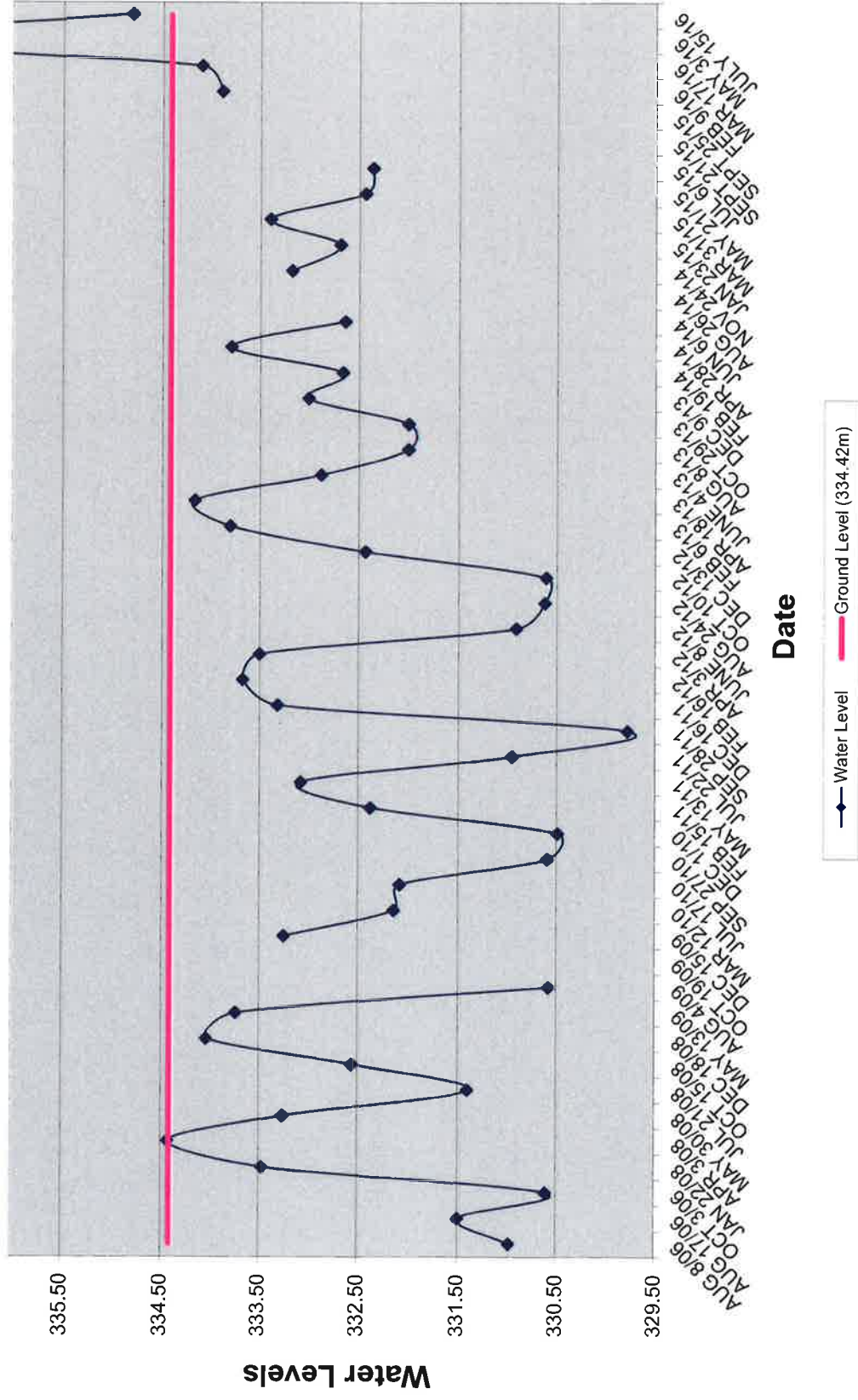
INSTALLED AUGUST 2006

WELL ID.	GROUND ELEVATION (m)	TOP OF CASING ELEVATION (m)	DATE>>	SEPT 25/15	FEB 9/16	MAR 17/16	MAY 3/16	JULY 15/16
BH 101	338.61	339.38		338.586	338.681	338.209	336.846	
BH 102	334.42	335.22		333.895	334.103	337.911	334.806	
BH 103 U	344.44	345.74		344.172	344.52	337.741	336.536	
BH 103 L	344.44	345.70		342.889	343.329	336.691	334.486	
BH 104 U	339.95	340.66		338.847	339.196	337.486	335.776	
BH 104 L	339.95	340.59		337.889	338.248	336.526	336.106	
BH 105 U	343.82	344.49		342.999	343.618	338.176	337.106	
BH 105 L	343.82	344.41		335.251	336.283	332.116	332.106	
BH 106 U	347.25	347.98		345.713	345.983	336.726	335.686	
BH 106 L	347.25	347.92	342.986	345.688	345.966	336.776	332.106	
BH 107 U	345.47	346.21	343.839	345.236	345.296	338.266	336.566	
BH 107 L	345.47	346.17		345.23				
BH 108	342.70	343.25						
BH 109	326.19	326.83		323.084	323.439	335.753	335.356	
BH 110	323.60	324.25	322.777	321.635	321.934	336.931	337.006	

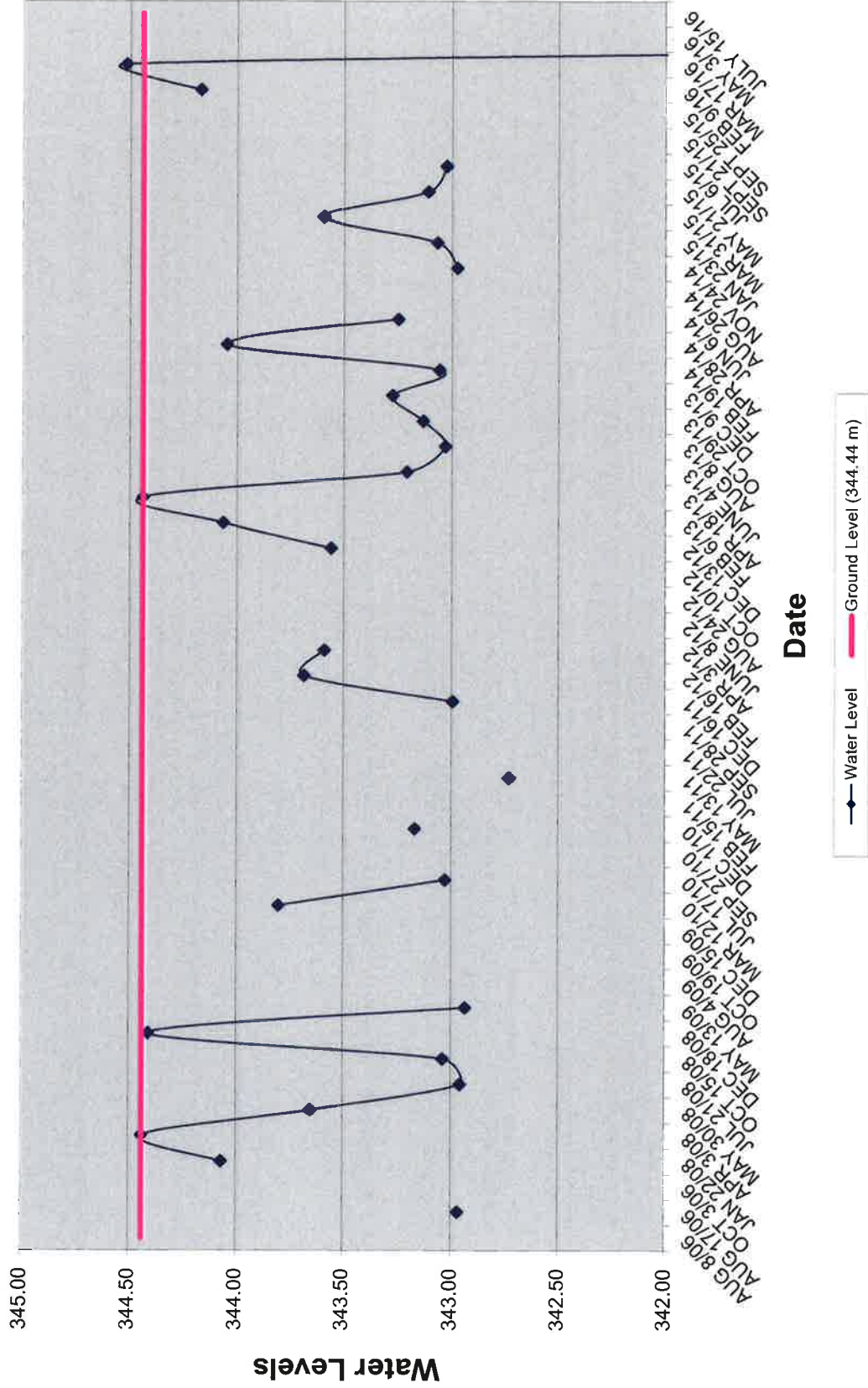
Cityview Ridge Subdivision Monitoring Well BH 101



Cityview Ridge Subdivision Monitoring Well BH 102



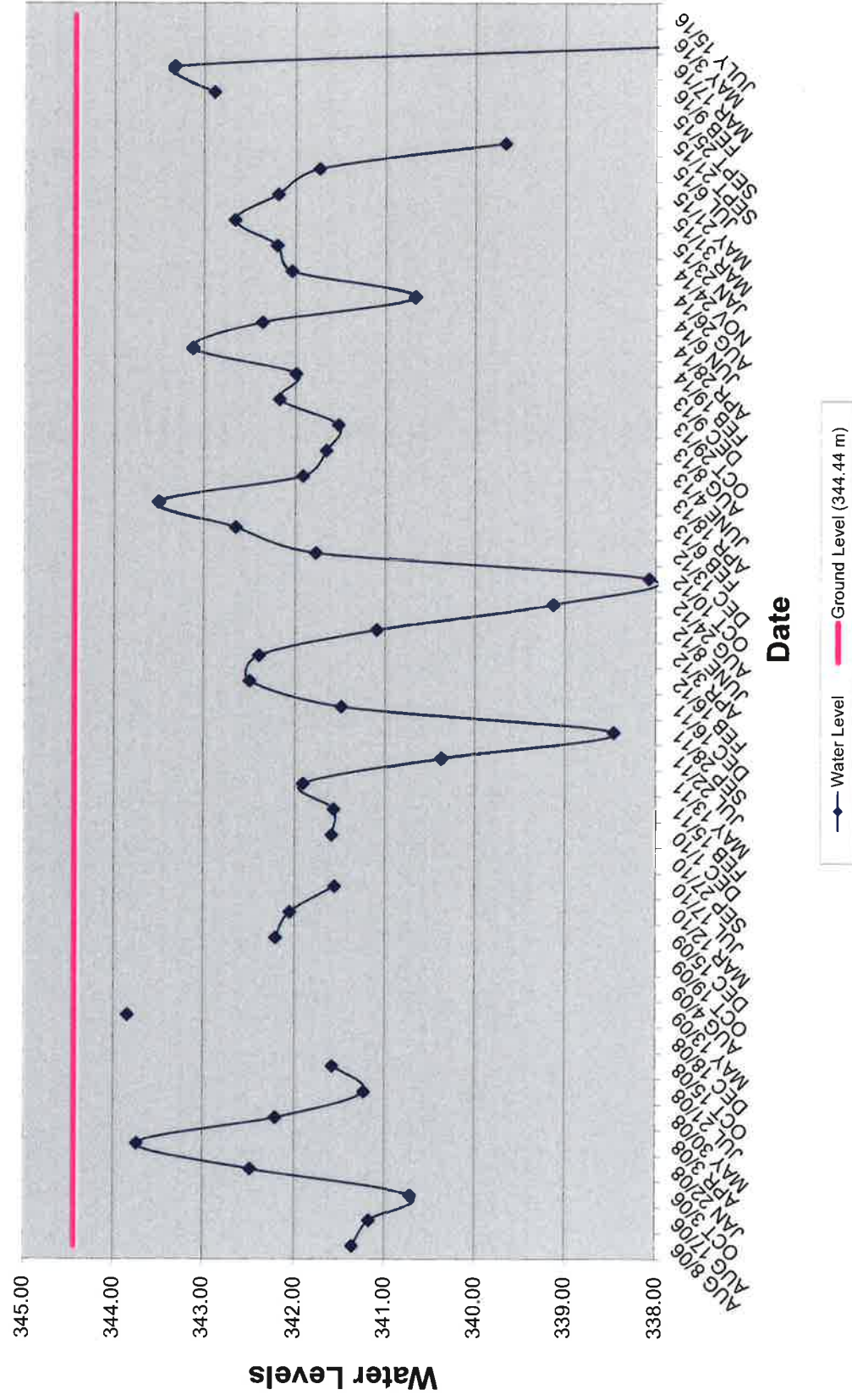
Cityview Ridge Subdivision Monitoring BH Well 103 U



Cityview Ridge Subdivision Monitoring Well BH 103 L

The graph displays the water level in monitoring well BH 103 L over a ten-year period. The vertical axis represents water levels in meters, ranging from 338.00 to 345.00. The horizontal axis represents the date, from August 2006 to July 2016. A horizontal pink line marks the ground level at 344.44 meters. The water level data is plotted as a blue line with diamond markers. The water level starts at approximately 341.5 m in August 2006, rises to a peak of about 344.5 m in late 2006, then fluctuates between 341.0 m and 343.5 m until 2014. In early 2016, the water level drops sharply to its lowest point of approximately 338.5 m before rising back to about 343.0 m by July 2016.

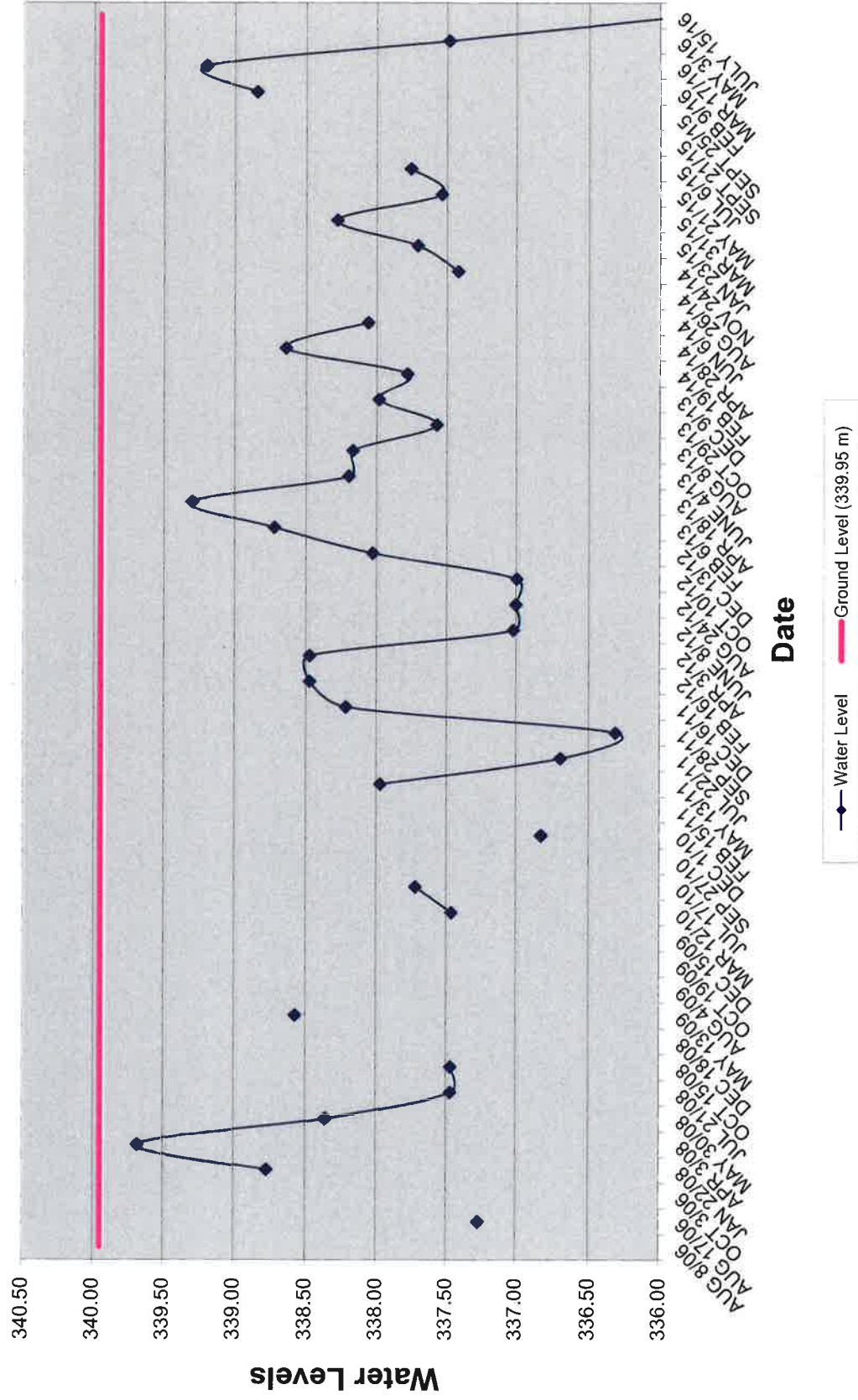
Date	Water Level (m)
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AUG 15/06	341.5
AUG 22/06	341.5
SEP 5/06	341.5
SEP 12/06	341.5
SEP 19/06	341.5
SEP 26/06	341.5
OCT 3/06	341.5
OCT 10/06	341.5
OCT 17/06	341.5
OCT 24/06	341.5
NOV 1/06	341.5
NOV 8/06	341.5
NOV 15/06	341.5
NOV 22/06	341.5
DEC 1/06	341.5
DEC 8/06	341.5
DEC 15/06	341.5
DEC 22/06	341.5
JAN 5/07	341.5
JAN 12/07	341.5
JAN 19/07	341.5
JAN 26/07	341.5
FEB 2/07	341.5
FEB 9/07	341.5
FEB 16/07	341.5
FEB 23/07	341.5
MAR 1/07	341.5
MAR 8/07	341.5
MAR 15/07	341.5
MAR 22/07	341.5
APR 5/07	341.5
APR 12/07	341.5
APR 19/07	341.5
APR 26/07	341.5
MAY 3/07	341.5
MAY 10/07	341.5
MAY 17/07	341.5
MAY 24/07	341.5
JUN 1/07	341.5
JUN 8/07	341.5
JUN 15/07	341.5
JUN 22/07	341.5
JUL 1/07	341.5
JUL 8/07	341.5
JUL 15/07	341.5
JUL 22/07	341.5
AUG 5/07	341.5
AUG 12/07	341.5
AUG 19/07	341.5
AUG 26/07	341.5
SEP 2/07	341.5
SEP 9/07	341.5
SEP 16/07	341.5
SEP 23/07	341.5
OCT 1/07	341.5
OCT 8/07	341.5
OCT 15/07	341.5
OCT 22/07	341.5
NOV 5/07	341.5
NOV 12/07	341.5
NOV 19/07	341.5
NOV 26/07	341.5
DEC 3/07	341.5
DEC 10/07	341.5
DEC 17/07	341.5
DEC 24/07	341.5
JAN 1/08	341.5
JAN 8/08	341.5
JAN 15/08	341.5
JAN 22/08	341.5
FEB 5/08	341.5
FEB 12/08	341.5
FEB 19/08	341.5
FEB 26/08	341.5
MAR 5/08	341.5
MAR 12/08	341.5
MAR 19/08	341.5
MAR 26/08	341.5
APR 2/08	341.5
APR 9/08	341.5
APR 16/08	341.5
APR 23/08	341.5
MAY 1/08	341.5
MAY 8/08	341.5
MAY 15/08	341.5
MAY 22/08	341.5
JUN 5/08	341.5
JUN 12/08	341.5
JUN 19/08	341.5
JUN 26/08	341.5
JUL 3/08	341.5
JUL 10/08	341.5
JUL 17/08	341.5
JUL 24/08	341.5
AUG 1/08	341.5
AUG 8/08	341.5
AUG 15/08	341.5
AUG 22/08	341.5
SEP 5/08	341.5
SEP 12/08	341.5
SEP 19/08	341.5
SEP 26/08	341.5
OCT 3/08	341.5
OCT 10/08	341.5
OCT 17/08	341.5
OCT 24/08	341.5
NOV 1/08	341.5
NOV 8/08	341.5
NOV 15/08	341.5
NOV 22/08	341.5
DEC 1/08	341.5
DEC 8/08	341.5
DEC 15/08	341.5
DEC 22/08	341.5
JAN 5/09	341.5
JAN 12/09	341.5
JAN 19/09	341.5
JAN 26/09	341.5
FEB 2/09	341.5
FEB 9/09	341.5
FEB 16/09	341.5
FEB 23/09	341.5
MAR 1/09	341.5
MAR 8/09	341.5
MAR 15/09	341.5
MAR 22/09	341.5
APR 5/09	341.5
APR 12/09	341.5
APR 19/09	341.5
APR 26/09	341.5
MAY 3/09	341.5
MAY 10/09	341.5
MAY 17/09	341.5
MAY 24/09	341.5
JUN 1/09	341.5
JUN 8/09	341.5
JUN 15/09	341.5
JUN 22/09	341.5
JUL 1/09	341.5
JUL 8/09	341.5
JUL 15/09	341.5
JUL 22/09	341.5
AUG 5/09	341.5</



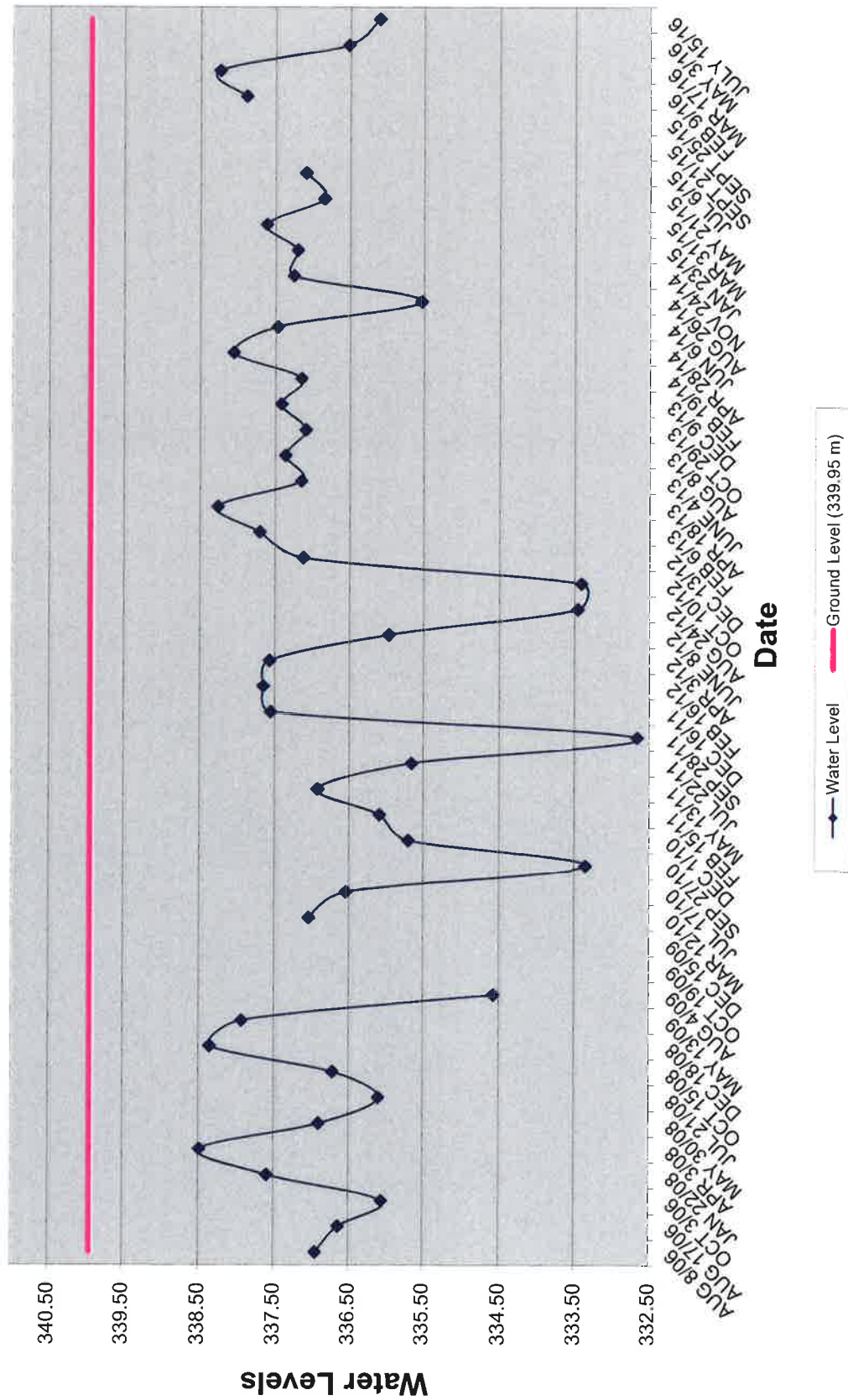
Cityview Ridge Subdivision Monitoring Well BH 104 U

The graph displays the water level in monitoring well BH 104 U over a ten-year period. The water level is represented by a blue line with diamond markers, and the ground level is indicated by a horizontal pink line at 339.95 m. The water level shows seasonal fluctuations, with higher levels generally occurring in the winter months and lower levels in the summer months. There are several notable peaks and troughs throughout the period.

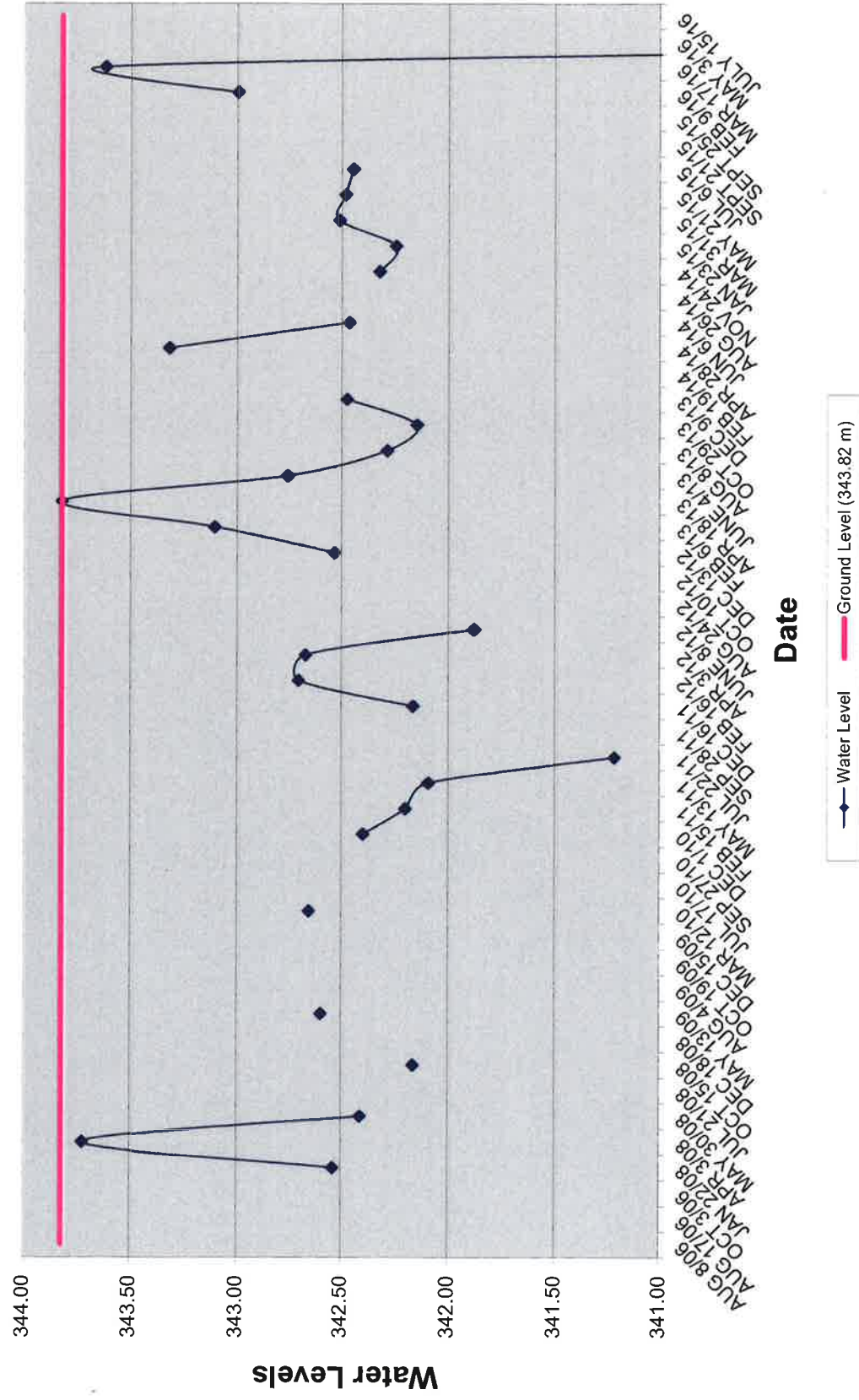
Date	Water Level (m)
AUG 8/06	337.20
AUG 17/06	337.50
SEP 1/06	337.50
SEP 15/06	337.50
OCT 1/06	337.50
OCT 15/06	337.50
NOV 1/06	337.50
NOV 15/06	337.50
DEC 1/06	337.50
DEC 15/06	337.50
JAN 1/07	337.50
JAN 15/07	337.50
FEB 1/07	337.50
FEB 15/07	337.50
MAR 1/07	337.50
MAR 15/07	337.50
APR 1/07	337.50
APR 15/07	337.50
MAY 1/07	337.50
MAY 15/07	337.50
JUN 1/07	337.50
JUN 15/07	337.50
JUL 1/07	337.50
JUL 15/07	337.50
AUG 1/07	337.50
AUG 15/07	337.50
SEP 1/07	337.50
SEP 15/07	337.50
OCT 1/07	337.50
OCT 15/07	337.50
NOV 1/07	337.50
NOV 15/07	337.50
DEC 1/07	337.50
DEC 15/07	337.50
JAN 1/08	337.50
JAN 15/08	337.50
FEB 1/08	337.50
FEB 15/08	337.50
MAR 1/08	337.50
MAR 15/08	337.50
APR 1/08	337.50
APR 15/08	337.50
MAY 1/08	337.50
MAY 15/08	337.50
JUN 1/08	337.50
JUN 15/08	337.50
JUL 1/08	337.50
JUL 15/08	337.50
AUG 1/08	337.50
AUG 15/08	337.50
SEP 1/08	337.50
SEP 15/08	337.50
OCT 1/08	337.50
OCT 15/08	337.50
NOV 1/08	337.50
NOV 15/08	337.50
DEC 1/08	337.50
DEC 15/08	337.50
JAN 1/09	337.50
JAN 15/09	337.50
FEB 1/09	337.50
FEB 15/09	337.50
MAR 1/09	337.50
MAR 15/09	337.50
APR 1/09	337.50
APR 15/09	337.50
MAY 1/09	337.50
MAY 15/09	337.50
JUN 1/09	337.50
JUN 15/09	337.50
JUL 1/09	337.50
JUL 15/09	337.50
AUG 1/09	337.50
AUG 15/09	337.50
SEP 1/09	337.50
SEP 15/09	337.50
OCT 1/09	337.50
OCT 15/09	337.50
NOV 1/09	337.50
NOV 15/09	337.50
DEC 1/09	337.50
DEC 15/09	337.50
JAN 1/10	337.50
JAN 15/10	337.50
FEB 1/10	337.50
FEB 15/10	337.50
MAR 1/10	337.50
MAR 15/10	337.50
APR 1/10	337.50
APR 15/10	337.50
MAY 1/10	337.50
MAY 15/10	337.50
JUN 1/10	337.50
JUN 15/10	337.50
JUL 1/10	337.50
JUL 15/10	337.50
AUG 1/10	337.50
AUG 15/10	337.50
SEP 1/10	337.50
SEP 15/10	337.50
OCT 1/10	337.50
OCT 15/10	337.50
NOV 1/10	337.50
NOV 15/10	337.50
DEC 1/10	337.50
DEC 15/10	337.50
JAN 1/11	337.50
JAN 15/11	337.50
FEB 1/11	337.50
FEB 15/11	337.50
MAR 1/11	337.50
MAR 15/11	337.50
APR 1/11	337.50
APR 15/11	337.50
MAY 1/11	337.50
MAY 15/11	337.50
JUN 1/11	337.50
JUN 15/11	337.50
JUL 1/11	337.50
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AUG 1/11	337.50
AUG 15/11	337.50
SEP 1/11	337.50
SEP 15/11	337.50
OCT 1/11	337.50
OCT 15/11	337.50
NOV 1/11	337.50
NOV 15/11	337.50
DEC 1/11	337.50
DEC 15/11	337.50
JAN 1/12	337.50
JAN 15/12	337.50
FEB 1/12	337.50
FEB 15/12	337.50
MAR 1/12	337.50
MAR 15/12	337.50
APR 1/12	337.50
APR 15/12	337.50
MAY 1/12	337.50
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JUN 1/12	337.50
JUN 15/12	337.50
JUL 1/12	337.50
JUL 15/12	337.



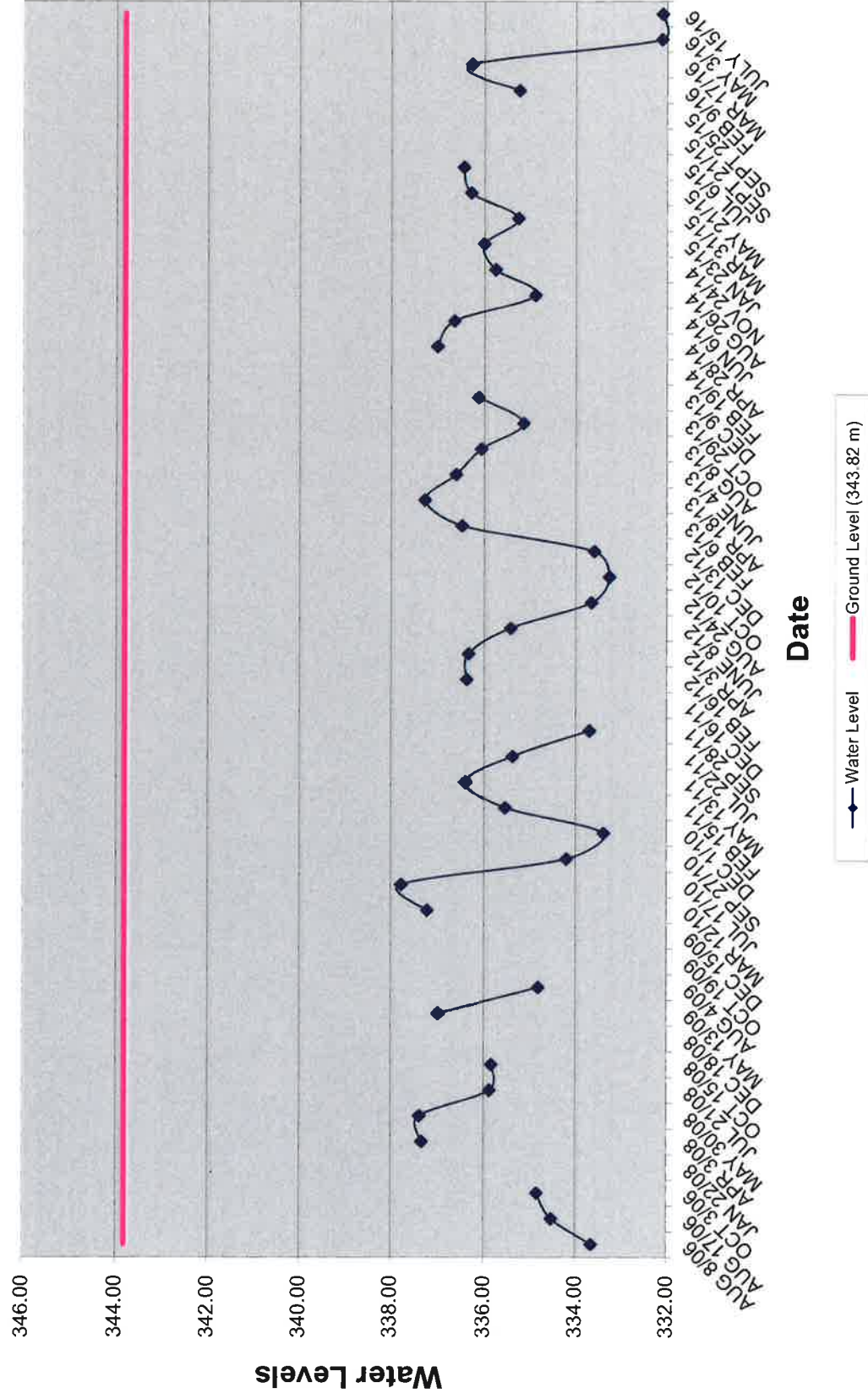
Cityview Ridge Subdivision Monitoring Well BH 104 L



Cityview Ridge Subdivision Monitoring Well BH 105 U



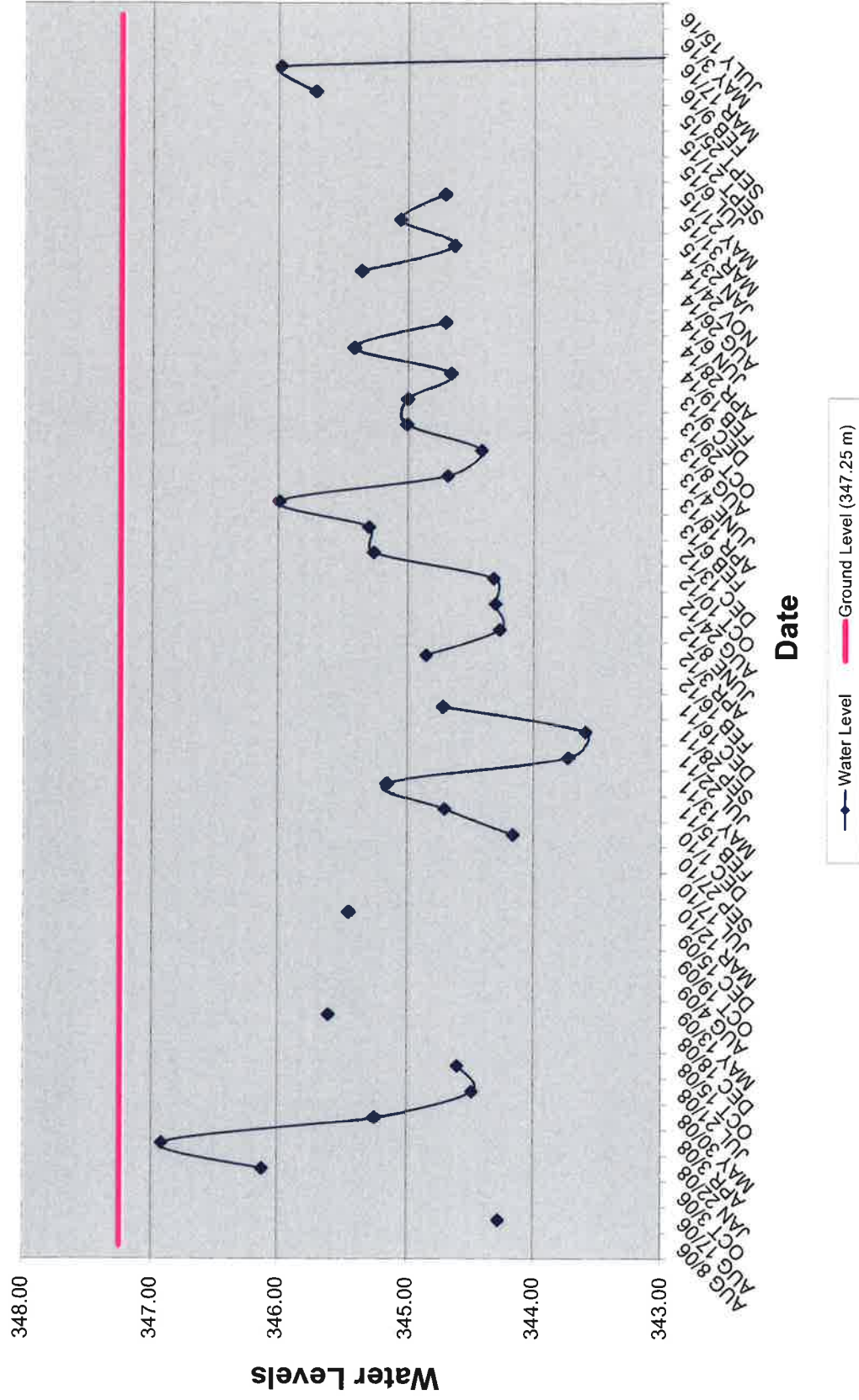
Cityview Ridge Subdivision Monitoring Well BH 105 L



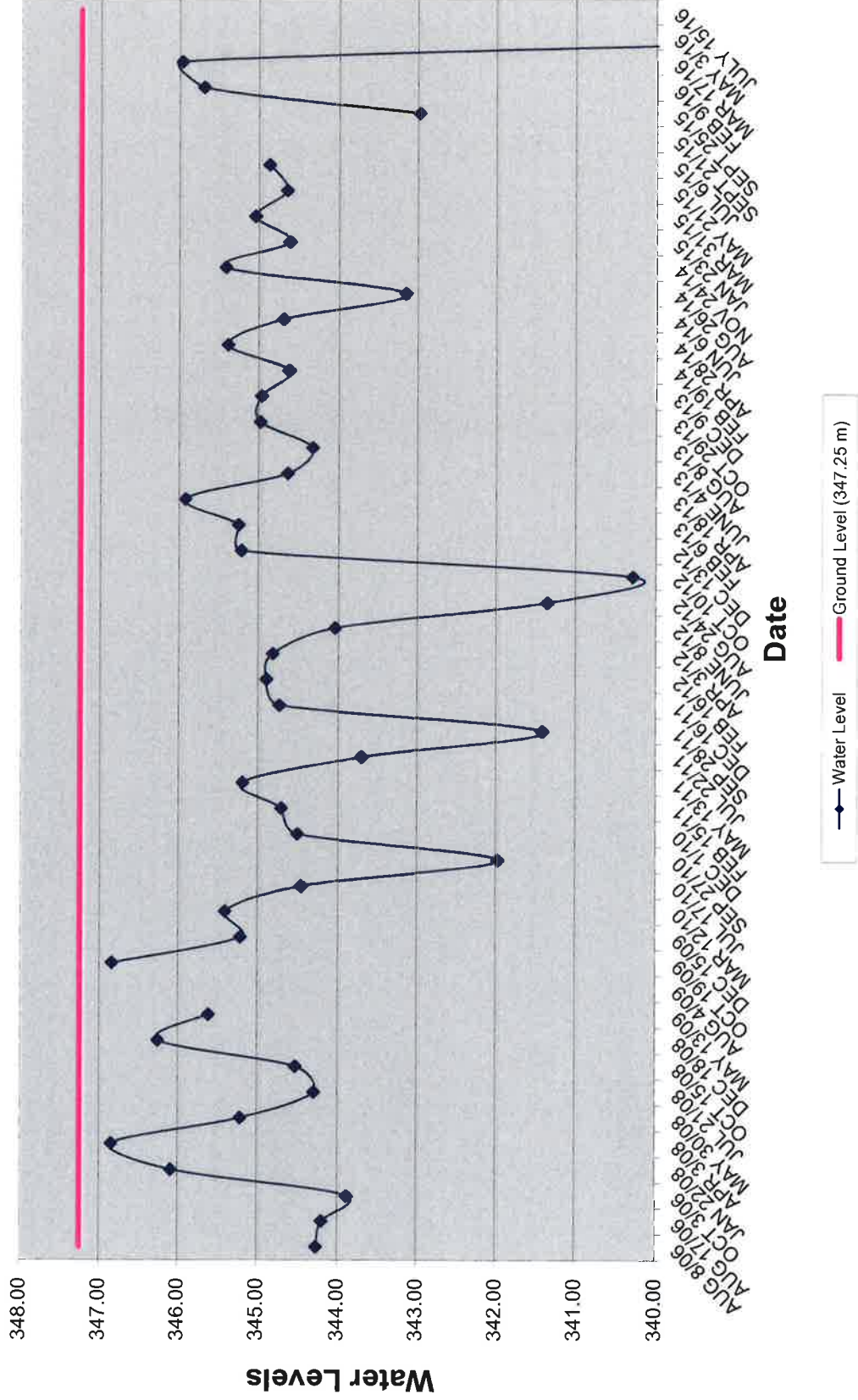
Cityview Ridge Subdivision Monitoring Well BH 106 U

The graph displays the water level data for Monitoring Well BH 106 U over a ten-year period. The vertical axis represents the water level in meters, ranging from 343.00 to 348.00. The horizontal axis represents the date, from August 8, 2006, to July 15, 2016. A horizontal pink line marks the ground level at 347.25 meters. The water level is plotted as a blue line with diamond markers. The data shows significant fluctuations, with the water level generally staying between 344.00 m and 346.50 m. There is a notable peak around 346.50 m in late 2015, followed by a sharp decline to approximately 344.00 m in early 2016.

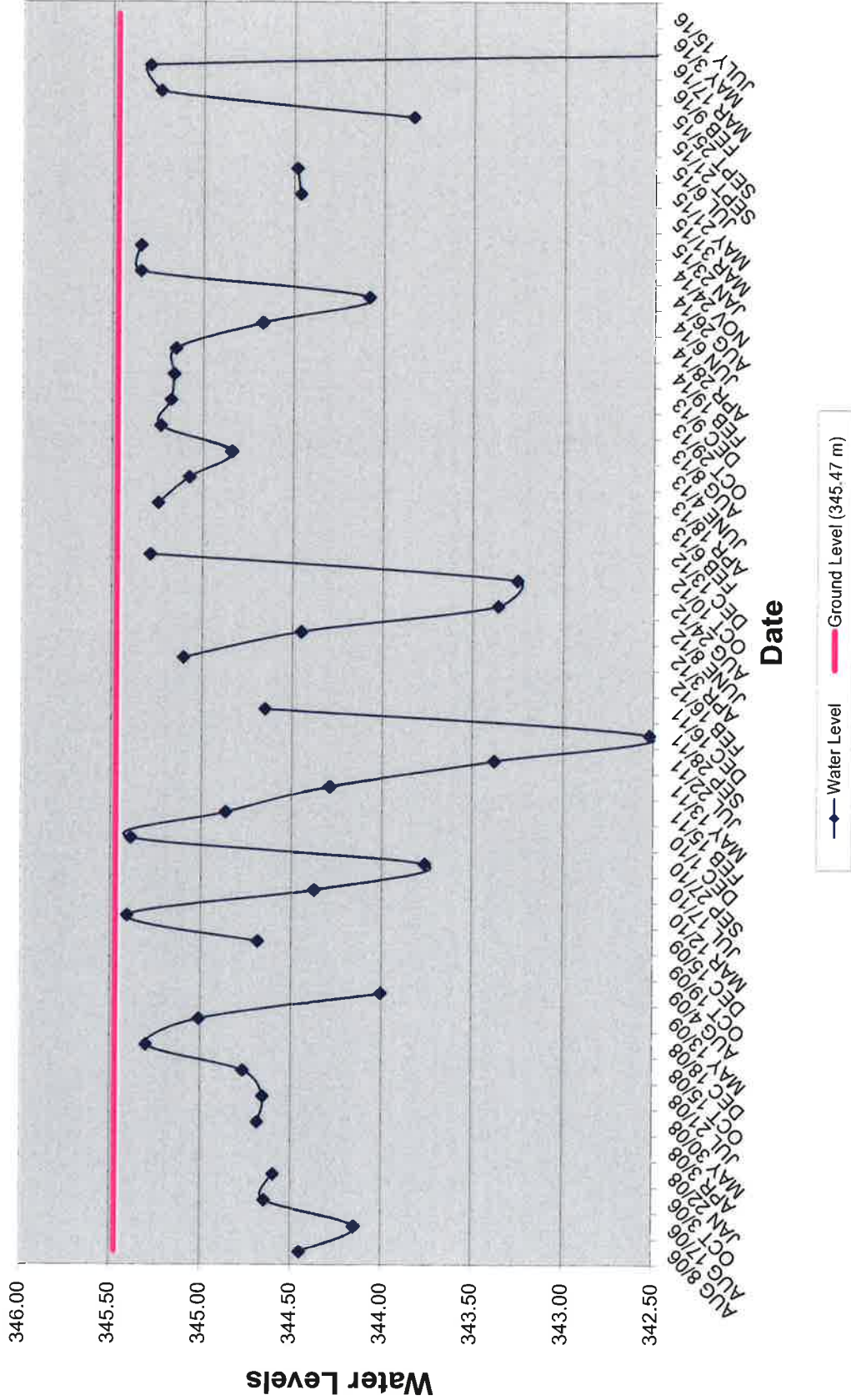
Date	Water Level (m)
Aug 8/06	344.50
Oct 17/06	344.00
Jan 3/08	345.00
Apr 22/08	345.50
May 3/08	345.50
Jun 15/08	345.50
Jul 2/08	345.50
Aug 13/08	345.50
Oct 1/08	345.50
Dec 15/08	345.50
Feb 1/09	345.50
Mar 12/09	345.50
Apr 19/09	345.50
Jun 1/09	345.50
Jul 15/09	345.50
Aug 27/09	345.50
Oct 1/09	345.50
Dec 15/09	345.50
Feb 1/10	345.50
Mar 12/10	345.50
Apr 19/10	345.50
Jun 1/10	345.50
Jul 15/10	345.50
Aug 27/10	345.50
Oct 1/10	345.50
Dec 15/10	345.50
Feb 1/11	345.50
Mar 12/11	345.50
Apr 19/11	345.50
Jun 1/11	345.50
Jul 15/11	345.50
Aug 27/11	345.50
Oct 1/11	345.50
Dec 15/11	345.50
Feb 1/12	345.50
Mar 12/12	345.50
Apr 19/12	345.50
Jun 1/12	345.50
Jul 15/12	345.50
Aug 27/12	345.50
Oct 1/12	345.50
Dec 15/12	345.50
Feb 1/13	345.50
Mar 12/13	345.50
Apr 19/13	345.50
Jun 1/13	345.50
Jul 15/13	345.50
Aug 27/13	345.50
Oct 1/13	345.50
Dec 15/13	345.50
Feb 1/14	345.50
Mar 12/14	345.50
Apr 19/14	345.50
Jun 1/14	345.50
Jul 15/14	345.50
Aug 27/14	345.50
Oct 1/14	345.50
Dec 15/14	345.50
Feb 1/15	345.50
Mar 12/15	345.50
Apr 19/15	345.50
Jun 1/15	345.50
Jul 15/15	345.50
Aug 27/15	345.50
Oct 1/15	345.50
Dec 15/15	345.50
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Mar 12/16	345.50
Apr 19/16	345.50
Jun 1/16	345.50
Jul 15/16	345.50



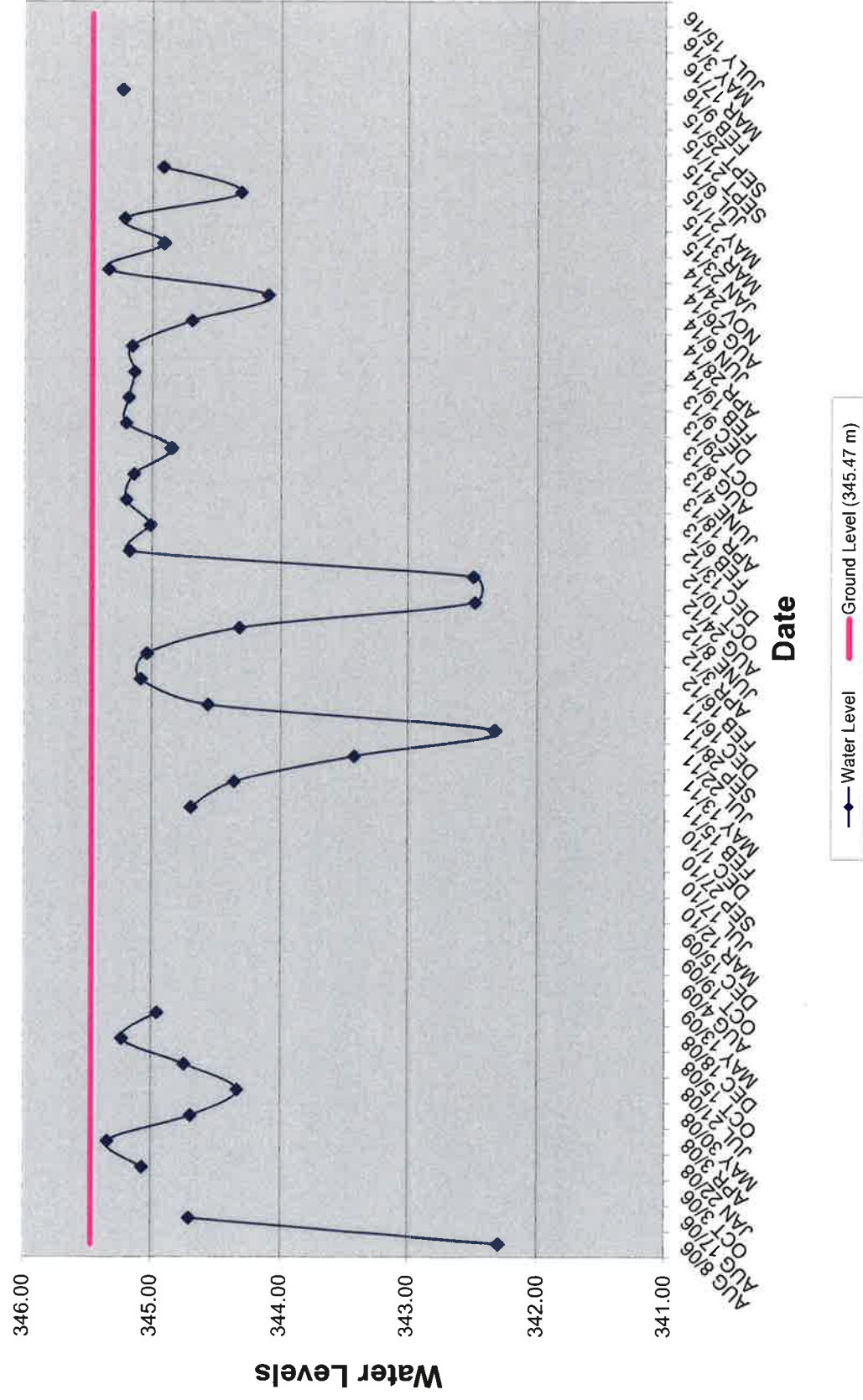
Cityview Ridge Subdivision Monitoring Well BH 106 L



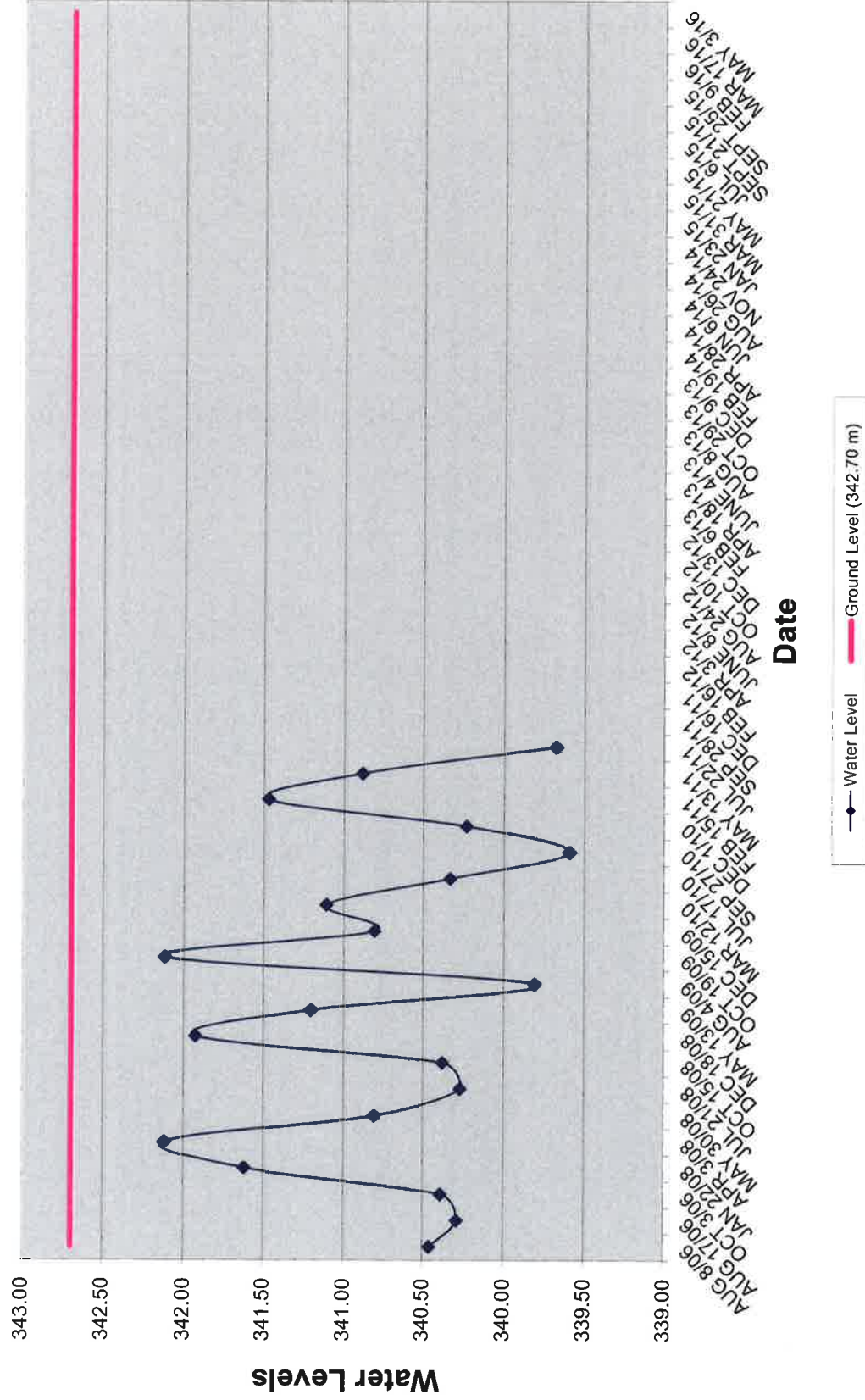
Cityview Ridge Subdivision Monitoring Well BH 107 U



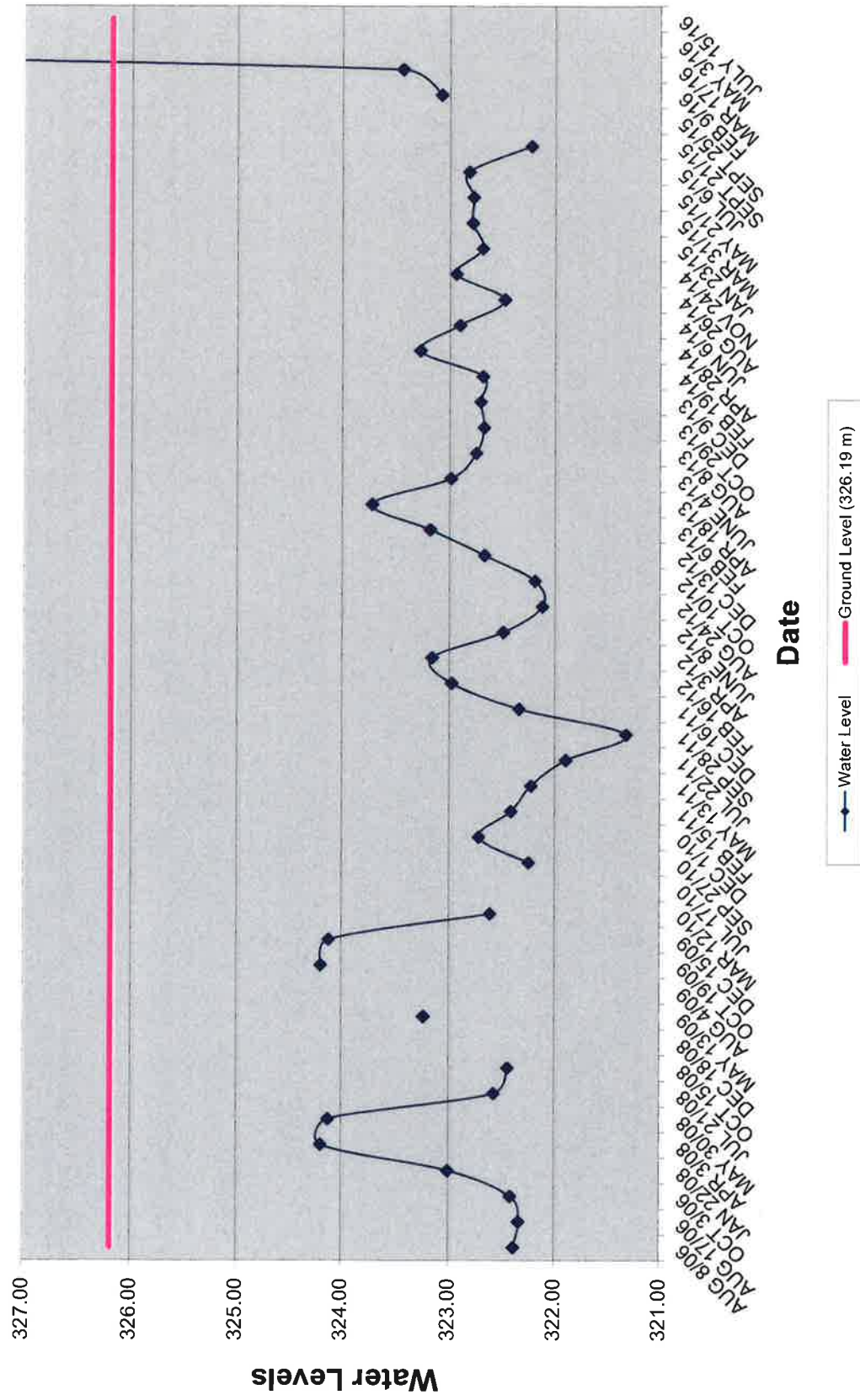
Cityview Ridge Subdivision Monitoring Well BH 107 L



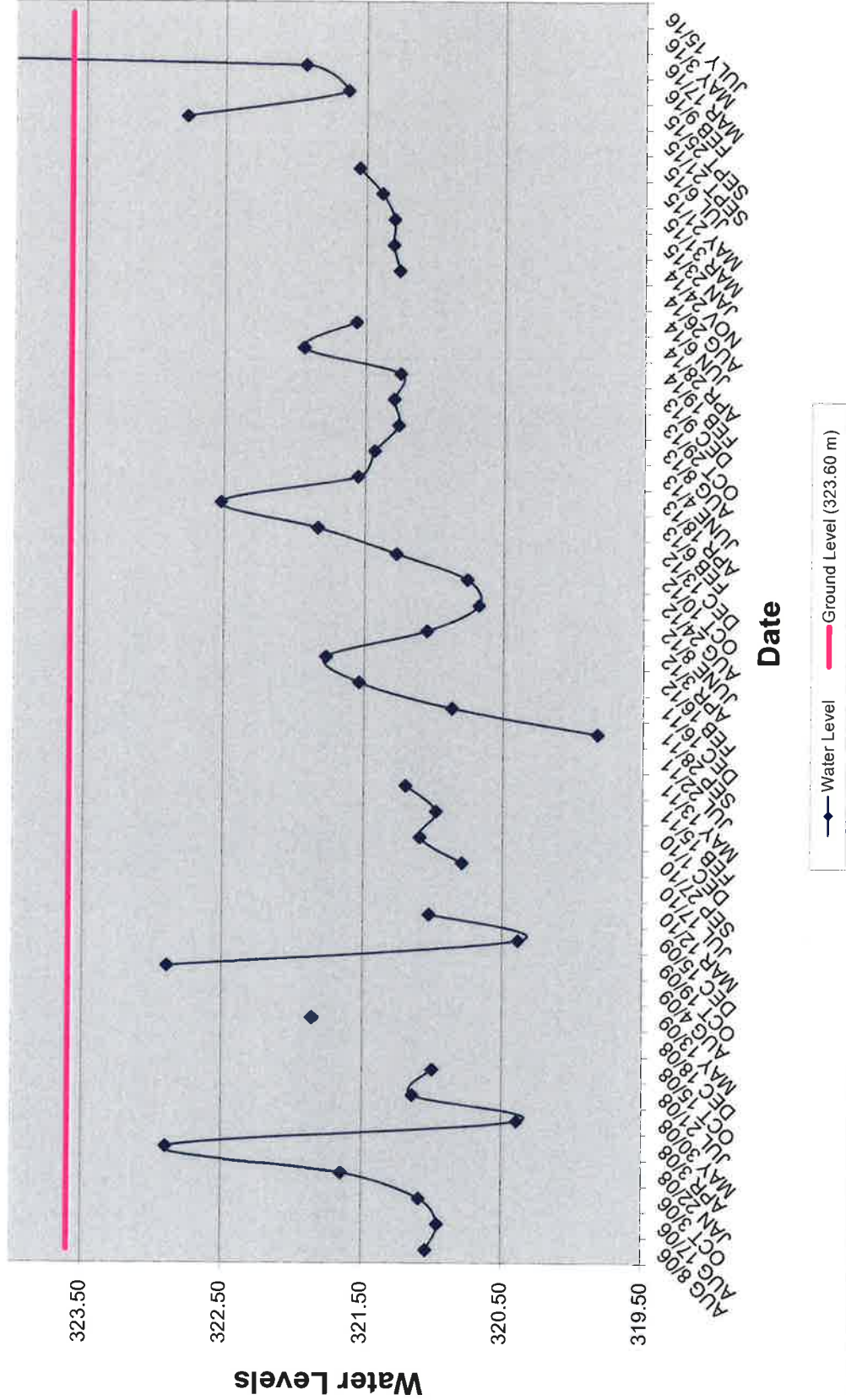
Cityview Ridge Subdivision Monitoring Well BH 108



Cityview Ridge Subdivision Monitoring Well BH 109



Cityview Ridge Subdivision Monitoring Well BH 110



**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “D”

**Hydrogeological Investigation
Banks Groundwater Engineering Limited
(November 2014)**

Technical Memorandum (DRAFT)

 Banks Groundwater Engineering Limited

940 Watson Road South, RR 1 Puslinch, Ontario NOB 2J0

519.829.4808 www.banksgroundwater.ca

17 November 2014

To: Carson Reid – Cityview Ridge Developments Inc.

Copies: Angela Kroetsch – GM BluePlan Engineering Limited
Mirek Sharp – North-South Environmental Inc.
Nancy Shoemaker – Black, Shoemaker, Robinson & Donaldson Limited

From: Bill Banks

Re: Hydrogeological Investigation
Environmental Impact Study
Proposed Cityview Ridge Development, City of Guelph

1 Introduction

This Technical Memorandum presents the updated results of a hydrogeological investigation completed for this proposed development. The site is located immediately northwest of the intersection of York Road and Watson Parkway, adjacent to Cityview Drive, and north of the Canadian National Railway, in the City of Guelph.

The results of the hydrogeological investigation have been updated to include additional groundwater monitoring conducted on-site from December 2012 to October 2014. This investigation was also completed to support pre- and post-development water balance calculations, by providing estimates of current on-site infiltration of precipitation and groundwater discharge to an on-site wetland and adjacent creek. The results and the interpretation of hydrogeological conditions are provided for inclusion or reference in an Environmental Impact Study (EIS) for this proposed development. The hydrogeological investigation included the following tasks:

- ▼ Review of available information including: draft site plan, previous geotechnical investigation data, published geology maps and reports, City of Guelph groundwater study reports, aerial photography, wetland mapping and analyses, and stormwater management plans
- ▼ Site reconnaissance
- ▼ Initial installation of shallow piezometers in 2009 at three locations adjacent to an on-site wetland and creek, and the subsequent installation in 2012 of shallow piezometers at one additional location adjacent to the on-site wetland
- ▼ Initial short-term monitoring of groundwater levels in 2009 to determine hydraulic gradients and evaluate groundwater flows to the on-site wetland and adjacent creek
- ▼ Subsequent longer-term monitoring of groundwater levels in shallow piezometers to assess seasonal variations in groundwater discharge to the on-site wetland and adjacent creek
- ▼ Monitoring of groundwater levels in existing on-site monitoring wells
- ▼ Analysis of the results of the background review, groundwater monitoring and the local hydrogeological conditions

- ▼ Analysis of groundwater levels to establish depths to water table, directions and rates of groundwater flow, the need for stormwater management systems, and the interaction of groundwater and the wetland
- ▼ Consideration and evaluation of source water protection related to City of Guelph municipal wells.

Presented below is a summary of the geology and hydrogeology of the area in which the site is located, followed by the results of the groundwater monitoring, and analysis of groundwater recharge and discharge in relation to the wetland.

2 Surficial Geology

The study site is situated within the Guelph Drumlin Fields physiographic region, as defined by Chapman and Putnam (1984). The Guelph Drumlin Field consists of a series of northwest-southeast trending drumlins that are regionally situated to the northwest of the Paris Moraine. The drumlins are characterized by a series of elongated oval-shaped hills. The topography of the local area is dominated by three closely-spaced drumlins. The proposed residential development area of the site is located on the southern end of the middle drumlin. The eastern part of the site encompasses the slope of the drumlin and lower lying areas. Multiple residential development is proposed for the easternmost part of the site adjacent to Watson Parkway North.

The drumlins in the Guelph Drumlin Field are comprised of a sandy facies (up to 40 percent sand) of the Port Stanley Till, which is typically a silt to sandy silt till (Karrow, 1968, 1987). Overburden thickness is more than 30 m at the highest elevation of the drumlins. The overburden deposits in the lower areas comprise a series of terraced deposits of glacial outwash (sand and gravel) and lacustrine (sand) materials. The overburden thins to less than 4 m in the lower-lying areas. Wetland areas are generally found associated with the glacial outwash deposits within these lower lying areas. A wetland occurs in the south-eastern area of the site at the base of the drumlin, and is interpreted to drain to the adjacent Clyde Creek.

The results of a previous geotechnical investigation of this site, which included drilling and soil sampling at 10 locations on-site, confirmed the shallow soils on the drumlin comprise a sandy silt till and the shallow soils in the eastern part of the site comprise sand and gravel (Naylor Engineering Associates, 2006).

3 Overburden Hydrogeology

Groundwater occurs within the bedrock formations and overburden deposits throughout the region and flows horizontally and vertically under hydraulic gradients. The rate of groundwater flow is dependent on the hydraulic conductivity of the deposits and formations, as well as the magnitude of the local and regional hydraulic gradients. The rate of groundwater flow is typically very slow relative to the flow of surface water in creeks, streams, and rivers.

Groundwater flow in the local area is interpreted to be southerly towards discharge to the Eramosa River, which is about 700 metres south of the site. A component of localized groundwater flow on-site is expected to be south-easterly towards discharge to the wetland and Clyde Creek.

Drumlins comprising a silt to sandy silt glacial till typically have limited intergranular porosity and hydraulic conductivity. These deposits do not transmit water readily and will likely act to limit the flow of groundwater. The logs of the eight boreholes drilled on the drumlin indicate the sandy silt till increased in density with depth, with borehole depths ranging from 5.7 to 11.1 metres. Given the characteristics of the drumlin at this site it is interpreted that a limited amount of precipitation infiltrates in the upland portion and to a lesser extent along the slopes. This infiltration would recharge the local groundwater system, but it is expected that most of this shallow groundwater would flow towards the sand and gravel deposits situated around the southerly and easterly base

of the drumlin. Infiltration in the area of the sand and gravel surficial deposits would be significantly greater. Groundwater flow in the sand and gravel deposits on-site is interpreted to be southerly towards discharge to the wetland and Clythe Creek. Groundwater seeps (i.e. surface discharge areas) were observed at several locations up-gradient of the wetland.

4 Groundwater Monitoring

4.1 Wetland Piezometers (2009)

To confirm the occurrence of groundwater flow and discharge to the wetland located in the southeast area of the site, shallow piezometers were installed at two locations (Refer to Plates 1 and 2). Shallow piezometers were also installed at a third location to determine if shallow groundwater discharge was occurring adjacent to Clythe Creek along the southern boundary of the site (Refer to Plate 3). The locations were selected during a site reconnaissance in early May 2009, when the groundwater seeps were visible and the area upgradient of the wetland was saturated.

At each site the piezometers were installed in pairs, with one set at a shallow depth (about 0.5 m) and another at an intermediate depth (about 1.1 m), to provide for measurement of the vertical hydraulic gradient at various times. Groundwater levels were measured in each piezometer and recorded relative to adjacent ground surface on three occasions: 13 and 25 May, and 4 June 2009.



Plate 1: Piezometer Station 1



Plate 2: Piezometer Station 2

On each occasion the monitoring at Stations 1 and 2 confirmed groundwater discharge conditions adjacent to the wetland and upgradient. Confirmation of local groundwater discharge to the wetland is based on the observation of groundwater seeps along the upgradient slope on the north edge of the wetland on each monitoring occasion. Shallow groundwater flow to the wetland is also confirmed by the groundwater levels in piezometers that were observed at or just above ground surface. On these three monitoring occasions a downward gradient was observed, as the groundwater level in the intermediate piezometer was below the adjacent groundwater level in the shallow piezometer.

This initial short-term monitoring indicated that the upgradient groundwater seeps, combined with shallow groundwater flow along the fringe of the wetland are important in terms of maintaining water levels in the wetland. These observations demonstrated the wetland's dependence on groundwater flow during this brief monitoring period.



Plate 3: Piezometer Station 3

The third pair of shallow piezometers located along the southern edge of the site, just west of the Clyde Creek culvert under the railway, indicated groundwater was at a depth of 1.2 m on 13 May, but declined below the intermediate piezometer soon after. The shallow piezometer was dry on each occasion. The monitoring confirmed there was no shallow groundwater discharge at this location on these occasions. It is considered possible that groundwater is discharging directly to Clyde Creek in this area.

These monitoring results confirmed that the shallow groundwater system was discharging to the wetland along the base of the drumlin during the mid- to late-spring 2009 monitoring period. It is expected that these conditions occur each spring; however, due to the limited period of monitoring it was uncertain if these discharge conditions continue during drier seasonal periods.

4.2 Wetland Piezometers (2012 - 2014)

In recognition of the need for seasonal monitoring of groundwater levels and discharge to the wetland, a second period of monitoring was initiated in December 2012. Prior to the start of this monitoring, another pair of shallow piezometers was installed at a third location that was at the edge of the wetland and downgradient of a groundwater seep area. Plate 4 is a photograph of Station 4 in December 2012. The groundwater discharge in this area is visible where the warmer groundwater is melting the recently-fallen snow. The approximate locations of the three piezometer stations are shown in the appended Figure 1.



Plate 4: Piezometer Station 4

Groundwater levels were then measured and recorded in piezometers at Stations 1, 2 and 4 on 14 December 2012. The groundwater in piezometers is typically frozen in January and February, and therefore was not measured during these months in 2013. Monitoring resumed on 15 March 2013 and continued on a monthly basis until 12 December 2013. During 2014 monitoring occurred in April, July and October. The groundwater monitoring data and discharge observations for 2009 and 2012 to 2014 are summarized in the appended Table 1.

Groundwater level monitoring and discharge observations from December 2012 to October 2014 confirmed that groundwater levels in the shallow piezometers were close to, and on some occasions above, ground surface. This confirmed that groundwater was flowing toward and discharging into the wetland on all monitoring occasions. Without continuous monitoring it cannot be concluded that discharge was constant; however, observations made during months with below-average precipitation during 2013 (i.e. March, May, August, September, November and December) confirmed discharge was occurring during "drier" periods. The quarterly monitoring events in 2014 occurred during months of above-average total precipitation, thus resulting in higher groundwater levels and flow conditions.

4.3 Monitoring Wells

Groundwater levels were also measured in each of the 10 on-site monitoring wells on 13 May 2009, for the purpose of assessing horizontal and vertical flow directions. At five locations pairs of monitoring wells were installed in the same borehole to provide for measurement of the vertical hydraulic gradient at various times. Groundwater elevations were representative of spring levels, with depths to groundwater ranging from 0.5 to 1.6 metres below ground surface in the seven shallow monitors (i.e. completed at depths less than 4.0 m). Groundwater levels ranged from 0.5 to 6.8 metres below ground surface in the eight deeper monitors. The lowest groundwater elevation occurred in the central part of the site in the deepest monitor, which is completed at a depth of about 10 metres at the crest of the southern slope of the drumlin.

Groundwater elevations in the shallow monitors confirm groundwater flow directions are radial from the top of the drumlin towards the base (i.e. ranging from southwest to east). A comparison of shallow and deeper groundwater elevations indicates a downward hydraulic gradient in the drumlin, as would be expected.

5 Groundwater Recharge and Discharge

Based on a review of local geology and hydrogeology and the results of the shallow groundwater monitoring, it is evident that there is limited groundwater recharge on the drumlin that dominates much of the site. It is interpreted that the rate of groundwater recharge and flow is more significant in the lower-lying, eastern part of the site, where the outwash sand and gravel deposit occurs at surface. The limited amount of groundwater that discharges along the eastern base of the drumlin likely flows through the outwash deposit, eventually discharging into the on-site wetland. It is further interpreted that a portion of the surface water runoff from up the slope and on the top of the drumlin also flows to the wetland.

The average annual precipitation has been estimated from an averaging of precipitation normals from meteorological stations in Guelph and the surrounding area, for the period 1981 to 2010. The average annual precipitation, for the area in which the study site is located, is estimated to be about 925 mm. It has also been estimated that the average annual evapotranspiration for this area is about 555 mm; however, evapotranspiration rates across a site will vary in relation to the depth to water table, soil texture, topography, extent of vegetation cover, and type of vegetation. Based on the results of research conducted in other parts of the Eramosa River and Speed River subwatersheds, estimates of evapotranspiration rates can be made for this site. It is estimated that evapotranspiration rates on the drumlin will average about 555 mm/year, whereas in the well-drained outwash sand and gravel deposit the rate is estimated to be about 495 mm/year. The net water available for infiltration and surface runoff is 370 mm on the drumlin and 430 mm in the sand and gravel area, on an annual average basis.

For the purpose of estimating recharge to the groundwater system, on and adjacent to the drumlin, that maintains discharge to the wetland, it is estimated that the average annual groundwater recharge on the drumlin under current conditions is 180 mm. The remaining 190 mm is the average annual surface runoff. These estimates are based on previous analyses completed for developments in Guelph where drumlins exist. The average annual rate of recharge in the eastern sand and gravel area is estimated to be as high as 380 mm, with the remaining 50 mm allocated to surface runoff.

The total area of the subject lands comprises 17.682 ha. However, a total area of 18.28 ha has been used for the purposes of a water budget, which includes the southern section of Cityview Drive. Reference should be made to the site description and maps included in the Preliminary Servicing and Stormwater Management Report (Gamsby and Mannerow Limited, 2012). The western and central parts of the development site (i.e. on top of the drumlins and on the western slope, which includes Catchments 10 and 20 of the existing conditions drainage area) represents an area of 11.80 ha. Accounting for no infiltration on a 0.56 ha impervious area within this part of the site, the average annual rate of recharge on this part of the site under existing conditions is estimated to be 20 230 m³/year. It is interpreted that the recharge in this part of the site maintains local groundwater levels and groundwater flow in the overburden deposits in a southerly direction from the site.

The eastern 6.48 ha of the site (i.e. Catchment 30 of the existing conditions drainage area) comprises an area of about 2.1 ha along the eastern slope of the drumlin and about 4.38 ha in the sand and gravel outwash deposit area. Accounting for these areas and the differences in surficial soil types and slopes, the average annual rate of recharge in the eastern part of the site is estimated to be 20 420 m³/year. It is interpreted that much of the recharge occurring in the eastern part of the site would maintain the shallow groundwater discharging to the wetland and Clyde Creek. The net total recharge for the site under existing conditions is therefore estimated to be about 40 650 m³/year.

Surface water runoff onsite under existing conditions is estimated to be about 31 600 m³/year, of which 25 420 m³/year occurs in the western and central parts of the site (i.e. Catchments 10 and 20), and 6 180 m³/year occurs in the eastern part of the site (i.e. Catchment 30).

It is anticipated that a monthly water budget under existing conditions will be requested by the City of Guelph at a later stage in the review/approval process. This will provide a comparison of pre- and post-development monthly and annual rates of recharge and runoff, that will be based on the stormwater management systems proposed for this site.

6 Stormwater Management

It is understood that stormwater management facilities will be designed to manage surface water runoff in the developed areas of the site (i.e. post-development catchments 100, 201, and 202). Based on the proposed development plan, groundwater recharge and surface water runoff on the eastern slope of the drumlin and within the eastern part of the site are expected to remain unchanged following development. The multiple residential development within a 0.68 ha area of the north-eastern part of the site will require separate stormwater management facilities designed to maintain the current rate of groundwater recharge in this area that will contribute to discharge to the wetland located on-site and to Clythe Creek.

The remaining part of the eastern low-lying area is to remain in the current natural state and it is expected that stormwater management in this area is not required. It can therefore be concluded that surface water runoff and shallow groundwater flow in the undeveloped area will continue to contribute to the maintenance of the wetland and flow in Clythe Creek.

7 Future Groundwater Monitoring

An on-site groundwater monitoring program is recommended to assess changes in groundwater elevations and quality during and following development of the site, as well as to assess the performance of the stormwater management facilities. The locations for groundwater monitoring would be established during preparation of the Environmental Implementation Report for review and consideration by City of Guelph staff.

Initially, groundwater levels should be monitored on a quarterly basis at a minimum in all available on-site monitoring wells before and, where possible, during grading of the site. The preferred monitoring periods would be January, April, July and October. Groundwater samples should be collected each spring and analyzed for general chemical parameters. Similar to other local sites, monitoring of groundwater levels and quality should continue for a period of up to two years following 75 percent completion of the development.

A review of the Ontario Ministry of the Environment on-line well record information service indicates there are (or were) several private water supply wells located in the vicinity of the site. The records for wells in this local area indicate each well has been completed in, and derives its' water supply from, the underlying bedrock aquifer. The records indicate the overburden in this area ranges in thickness from less than 10 m to more than 30 m, and wells are completed at depths ranging from about 20 m to more than 60 m below ground surface. If any of these wells are currently in use, the quantity and quality of water obtained from each well should not be affected by the proposed development, as groundwater flow in the overburden beneath the site is to the south and southeast. It is also noted that a number of water supply wells have been decommissioned and presumably residents are now obtaining their water from the municipal supply system.

If concerns are expressed by well owners regarding the potential for changes in quality and/or quantity of their water supply, baseline testing could be conducted before grading begins on the development site. This would provide background data that could be referenced in the event a well owner indicates they believe their water supply has been affected either during, or following,

development in this area. Municipal water supply is available to all local residences and businesses within this part of the City of Guelph. If it were confirmed that the water quality and/or quantity available from a private well was detrimentally affected by local land development, a municipal water supply could be readily provided.

8 Source Water Protection

The Grand River Source Protection Area Approved Assessment Report (Lake Erie Region Source Protection Committee, 2012) includes mapping of Wellhead Protection Areas (WHPA) and Groundwater Vulnerability for the City of Guelph Municipal Well System. There are currently several municipal wells in the northeast part of Guelph and the mapping indicates part of the proposed residential development site is located within the WHPA-B zone (i.e. 2-year time-of-travel capture zone) for one or more of these wells. The Groundwater Vulnerability mapping indicates the site is located in an area with a vulnerability score that ranges from a value of 6 (i.e. medium) to a value of 10 (i.e. the highest value). It is therefore apparent that there may be source water protection implications related to this proposed development.

Proposed Source Protection Policies have been developed by the City of Guelph and submitted for approval by the Ontario Ministry of the Environment. Once approved (likely in 2015), the requirements of these policies can be expected to apply to this site. Various measures may be required to manage the risk of potential threats to groundwater quality, such as on-going educational measures directed at residents regarding the Province's ban on the use of cosmetic pesticides.

9 Summary

On the basis of an assessment of current site conditions, the net total average annual, pre-development, groundwater recharge for the site is estimated to be about 40 650 m³/year. It is estimated that the average annual rate of recharge to the groundwater system in the western and central parts of the site, comprising an area of 11.80 ha (i.e. Catchments 10 and 20), is 20 230 m³/year. It is also estimated that the average annual rate of recharge to the groundwater system in the eastern 6.48 ha of the site, including part of the eastern slope of the drumlin (i.e. Catchment 30), is 20 420 m³/year.

It is interpreted that much of the recharge in the eastern area currently maintains the shallow groundwater discharging to the wetland and Clyde Creek occurring in the south-eastern part of the site. Under the proposed development, only a limited area along the top of the eastern slope of the drumlin will be developed for residential use and most of this area will comprise rear yards. Groundwater recharge along most of the eastern slope of the drumlin is expected to remain unchanged. Groundwater recharge within the remaining eastern part of the site should also remain unchanged as much of this area will not be developed.

The proposed multiple residential lands within a 0.68 ha area of the north-eastern part of the site will require stormwater management facilities designed to maintain the current rate of groundwater recharge in this area. Groundwater discharge to the wetland located on-site and to Clyde Creek should therefore continue to be maintained following the proposed development of this site. It is anticipated that a monthly water budget under existing conditions will be requested by the City of Guelph at a later stage in the review/approval process. This will provide a comparison of pre- and post-development monthly and annual rates of recharge and runoff, that will be based on the stormwater management systems proposed for this site.

An on-site groundwater monitoring program is recommended to assess any changes in groundwater elevations and quality during and following development of the site, as well as to assess the performance of the stormwater management facilities. The locations for groundwater

monitoring would be established during preparation of the Environmental Implementation Report for review and consideration by City of Guelph staff.

There may be several private water supply wells located in the vicinity of the site. If concerns are expressed by well owners regarding the potential for changes in quality and/or quantity of their water supply, baseline testing could be conducted before grading begins on the development site. This would provide background data that could be referenced in the event a well owner indicates they believe their water supply has been affected either during, or following, development in this area. Municipal water supply is available to all local residences and businesses within this part of the City of Guelph.

Based on recent Source Water Protection mapping for the City of Guelph municipal well system, it is apparent that there may be source water protection implications related to this proposed development. Once Source Protection Policies are approved in the coming year, various measures may be required to manage the risk of potential threats to groundwater quality, and these will be explored as part of the detailed Environmental Implementation Report.

10 References

- Chapman, L. J. and D.F. Putnam. 1984. The Physiography of Southern Ontario. Ontario Geological Survey.
- Gamsby and Mannerow Limited. 2012. Preliminary Servicing and Stormwater Management Report, Cityview Ridge Subdivision, City of Guelph.
- Lake Erie Region Source Protection Committee. 2012. Grand River Source Protection Area Approved Assessment Report. Chapter 8, City of Guelph.
- Karrow, P.F. 1968. Pleistocene Geology of the Guelph Area. Ontario Department of Mines, Geological Report 61.
- Karrow, P.F. 1987. Quaternary Geology of the Hamilton-Cambridge Area, Southern Ontario. Ministry of Northern Development and Mines, Ontario Geological Survey Report 255.
- Naylor Engineering Associates Ltd. 2006 (Revised 2012). Geotechnical Investigation, P.T. Valeriotte Subdivision, Cityview Drive, Guelph, Ontario, for Carson Reid Homes Ltd.

Respectfully submitted,
Banks Groundwater Engineering Limited

final version to be signed by:

William D. Banks, P.Eng.
Principal Hydrogeologist

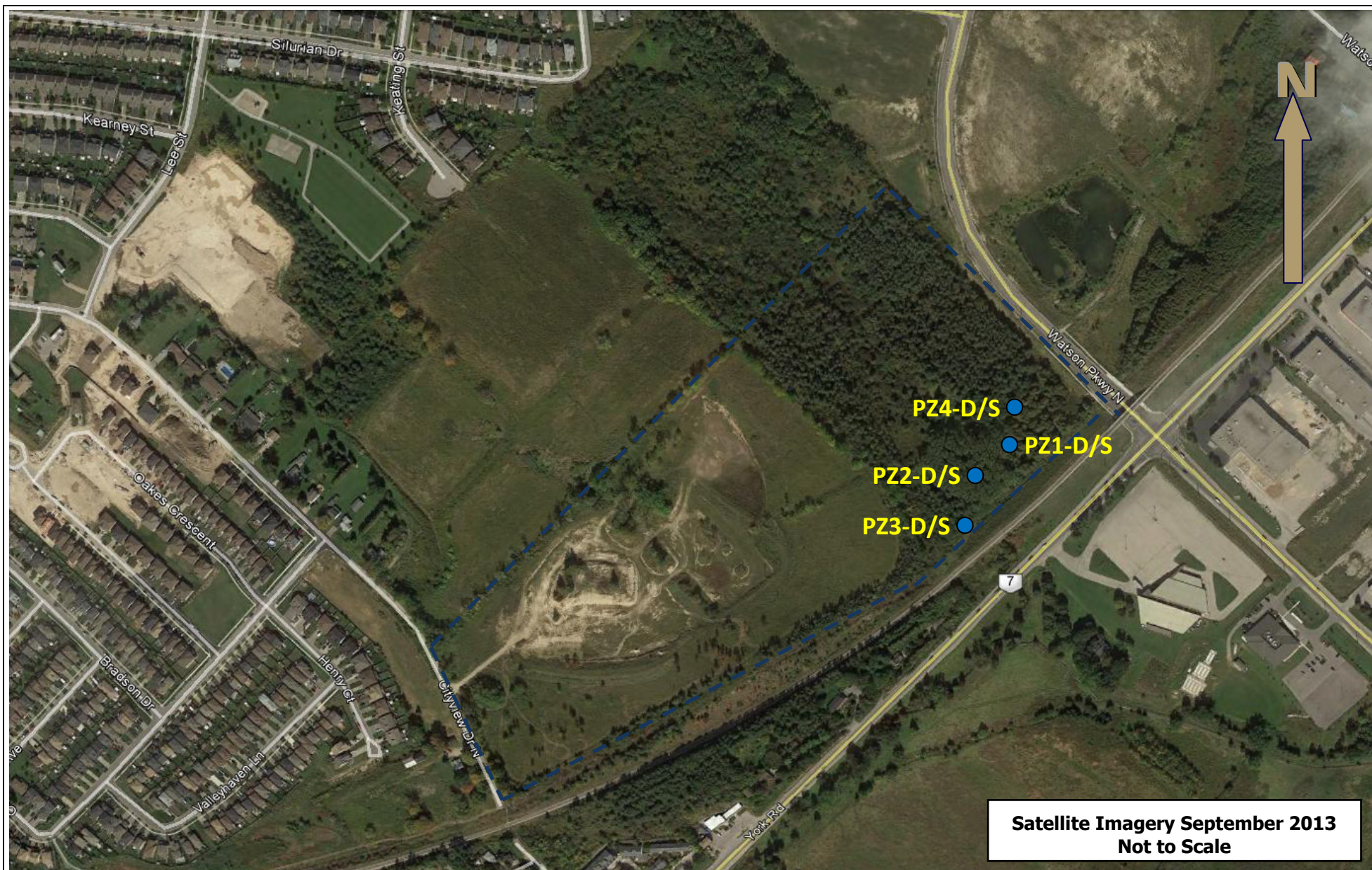


Table 1: Groundwater Levels Measured (metres below ground level*)

Date	PZ1-D	PZ1-S	PZ2-D	PZ2-S	PZ3-D	PZ3-S	PZ4-D	PZ4-S	Groundwater Discharge Observations
13-May-09	0.03	0.08	0.90	0.01	0.95	dry	-	-	low to moderate flow from seeps
25-May-09	0.01	-0.01	0.75	0.02	1.10	dry	-	-	low to moderate flow from seeps
04-Jun-09	0.01	-0.01	0.69	0.05	dry	dry	-	-	low to moderate flow from seeps
14-Dec-12	0.04	0.07	0.26	0.10	-	-	-0.07	-0.04	low to moderate flow from seeps
15-Mar-13	0.00	0.02	0.24	0.06	-	-	-0.11	-0.04	higher flows from seeps
26-Apr-13	0.00	0.02	0.23	0.06	-	-	-0.10	-0.04	higher flows from seeps
15-May-13	0.01	0.01	0.23	0.06	-	-	-0.09	-0.03	moderate flow from seeps
11-Jun-13	0.01	0.00	0.23	0.07	-	-	-0.08	-0.03	low to moderate flow from seeps
11-Jul-13	0.00	0.00	0.22	0.08	-	-	-0.09	-0.03	higher flows from seeps
09-Aug-13	0.00	0.00	0.22	0.04	-	-	-0.08	-0.02	low to moderate flow from seeps
09-Sep-13	0.01	0.00	0.20	0.06	-	-	-0.06	-0.02	lower flow from seeps
08-Oct-13	0.01	-0.01	0.20	0.05	-	-	-0.07	-0.02	lower flow from seeps
14-Nov-13	0.00	-0.02	0.20	0.06	-	-	-0.06	-0.02	low to moderate flow from seeps
12-Dec-13	0.01	-0.01	0.21	0.06	-	-	-0.06	-0.02	low to moderate flow from seeps
30-Apr-14	0.02	0.04	0.19	0.04	-	-	-0.09	-0.02	higher flows from seeps
16-Jul-14	0.03	0.04	0.18	0.08	-	-	-0.06	-0.01	very low flow from seeps
23-Oct-14	0.02	0.03	0.18	0.05	-	-	-0.07	-0.01	moderate flow from seeps

* negative values indicate groundwater above ground level

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “E”

STORMWATER MANAGEMENT ANALYSIS

- **Existing Condition Modelling Files**
 - **Hadati Creek Allowable Modelling Files**
 - **Figure No. 8 – Hadati Creek Modelling Schematic**
 - **Hadati Creek Post-Development Modelling Files
(Western Portion of Cityview Ridge Subdivision)**
 - **Post Development Uncontrolled Condition Modelling
Files (Eastern Portion of Cityview Ridge Subdivision)**
 - **Stage/Storage/Discharge Tables**
 - **Post Development Controlled Condition Modelling Files
(Eastern Portion of Cityview Ridge Subdivision)**
 - **Cooling Trench Calculations**
 - **Forebay Calculations**
 - **Oil/Grit Separator Sizing Calculations**
-


```

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"    1500.000 Max. Hydrograph"
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"      6.000 Constant B"
"      0.799 Exponent C"
"      0.400 Fraction R"
"     170.000 Duration"
"      1.000 Time step multiplier"
"      Maximum intensity        105.606 mm/hr"
"      Total depth              33.816 mm"
"      6 002hyd Hydrograph extension used in this file"
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"      1 Triangular scs"
"      1 Equal length"
"      2 Horton equation"
"     10 Catchment 10 - To Hadati Creek"
"      8.000 % Impervious"
"      7.020 Total Area"
"     45.000 Flow length"
"      2.000 Overland slope"
"      6.458 Pervious Area"
"     45.000 Pervious length"
"      2.000 Pervious slope"
"      0.562 Impervious Area"
"     45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"     75.000 Pervious Max.infiltration"
"     12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"              0.130      0.000      0.000      0.000 c.m/sec"
"      Catchment 10      Pervious      Impervious      Total Area "
"      Surface Area      6.458      0.562      7.020      hectare"
"      Time of concentration      28.300      2.768      13.823      minutes"
"      Time to Centroid      98.613      85.041      90.917      minutes"
"      Rainfall depth      33.816      33.816      33.816      mm"
"      Rainfall volume      2183.97      189.91      2373.88      c.m"
"      Rainfall losses      31.709      2.082      29.339      mm"
"      Runoff depth      2.107      31.734      4.477      mm"
"      Runoff volume      136.09      178.22      314.31      c.m"
"      Runoff coefficient      0.000      0.000      0.000      "
"      Maximum flow      0.073      0.119      0.130      c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "

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"	6	Combine "		
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"	Hydrograph volume	314.307	c.m"	
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"	1	Triangular SCS"		
"	1	Equal length"		
"	2	Horton equation"		
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"	4.780	Total Area"		
"	45.000	Flow length"		
"	2.000	Overland slope"		
"	4.780	Pervious Area"		
"	45.000	Pervious length"		
"	2.000	Pervious slope"		
"	0.000	Impervious Area"		
"	45.000	Impervious length"		
"	2.000	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious Max.infiltration"		
"	12.500	Pervious Min.infiltration"		
"	0.250	Pervious Lag constant (hours)"		
"	5.000	Pervious Depression storage"		
"	0.015	Impervious Manning 'n'"		
"	0.000	Impervious Max.infiltration"		
"	0.000	Impervious Min.infiltration"		
"	0.050	Impervious Lag constant (hours)"		
"	1.500	Impervious Depression storage"		
"	0.054	0.000	0.130	0.130 c.m/sec"
"	Catchment 20	Pervious	Impervious	Total Area "
"	Surface Area	4.780	0.000	4.780 hectare"
"	Time of concentration	28.300	2.768	28.300 minutes"
"	Time to Centroid	98.613	85.041	98.613 minutes"
"	Rainfall depth	33.816	33.816	33.816 mm"
"	Rainfall volume	1616.40	0.00	1616.40 c.m"
"	Rainfall losses	31.709	2.082	31.709 mm"
"	Runoff depth	2.107	31.734	2.107 mm"
"	Runoff volume	100.72	0.00	100.72 c.m"
"	Runoff coefficient	0.000	0.000	0.000 "
"	Maximum flow	0.054	0.000	0.054 c.m/sec"
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"	4	Add Runoff "		
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"	1	Triangular SCS"		
"	1	Equal length"		
"	2	Horton equation"		
"	30	Catchment 30 - To Clythe Creek"		
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"	6.480	Total Area"		
"	45.000	Flow length"		
"	2.000	Overland slope"		


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" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
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" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      0.073      0.054      0.130      0.130 c.m/sec"
"      Catchment 30      Pervious      Impervious      Total Area "
"      Surface Area      6.480      0.000      6.480      hectare"
"      Time of concentration      28.300      2.768      28.300      minutes"
"      Time to Centroid      98.613      85.041      98.613      minutes"
"      Rainfall depth      33.816      33.816      33.816      mm"
"      Rainfall volume      2191.27      0.00      2191.27      c.m"
"      Rainfall losses      31.709      2.082      31.709      mm"
"      Runoff depth      2.107      31.734      2.107      mm"
"      Runoff volume      136.54      0.00      136.55      c.m"
"      Runoff coefficient      0.000      0.000      0.000      "
"      Maximum flow      0.073      0.000      0.073      c.m/sec"
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" 8 Copy to Outflow"
"      0.073      0.127      0.127      0.130"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
"      Total Discharge"
"      Maximum flow      0.220      c.m/sec"
"      Hydrograph volume      551.577      c.m"
"      0.073      0.127      0.127      0.220"
" 40 HYDROGRAPH Confluence 1"
" 7 Confluence "
" 1 Node #"
"      Total Discharge"
"      Maximum flow      0.220      c.m/sec"
"      Hydrograph volume      551.577      c.m"
"      0.073      0.220      0.127      0.000"
" 38 START/RE-START TOTALS 1"
" 3 Runoff Totals on EXIT"
"      Total Catchment area      18.280      hectare"
"      Total Impervious area      0.562      hectare"
"      Total % impervious      3.072"
" 19 EXIT"

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"      2 Horton equation"
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"      8.000 % Impervious"
"      7.020 Total Area"
"     45.000 Flow length"
"      2.000 Overland slope"
"      6.458 Pervious Area"
"     45.000 Pervious length"
"      2.000 Pervious slope"
"      0.562 Impervious Area"
"     45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"     75.000 Pervious Max.infiltration"
"     12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"          0.492      0.000      0.000      0.000 c.m/sec"
"      Catchment 10 Pervious Impervious Total Area "
"      Surface Area      6.458      0.562      7.020 hectare"
"      Time of concentration 19.590      2.510      15.110 minutes"
"      Time to Centroid 92.382      83.161      89.963 minutes"
"      Rainfall depth 46.775      46.775      46.775 mm"
"      Rainfall volume 3020.92      262.69      3283.61 c.m"
"      Rainfall losses 35.903      2.312      33.216 mm"
"      Runoff depth 10.872      44.463      13.559 mm"
"      Runoff volume 702.15      249.70      951.85 c.m"
"      Runoff coefficient 0.000      0.000      0.000 "
"      Maximum flow 0.443      0.162      0.492 c.m/sec"
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"      4 Add Runoff "

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"	Hydrograph volume	951.854	c.m"	
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"	2.000	Overland slope"		
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"	2.000	Pervious slope"		
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"	45.000	Impervious length"		
"	2.000	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious Max.infiltration"		
"	12.500	Pervious Min.infiltration"		
"	0.250	Pervious Lag constant (hours)"		
"	5.000	Pervious Depression storage"		
"	0.015	Impervious Manning 'n'"		
"	0.000	Impervious Max.infiltration"		
"	0.000	Impervious Min.infiltration"		
"	0.050	Impervious Lag constant (hours)"		
"	1.500	Impervious Depression storage"		
"	0.328	0.000	0.492	0.492 c.m/sec"
"	Catchment 20	Pervious	Impervious	Total Area "
"	Surface Area	4.780	0.000	4.780 hectare"
"	Time of concentration	19.590	2.510	19.590 minutes"
"	Time to Centroid	92.382	83.161	92.382 minutes"
"	Rainfall depth	46.775	46.775	46.775 mm"
"	Rainfall volume	2235.84	0.00	2235.85 c.m"
"	Rainfall losses	35.903	2.312	35.903 mm"
"	Runoff depth	10.872	44.463	10.872 mm"
"	Runoff volume	519.68	0.00	519.68 c.m"
"	Runoff coefficient	0.000	0.000	0.000 "
"	Maximum flow	0.328	0.000	0.328 c.m/sec"
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"	1	Equal length"		
"	2	Horton equation"		
"	30	Catchment 30 - To Clythe Creek"		
"	0.000	% Impervious"		
"	6.480	Total Area"		
"	45.000	Flow length"		
"	2.000	Overland slope"		

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"                                     105172 Ex Cond 5year
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"      45.000 Pervious length"
"      2.000  Pervious slope"
"      0.000  Impervious Area"
"      45.000 Impervious length"
"      2.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250  Pervious Lag constant (hours)"
"      5.000  Pervious Depression storage"
"      0.015  Impervious Manning 'n'"
"      0.000  Impervious Max.infiltration"
"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"      0.444      0.328      0.492      0.492 c.m/sec"
"      Catchment 30      Pervious      Impervious      Total Area "
"      Surface Area      6.480      0.000      6.480      hectare"
"      Time of concentration 19.590      2.510      19.590      minutes"
"      Time to Centroid      92.382      83.161      92.382      minutes"
"      Rainfall depth      46.775      46.775      46.775      mm"
"      Rainfall volume      3031.02      0.00      3031.02      c.m"
"      Rainfall losses      35.903      2.312      35.903      mm"
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"      Runoff volume      704.50      0.00      704.50      c.m"
"      Runoff coefficient      0.000      0.000      0.000      "
"      Maximum flow      0.444      0.000      0.444      c.m/sec"
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"      4      Add Runoff "
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"      8      Copy to Outflow"
"      0.444      0.772      0.772      0.492"
" 40      HYDROGRAPH Combine 1"
"      6      Combine "
"      1      Node #"
"      Total Discharge"
"      Maximum flow      1.265      c.m/sec"
"      Hydrograph volume      2176.031      c.m"
"      0.444      0.772      0.772      1.265"
" 40      HYDROGRAPH Confluence 1"
"      7      Confluence "
"      1      Node #"
"      Total Discharge"
"      Maximum flow      1.265      c.m/sec"
"      Hydrograph volume      2176.031      c.m"
"      0.444      1.265      0.772      0.000"
" 38      START/RE-START TOTALS 1"
"      3      Runoff Totals on EXIT"
"      Total Catchment area      18.280      hectare"
"      Total Impervious area      0.562      hectare"
"      Total % impervious      3.072"
" 19      EXIT"

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" Licensee name:                      "
" Company                            Gamsby and Mannerow Limited"
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" 5.000 Time Step"
" 210.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
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" 1 Chicago storm"
" 3158.000 Coefficient A"
" 15.000 Constant B"
" 0.936 Exponent C"
" 0.400 Fraction R"
" 210.000 Duration"
" 1.000 Time step multiplier"
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" Total depth                          69.476 mm"
" 6 025hyd Hydrograph extension used in this file"
" 33 CATCHMENT 10"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 10 Catchment 10 - To Hadati Creek"
" 8.000 % Impervious"
" 7.020 Total Area"
" 45.000 Flow length"
" 2.000 Overland slope"
" 6.458 Pervious Area"
" 45.000 Pervious length"
" 2.000 Pervious slope"
" 0.562 Impervious Area"
" 45.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.344 0.000 0.000 0.000 c.m/sec"
" Catchment 10 Pervious Impervious Total Area "
" Surface Area 6.458 0.562 7.020 hectare"
" Time of concentration 14.371 2.291 12.330 minutes"
" Time to Centroid 105.688 98.958 104.551 minutes"
" Rainfall depth 69.476 69.476 69.476 mm"
" Rainfall volume 4487.06 390.18 4877.24 c.m"
" Rainfall losses 40.830 2.498 37.763 mm"
" Runoff depth 28.647 66.978 31.713 mm"
" Runoff volume 1850.11 376.15 2226.26 c.m"
" Runoff coefficient 0.000 0.000 0.000 "
" Maximum flow 1.257 0.234 1.344 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "

```

		105172 Ex Cond 25year		
"	1.344	1.344	0.000	0.000"
" 40	HYDROGRAPH Copy to Outflow"			
"	8	Copy to Outflow"		
"	1.344	1.344	1.344	0.000"
" 40	HYDROGRAPH " Combine 1"			
"	6	Combine "		
"	1	Node #"		
"	Total Discharge"			
"	Maximum flow	1.344	c.m/sec"	
"	Hydrograph volume	2226.261	c.m"	
"	1.344	1.344	1.344	1.344"
" 40	HYDROGRAPH Start - New Tributary"			
"	2	Start - New Tributary"		
"	1.344	0.000	1.344	1.344"
" 33	CATCHMENT 20"			
"	1	Triangular SCS"		
"	1	Equal length"		
"	2	Horton equation"		
"	20	Catchment 20 - To Clythe Creeek"		
"	0.000	% Impervious"		
"	4.780	Total Area"		
"	45.000	Flow length"		
"	2.000	Overland Slope"		
"	4.780	Pervious Area"		
"	45.000	Pervious length"		
"	2.000	Pervious slope"		
"	0.000	Impervious Area"		
"	45.000	Impervious length"		
"	2.000	Impervious slope"		
"	0.250	Pervious Manning 'n'"		
"	75.000	Pervious Max.infiltration"		
"	12.500	Pervious Min.infiltration"		
"	0.250	Pervious Lag constant (hours)"		
"	5.000	Pervious Depression storage"		
"	0.015	Impervious Manning 'n'"		
"	0.000	Impervious Max.infiltration"		
"	0.000	Impervious Min.infiltration"		
"	0.050	Impervious Lag constant (hours)"		
"	1.500	Impervious Depression storage"		
"	0.931	0.000	1.344	1.344 c.m/sec"
"	Catchment 20	Pervious	Impervious	Total Area "
"	Surface Area	4.780	0.000	4.780 hectare"
"	Time of concentration	14.371	2.291	14.371 minutes"
"	Time to Centroid	105.688	98.958	105.688 minutes"
"	Rainfall depth	69.476	69.476	69.476 mm"
"	Rainfall volume	3320.97	0.00	3320.97 c.m"
"	Rainfall losses	40.830	2.498	40.830 mm"
"	Runoff depth	28.647	66.978	28.647 mm"
"	Runoff volume	1369.31	0.00	1369.31 c.m"
"	Runoff coefficient	0.000	0.000	0.000 "
"	Maximum flow	0.930	0.000	0.931 c.m/sec"
" 40	HYDROGRAPH Add Runoff "			
"	4	Add Runoff "		
"	0.931	0.931	1.344	1.344"
" 33	CATCHMENT 30"			
"	1	Triangular SCS"		
"	1	Equal length"		
"	2	Horton equation"		
"	30	Catchment 30 - To Clythe Creek"		
"	0.000	% Impervious"		
"	6.480	Total Area"		
"	45.000	Flow length"		
"	2.000	overland Slope"		


```

"                                     105172 Ex Cond 25year
" 6.480 Pervious Area"
" 45.000 Pervious length"
" 2.000 Pervious slope"
" 0.000 Impervious Area"
" 45.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.261 0.931 1.344 1.344 c.m/sec"
" Catchment 30 Pervious Impervious Total Area "
" Surface Area 6.480 0.000 6.480 hectare"
" Time of concentration 14.371 2.291 14.371 minutes"
" Time to Centroid 105.688 98.958 105.688 minutes"
" Rainfall depth 69.476 69.476 69.476 mm"
" Rainfall volume 4502.07 0.00 4502.07 c.m"
" Rainfall losses 40.830 2.498 40.830 mm"
" Runoff depth 28.647 66.978 28.647 mm"
" Runoff volume 1856.30 0.00 1856.30 c.m"
" Runoff coefficient 0.000 0.000 0.000 "
" Maximum flow 1.261 0.000 1.261 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.261 2.192 1.344 1.344"
" 40 HYDROGRAPH Copy to Outflow"
" 8 Copy to Outflow"
" 1.261 2.192 2.192 1.344"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
" Total Discharge"
" Maximum flow 3.536 c.m/sec"
" Hydrograph volume 5451.871 c.m"
" 1.261 2.192 2.192 3.536"
" 40 HYDROGRAPH Confluence 1"
" 7 Confluence "
" 1 Node #"
" Total Discharge"
" Maximum flow 3.536 c.m/sec"
" Hydrograph volume 5451.870 c.m"
" 1.261 3.536 2.192 0.000"
" 38 START/RE-START TOTALS 1"
" 3 Runoff Totals on EXIT"
" Total Catchment area 18.280 hectare"
" Total Impervious area 0.562 hectare"
" Total % impervious 3.072"
" 19 EXIT"

```

```

"                                105172 Ex Cond 100year
"                                MIDUSS Output ----->"
"                                MIDUSS version                Version 2.07 rev. 379"
"                                MIDUSS created                April 25, 2005"
"                                10 Units used:                ie METRIC"
"                                Job folder:                    Y:\SPrimmer\Miduss Modelling\105172"
"                                Output filename:                105172 Ex Cond 100year REV.out"
"                                Licensee name:
"                                Company                        Gamsby and Mannerow Limited"
"                                Date & Time last used:          04/04/2011 at 12:01:05 PM"
" 31 TIME PARAMETERS"
"      5.000 Time Step"
"      210.000 Max. Storm length"
"      1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
"      1 Chicago storm"
"      4688.000 Coefficient A"
"      17.000 Constant B"
"      0.962 Exponent C"
"      0.400 Fraction R"
"      210.000 Duration"
"      1.000 Time step multiplier"
"      Maximum intensity                213.574 mm/hr"
"      Total depth                      88.830 mm"
"      6 100hyd Hydrograph extension used in this file"
" 33 CATCHMENT 10"
"      1 Triangular SCS"
"      1 Equal length"
"      2 Horton equation"
"      10 Catchment 10 - To Hadati Creek"
"      8.000 % Impervious"
"      7.020 Total Area"
"      45.000 Flow length"
"      2.000 Overland Slope"
"      6.458 Pervious Area"
"      45.000 Pervious length"
"      2.000 Pervious slope"
"      0.562 Impervious Area"
"      45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"      2.160 0.000 0.000 0.000 c.m/sec"
"      Catchment 10 Pervious Impervious Total Area "
"      Surface Area 6.458 0.562 7.020 hectare"
"      Time of concentration 11.869 2.089 10.485 minutes"
"      Time to Centroid 104.828 98.071 103.872 minutes"
"      Rainfall depth 88.830 88.830 88.830 mm"
"      Rainfall volume 5736.98 498.87 6235.85 c.m"
"      Rainfall losses 43.360 2.670 40.105 mm"
"      Runoff depth 45.470 86.160 48.725 mm"
"      Runoff volume 2936.64 483.87 3420.51 c.m"
"      Runoff coefficient 0.000 0.000 0.000 "
"      Maximum flow 1.965 0.297 2.160 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "

```

		105172	Ex	Cond	100year	
"	2.160	2.160	0.000	0.000"		
" 40	HYDROGRAPH Copy to Outflow"					
"	8	Copy to Outflow"				
"	2.160	2.160	2.160	0.000"		
" 40	HYDROGRAPH Combine 1"					
"	6	Combine "				
"	1	Node #"				
"	Total Discharge"					
"	Maximum flow	2.160	c.m/sec"			
"	Hydrograph volume	3420.511	c.m"			
"	2.160	2.160	2.160	2.160"		
" 40	HYDROGRAPH Start - New Tributary"					
"	2	Start - New Tributary"				
"	2.160	0.000	2.160	2.160"		
" 33	CATCHMENT 20"					
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	20	Catchment 20 - To Clythe Creeek"				
"	0.000	% Impervious"				
"	4.780	Total Area"				
"	45.000	Flow length"				
"	2.000	Overland slope"				
"	4.780	Pervious Area"				
"	45.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.000	Impervious Area"				
"	45.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"	1.454	0.000	2.160	2.160 c.m/sec"		
"	Catchment 20	Pervious	Impervious	Total Area	"	
"	Surface Area	4.780	0.000	4.780	hectare"	
"	Time of concentration	11.869	2.089	11.869	minutes"	
"	Time to Centroid	104.828	98.071	104.828	minutes"	
"	Rainfall depth	88.830	88.830	88.830	mm"	
"	Rainfall volume	4246.06	0.00	4246.07	c.m"	
"	Rainfall losses	43.360	2.670	43.360	mm"	
"	Runoff depth	45.470	86.160	45.470	mm"	
"	Runoff volume	2173.47	0.00	2173.47	c.m"	
"	Runoff coefficient	0.000	0.000	0.000	"	
"	Maximum flow	1.454	0.000	1.454	c.m/sec"	
" 40	HYDROGRAPH Add Runoff "					
"	4	Add Runoff "				
"	1.454	1.454	2.160	2.160"		
" 33	CATCHMENT 30"					
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	30	Catchment 30 - To Clythe Creek"				
"	0.000	% Impervious"				
"	6.480	Total Area"				
"	45.000	Flow length"				
"	2.000	Overland slope"				

```

"                                     105172 Ex Cond 100year
" 6.480 Pervious Area"
" 45.000 Pervious length"
" 2.000 Pervious slope"
" 0.000 Impervious Area"
" 45.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.971 1.454 2.160 2.160 c.m/sec"
" Catchment 30 Pervious Impervious Total Area "
" Surface Area 6.480 0.000 6.480 hectare"
" Time of concentration 11.869 2.089 11.869 minutes"
" Time to Centroid 104.828 98.071 104.828 minutes"
" Rainfall depth 88.830 88.830 88.830 mm"
" Rainfall volume 5756.17 0.01 5756.17 c.m"
" Rainfall losses 43.360 2.670 43.360 mm"
" Runoff depth 45.470 86.160 45.470 mm"
" Runoff volume 2946.46 0.01 2946.46 c.m"
" Runoff coefficient 0.000 0.000 0.000 "
" Maximum flow 1.971 0.000 1.971 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.971 3.425 2.160 2.160"
" 40 HYDROGRAPH Copy to Outflow"
" 8 Copy to Outflow"
" 1.971 3.425 3.425 2.160"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
" Total Discharge"
" Maximum flow 5.585 c.m/sec"
" Hydrograph volume 8540.444 c.m"
" 1.971 3.425 3.425 5.585"
" 40 HYDROGRAPH Confluence 1"
" 7 Confluence "
" 1 Node #"
" Total Discharge"
" Maximum flow 5.585 c.m/sec"
" Hydrograph volume 8540.444 c.m"
" 1.971 5.585 3.425 0.000"
" 38 START/RE-START TOTALS 1"
" 3 Runoff Totals on EXIT"
" Total Catchment area 18.280 hectare"
" Total Impervious area 0.562 hectare"
" Total % impervious 3.072"
" 19 EXIT"

```

```

"                                105172 Ex Cond Regional
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.07 rev. 379"
" MIDUSS created                      April 25, 2005"
" 10 Units used:                      ie METRIC"
" Job folder:                        Y:\SPrimmer\Miduss Modelling\105172"
" Output filename:                   105172 Ex Cond Regional REV.out"
" Licensee name:
" Company                           Gamsby and Mannerow Limited"
" Date & Time last used:             04/04/2011 at 12:01:39 PM"
" 31 TIME PARAMETERS"
" 60.000 Time Step"
" 2880.000 Max. Storm length"
" 3600.000 Max. Hydrograph"
" 32 STORM Historic"
" 5 Historic"
" 2880.000 Duration"
" 48.000 Rainfall intensity values"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.026      2.026      2.206      2.028"
"      2.026      6.000      4.000      6.000      13.000"
"      17.000     13.000     23.000     13.000     13.000"
"      53.000     38.000     13.000"
" Maximum intensity                   53.000 mm/hr"
" Total depth                         285.180 mm"
" 6 001hyd Hydrograph extension used in this file"
" 33 CATCHMENT 10"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 10 Catchment 10 - To Hadati Creek"
" 8.000 % Impervious"
" 7.020 Total Area"
" 45.000 Flow length"
" 2.000 Overland slope"
" 6.458 Pervious Area"
" 45.000 Pervious length"
" 2.000 Pervious slope"
" 0.562 Impervious Area"
" 45.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      0.587      0.000      0.000      0.000 c.m/sec"
" Catchment 10 Pervious Impervious Total Area "
" Surface Area 6.458 0.562 7.020 hectare"
" Time of concentration 21.969 3.647 18.018 minutes"
" Time to Centroid 2780.245 2236.863 2663.074 minutes"
" Rainfall depth 285.180 285.180 285.180 mm"
" Rainfall volume 1.8418 0.1602 2.0020 ha-m"
" Rainfall losses 207.172 38.558 193.683 mm"

```

105172 Ex Cond Regional					
"	Runoff depth	78.008	246.622	91.497	mm"
"	Runoff volume	5038.08	1385.03	6423.11	c.m"
"	Runoff coefficient	0.000	0.000	0.000	"
"	Maximum flow	0.537	0.071	0.587	c.m/sec"
40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"	0.587 0.587 0.000 0.000"				
40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"	0.587 0.587 0.587 0.000"				
40	HYDROGRAPH Combine 1"				
"	6 Combine "				
"	1 Node #"				
"	Total Discharge"				
"	Maximum flow	0.587		c.m/sec"	
"	Hydrograph volume	6423.105		c.m"	
"	0.587 0.587 0.587 0.587"				
40	HYDROGRAPH Start - New Tributary"				
"	2 Start - New Tributary"				
"	0.587 0.000 0.587 0.587"				
33	CATCHMENT 20"				
"	1 Triangular SCS"				
"	1 Equal length"				
"	2 Horton equation"				
"	20 Catchment 20 - To Clythe creek"				
"	0.000 % Impervious"				
"	4.780 Total Area"				
"	45.000 Flow length"				
"	2.000 Overland Slope"				
"	4.780 Pervious Area"				
"	45.000 Pervious length"				
"	2.000 Pervious slope"				
"	0.000 Impervious Area"				
"	45.000 Impervious length"				
"	2.000 Impervious slope"				
"	0.250 Pervious Manning 'n'"				
"	75.000 Pervious Max.infiltration"				
"	12.500 Pervious Min.infiltration"				
"	0.250 Pervious Lag constant (hours)"				
"	5.000 Pervious Depression storage"				
"	0.015 Impervious Manning 'n'"				
"	0.000 Impervious Max.infiltration"				
"	0.000 Impervious Min.infiltration"				
"	0.050 Impervious Lag constant (hours)"				
"	1.500 Impervious Depression storage"				
"	0.397 0.000 0.587 0.587 c.m/sec"				
"	Catchment 20 Pervious Impervious Total Area "				
"	Surface Area 4.780 0.000 4.780 hectare"				
"	Time of concentration 21.969 3.647 21.969 minutes"				
"	Time to Centroid 2780.245 2236.863 2780.243 minutes"				
"	Rainfall depth 285.180 285.180 285.180 mm"				
"	Rainfall volume 1.3632 0.0000 1.3632 ha-m"				
"	Rainfall losses 207.172 38.558 207.172 mm"				
"	Runoff depth 78.008 246.622 78.008 mm"				
"	Runoff volume 3728.78 0.01 3728.80 c.m"				
"	Runoff coefficient 0.000 0.000 0.000 "				
"	Maximum flow 0.397 0.000 0.397 c.m/sec"				
40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"	0.397 0.397 0.587 0.587"				
33	CATCHMENT 30"				
"	1 Triangular SCS"				
"	1 Equal length"				


```

"          105172 Ex Cond Regional
"          2 Horton equation"
"          30 Catchment 30 - To Clythe Creek"
"          0.000 % Impervious"
"          6.480 Total Area"
"          45.000 Flow length"
"          2.000 Overland Slope"
"          6.480 Pervious Area"
"          45.000 Pervious length"
"          2.000 Pervious slope"
"          0.000 Impervious Area"
"          45.000 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          75.000 Pervious Max.infiltration"
"          12.500 Pervious Min.infiltration"
"          0.250 Pervious Lag constant (hours)"
"          5.000 Pervious Depression storage"
"          0.015 Impervious Manning 'n'"
"          0.000 Impervious Max.infiltration"
"          0.000 Impervious Min.infiltration"
"          0.050 Impervious Lag constant (hours)"
"          1.500 Impervious Depression storage"
"          0.538 0.397 0.587 0.587 c.m/sec"
"          Catchment 30 Pervious Impervious Total Area "
"          Surface Area 6.480 0.000 6.480 hectare"
"          Time of concentration 21.969 3.647 21.969 minutes"
"          Time to Centroid 2780.244 2236.863 2780.243 minutes"
"          Rainfall depth 285.180 285.180 285.180 mm"
"          Rainfall volume 1.8480 0.0000 1.8480 ha-m"
"          Rainfall losses 207.172 38.558 207.172 mm"
"          Runoff depth 78.008 246.622 78.008 mm"
"          Runoff volume 5054.92 0.02 5054.94 c.m"
"          Runoff coefficient 0.000 0.000 0.000 "
"          Maximum flow 0.538 0.000 0.538 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"          0.538 0.936 0.587 0.587"
" 40 HYDROGRAPH Copy to Outflow"
" 8 Copy to Outflow"
"          0.538 0.936 0.936 0.587"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
"          Total Discharge"
"          Maximum flow 1.522 c.m/sec"
"          Hydrograph volume 15206.841 c.m"
"          0.538 0.936 0.936 1.522"
" 40 HYDROGRAPH Confluence 1"
" 7 Confluence "
" 1 Node #"
"          Total Discharge"
"          Maximum flow 1.522 c.m/sec"
"          Hydrograph volume 15206.841 c.m"
"          0.538 1.522 0.936 0.000"
" 38 START/RE-START TOTALS 1"
" 3 Runoff Totals on EXIT"
"          Total Catchment area 18.280 hectare"
"          Total Impervious area 0.562 hectare"
"          Total % impervious 3.072"
" 19 EXIT"

```

Hadati Creek Watershed - Allowable

```

V      V      I      SSSSS  U      U      A      L
V      V      I      SS      U      U      A A     L
V      V      I      SS      U      U      AAAAA  L
V      V      I      SS      U      U      A      A  L
VV      I      SSSSS  UUUUU  A      A  LLLLL

000      TTTTT  TTTTT  H      H      Y      Y  M      M      000
O      O      T      T      H      H      Y Y     MM MM  O      O
O      O      T      T      H      H      Y      M      M  O      O

000      T      T      H      H      Y      M      M      000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files\Visual OTTHYMO 2.3.2\voin.dat

Output filename: Y:\SPrimmer\Miduss Modelling\105172\Cityview Ridge - Ex Pond Allowable\Hadati Creek Watershed - Allowable.out

Summary filename: Y:\SPrimmer\Miduss Modelling\105172\Cityview Ridge - Ex Pond Allowable\Hadati Creek Watershed - Allowable.sum

DATE: 8/7/2012

TIME: 2:54:51 PM

USER:

COMMENTS: _____

```

*****
** SIMULATION NUMBER: 1 **
*****

```

READ STORM

Ptotal= 25.00 mm

Filename: Y:\SPrimmer\Miduss Modelling\105172\Cityview Ridge\25mm4hr.stm
 Comments: 25 mm - 4 hour - 10 Minute Time Step

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	.53	1.17	17.57	2.17	2.95	3.17	.76
.33	.71	1.33	61.55	2.33	2.19	3.33	.65
.50	.99	1.50	24.02	2.50	1.69	3.50	.57
.67	1.51	1.67	11.16	2.67	1.34	3.67	.49
.83	2.57	1.83	6.44	2.83	1.09	3.83	.44
1.00	5.31	2.00	4.20	3.00	.90	4.00	.38

Hadati Creek watershed - Allowable

CALIB
STANDHYD (0544)
ID= 1 DT= 5.0 min

Area (ha)= 1.13
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.90	.23
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	.55	.55
Length	(m)=	50.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.53	1.083	17.57	2.083	2.95	3.08	.76
.167	.53	1.167	17.57	2.167	2.95	3.17	.76
.250	.71	1.250	61.55	2.250	2.19	3.25	.65
.333	.71	1.333	61.55	2.333	2.19	3.33	.65
.417	.99	1.417	24.02	2.417	1.69	3.42	.57
.500	.99	1.500	24.02	2.500	1.69	3.50	.57
.583	1.51	1.583	11.16	2.583	1.34	3.58	.49
.667	1.51	1.667	11.16	2.667	1.34	3.67	.49
.750	2.57	1.750	6.44	2.750	1.09	3.75	.44
.833	2.57	1.833	6.44	2.833	1.09	3.83	.44
.917	5.31	1.917	4.20	2.917	.90	3.92	.38
1.000	5.31	2.000	4.20	3.000	.90	4.00	.38

Max.Eff.Inten.(mm/hr)= 61.55
over (min) 5.00
Storage Coeff. (min)= 2.45 (ii) 320.46 (ii)
Unit Hyd. Tpeak (min)= 5.00 325.00
Unit Hyd. peak (cms)= .30 .00

TOTALS
.151 (iii)
1.33
18.56
25.00
.74

PEAK FLOW (cms)= .15
TIME TO PEAK (hrs)= 1.33
RUNOFF VOLUME (mm)= 23.50
TOTAL RAINFALL (mm)= 25.00
RUNOFF COEFFICIENT = .94

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0543)
ID= 1 DT= 5.0 min

Area (ha)= 14.99
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	11.99	3.00
Dep. Storage	(mm)=	1.50	5.00

Hadati Creek watershed - Allowable

Average Slope (%)=	.55	.55
Length (m)=	200.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	61.55	.00
over (min)	5.00	325.00
Storage Coeff. (min)=	5.63 (ii)	323.64 (ii)
Unit Hyd. Tpeak (min)=	5.00	325.00
Unit Hyd. peak (cms)=	.20	.00

PEAK FLOW (cms)=	1.77	.00	*TOTALS*
TIME TO PEAK (hrs)=	1.33	.00	1.767 (iii)
RUNOFF VOLUME (mm)=	23.50	.00	1.33
TOTAL RAINFALL (mm)=	25.00	25.00	18.56
RUNOFF COEFFICIENT =	.94	.00	25.00
			.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0542)	Area (ha)= 25.25
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	20.20	5.05
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	350.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	61.55	.00
over (min)	10.00	330.00
Storage Coeff. (min)=	7.87 (ii)	325.88 (ii)
Unit Hyd. Tpeak (min)=	10.00	330.00
Unit Hyd. peak (cms)=	.13	.00

PEAK FLOW (cms)=	2.41	.00	*TOTALS*
TIME TO PEAK (hrs)=	1.42	.00	2.408 (iii)
RUNOFF VOLUME (mm)=	23.50	.00	1.42
TOTAL RAINFALL (mm)=	25.00	25.00	18.56
RUNOFF COEFFICIENT =	.94	.00	25.00
			.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0510)	Area (ha)= 16.00

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Hadati Creek watershed - Allowable
 ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		10.00	440.00	
Storage Coeff. (min)=		8.77 (ii)	439.54 (ii)	
Unit Hyd. Tpeak (min)=		10.00	440.00	
Unit Hyd. peak (cms)=		.12	.00	
				TOTALS
PEAK FLOW (cms)=		1.48	.00	1.475 (iii)
TIME TO PEAK (hrs)=		1.42	.00	1.42
RUNOFF VOLUME (mm)=		23.50	.00	18.56
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.00	.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0500)
 ID= 1 DT= 5.0 min | Area (ha)= 244.00
 Total Imp(%)= 46.00 Dir. Conn.(%)= 26.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		42.79	5.28	
over (min)		20.00	55.00	
Storage Coeff. (min)=		17.67 (ii)	51.28 (ii)	
Unit Hyd. Tpeak (min)=		20.00	55.00	
Unit Hyd. peak (cms)=		.06	.02	
				TOTALS
PEAK FLOW (cms)=		5.07	.82	5.342 (iii)
TIME TO PEAK (hrs)=		1.58	2.17	1.58
RUNOFF VOLUME (mm)=		23.50	2.25	7.77
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.31

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek watershed - Allowable

<div> <div>CALIB</div> <div>STANDHYD (0540)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 4.63		
		Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		5.00	325.00	
Storage Coeff. (min)=		4.73 (ii)	322.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	325.00	
Unit Hyd. peak (cms)=		.22	.00	
				TOTALS
PEAK FLOW (cms)=		.57	.00	.569 (iii)
TIME TO PEAK (hrs)=		1.33	.00	1.33
RUNOFF VOLUME (mm)=		23.50	.00	18.56
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.00	.74

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> <div>CALIB</div> <div>STANDHYD (0484)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 12.60		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.29	7.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		10.00	35.00	
Storage Coeff. (min)=		7.96 (ii)	30.70 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.13	.04	
				TOTALS
PEAK FLOW (cms)=		.32	.07	.334 (iii)
TIME TO PEAK (hrs)=		1.42	1.83	1.42
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Hadati Creek watershed - Allowable

- Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0565) ID= 1 DT= 5.0 min		Area (ha)= 11.10		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	4.66	6.44	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		10.00	35.00	
Storage Coeff. (min)=		7.96 (ii)	30.70 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.13	.04	
				TOTALS
PEAK FLOW (cms)=		.28	.06	.294 (iii)
TIME TO PEAK (hrs)=		1.42	1.83	1.42
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0481) ID= 1 DT= 5.0 min		Area (ha)= 5.90		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.48	3.42	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		10.00	35.00	
Storage Coeff. (min)=		7.96 (ii)	30.70 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.13	.04	
				TOTALS
PEAK FLOW (cms)=		.15	.03	.156 (iii)
TIME TO PEAK (hrs)=		1.42	1.83	1.42
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

Hadati Creek watershed - Allowable

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0410) ID= 1 DT= 5.0 min		Area (ha)= 24.20 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	10.16	14.04	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	401.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		5.80 (ii)	28.54 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.20	.04	
PEAK FLOW (cms)=		.75	.14	*TOTALS*
TIME TO PEAK (hrs)=		1.33	1.75	.770 (iii)
RUNOFF VOLUME (mm)=		23.50	2.16	1.33
TOTAL RAINFALL (mm)=		25.00	25.00	6.64
RUNOFF COEFFICIENT =		.94	.09	25.00
				.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0415) ID= 1 DT= 5.0 min		Area (ha)= 4.99 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.10	2.89	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.86	2.86	
Length	(m)=	185.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	8.82	
over (min)		5.00	25.00	
Storage Coeff. (min)=		3.27 (ii)	21.96 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.27	.05	
PEAK FLOW (cms)=		.17	.04	*TOTALS*
TIME TO PEAK (hrs)=		1.33	1.67	.179 (iii)
RUNOFF VOLUME (mm)=		23.50	2.16	1.33
				6.64

Hadati Creek Watershed - Allowable

TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.09	.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0110) ID= 1 DT= 5.0 min	Area (ha)= 19.00 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
---	---	----------------------

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	7.98	11.02	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	365.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	61.55	7.05	
over (min)	5.00	30.00	
Storage Coeff. (min)=	5.48 (ii)	28.22 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	.20	.04	
PEAK FLOW (cms)=	.60	.11	*TOTALS*
TIME TO PEAK (hrs)=	1.33	1.75	.614 (iii)
RUNOFF VOLUME (mm)=	23.50	2.16	1.33
TOTAL RAINFALL (mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT =	.94	.09	25.00
			.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min	Area (ha)= 16.32 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
---	---	----------------------

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	6.85	9.47
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	309.00	40.00
Mannings n =	.013	.300
Max.Eff.Inten.(mm/hr)=	61.55	7.05
over (min)	5.00	30.00
Storage Coeff. (min)=	4.96 (ii)	27.70 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.22	.04

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PEAK FLOW	(cms)=	.53	.10	*TOTALS*
TIME TO PEAK	(hrs)=	1.33	1.75	.540 (iii)
RUNOFF VOLUME	(mm)=	23.50	2.16	1.33
TOTAL RAINFALL	(mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT	=	.94	.09	25.00
				.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0102)	Area (ha)=	14.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	6.01	8.31
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	287.00	40.00
Mannings n	=	.013	.300

Max.Eff.Inten.(mm/hr)=	61.55	7.05
over (min)	5.00	30.00
Storage Coeff. (min)=	4.74 (ii)	27.48 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.22	.04

PEAK FLOW	(cms)=	.47	.09	*TOTALS*
TIME TO PEAK	(hrs)=	1.33	1.75	.479 (iii)
RUNOFF VOLUME	(mm)=	23.50	2.16	1.33
TOTAL RAINFALL	(mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT	=	.94	.09	25.00
				.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0105)	Area (ha)=	51.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	21.55	29.77
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	550.00	40.00
Mannings n	=	.013	.300

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Max.Eff.Inten.(mm/hr)=	61.55	7.05	
over (min)	5.00	30.00	
Storage Coeff. (min)=	7.01 (ii)	29.75 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	.17	.04	
			TOTALS
PEAK FLOW (cms)=	1.50	.30	1.538 (iii)
TIME TO PEAK (hrs)=	1.33	1.75	1.33
RUNOFF VOLUME (mm)=	23.50	2.16	6.64
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0365)
 ID= 1 DT= 5.0 min

Area (ha)= 117.50
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	49.35	68.15		
Dep. Storage (mm)=	1.50	5.00		
Average Slope (%)=	2.00	2.00		
Length (m)=	885.00	40.00		
Mannings n =	.013	.300		
Max.Eff.Inten.(mm/hr)=	61.55	7.05		
over (min)	10.00	35.00		
Storage Coeff. (min)=	9.32 (ii)	32.06 (ii)		
Unit Hyd. Tpeak (min)=	10.00	35.00		
Unit Hyd. peak (cms)=	.12	.03		
			TOTALS	
PEAK FLOW (cms)=	2.82	.62	2.960 (iii)	
TIME TO PEAK (hrs)=	1.42	1.83	1.42	
RUNOFF VOLUME (mm)=	23.50	2.16	6.64	
TOTAL RAINFALL (mm)=	25.00	25.00	25.00	
RUNOFF COEFFICIENT =	.94	.09	.27	

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0355)
 ID= 1 DT= 5.0 min

Area (ha)= 12.30
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.17	7.13	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.60	1.60	

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Length (m)=	286.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	61.55	7.05
over (min)	5.00	30.00
Storage Coeff. (min)=	5.06 (ii)	29.38 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.21	.04

PEAK FLOW (cms)=	.40	.07	*TOTALS*
TIME TO PEAK (hrs)=	1.33	1.75	.405 (iii)
RUNOFF VOLUME (mm)=	23.50	2.16	1.33
TOTAL RAINFALL (mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT =	.94	.09	25.00
			.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0350) ID= 1 DT= 5.0 min	Area (ha)= 16.30	Dir. Conn.(%)= 21.00
	Total Imp(%)= 42.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.45	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.00	1.00	
Length (m)=	330.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	61.55	5.04	
over (min)	5.00	40.00	
Storage Coeff. (min)=	6.35 (ii)	38.38 (ii)	
Unit Hyd. Tpeak (min)=	5.00	40.00	
Unit Hyd. peak (cms)=	.19	.03	
PEAK FLOW (cms)=	.49	.07	*TOTALS*
TIME TO PEAK (hrs)=	1.33	1.92	.499 (iii)
RUNOFF VOLUME (mm)=	23.50	2.16	1.33
TOTAL RAINFALL (mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT =	.94	.09	25.00
			.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0360) ID= 1 DT= 5.0 min	Area (ha)= 30.00	Dir. Conn.(%)= 19.00
	Total Imp(%)= 37.00	

IMPERVIOUS PERVIOUS (i)

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Surface Area	(ha)=	11.10	18.90	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	447.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	2.81	
over (min)		5.00	40.00	
Storage Coeff. (min)=		6.19 (ii)	39.07 (ii)	
Unit Hyd. Tpeak (min)=		5.00	40.00	
Unit Hyd. peak (cms)=		.19	.03	
				TOTALS
PEAK FLOW (cms)=		.83	.08	.834 (iii)
TIME TO PEAK (hrs)=		1.33	1.92	1.33
RUNOFF VOLUME (mm)=		23.50	1.27	5.50
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.05	.22

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0395)		Area (ha)= 51.20		
ID= 1 DT= 5.0 min		Total Imp(%)= 10.00	Dir. Conn.(%)= 5.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.12	46.08	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		10.00	230.00	
Storage Coeff. (min)=		9.42 (ii)	225.31 (ii)	
Unit Hyd. Tpeak (min)=		10.00	230.00	
Unit Hyd. peak (cms)=		.12	.00	
				TOTALS
PEAK FLOW (cms)=		.29	.00	.292 (iii)
TIME TO PEAK (hrs)=		1.42	.00	1.42
RUNOFF VOLUME (mm)=		23.50	.00	1.17
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.00	.05

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek Watershed - Allowable

CALIB
STANDHYD (0455)
ID= 1 DT= 5.0 min

Area (ha)= 12.70
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		5.11 (ii)	28.94 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.21	.04	
				TOTALS
PEAK FLOW (cms)=		.41	.07	.417 (iii)
TIME TO PEAK (hrs)=		1.33	1.75	1.33
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0460)
ID= 1 DT= 5.0 min

Area (ha)= 36.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		6.31 (ii)	28.95 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.19	.04	
				TOTALS
PEAK FLOW (cms)=		1.09	.21	1.117 (iii)
TIME TO PEAK (hrs)=		1.33	1.75	1.33
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

Hadati Creek Watershed - Allowable

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	18.10	25.00	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		10.00	35.00	
Storage Coeff. (min)=		7.96 (ii)	30.70 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.13	.04	
				TOTALS
PEAK FLOW (cms)=		1.09	.23	1.142 (iii)
TIME TO PEAK (hrs)=		1.42	1.83	1.42
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)
ID= 1 DT=****min

AREA (ha)= .00
QPEAK (cms)= .00
TPEAK (hrs)= .00
VOLUME (mm)=*****

DUHYD (0505)
Inlet Cap.=9.000
#of Inlets= 1
Total(cms)= 9.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	5.34	1.58	7.77
MAJOR SYS.(ID= 2):	.00	.00	.00	.00
MINOR SYS.(ID= 3):	244.00	5.34	1.58	7.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0566)
1 + 2 = 3

AREA QPEAK TPEAK R.V.
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	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0484):	12.60	.334	1.42	6.64
+ ID2= 2 (0565):	11.10	.294	1.42	6.64
<hr/>				
ID = 3 (0566):	23.70	.628	1.42	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> <div>ADD HYD (0420)</div> <div>1 + 2 = 3</div> </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0410):	24.20	.770	1.33	6.64
+ ID2= 2 (0415):	4.99	.179	1.33	6.64
<hr/>				
ID = 3 (0420):	29.19	.948	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> <div>RESERVOIR (0111)</div> <div>IN= 2---> OUT= 1</div> <div>DT= 5.0 min</div> </div>				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	.614	1.33	6.64
OUTFLOW: ID= 1 (0111)	19.000	.024	2.92	6.63
<div> <div>PEAK FLOW REDUCTION [Qout/Qin](%)= 3.93</div> <div>TIME SHIFT OF PEAK FLOW (min)= 95.00</div> <div>MAXIMUM STORAGE USED (ha.m.)= .1111</div> </div>				

<div> <div>ADD HYD (0103)</div> <div>1 + 2 = 3</div> </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	16.32	.540	1.33	6.64
+ ID2= 2 (0102):	14.32	.479	1.33	6.64
<hr/>				
ID = 3 (0103):	30.64	1.019	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> <div>RESERVOIR (0106)</div> <div>IN= 2---> OUT= 1</div> <div>DT= 5.0 min</div> </div>				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.5000	.4000
	.0100	.0100	6.6000	.8000
	.0260	.2300	.0000	.0000

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	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0105)	51.320	1.538	1.33	6.64
OUTFLOW: ID= 1 (0106)	51.320	.155	2.42	6.63

PEAK FLOW REDUCTION [Qout/Qin](%)= 10.08
TIME SHIFT OF PEAK FLOW (min)= 65.00
MAXIMUM STORAGE USED (ha.m.)= .2763

ROUTE CHN (0358)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		<---- hydrograph ---->				<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
INFLOW : ID= 2 (0355)	12.30	.40	1.33	6.64	.11	.72	
OUTFLOW: ID= 1 (0358)	12.30	.15	1.58	6.59	.08	.52	

ROUTE CHN (0353)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel

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5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

		<---- hydrograph ---->			<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW :	ID= 2 (0350)	16.30	.50	1.33	6.64	.12
OUTFLOW:	ID= 1 (0353)	16.30	.22	1.58	6.60	.09
						MAX VEL (m/s)
						.78
						.57

ROUTE CHN (0362)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36

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.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0360)	30.00	.83	1.33	5.50	.14	.96
OUTFLOW:	ID= 1 (0362)	30.00	.41	1.50	5.48	.11	.71

ADD HYD (0465)					
1 + 2 = 3					

	ID1= 1 (0455):	12.70	.417	1.33	6.64
	+ ID2= 2 (0460):	36.00	1.117	1.33	6.64
	=====				
	ID = 3 (0465):	48.70	1.534	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)					
1 + 2 = 3					

	ID1= 1 (0510):	16.00	1.475	1.42	18.56
	+ ID2= 2 (0505):	244.00	5.342	1.58	7.77
	=====				
	ID = 3 (0515):	260.00	6.307	1.58	8.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0564)		Routing time step (min)'= 5.00
IN= 2---> OUT= 1		

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	101.50	.0500	
1.00	100.70	.0500	
1.50	100.55	.0500 / .0300	Main Channel
2.00	99.50	.0300	Main Channel
3.50	99.60	.0300	Main Channel
4.50	100.65	.0300 / .0500	Main Channel
6.00	101.45	.0500	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69

Hadati Creek watershed - Allowable					
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: INFLOW HYDROGRAPH IS DRY!!

ROUTE CHN (0563)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.573E+01	.0	.67	2.23
.11	.11	.135E+02	.1	.99	1.51
.16	.16	.232E+02	.3	1.23	1.22
.21	.21	.349E+02	.5	1.42	1.06
.26	.26	.486E+02	.9	1.58	.95
.32	.32	.643E+02	1.2	1.73	.87
.37	.37	.820E+02	1.7	1.86	.81
.42	.42	.102E+03	2.2	1.98	.76
.47	.47	.123E+03	2.9	2.10	.71
.53	.53	.147E+03	3.6	2.21	.68
.58	.58	.173E+03	4.4	2.31	.65
.63	.63	.200E+03	5.4	2.42	.62
.68	.68	.230E+03	6.4	2.51	.60
.74	.74	.262E+03	7.6	2.61	.58
.79	.79	.295E+03	8.9	2.70	.56
.84	.84	.331E+03	10.3	2.79	.54
.89	.89	.369E+03	11.8	2.88	.52
.95	.95	.408E+03	13.5	2.97	.51
1.00	1.00	.450E+03	15.2	3.05	.49

<---- hydrograph ---->				<-pipe / channel->	
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)

Hadati Creek watershed - Allowable

INFLOW : ID= 2 (0566)	23.70	.63	1.42	6.64	.22	1.45
OUTFLOW: ID= 1 (0563)	23.70	.65	1.42	6.64	.23	1.47

DUHYD (0425)
Inlet Cap.=1.980
#of Inlets= 1
Total(cms)= 2.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	.95	1.33	6.64
MAJOR SYS.(ID= 2):	.00	.00	.00	.00
MINOR SYS.(ID= 3):	29.19	.95	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	.5000
.0100	.0100	10.0000	.6000
.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	1.019	1.33	6.64
OUTFLOW: ID= 1 (0104)	30.640	.097	2.33	6.63

PEAK FLOW REDUCTION [Qout/Qin](%)= 9.52
TIME SHIFT OF PEAK FLOW (min)= 60.00
MAXIMUM STORAGE USED (ha.m.)= .1639

ADD HYD (0359)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0358):	12.30	.153	1.58	6.59
+ ID2= 2 (0353):	16.30	.216	1.58	6.60
ID = 3 (0359):	28.60	.369	1.58	6.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0363)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0359):	28.60	.369	1.58	6.60
+ ID2= 2 (0362):	30.00	.406	1.50	5.48
ID = 3 (0363):	58.60	.769	1.50	6.03

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek watershed - Allowable					
.84	.84	.184E+03	11.6	3.14	.27
.89	.89	.205E+03	13.2	3.23	.26
.95	.95	.227E+03	15.0	3.31	.25
1.00	1.00	.250E+03	17.0	3.40	.25

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
<---- hydrograph ---->							
<--pipe / channel-->							
INFLOW : ID= 2 (0563)		23.70	.65	1.42	6.64	.21	1.73
OUTFLOW: ID= 1 (0561)		23.70	.66	1.42	6.64	.21	1.73

ADD HYD (0114)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0111):		19.00	.024	2.92	6.63
+ ID2= 2 (0104):		30.64	.097	2.33	6.63
=====					
ID = 3 (0114):		49.64	.118	2.42	6.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0365):		117.50	2.960	1.42	6.64
+ ID2= 2 (0363):		58.60	.769	1.50	6.03
=====					
ID = 3 (0380):		176.10	3.653	1.42	6.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)	
IN= 2--->	OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	324.60	.0500
115.00	321.60	.0500
120.00	320.80	.0500 / .0300
122.00	320.80	.0300 / .0500
138.00	321.60	.0500
148.00	322.30	.0500
154.00	323.10	.0500
164.00	324.60	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61

Hadati Creek watershed - Allowable					
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

		<---- hydrograph ---->				<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0470)	48.70	1.53	1.33	6.64	.26	.91
OUTFLOW:	ID= 1 (0475)	48.70	1.10	1.42	6.64	.23	.87

ADD HYD (0526)					
1 + 2 = 3					
ID1= 1 (0520):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0525):		59.59	3.257	1.58	8.44
		.00	.001	.00	*****
ID = 3 (0526):		59.59	3.257	1.58	8.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)					
1 + 2 = 3					
ID1= 1 (0561):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0481):		23.70	.656	1.42	6.64
		5.90	.156	1.42	6.64
ID = 3 (0492):		29.60	.812	1.42	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
ID1= 1 (0114):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0106):		49.64	.118	2.42	6.63
		51.32	.155	2.42	6.63
ID = 3 (0115):		100.96	.273	2.42	6.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| RESERVOIR (0390) |

Hadati Creek watershed - Allowable

IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	3.653	1.42	6.44
OUTFLOW: ID= 1 (0390)	176.100	.982	2.25	6.43

PEAK FLOW REDUCTION [Qout/Qin](%)= 26.88
TIME SHIFT OF PEAK FLOW (min)= 50.00
MAXIMUM STORAGE USED (ha.m.)= .5820

ROUTE CHN (0527)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	59.59	3.26	1.58	8.44	1.66	1.16
OUTFLOW: ID= 1 (0527)	59.59	2.80	1.67	8.44	1.54	1.21

RESERVOIR (0482)

Hadati Creek watershed - Allowable

IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	29.600	.812	1.42	6.64
OUTFLOW: ID= 1 (0482)	29.600	.262	2.00	6.64

PEAK FLOW REDUCTION [Qout/Qin] (%)= 32.30
TIME SHIFT OF PEAK FLOW (min)= 35.00
MAXIMUM STORAGE USED (ha.m.)= .0866

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0390):	176.10	.982	2.25	6.43
+ ID2= 2 (0395):	51.20	.292	1.42	1.17
ID = 3 (0400):	227.30	1.022	1.58	5.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97

Hadati Creek watershed - Allowable					
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0400)	227.30	1.02	1.58	5.25	.17	.73
OUTFLOW:	ID= 1 (0403)	227.30	.88	3.17	5.25	.16	.71

ADD HYD (0407)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0115):	100.96	.273	2.42	6.63
+	ID2= 2 (0403):	227.30	.881	3.17	5.25
=====					
ID =	3 (0407):	328.26	1.112	2.83	5.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0113)			
IN= 2---> OUT= 1			
DT= 5.0 min			
	OUTFLOW (cms)	STORAGE (ha.m.)	
	.0000	.0000	
	1.1000	2.9000	
	1.3000	4.3000	

	OUTFLOW (cms)	STORAGE (ha.m.)
	1.6000	6.4000
	9.1000	10.0000
	12.0000	20.0000

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW :	ID= 2 (0407)	328.260	1.112	2.83	5.67
OUTFLOW:	ID= 1 (0113)	328.260	.354	5.83	5.67

PEAK FLOW REDUCTION [Qout/Qin](%)= 31.88
 TIME SHIFT OF PEAK FLOW (min)=180.00
 MAXIMUM STORAGE USED (ha.m.)= .9343

ADD HYD (0430)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0425):	29.19	.948	1.33	6.64
+	ID2= 2 (0113):	328.26	.354	5.83	5.67
=====					
ID =	3 (0430):	357.45	.951	1.33	5.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)		
IN= 2---> OUT= 1		Routing time step (min)'= 5.00

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Hadati Creek Watershed - Allowable

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	325.40	.0600	
120.00	324.60	.0600	
126.00	323.90	.0600	
130.00	323.00	.0600	
140.00	322.30	.0600 / .0300	Main Channel
142.00	322.30	.0300 / .0600	Main Channel
150.00	323.90	.0600	
155.00	324.60	.0600	
160.00	325.40	.0600	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

<----- hydrograph ----->			<-pipe / channel->		
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW : ID= 2 (0430)	357.45	.95	1.33	5.75	.20
OUTFLOW: ID= 1 (0440)	357.45	.72	1.42	5.75	.18

ADD HYD (0485)				
1	+	2	=	3
ID1= 1 (0440):		357.45	.720	1.42
+ ID2= 2 (0475):		48.70	1.101	1.42
ID = 3 (0485):		406.15	1.820	1.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)				
1	+	2	=	3
ID1= 1 (0485):		406.15	1.820	1.42

Hadati Creek watershed - Allowable

+ ID2= 2 (0480):	43.10	1.142	1.42	6.64
<hr/>				
ID = 3 (0490):	449.25	2.962	1.42	5.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0482):	29.60	.262	2.00	6.64
+ ID2= 2 (0490):	449.25	2.962	1.42	5.93
<hr/>				
ID = 3 (0491):	478.85	3.142	1.42	5.98

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	7.0800	2.4860
	.2760	.0600	8.1000	3.3240
	1.2000	.3400	9.7980	4.6420
	2.0400	.6182	10.4940	7.4397
	2.6400	1.1630	11.6850	10.3000
	3.1200	1.7070	12.3480	11.4000
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0491)	478.850	3.142	1.42	5.98
OUTFLOW: ID= 1 (0483)	478.850	1.356	2.00	5.98
PEAK FLOW REDUCTION [Qout/Qin] (%)= 43.16				
TIME SHIFT OF PEAK FLOW (min)= 35.00				
MAXIMUM STORAGE USED (ha.m.)= .3923				

ADD HYD (0530)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0540):	4.63	.569	1.33	18.56
+ ID2= 2 (0483):	478.85	1.356	2.00	5.98
<hr/>				
ID = 3 (0530):	483.48	1.402	2.00	6.10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0527):	59.59	2.796	1.67	8.44
+ ID2= 2 (0530):	483.48	1.402	2.00	6.10

Hadati Creek Watershed - Allowable
ID = 3 (0545): 543.07 4.103 1.67 6.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0542):		25.25	2.408	1.42	18.56
+ ID2= 2 (0545):		543.07	4.103	1.67	6.35
ID = 3 (0546):		568.32	5.491	1.58	6.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0543):		14.99	1.767	1.33	18.56
+ ID2= 2 (0546):		568.32	5.491	1.58	6.90
ID = 3 (0547):		583.31	6.172	1.50	7.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0544):		1.13	.151	1.33	18.56
+ ID2= 2 (0547):		583.31	6.172	1.50	7.20
ID = 3 (0548):		584.44	6.233	1.50	7.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

** SIMULATION NUMBER: 2 **

READ STORM	Filename: Y:\SPrimmer\Miduss Modelling\105172\Ci
Ptotal= 53.41 mm	tyview Ridge\5yrSCS12hr.stm
	Comments: 5 year SCS Type II 12hour design storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	1.34	3.25	2.14	6.25	9.61	9.25	1.87
.50	1.34	3.50	2.14	6.50	9.61	9.50	1.87
.75	1.34	3.75	2.14	6.75	4.27	9.75	1.87
1.00	1.34	4.00	2.14	7.00	4.27	10.00	1.87
1.25	1.34	4.25	3.20	7.25	3.20	10.25	1.07
1.50	1.34	4.50	3.20	7.50	3.20	10.50	1.07
1.75	1.34	4.75	4.27	7.75	3.20	10.75	1.07

Hadati Creek watershed - Allowable							
2.00	1.34	5.00	4.27	8.00	3.20	11.00	1.07
2.25	1.60	5.25	6.41	8.25	1.87	11.25	1.07
2.50	1.60	5.50	6.41	8.50	1.87	11.50	1.07
2.75	1.60	5.75	25.64	8.75	1.87	11.75	1.07
3.00	1.60	6.00	70.50	9.00	1.87	12.00	1.07

CALIB
STANDHYD (0544)
ID= 1 DT= 5.0 min

Area (ha)= 1.13
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.90	.23
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	50.00	40.00
Mannings n =	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.34	3.083	2.14	6.083	9.61	9.08	1.87
.167	1.34	3.167	2.14	6.167	9.61	9.17	1.87
.250	1.34	3.250	2.14	6.250	9.61	9.25	1.87
.333	1.34	3.333	2.14	6.333	9.61	9.33	1.87
.417	1.34	3.417	2.14	6.417	9.61	9.42	1.87
.500	1.34	3.500	2.14	6.500	9.61	9.50	1.87
.583	1.34	3.583	2.14	6.583	4.27	9.58	1.87
.667	1.34	3.667	2.14	6.667	4.27	9.67	1.87
.750	1.34	3.750	2.14	6.750	4.27	9.75	1.87
.833	1.34	3.833	2.14	6.833	4.27	9.83	1.87
.917	1.34	3.917	2.14	6.917	4.27	9.92	1.87
1.000	1.34	4.000	2.14	7.000	4.27	10.00	1.87
1.083	1.34	4.083	3.20	7.083	3.20	10.08	1.07
1.167	1.34	4.167	3.20	7.167	3.20	10.17	1.07
1.250	1.34	4.250	3.20	7.250	3.20	10.25	1.07
1.333	1.34	4.333	3.20	7.333	3.20	10.33	1.07
1.417	1.34	4.417	3.20	7.417	3.20	10.42	1.07
1.500	1.34	4.500	3.20	7.500	3.20	10.50	1.07
1.583	1.34	4.583	4.27	7.583	3.20	10.58	1.07
1.667	1.34	4.667	4.27	7.667	3.20	10.67	1.07
1.750	1.34	4.750	4.27	7.750	3.20	10.75	1.07
1.833	1.34	4.833	4.27	7.833	3.20	10.83	1.07
1.917	1.34	4.917	4.27	7.917	3.20	10.92	1.07
2.000	1.34	5.000	4.27	8.000	3.20	11.00	1.07
2.083	1.60	5.083	6.41	8.083	1.87	11.08	1.07
2.167	1.60	5.167	6.41	8.167	1.87	11.17	1.07
2.250	1.60	5.250	6.41	8.250	1.87	11.25	1.07
2.333	1.60	5.333	6.41	8.333	1.87	11.33	1.07
2.417	1.60	5.417	6.41	8.417	1.87	11.42	1.07
2.500	1.60	5.500	6.41	8.500	1.87	11.50	1.07
2.583	1.60	5.583	25.64	8.583	1.87	11.58	1.07
2.667	1.60	5.667	25.64	8.667	1.87	11.67	1.07
2.750	1.60	5.750	25.64	8.750	1.87	11.75	1.07
2.833	1.60	5.833	70.50	8.833	1.87	11.83	1.07
2.917	1.60	5.917	70.50	8.917	1.87	11.92	1.07
3.000	1.60	6.000	70.50	9.000	1.87	12.00	1.07

Hadati Creek Watershed - Allowable

Max.Eff.Inten.(mm/hr)=	70.50	30.06	
over (min)	5.00	25.00	
Storage Coeff. (min)=	2.32 (ii)	21.08 (ii)	
Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	.30	.05	
			TOTALS
PEAK FLOW (cms)=	.17	.01	.178 (iii)
TIME TO PEAK (hrs)=	6.00	6.25	6.00
RUNOFF VOLUME (mm)=	51.91	9.54	43.01
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.18	.81

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0543)	Area (ha)= 14.99		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.99	3.00	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	200.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	30.06	
over (min)	5.00	25.00	
Storage Coeff. (min)=	5.33 (ii)	24.09 (ii)	
Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	.21	.05	
			TOTALS
PEAK FLOW (cms)=	2.23	.12	2.271 (iii)
TIME TO PEAK (hrs)=	6.00	6.33	6.00
RUNOFF VOLUME (mm)=	51.91	9.54	43.01
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.18	.81

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0542)	Area (ha)= 25.25		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	20.20	5.05	
Dep. Storage (mm)=	1.50	5.00	

Hadati Creek Watershed - Allowable

Average Slope	(%)=	.55	.55	
Length	(m)=	350.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	30.06	
over (min)		5.00	30.00	
Storage Coeff. (min)=		7.45 (ii)	26.21 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.17	.04	
PEAK FLOW	(cms)=	3.56	.19	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.33	3.608 (iii)
RUNOFF VOLUME	(mm)=	51.91	9.54	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	43.01
RUNOFF COEFFICIENT	=	.97	.18	53.41
				.81

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0510)
ID= 1 DT= 5.0 min

Area (ha)= 16.00
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	20.04	
over (min)		10.00	40.00	
Storage Coeff. (min)=		8.31 (ii)	38.19 (ii)	
Unit Hyd. Tpeak (min)=		10.00	40.00	
Unit Hyd. peak (cms)=		.13	.03	
PEAK FLOW	(cms)=	2.06	.09	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.50	2.080 (iii)
RUNOFF VOLUME	(mm)=	51.91	9.54	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	43.01
RUNOFF COEFFICIENT	=	.97	.18	53.41
				.81

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0500)
ID= 1 DT= 5.0 min

Area (ha)= 244.00
Total Imp(%)= 46.00 Dir. Conn.(%)= 26.00

Hadati Creek Watershed - Allowable

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	78.43	
over (min)		15.00	30.00	
Storage Coeff. (min)=		14.47 (ii)	25.89 (ii)	
Unit Hyd. Tpeak (min)=		15.00	30.00	
Unit Hyd. peak (cms)=		.08	.04	
PEAK FLOW	(cms)=	8.08	9.34	*TOTALS*
TIME TO PEAK	(hrs)=	6.08	6.33	14.467 (iii)
RUNOFF VOLUME	(mm)=	51.91	14.36	6.25
TOTAL RAINFALL	(mm)=	53.41	53.41	24.12
RUNOFF COEFFICIENT	=	.97	.27	53.41
				.45

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0540)
ID= 1 DT= 5.0 min

Area (ha)= 4.63
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	30.06	
over (min)		5.00	25.00	
Storage Coeff. (min)=		4.48 (ii)	23.24 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.23	.05	
PEAK FLOW	(cms)=	.70	.04	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.25	.713 (iii)
RUNOFF VOLUME	(mm)=	51.91	9.54	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	43.01
RUNOFF COEFFICIENT	=	.97	.18	53.41
				.81

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek Watershed - Allowable

CALIB
STANDHYD (0484)
ID= 1 DT= 5.0 min

Area (ha)= 12.60
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.29	7.31	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.54 (ii)	16.07 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.06	
PEAK FLOW (cms)=	.44	.75	*TOTALS* 1.055 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.08
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0565)
ID= 1 DT= 5.0 min

Area (ha)= 11.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	4.66	6.44	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.54 (ii)	16.07 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.06	
PEAK FLOW (cms)=	.39	.66	*TOTALS* .929 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.08
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek Watershed - Allowable

CALIB
STANDHYD (0481)
ID= 1 DT= 5.0 min

Area (ha)= 5.90
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.48	3.42
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	680.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	70.50	81.70
over (min)	10.00	20.00
Storage Coeff. (min)=	7.54 (ii)	16.07 (ii)
Unit Hyd. Tpeak (min)=	10.00	20.00
Unit Hyd. peak (cms)=	.13	.06

			TOTALS
PEAK FLOW (cms)=	.21	.35	.494 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.08
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0410)
ID= 1 DT= 5.0 min

Area (ha)= 24.20
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	10.16	14.04
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	401.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	70.50	81.70
over (min)	5.00	15.00
Storage Coeff. (min)=	5.49 (ii)	14.03 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.20	.08

			TOTALS
PEAK FLOW (cms)=	.95	1.66	2.307 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

Hadati Creek watershed - Allowable

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area	(ha)=	4.99		
STANDHYD (0415)		Total	Imp(%)=	42.00	Dir. Conn.(%)=	21.00
ID= 1 DT= 5.0 min						
			IMPERVIOUS		PERVIOUS (i)	
Surface Area	(ha)=	2.10		2.89		
Dep. Storage	(mm)=	1.50		5.00		
Average Slope	(%)=	2.86		2.86		
Length	(m)=	185.00		40.00		
Mannings n	=	.013		.300		
Max.Eff.Inten.(mm/hr)=		70.50		81.70		
over (min)		5.00		15.00		
Storage Coeff. (min)=		3.10 (ii)		10.77 (ii)		
Unit Hyd. Tpeak (min)=		5.00		15.00		
Unit Hyd. peak (cms)=		.27		.09		
						TOTALS
PEAK FLOW (cms)=		.20		.39		.532 (iii)
TIME TO PEAK (hrs)=		6.00		6.08		6.00
RUNOFF VOLUME (mm)=		51.91		14.24		22.15
TOTAL RAINFALL (mm)=		53.41		53.41		53.41
RUNOFF COEFFICIENT =		.97		.27		.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area	(ha)=	19.00		
STANDHYD (0110)		Total	Imp(%)=	42.00	Dir. Conn.(%)=	21.00
ID= 1 DT= 5.0 min						
			IMPERVIOUS		PERVIOUS (i)	
Surface Area	(ha)=	7.98		11.02		
Dep. Storage	(mm)=	1.50		5.00		
Average Slope	(%)=	2.00		2.00		
Length	(m)=	365.00		40.00		
Mannings n	=	.013		.300		
Max.Eff.Inten.(mm/hr)=		70.50		81.70		
over (min)		5.00		15.00		
Storage Coeff. (min)=		5.19 (ii)		13.73 (ii)		
Unit Hyd. Tpeak (min)=		5.00		15.00		
Unit Hyd. peak (cms)=		.21		.08		
						TOTALS
PEAK FLOW (cms)=		.75		1.32		1.831 (iii)
TIME TO PEAK (hrs)=		6.00		6.08		6.00
RUNOFF VOLUME (mm)=		51.91		14.24		22.15
TOTAL RAINFALL (mm)=		53.41		53.41		53.41
RUNOFF COEFFICIENT =		.97		.27		.41

Hadati Creek Watershed - Allowable

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min	Area (ha)= 16.32 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
---	---

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.47	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	309.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.70 (ii)	13.23 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.08	
			TOTALS
PEAK FLOW (cms)=	.65	1.15	1.601 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0102) ID= 1 DT= 5.0 min	Area (ha)= 14.32 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
---	---

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.01	8.31	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	287.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.49 (ii)	13.03 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.23	.08	
			TOTALS
PEAK FLOW (cms)=	.58	1.02	1.415 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00

Hadati Creek watershed - Allowable

RUNOFF VOLUME	(mm)=	51.91	14.24	22.15
TOTAL RAINFALL	(mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT	=	.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0105)	Area (ha)=	51.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	21.55	29.77	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	550.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.64 (ii)	15.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.18	.07	
				TOTALS
PEAK FLOW (cms)=		1.96	3.14	3.870 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.08
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0365)	Area (ha)=	117.50	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.83 (ii)	17.37 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	

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Unit Hyd. peak (cms)=	.12	.06	
			TOTALS
PEAK FLOW (cms)=	3.95	6.70	9.481 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.08
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0355)	Area (ha)= 12.30
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=		5.17	7.13
Dep. Storage (mm)=		1.50	5.00
Average Slope (%)=		1.60	1.60
Length (m)=		286.00	40.00
Mannings n =		.013	.300
Max.Eff.Inten.(mm/hr)=		70.50	81.70
over (min)		5.00	15.00
Storage Coeff. (min)=	4.79 (ii)		13.92 (ii)
Unit Hyd. Tpeak (min)=	5.00		15.00
Unit Hyd. peak (cms)=	.22		.08
			TOTALS
PEAK FLOW (cms)=	.49	.85	1.183 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0350)	Area (ha)= 16.30
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=		6.85	9.45
Dep. Storage (mm)=		1.50	5.00
Average Slope (%)=		1.00	1.00
Length (m)=		330.00	40.00
Mannings n =		.013	.300

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Max.Eff.Inten.(mm/hr)=	70.50	77.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.01 (ii)	16.75 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.19	.06	
			TOTALS
PEAK FLOW (cms)=	.63	.95	1.186 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.00
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0360)	Area (ha)= 30.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 37.00	Dir. Conn.(%)= 19.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.10	18.90	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	447.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	75.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.86 (ii)	14.65 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.20	.08	
			TOTALS
PEAK FLOW (cms)=	1.06	1.94	2.582 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	51.91	13.31	20.64
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.25	.39

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0395)	Area (ha)= 51.20		
ID= 1 DT= 5.0 min	Total Imp(%)= 10.00	Dir. Conn.(%)= 5.00	

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.12	46.08

Hadati Creek watershed - Allowable

Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	58.39	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.92 (ii)	18.68 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
PEAK FLOW	(cms)=	.41	2.36	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.25	2.601 (iii)
RUNOFF VOLUME	(mm)=	51.91	9.64	6.17
TOTAL RAINFALL	(mm)=	53.41	53.41	11.75
RUNOFF COEFFICIENT	=	.97	.18	53.41
				.22

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0455)	Area (ha)=	12.70	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.84 (ii)	13.78 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.08	
PEAK FLOW	(cms)=	.51	.88	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	1.226 (iii)
RUNOFF VOLUME	(mm)=	51.91	14.24	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	22.15
RUNOFF COEFFICIENT	=	.97	.27	53.41
				.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0460)
ID= 1 DT= 5.0 min

Area (ha)= 36.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	15.12	20.88	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.03	2.03	
Length (m)=	465.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.97 (ii)	14.47 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.08	
PEAK FLOW (cms)=	1.40	2.42	*TOTALS* 3.376 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	18.10	25.00	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	81.70	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.54 (ii)	16.07 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.06	
PEAK FLOW (cms)=	1.52	2.56	*TOTALS* 3.608 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.08
RUNOFF VOLUME (mm)=	51.91	14.24	22.15
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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STORE HYD (0525)	AREA	(ha)=	.00
ID= 1 DT=****min	QPEAK	(cms)=	.00
	TPEAK	(hrs)=	.00
	VOLUME	(mm)=	*****

DUHYD (0505)	AREA	QPEAK	TPEAK	R.V.
Inlet Cap.=9.000	(ha)	(cms)	(hrs)	(mm)
#of Inlets= 1				
Total(cms)= 9.0				
TOTAL HYD.(ID= 1):	244.00	14.47	6.25	24.12
MAJOR SYS.(ID= 2):	33.53	5.47	6.25	24.12
MINOR SYS.(ID= 3):	210.47	9.00	6.00	24.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0566)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0484):	12.60	1.055	6.08	22.15
+ ID2= 2 (0565):	11.10	.929	6.08	22.15
ID = 3 (0566):	23.70	1.984	6.08	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0420)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0410):	24.20	2.307	6.00	22.15
+ ID2= 2 (0415):	4.99	.532	6.00	22.15
ID = 3 (0420):	29.19	2.839	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)	OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1	(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min				
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0110)	19.000	1.831	6.00	22.15
OUTFLOW: ID= 1 (0111)	19.000	.238	6.58	22.14

Hadati Creek Watershed - Allowable
 PEAK FLOW REDUCTION [Qout/Qin](%)= 12.98
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= .3060

ADD HYD (0103)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	16.32	1.601	6.00	22.15
+ ID2= 2 (0102):	14.32	1.415	6.00	22.15
=====				
ID = 3 (0103):	30.64	3.016	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0106)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	3.870	6.08	22.15
OUTFLOW: ID= 1 (0106)	51.320	2.731	6.33	22.14

PEAK FLOW REDUCTION [Qout/Qin](%)= 70.57
 TIME SHIFT OF PEAK FLOW (min)= 15.00
 MAXIMUM STORAGE USED (ha.m.)= .5507

ROUTE CHN (0358)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72

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.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		<---- hydrograph ---->				<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0355)		12.30	1.18	6.00	22.15	.16	1.10
OUTFLOW: ID= 1 (0358)		12.30	.74	6.17	22.10	.13	.92

ROUTE CHN (0353)	
IN= 2----> OUT= 1	
Routing time step (min)'= 5.00	

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

		<---- hydrograph ---->				<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0350)		16.30	1.19	6.00	22.15	.16	1.10
OUTFLOW: ID= 1 (0353)		16.30	.95	6.25	22.11	.15	1.02

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ROUTE CHN (0362)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .40 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .40 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .02 .02 .176E+02 .0 .21 80.52
 .04 .04 .702E+02 .0 .33 50.72
 .06 .06 .158E+03 .1 .43 38.71
 .08 .08 .281E+03 .1 .52 31.95
 .09 .09 .438E+03 .3 .62 26.84
 .11 .11 .607E+03 .5 .77 21.66
 .13 .13 .776E+03 .7 .90 18.45
 .15 .15 .944E+03 1.0 1.03 16.22
 .17 .17 .116E+04 1.3 1.16 14.36
 .20 .20 .140E+04 1.8 1.27 13.13
 .22 .22 .166E+04 2.3 1.36 12.24
 .24 .24 .194E+04 2.8 1.44 11.58
 .26 .26 .225E+04 3.4 1.51 11.05
 .29 .29 .258E+04 4.0 1.57 10.63
 .31 .31 .293E+04 4.8 1.62 10.27
 .33 .33 .331E+04 5.5 1.67 9.97
 .35 .35 .371E+04 6.4 1.72 9.71
 .38 .38 .413E+04 7.3 1.76 9.48
 .40 .40 .457E+04 8.2 1.80 9.28

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0360) 30.00 2.58 6.00 20.64 .23 1.41
 OUTFLOW: ID= 1 (0362) 30.00 2.01 6.17 20.63 .21 1.31

ADD HYD (0465)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0455):	12.70	1.226	6.00	22.15
+ ID2= 2 (0460):	36.00	3.376	6.00	22.15
=====				
ID = 3 (0465):	48.70	4.602	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)
1 + 2 = 3

AREA	QPEAK	TPEAK	R.V.
------	-------	-------	------

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	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0510):	16.00	2.080	6.00	43.01
+ ID2= 2 (0505):	210.47	9.000	6.00	24.12
ID = 3 (0515):	226.47	11.080	6.00	25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0564)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	101.50	.0500	
1.00	100.70	.0500	
1.50	100.55	.0500 / .0300	Main Channel
2.00	99.50	.0300	Main Channel
3.50	99.60	.0300	Main Channel
4.50	100.65	.0300 / .0500	Main Channel
6.00	101.45	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0505)	33.53	5.47	6.25	24.12	1.58	1.28
OUTFLOW: ID= 1 (0564)	33.53	4.91	6.33	24.12	1.50	1.25

ROUTE CHN (0563)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel

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4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.573E+01	.0	.67	2.23
.11	.11	.135E+02	.1	.99	1.51
.16	.16	.232E+02	.3	1.23	1.22
.21	.21	.349E+02	.5	1.42	1.06
.26	.26	.486E+02	.9	1.58	.95
.32	.32	.643E+02	1.2	1.73	.87
.37	.37	.820E+02	1.7	1.86	.81
.42	.42	.102E+03	2.2	1.98	.76
.47	.47	.123E+03	2.9	2.10	.71
.53	.53	.147E+03	3.6	2.21	.68
.58	.58	.173E+03	4.4	2.31	.65
.63	.63	.200E+03	5.4	2.42	.62
.68	.68	.230E+03	6.4	2.51	.60
.74	.74	.262E+03	7.6	2.61	.58
.79	.79	.295E+03	8.9	2.70	.56
.84	.84	.331E+03	10.3	2.79	.54
.89	.89	.369E+03	11.8	2.88	.52
.95	.95	.408E+03	13.5	2.97	.51
1.00	1.00	.450E+03	15.2	3.05	.49

<---- hydrograph ---->				<-pipe / channel->		
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0566)	23.70	1.98	6.08	22.15	.40	1.92
OUTFLOW: ID= 1 (0563)	23.70	1.97	6.08	22.15	.39	1.92

DUHYD (0425)
Inlet Cap.=1.980
#of Inlets= 1
Total(cms)= 2.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	2.84	6.00	22.15
MAJOR SYS.(ID= 2):	2.28	.86	6.00	22.15
MINOR SYS.(ID= 3):	26.91	1.98	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	.5000
.0100	.0100	10.0000	.6000
.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	3.016	6.00	22.15
OUTFLOW: ID= 1 (0104)	30.640	.801	6.42	22.14

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PEAK FLOW REDUCTION [Qout/Qin](%)= 26.57
 TIME SHIFT OF PEAK FLOW (min)= 25.00
 MAXIMUM STORAGE USED (ha.m.)= .4263

ADD HYD (0359)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0358):	12.30	.744	6.17	22.10
+ ID2= 2 (0353):	16.30	.952	6.25	22.11
<hr/>				
ID = 3 (0359):	28.60	1.680	6.25	22.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0363)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0359):	28.60	1.680	6.25	22.11
+ ID2= 2 (0362):	30.00	2.013	6.17	20.63
<hr/>				
ID = 3 (0363):	58.60	3.649	6.17	21.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0470)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0465):	48.70	4.602	6.00	22.15
+ ID2= 2 (0425):	2.28	.859	6.00	22.15
<hr/>				
ID = 3 (0470):	50.98	5.461	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0520)				
Inlet Cap.=3.050				
#of Inlets= 1				
Total(cms)= 3.0				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	226.47	11.08	6.00	25.46
<hr/>				
MAJOR SYS.(ID= 2):	88.85	8.03	6.00	25.46
MINOR SYS.(ID= 3):	137.62	3.05	5.75	25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0561)	
IN= 2---> OUT= 1	Routing time step (min)'= 5.00

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<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.319E+01	.1	.87	.95
.11	.11	.748E+01	.2	1.26	.66
.16	.16	.129E+02	.4	1.54	.54
.21	.21	.194E+02	.7	1.75	.48
.26	.26	.270E+02	1.0	1.93	.43
.32	.32	.357E+02	1.5	2.08	.40
.37	.37	.456E+02	2.0	2.22	.38
.42	.42	.565E+02	2.6	2.34	.36
.47	.47	.686E+02	3.4	2.46	.34
.53	.53	.817E+02	4.2	2.57	.32
.58	.58	.960E+02	5.1	2.68	.31
.63	.63	.111E+03	6.2	2.78	.30
.68	.68	.128E+03	7.3	2.87	.29
.74	.74	.145E+03	8.6	2.97	.28
.79	.79	.164E+03	10.0	3.06	.27
.84	.84	.184E+03	11.6	3.14	.27
.89	.89	.205E+03	13.2	3.23	.26
.95	.95	.227E+03	15.0	3.31	.25
1.00	1.00	.250E+03	17.0	3.40	.25

	AREA (ha)	<---- hydrograph ---->			<--pipe / channel-->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0563)	23.70	1.97	6.08	22.15	.36	2.20
OUTFLOW: ID= 1 (0561)	23.70	1.95	6.08	22.15	.36	2.20

ADD HYD (0114)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0111):	19.00	.238	6.58	22.14	
+ ID2= 2 (0104):	30.64	.801	6.42	22.14	
=====					
ID = 3 (0114):	49.64	1.029	6.50	22.14	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0365):	117.50	9.481	6.08	22.15	
+ ID2= 2 (0363):	58.60	3.649	6.17	21.35	
=====					
ID = 3 (0380):	176.10	12.674	6.17	21.88	

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 100.00 324.60 .0500
 115.00 321.60 .0500
 120.00 320.80 .0500 / .0300 Main Channel
 122.00 320.80 .0300 / .0500 Main Channel
 138.00 321.60 .0500
 148.00 322.30 .0500
 154.00 323.10 .0500
 164.00 324.60 .0500

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .20 321.00 .398E+03 .8 .84 8.53
 .40 321.20 .125E+04 3.3 1.13 6.33
 .60 321.40 .255E+04 8.1 1.36 5.27
 .80 321.60 .430E+04 15.6 1.56 4.59
 1.00 321.80 .644E+04 26.8 1.79 4.01
 1.20 322.00 .892E+04 41.2 1.99 3.61
 1.40 322.20 .117E+05 59.3 2.17 3.30
 1.60 322.40 .148E+05 81.9 2.37 3.02
 1.80 322.60 .182E+05 109.1 2.58 2.78
 2.00 322.80 .218E+05 140.2 2.77 2.59
 2.20 323.00 .256E+05 175.3 2.95 2.43
 2.40 323.20 .296E+05 214.7 3.12 2.29
 2.60 323.40 .338E+05 258.6 3.29 2.18
 2.80 323.60 .382E+05 306.7 3.46 2.07
 3.00 323.80 .428E+05 359.1 3.61 1.98
 3.20 324.00 .476E+05 416.0 3.76 1.91
 3.40 324.20 .526E+05 477.5 3.91 1.83
 3.60 324.40 .578E+05 543.5 4.05 1.77
 3.80 324.60 .632E+05 614.3 4.18 1.71

<----- hydrograph -----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0470) 50.98 5.46 6.00 22.15 .49 1.23
 OUTFLOW: ID= 1 (0475) 50.98 4.60 6.08 22.15 .45 1.19

ADD HYD (0526)
1 + 2 = 3

AREA QPEAK TPEAK R.V.
 (ha) (cms) (hrs) (mm)
 ID1= 1 (0520): 88.85 8.030 6.00 25.46
 + ID2= 2 (0525): .00 .001 .00 *****
 ID = 3 (0526): 88.85 8.030 6.00 25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0492)					
1 + 2 = 3					
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0561):	23.70	1.953	6.08	22.15	
+ ID2= 2 (0481):	5.90	.494	6.08	22.15	
=====					
ID = 3 (0492):	29.60	2.447	6.08	22.15	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0114):		49.64	1.029	6.50	22.14
+ ID2= 2 (0106):		51.32	2.731	6.33	22.14
=====					
ID = 3 (0115):		100.96	3.732	6.33	22.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0390)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	1.3100	1.6000
	.7700	.2870	1.8600	23.2300
	1.2600	.9680	.0000	.0000
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0380)	176.100	12.674	6.17	21.88
OUTFLOW: ID= 1 (0390)	176.100	1.333	7.08	21.88
PEAK FLOW REDUCTION [Qout/Qin](%)= 10.52				
TIME SHIFT OF PEAK FLOW (min)= 55.00				
MAXIMUM STORAGE USED (ha.m.)= 2.5065				

ROUTE CHN (0527)		Routing time step (min)'= 5.00			
IN= 2---> OUT= 1					

<----- DATA FOR SECTION (1.1) ----->					
Distance	Elevation	Manning			
100.00	313.20	.0500			
140.00	312.40	.0500 / .0300	Main Channel		
140.50	310.80	.0300	Main Channel		
141.50	310.80	.0300	Main Channel		
142.00	312.40	.0300 / .0500	Main Channel		
160.00	313.20	.0500			
<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13

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.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0526)	88.85	8.03	6.00	25.46	2.05	.76
OUTFLOW:	ID= 1 (0527)	88.85	6.50	6.42	25.46	1.97	.79

RESERVOIR (0482)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	29.600	2.447	6.08	22.15
OUTFLOW: ID= 1 (0482)	29.600	.293	6.83	22.15

PEAK FLOW REDUCTION [Qout/Qin](%)= 11.99
TIME SHIFT OF PEAK FLOW (min)= 45.00
MAXIMUM STORAGE USED (ha.m.)= .4082

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0390):	176.10	1.333	7.08	21.88
+ ID2= 2 (0395):	51.20	2.601	6.17	11.75
ID = 3 (0400):	227.30	3.883	6.17	19.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)

| IN= 2---> OUT= 1 | Hadati Creek Watershed - Allowable
Routing time step (min)'= 5.00

```

<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
100.00        338.30        .0500
110.00        336.80        .0500
135.00        336.00        .0300      Main Channel
142.00        335.30        .0500
148.00        335.30        .0500
156.00        336.00        .0500
165.00        338.30        .0000
  
```

```

<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)         (m)         (cu.m.)      (cms)          (m/s)         (min)
.16        335.46      .231E+04      .9             .71           44.52
.32        335.62      .563E+04      3.2            1.09          29.11
.47        335.77      .997E+04      7.3            1.39          22.72
.63        335.93      .153E+05      13.4           1.66          19.04
.79        336.09      .218E+05      22.7           1.97          16.04
.95        336.25      .299E+05      35.3           2.25          14.10
1.11       336.41      .396E+05      51.2           2.46          12.89
1.26       336.56      .510E+05      70.7           2.63          12.02
1.42       336.72      .641E+05      94.1           2.79          11.35
1.58       336.88      .787E+05      122.4          2.96          10.71
1.74       337.04      .939E+05      155.6          3.15          10.06
1.89       337.19      .110E+06      192.8          3.34           9.48
2.05       337.35      .126E+06      233.9          3.53           8.97
2.21       337.51      .143E+06      278.9          3.71           8.53
2.37       337.67      .160E+06      327.7          3.89           8.13
2.53       337.83      .178E+06      380.3          4.07           7.79
2.68       337.98      .196E+06      436.7          4.23           7.48
2.84       338.14      .215E+06      496.9          4.40           7.20
3.00       338.30      .234E+06      561.0          4.56           6.95
  
```

```

<---- hydrograph ---->      <-pipe / channel->
                        AREA      QPEAK      TPEAK      R.V.      MAX DEPTH      MAX VEL
                        (ha)      (cms)      (hrs)      (mm)      (m)            (m/s)
INFLOW : ID= 2 (0400)  227.30    3.88      6.17    19.60      .34            1.13
OUTFLOW: ID= 1 (0403)  227.30    2.23      6.42    19.60      .25            .89
  
```

```

| ADD HYD (0407) |
| 1 + 2 = 3 |
|-----|
| ID1= 1 (0115):  100.96  3.732  6.33  22.14 |
| + ID2= 2 (0403):  227.30  2.232  6.42  19.60 |
|-----|
| ID = 3 (0407):  328.26  5.857  6.33  20.38 |
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

| RESERVOIR (0113) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
|-----|
| OUTFLOW      STORAGE      OUTFLOW      STORAGE |
| (cms)        (ha.m.)      (cms)        (ha.m.) |
| .0000        .0000        1.6000        6.4000 |
| 1.1000      2.9000        9.1000       10.0000 |
  
```

Hadati Creek Watershed - Allowable

1.3000 4.3000 | 12.0000 20.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	5.857	6.33	20.38
OUTFLOW: ID= 1 (0113)	328.260	1.137	12.67	20.38

PEAK FLOW REDUCTION [Qout/Qin](%)= 19.42
 TIME SHIFT OF PEAK FLOW (min)=380.00
 MAXIMUM STORAGE USED (ha.m.)= 3.1599

ADD HYD (0430)				
1 + 2 = 3				
ID1= 1 (0425):	26.91	1.980	6.00	22.15
+ ID2= 2 (0113):	328.26	1.137	12.67	20.38
ID = 3 (0430):	355.17	2.137	6.17	20.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)	
IN= 2----> OUT= 1	Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	325.40	.0600	
120.00	324.60	.0600	
126.00	323.90	.0600	
130.00	323.00	.0600	
140.00	322.30	.0600 / .0300	Main Channel
142.00	322.30	.0300 / .0600	Main Channel
150.00	323.90	.0600	
155.00	324.60	.0600	
160.00	325.40	.0600	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

Hadati Creek Watershed - Allowable

		<---- hydrograph ---->			<--pipe / channel-->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0430)	355.17	2.14	6.17	20.51	.33	1.26
OUTFLOW: ID= 1 (0440)	355.17	2.11	6.17	20.51	.32	1.26

ADD HYD (0485)					
1	2	=	3		
ID1= 1 (0440):	355.17		2.113	6.17	20.51
+ ID2= 2 (0475):	50.98		4.600	6.08	22.15
ID = 3 (0485):	406.15		6.641	6.08	20.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)					
1	2	=	3		
ID1= 1 (0485):	406.15		6.641	6.08	20.72
+ ID2= 2 (0480):	43.10		3.608	6.08	22.15
ID = 3 (0490):	449.25		10.249	6.08	20.86

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)					
1	2	=	3		
ID1= 1 (0482):	29.60		.293	6.83	22.15
+ ID2= 2 (0490):	449.25		10.249	6.08	20.86
ID = 3 (0491):	478.85		10.519	6.08	20.94

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)					
IN= 2---> OUT= 1					
DT= 5.0 min					
OUTFLOW	STORAGE		OUTFLOW	STORAGE	
(cms)	(ha.m.)		(cms)	(ha.m.)	
.0000	.0000		7.0800	2.4860	
.2760	.0600		8.1000	3.3240	
1.2000	.3400		9.7980	4.6420	
2.0400	.6182		10.4940	7.4397	
2.6400	1.1630		11.6850	10.3000	
3.1200	1.7070		12.3480	11.4000	

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	478.850	10.519	6.08	20.94

Hadati Creek watershed - Allowable
 OUTFLOW: ID= 1 (0483) 478.850 2.914 6.67 20.94

PEAK FLOW REDUCTION [Qout/Qin](%)= 27.70
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= 1.4753

ADD HYD (0530)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0540):	4.63	.713	6.00	43.01
+ ID2= 2 (0483):	478.85	2.914	6.67	20.94
ID = 3 (0530):	483.48	3.009	6.50	21.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0527):	88.85	6.502	6.42	25.46
+ ID2= 2 (0530):	483.48	3.009	6.50	21.15
ID = 3 (0545):	572.33	9.488	6.50	21.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0542):	25.25	3.608	6.00	43.01
+ ID2= 2 (0545):	572.33	9.488	6.50	21.82
ID = 3 (0546):	597.58	10.369	6.00	22.71

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0543):	14.99	2.271	6.00	43.01
+ ID2= 2 (0546):	597.58	10.369	6.00	22.71
ID = 3 (0547):	612.57	12.640	6.00	23.21

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3				

Hadati Creek watershed - Allowable

	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0544):	1.13	.178	6.00	43.01
+ ID2= 2 (0547):	612.57	12.640	6.00	23.21
ID = 3 (0548):	613.70	12.818	6.00	23.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 ** SIMULATION NUMBER: 3 **

READ STORM	Filename: Y:\SPrimmer\Miduss Modelling\105172\Ci
Ptotal= 73.56 mm	tyview Ridge\25yrSCS12hr.stm
	Comments: 25 year SCS Type II 12hr design storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	1.84	3.25	2.94	6.25	13.24	9.25	2.58
.50	1.84	3.50	2.94	6.50	13.24	9.50	2.58
.75	1.84	3.75	2.94	6.75	5.89	9.75	2.58
1.00	1.84	4.00	2.94	7.00	5.89	10.00	2.58
1.25	1.84	4.25	4.41	7.25	4.41	10.25	1.47
1.50	1.84	4.50	4.41	7.50	4.41	10.50	1.47
1.75	1.84	4.75	5.89	7.75	4.41	10.75	1.47
2.00	1.84	5.00	5.89	8.00	4.41	11.00	1.47
2.25	2.21	5.25	8.83	8.25	2.58	11.25	1.47
2.50	2.21	5.50	8.83	8.50	2.58	11.50	1.47
2.75	2.21	5.75	35.31	8.75	2.58	11.75	1.47
3.00	2.21	6.00	97.10	9.00	2.58	12.00	1.47

CALIB	Area (ha)= 1.13
STANDHYD (0544)	Total Imp(%)= 80.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.90	.23
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	50.00	40.00
Mannings n =	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.84	3.083	2.94	6.083	13.24	9.08	2.58
.167	1.84	3.167	2.94	6.167	13.24	9.17	2.58
.250	1.84	3.250	2.94	6.250	13.24	9.25	2.58
.333	1.84	3.333	2.94	6.333	13.24	9.33	2.58
.417	1.84	3.417	2.94	6.417	13.24	9.42	2.58
.500	1.84	3.500	2.94	6.500	13.24	9.50	2.58
.583	1.84	3.583	2.94	6.583	5.89	9.58	2.58
.667	1.84	3.667	2.94	6.667	5.89	9.67	2.58
.750	1.84	3.750	2.94	6.750	5.89	9.75	2.58

	Hadati	Creek	watershed	- Allowable			
.833	1.84	3.833	2.94	6.833	5.89	9.83	2.58
.917	1.84	3.917	2.94	6.917	5.89	9.92	2.58
1.000	1.84	4.000	2.94	7.000	5.88	10.00	2.58
1.083	1.84	4.083	4.41	7.083	4.41	10.08	1.47
1.167	1.84	4.167	4.41	7.167	4.41	10.17	1.47
1.250	1.84	4.250	4.41	7.250	4.41	10.25	1.47
1.333	1.84	4.333	4.41	7.333	4.41	10.33	1.47
1.417	1.84	4.417	4.41	7.417	4.41	10.42	1.47
1.500	1.84	4.500	4.41	7.500	4.41	10.50	1.47
1.583	1.84	4.583	5.88	7.583	4.41	10.58	1.47
1.667	1.84	4.667	5.89	7.667	4.41	10.67	1.47
1.750	1.84	4.750	5.89	7.750	4.41	10.75	1.47
1.833	1.84	4.833	5.89	7.833	4.41	10.83	1.47
1.917	1.84	4.917	5.89	7.917	4.41	10.92	1.47
2.000	1.84	5.000	5.89	8.000	4.41	11.00	1.47
2.083	2.21	5.083	8.83	8.083	2.58	11.08	1.47
2.167	2.21	5.167	8.83	8.167	2.58	11.17	1.47
2.250	2.21	5.250	8.83	8.250	2.58	11.25	1.47
2.333	2.21	5.333	8.83	8.333	2.58	11.33	1.47
2.417	2.21	5.417	8.83	8.417	2.58	11.42	1.47
2.500	2.21	5.500	8.83	8.500	2.58	11.50	1.47
2.583	2.21	5.583	35.31	8.583	2.58	11.58	1.47
2.667	2.21	5.667	35.31	8.667	2.58	11.67	1.47
2.750	2.21	5.750	35.31	8.750	2.58	11.75	1.47
2.833	2.21	5.833	97.10	8.833	2.58	11.83	1.47
2.917	2.21	5.917	97.10	8.917	2.58	11.92	1.47
3.000	2.21	6.000	97.10	9.000	2.58	12.00	1.47

Max.Eff.Inten.(mm/hr)= 97.10 87.19
over (min) 5.00 15.00
Storage Coeff. (min)= 2.04 (ii) 14.29 (ii)
Unit Hyd. Tpeak (min)= 5.00 15.00
Unit Hyd. peak (cms)= .31 .08

PEAK FLOW (cms)= .24 .03
TIME TO PEAK (hrs)= 6.00 6.08
RUNOFF VOLUME (mm)= 72.06 21.22
TOTAL RAINFALL (mm)= 73.56 73.56
RUNOFF COEFFICIENT = .98 .29

TOTALS
.266 (iii)
6.00
61.38
73.56
.83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0543)	Area (ha)= 14.99		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	11.99	3.00
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	200.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)= 97.10 87.19

Hadati Creek watershed - Allowable

over (min)	5.00	20.00	
Storage Coeff. (min)=	4.69 (ii)	16.94 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.22	.06	
			TOTALS
PEAK FLOW (cms)=	3.11	.34	3.310 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.00
RUNOFF VOLUME (mm)=	72.06	21.22	61.38
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.29	.83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0542)	Area (ha)= 25.25		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	20.20	5.05	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	350.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	87.19	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.56 (ii)	18.81 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.18	.06	
			TOTALS
PEAK FLOW (cms)=	5.02	.53	5.333 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.00
RUNOFF VOLUME (mm)=	72.06	21.22	61.38
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.29	.83

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0510)	Area (ha)= 16.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	12.80	3.20	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.50	.20	

Hadati Creek watershed - Allowable

Length (m)=	400.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	97.10	65.53
over (min)	5.00	30.00
Storage Coeff. (min)=	7.31 (ii)	25.92 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.17	.04

PEAK FLOW (cms)=	3.12	.25	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.33	3.209 (iii)
RUNOFF VOLUME (mm)=	72.06	21.22	6.00
TOTAL RAINFALL (mm)=	73.56	73.56	61.38
RUNOFF COEFFICIENT =	.98	.29	73.56
			.83

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 244.00
STANDHYD (0500)	Total Imp(%)= 46.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)= 26.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	112.24	131.76
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.80	.80
Length (m)=	1275.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	97.10	120.22
over (min)	15.00	25.00
Storage Coeff. (min)=	12.73 (ii)	22.36 (ii)
Unit Hyd. Tpeak (min)=	15.00	25.00
Unit Hyd. peak (cms)=	.08	.05

PEAK FLOW (cms)=	11.66	18.11	*TOTALS*
TIME TO PEAK (hrs)=	6.08	6.25	27.658 (iii)
RUNOFF VOLUME (mm)=	72.06	26.62	6.17
TOTAL RAINFALL (mm)=	73.56	73.56	38.44
RUNOFF COEFFICIENT =	.98	.36	73.56
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 4.63
STANDHYD (0540)	Total Imp(%)= 80.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)= 79.00

IMPERVIOUS	PERVIOUS (i)
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Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	87.19	
over (min)		5.00	20.00	
Storage Coeff. (min)=		3.94 (ii)	16.20 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.24	.06	
				TOTALS
PEAK FLOW (cms)=		.97	.11	1.036 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.00
RUNOFF VOLUME (mm)=		72.06	21.22	61.38
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.29	.83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0484)	Area (ha)=	12.60	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.29	7.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		6.63 (ii)	13.97 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.18	.08	
				TOTALS
PEAK FLOW (cms)=		.66	1.43	1.918 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		72.06	26.53	36.09
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STANDHYD (0565)		Hadati Creek Watershed - Allowable	
ID= 1 DT= 5.0 min	Area (ha)= 11.10	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	4.66	6.44	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.63 (ii)	13.97 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.18	.08	
PEAK FLOW (cms)=	.59	1.26	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	1.689 (iii)
RUNOFF VOLUME (mm)=	72.06	26.53	6.00
TOTAL RAINFALL (mm)=	73.56	73.56	36.09
RUNOFF COEFFICIENT =	.98	.36	73.56
			.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0481)		Area (ha)= 5.90	
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.48	3.42	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.63 (ii)	13.97 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.18	.08	
PEAK FLOW (cms)=	.31	.67	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	.898 (iii)
RUNOFF VOLUME (mm)=	72.06	26.53	6.00
TOTAL RAINFALL (mm)=	73.56	73.56	36.09
RUNOFF COEFFICIENT =	.98	.36	73.56
			.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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<div> <div>CALIB</div> <div>STANDHYD (0410)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 24.20		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	10.16	14.04	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	401.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.83 (ii)	12.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.09	
PEAK FLOW (cms)=		1.33	2.92	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	3.938 (iii)
RUNOFF VOLUME (mm)=		72.06	26.53	6.00
TOTAL RAINFALL (mm)=		73.56	73.56	36.09
RUNOFF COEFFICIENT =		.98	.36	73.56
				.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> <div>CALIB</div> <div>STANDHYD (0415)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 4.99		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.10	2.89	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.86	2.86	
Length	(m)=	185.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.73 (ii)	9.32 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		.29	.12	
PEAK FLOW (cms)=		.28	.73	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.00	1.007 (iii)
RUNOFF VOLUME (mm)=		72.06	26.53	6.00
TOTAL RAINFALL (mm)=		73.56	73.56	36.09
RUNOFF COEFFICIENT =		.98	.36	73.56
				.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14

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Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0110) ID= 1 DT= 5.0 min		Area (ha)= 19.00	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)		
Surface Area	(ha)=	7.98	11.02		
Dep. Storage	(mm)=	1.50	5.00		
Average Slope	(%)=	2.00	2.00		
Length	(m)=	365.00	40.00		
Mannings n	=	.013	.300		
Max.Eff.Inten.(mm/hr)=		97.10	119.40		
over (min)		5.00	15.00		
Storage Coeff. (min)=		4.57 (ii)	11.90 (ii)		
Unit Hyd. Tpeak (min)=		5.00	15.00		
Unit Hyd. peak (cms)=		.23	.09		
PEAK FLOW (cms)=		1.05	2.32	*TOTALS*	3.122 (iii)
TIME TO PEAK (hrs)=		6.00	6.08		6.00
RUNOFF VOLUME (mm)=		72.06	26.53		36.09
TOTAL RAINFALL (mm)=		73.56	73.56		73.56
RUNOFF COEFFICIENT =		.98	.36		.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min		Area (ha)= 16.32	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)		
Surface Area	(ha)=	6.85	9.47		
Dep. Storage	(mm)=	1.50	5.00		
Average Slope	(%)=	2.00	2.00		
Length	(m)=	309.00	40.00		
Mannings n	=	.013	.300		
Max.Eff.Inten.(mm/hr)=		97.10	119.40		
over (min)		5.00	15.00		
Storage Coeff. (min)=		4.13 (ii)	11.47 (ii)		
Unit Hyd. Tpeak (min)=		5.00	15.00		
Unit Hyd. peak (cms)=		.24	.09		
PEAK FLOW (cms)=		.91	2.02	*TOTALS*	2.725 (iii)
TIME TO PEAK (hrs)=		6.00	6.08		6.00
RUNOFF VOLUME (mm)=		72.06	26.53		36.09
TOTAL RAINFALL (mm)=		73.56	73.56		73.56
RUNOFF COEFFICIENT =		.98	.36		.49

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***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0102)				
ID= 1 DT= 5.0 min				
		Area (ha)= 14.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.01	8.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	287.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.95 (ii)	11.29 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.24	.09	
PEAK FLOW (cms)=		.80	1.79	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	2.406 (iii)
RUNOFF VOLUME (mm)=		72.06	26.53	6.00
TOTAL RAINFALL (mm)=		73.56	73.56	36.09
RUNOFF COEFFICIENT =		.98	.36	73.56
				.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0105)				
ID= 1 DT= 5.0 min				
		Area (ha)= 51.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	21.55	29.77	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	550.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.84 (ii)	13.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.20	.08	
				TOTALS

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PEAK FLOW	(cms)=	2.76	5.98	8.044 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	72.06	26.53	36.09
TOTAL RAINFALL	(mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT	=	.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0365)	Area (ha)= 117.50		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		10.00	20.00	
Storage Coeff. (min)=		7.77 (ii)	15.10 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.13	.07	
				TOTALS
PEAK FLOW	(cms)=	5.65	11.98	16.238 (iii)
TIME TO PEAK	(hrs)=	6.00	6.17	6.08
RUNOFF VOLUME	(mm)=	72.06	26.53	36.09
TOTAL RAINFALL	(mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT	=	.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0355)	Area (ha)= 12.30		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.22 (ii)	12.06 (ii)	

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Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.24	.09	
			TOTALS
PEAK FLOW (cms)=	.68	1.49	2.015 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0350) ID= 1 DT= 5.0 min		Area (ha)= 16.30		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=		6.85	9.45	
Dep. Storage (mm)=		1.50	5.00	
Average Slope (%)=		1.00	1.00	
Length (m)=		330.00	40.00	
Mannings n =		.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)=		5.00	15.00	
Storage Coeff. (min)=		5.29 (ii)	14.32 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
				TOTALS
PEAK FLOW (cms)=		.89	1.82	2.485 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		72.06	26.53	36.09
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0360) ID= 1 DT= 5.0 min		Area (ha)= 30.00		
		Total Imp(%)= 37.00	Dir. Conn.(%)= 19.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=		11.10	18.90	
Dep. Storage (mm)=		1.50	5.00	
Average Slope (%)=		2.00	2.00	
Length (m)=		447.00	40.00	
Mannings n =		.013	.300	

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Max.Eff.Inten.(mm/hr)=	97.10	111.81	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.16 (ii)	12.69 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.21	.08	
			TOTALS
PEAK FLOW (cms)=	1.48	3.58	4.647 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	25.57	34.40
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.35	.47

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0395)	Area (ha)= 51.20		
ID= 1 DT= 5.0 min	Total Imp(%)= 10.00	Dir. Conn.(%)= 5.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.12	46.08	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	900.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	88.55	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.85 (ii)	16.11 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.06	
			TOTALS
PEAK FLOW (cms)=	.58	5.35	5.668 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.17
RUNOFF VOLUME (mm)=	72.06	21.36	23.89
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.29	.32

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0455)	Area (ha)= 12.70		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

Hadati Creek Watershed - Allowable

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.25 (ii)	11.94 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.23	.09	
PEAK FLOW	(cms)=	.71	1.55	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	2.088 (iii)
RUNOFF VOLUME	(mm)=	72.06	26.53	6.00
TOTAL RAINFALL	(mm)=	73.56	73.56	36.09
RUNOFF COEFFICIENT	=	.98	.36	73.56
				.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0460)	Area (ha)=	36.00	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.26 (ii)	12.56 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
PEAK FLOW	(cms)=	1.96	4.29	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	5.772 (iii)
RUNOFF VOLUME	(mm)=	72.06	26.53	6.00
TOTAL RAINFALL	(mm)=	73.56	73.56	36.09
RUNOFF COEFFICIENT	=	.98	.36	73.56
				.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

Max.Eff.Inten.(mm/hr)=	97.10	119.40
over (min)	5.00	15.00
Storage Coeff. (min)=	6.63 (ii)	13.97 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.18	.08

				TOTALS
PEAK FLOW	(cms)=	2.27	4.88	6.559 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	72.06	26.53	36.09
TOTAL RAINFALL	(mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT	=	.98	.36	.49

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)
ID= 1 DT=****min

AREA (ha)= .00
QPEAK (cms)= .00
TPEAK (hrs)= .00
VOLUME (mm)=*****

DUHYD (0505)
Inlet Cap.=9.000
#of Inlets= 1
Total(cms)= 9.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	27.66	6.17	38.44
MAJOR SYS.(ID= 2):	81.12	18.66	6.17	38.44
MINOR SYS.(ID= 3):	162.88	9.00	5.92	38.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0566)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0484):	12.60	1.918	6.00	36.09
+ ID2= 2 (0565):	11.10	1.689	6.00	36.09
ID = 3 (0566):	23.70	3.607	6.00	36.09

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0420)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0410):	24.20	3.938	6.00	36.09
+ ID2= 2 (0415):	4.99	1.007	6.00	36.09
<hr/>				
ID = 3 (0420):	29.19	4.945	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	3.122	6.00	36.09
OUTFLOW: ID= 1 (0111)	19.000	.447	6.58	36.08
PEAK FLOW REDUCTION [Qout/Qin](%)= 14.31				
TIME SHIFT OF PEAK FLOW (min)= 35.00				
MAXIMUM STORAGE USED (ha.m.)= .4965				

ADD HYD (0103)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	16.32	2.725	6.00	36.09
+ ID2= 2 (0102):	14.32	2.406	6.00	36.09
<hr/>				
ID = 3 (0103):	30.64	5.131	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0106)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.5000	.4000
	.0100	.0100	6.6000	.8000
	.0260	.2300	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	8.044	6.00	36.09
OUTFLOW: ID= 1 (0106)	51.320	5.545	6.17	36.09

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 PEAK FLOW REDUCTION [Qout/Qin](%)= 68.94
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= .7419

ROUTE CHN (0358)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0355)	12.30	2.02	6.00	36.09	.21	1.25
OUTFLOW: ID= 1 (0358)	12.30	1.38	6.17	36.04	.17	1.15

ROUTE CHN (0353)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

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<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

			<---- hydrograph ---->			<-pipe / channel->	
			AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW : ID= 2 (0350)			16.30	2.49	6.00	36.09	.23
OUTFLOW: ID= 1 (0353)			16.30	1.83	6.17	36.06	.20
							MAX VEL (m/s)
							1.29
							1.23

ROUTE CHN (0362)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63

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.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0360)	30.00	4.65	6.00	34.40	.31	1.61
OUTFLOW:	ID= 1 (0362)	30.00	3.64	6.17	34.39	.27	1.53

ADD HYD (0465)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0455):	12.70	2.088	6.00	36.09
+	ID2= 2 (0460):	36.00	5.772	6.00	36.09
<hr/>					
ID =	3 (0465):	48.70	7.859	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0510):	16.00	3.209	6.00	61.38
+	ID2= 2 (0505):	162.88	9.000	5.92	38.44
<hr/>					
ID =	3 (0515):	178.88	12.209	6.00	40.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0564)	
IN= 2--->	OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	101.50	.0500	
1.00	100.70	.0500	
1.50	100.55	.0500 / .0300	Main Channel
2.00	99.50	.0300	Main Channel
3.50	99.60	.0300	Main Channel
4.50	100.65	.0300 / .0500	Main Channel
6.00	101.45	.0500	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32

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.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

		<----- hydrograph ----->			<-pipe / channel->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0505)	81.12	18.66	6.17	38.44	1.72	1.34
OUTFLOW: ID= 1 (0564)	81.12	28.30	6.50	38.44	1.95	1.41

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

ROUTE CHN (0563)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->		
Distance	Elevation	Manning
.00	1.00	.0350
2.00	.50	.0350
4.00	.00	.0350 / .0350
4.50	.00	.0350
5.00	.00	.0350 / .0350
7.00	.50	.0350
9.00	1.00	.0350

Main Channel
Main Channel
Main Channel

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.573E+01	.0	.67	2.23
.11	.11	.135E+02	.1	.99	1.51
.16	.16	.232E+02	.3	1.23	1.22
.21	.21	.349E+02	.5	1.42	1.06
.26	.26	.486E+02	.9	1.58	.95
.32	.32	.643E+02	1.2	1.73	.87
.37	.37	.820E+02	1.7	1.86	.81
.42	.42	.102E+03	2.2	1.98	.76
.47	.47	.123E+03	2.9	2.10	.71
.53	.53	.147E+03	3.6	2.21	.68
.58	.58	.173E+03	4.4	2.31	.65
.63	.63	.200E+03	5.4	2.42	.62
.68	.68	.230E+03	6.4	2.51	.60
.74	.74	.262E+03	7.6	2.61	.58
.79	.79	.295E+03	8.9	2.70	.56
.84	.84	.331E+03	10.3	2.79	.54
.89	.89	.369E+03	11.8	2.88	.52
.95	.95	.408E+03	13.5	2.97	.51
1.00	1.00	.450E+03	15.2	3.05	.49

	<----- hydrograph ----->			<-pipe / channel->	
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL

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		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0566)		23.70	3.61	6.00	36.09	.53	2.21
OUTFLOW: ID= 1 (0563)		23.70	3.52	6.08	36.09	.52	2.20

DUHYD (0425)
Inlet Cap.=1.980
#of Inlets= 1
Total(cms)= 2.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	4.94	6.00	36.09
MAJOR SYS.(ID= 2):	7.51	2.96	6.00	36.09
MINOR SYS.(ID= 3):	21.68	1.98	5.83	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	.5000
.0100	.0100	10.0000	.6000
.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	5.131	6.00	36.09
OUTFLOW: ID= 1 (0104)	30.640	4.550	6.17	36.08

PEAK FLOW REDUCTION [Qout/Qin] (%)= 88.67
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= .5514

ADD HYD (0359)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0358):	12.30	1.378	6.17	36.04
+ ID2= 2 (0353):	16.30	1.826	6.17	36.06
ID = 3 (0359):	28.60	3.204	6.17	36.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0363)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0359):	28.60	3.204	6.17	36.05
+ ID2= 2 (0362):	30.00	3.642	6.17	34.39
ID = 3 (0363):	58.60	6.846	6.17	35.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek Watershed - Allowable

ADD HYD (0470)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0465):	48.70	7.859	6.00	36.09
+ ID2= 2 (0425):	7.51	2.965	6.00	36.09
=====				
ID = 3 (0470):	56.21	10.824	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0520)				
Inlet Cap.=3.050				
#of Inlets= 1				
Total(cms)= 3.0				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	178.88	12.21	6.00	40.49
=====				
MAJOR SYS.(ID= 2):	74.76	9.16	6.00	40.49
MINOR SYS.(ID= 3):	104.13	3.05	5.67	40.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0561)	
IN= 2---> OUT= 1	Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.319E+01	.1	.87	.95
.11	.11	.748E+01	.2	1.26	.66
.16	.16	.129E+02	.4	1.54	.54
.21	.21	.194E+02	.7	1.75	.48
.26	.26	.270E+02	1.0	1.93	.43
.32	.32	.357E+02	1.5	2.08	.40
.37	.37	.456E+02	2.0	2.22	.38
.42	.42	.565E+02	2.6	2.34	.36
.47	.47	.686E+02	3.4	2.46	.34
.53	.53	.817E+02	4.2	2.57	.32
.58	.58	.960E+02	5.1	2.68	.31
.63	.63	.111E+03	6.2	2.78	.30
.68	.68	.128E+03	7.3	2.87	.29
.74	.74	.145E+03	8.6	2.97	.28
.79	.79	.164E+03	10.0	3.06	.27
.84	.84	.184E+03	11.6	3.14	.27
.89	.89	.205E+03	13.2	3.23	.26

.95	.95	Hadati Creek watershed - Allowable			
1.00	1.00	.227E+03	15.0	3.31	.25
		.250E+03	17.0	3.40	.25

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0563)	23.70	3.52	6.08	36.09	.48	2.48
OUTFLOW: ID= 1 (0561)	23.70	3.57	6.08	36.09	.49	2.49

ADD HYD (0114)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0111):	19.00	.447	6.58	36.08	
+ ID2= 2 (0104):	30.64	4.550	6.17	36.08	
ID = 3 (0114):	49.64	4.877	6.17	36.08	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0365):	117.50	16.238	6.08	36.09	
+ ID2= 2 (0363):	58.60	6.846	6.17	35.20	
ID = 3 (0380):	176.10	22.579	6.08	35.79	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)		
IN= 2--->	OUT= 1	Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	324.60	.0500
115.00	321.60	.0500
120.00	320.80	.0500 / .0300
122.00	320.80	.0300 / .0500
138.00	321.60	.0500
148.00	322.30	.0500
154.00	323.10	.0500
164.00	324.60	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02

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1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

		<---- hydrograph ---->			<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW : ID= 2 (0470)		56.21	10.82	6.00	36.09	.67
OUTFLOW: ID= 1 (0475)		56.21	9.54	6.08	36.09	.64
						MAX VEL (m/s)
						1.43
						1.39

ADD HYD (0526)					
1 + 2 = 3					
ID1= 1 (0520):	74.76	9.159	6.00	40.49	
+ ID2= 2 (0525):	.00	.001	.00	*****	
=====					
ID = 3 (0526):	74.76	9.159	6.00	40.49	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)					
1 + 2 = 3					
ID1= 1 (0561):	23.70	3.571	6.08	36.09	
+ ID2= 2 (0481):	5.90	.898	6.00	36.09	
=====					
ID = 3 (0492):	29.60	4.410	6.08	36.09	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
ID1= 1 (0114):	49.64	4.877	6.17	36.08	
+ ID2= 2 (0106):	51.32	5.545	6.17	36.09	
=====					
ID = 3 (0115):	100.96	10.422	6.17	36.08	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0390)					
IN= 2---> OUT= 1					
DT= 5.0 min					
		OUTFLOW	STORAGE	OUTFLOW	STORAGE

Hadati Creek watershed - Allowable

(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	22.579	6.08	35.79
OUTFLOW: ID= 1 (0390)	176.100	1.387	7.17	35.79

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.14
 TIME SHIFT OF PEAK FLOW (min)= 65.00
 MAXIMUM STORAGE USED (ha.m.)= 4.6291

ROUTE CHN (0527)
 IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel->	
					MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	74.76	9.16	6.00	40.49	2.09	.74
OUTFLOW: ID= 1 (0527)	74.76	7.08	6.17	40.49	2.01	.77

RESERVOIR (0482)
 IN= 2----> OUT= 1
 DT= 5.0 min

OUTFLOW STORAGE | OUTFLOW STORAGE

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(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	29.600	4.410	6.08	36.09
OUTFLOW: ID= 1 (0482)	29.600	2.218	6.33	36.09

PEAK FLOW REDUCTION [Qout/Qin](%)= 50.29
 TIME SHIFT OF PEAK FLOW (min)= 15.00
 MAXIMUM STORAGE USED (ha.m.)= .5440

ADD HYD (0400)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0390):	176.10	1.387	7.17	35.79
+ ID2= 2 (0395):	51.20	5.668	6.17	23.89
ID = 3 (0400):	227.30	6.995	6.17	33.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13

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2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0400)		227.30	7.00	6.17	33.11	.46	1.36
OUTFLOW: ID= 1 (0403)		227.30	4.32	6.33	33.11	.36	1.16

ADD HYD (0407)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0115):	100.96	10.422	6.17	36.08	
+ ID2= 2 (0403):	227.30	4.324	6.33	33.11	
=====					
ID = 3 (0407):	328.26	13.657	6.17	34.03	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0113)					
IN= 2---> OUT= 1					
DT= 5.0 min					
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)	
	.0000	.0000	1.6000	6.4000	
	1.1000	2.9000	9.1000	10.0000	
	1.3000	4.3000	12.0000	20.0000	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
INFLOW : ID= 2 (0407)	328.260	13.657	6.17	34.03	
OUTFLOW: ID= 1 (0113)	328.260	1.367	15.17	34.02	
PEAK FLOW REDUCTION [Qout/Qin] (%) = 10.01					
TIME SHIFT OF PEAK FLOW (min) = 540.00					
MAXIMUM STORAGE USED (ha.m.) = 4.7719					

ADD HYD (0430)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0425):	21.68	1.980	5.83	36.09	
+ ID2= 2 (0113):	328.26	1.367	15.17	34.02	
=====					
ID = 3 (0430):	349.94	2.494	6.25	34.15	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)		
IN= 2---> OUT= 1	Routing time step (min) '=	5.00

<----- DATA FOR SECTION (1.1) ----->

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Distance	Elevation	Manning	
100.00	325.40	.0600	
120.00	324.60	.0600	
126.00	323.90	.0600	
130.00	323.00	.0600	
140.00	322.30	.0600 / .0300	Main Channel
142.00	322.30	.0300 / .0600	Main Channel
150.00	323.90	.0600	
155.00	324.60	.0600	
160.00	325.40	.0600	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0430)	349.94	2.49	6.25	34.15	.35	1.29
OUTFLOW: ID= 1 (0440)	349.94	2.40	6.33	34.15	.34	1.28

ADD HYD (0485)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	2 = 3				
ID1= 1 (0440):		349.94	2.403	6.33	34.15
+ ID2= 2 (0475):		56.21	9.543	6.08	36.09
ID = 3 (0485):		406.15	11.718	6.08	34.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	2 = 3				
ID1= 1 (0485):		406.15	11.718	6.08	34.42
+ ID2= 2 (0480):		43.10	6.559	6.00	36.09

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ID = 3 (0490): 449.25 17.844 6.08 34.58

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0482):	29.60	2.218	6.33	36.09
+ ID2= 2 (0490):	449.25	17.844	6.08	34.58
ID = 3 (0491):	478.85	18.134	6.08	34.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min	.0000	.0000	7.0800	2.4860
	.2760	.0600	8.1000	3.3240
	1.2000	.3400	9.7980	4.6420
	2.0400	.6182	10.4940	7.4397
	2.6400	1.1630	11.6850	10.3000
	3.1200	1.7070	12.3480	11.4000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	478.850	18.134	6.08	34.67
OUTFLOW: ID= 1 (0483)	478.850	7.118	6.50	34.67

PEAK FLOW REDUCTION [Qout/Qin] (%)= 39.25
 TIME SHIFT OF PEAK FLOW (min)= 25.00
 MAXIMUM STORAGE USED (ha.m.)= 2.5265

ADD HYD (0530)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0540):	4.63	1.036	6.00	61.38
+ ID2= 2 (0483):	478.85	7.118	6.50	34.67
ID = 3 (0530):	483.48	7.293	6.50	34.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0527):	74.76	7.076	6.17	40.49
+ ID2= 2 (0530):	483.48	7.293	6.50	34.93
ID = 3 (0545):	558.24	14.150	6.50	35.67

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0542):		25.25	5.333	6.00	61.38
+ ID2= 2 (0545):		558.24	14.150	6.50	35.67
<hr/>					
ID = 3 (0546):		583.49	15.241	6.42	36.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0543):		14.99	3.310	6.00	61.38
+ ID2= 2 (0546):		583.49	15.241	6.42	36.79
<hr/>					
ID = 3 (0547):		598.48	18.314	6.00	37.40

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0544):		1.13	.266	6.00	61.38
+ ID2= 2 (0547):		598.48	18.314	6.00	37.40
<hr/>					
ID = 3 (0548):		599.61	18.579	6.00	37.45

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 ** SIMULATION NUMBER: 4 **

READ STORM		Filename: Y:\SPrimmer\Miduss Modelling\105172\Ci
Ptotal= 90.18 mm		tyview Ridge\100yrSCS12hr.stm
		Comments: 100 year SCS Type II 12hr design storm

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.25	2.26	3.25	3.61	6.25	16.23	9.25	3.16
.50	2.26	3.50	3.61	6.50	16.23	9.50	3.16
.75	2.26	3.75	3.61	6.75	7.21	9.75	3.16
1.00	2.26	4.00	3.61	7.00	7.21	10.00	3.16
1.25	2.26	4.25	5.41	7.25	5.41	10.25	1.80
1.50	2.26	4.50	5.41	7.50	5.41	10.50	1.80
1.75	2.26	4.75	7.21	7.75	5.41	10.75	1.80
2.00	2.26	5.00	7.21	8.00	5.41	11.00	1.80
2.25	2.70	5.25	10.82	8.25	3.16	11.25	1.80

Hadati Creek watershed - Allowable							
2.50	2.70	5.50	10.82	8.50	3.16	11.50	1.80
2.75	2.70	5.75	43.29	8.75	3.16	11.75	1.80
3.00	2.70	6.00	119.04	9.00	3.16	12.00	1.80

CALIB
STANDHYD (0544)
ID= 1 DT= 5.0 min

Area (ha)= 1.13
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.90	.23
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	50.00	40.00
Mannings n =	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	2.26	3.083	3.61	6.083	16.23	9.08	3.16
.167	2.26	3.167	3.61	6.167	16.23	9.17	3.16
.250	2.26	3.250	3.61	6.250	16.23	9.25	3.16
.333	2.26	3.333	3.61	6.333	16.23	9.33	3.16
.417	2.26	3.417	3.61	6.417	16.23	9.42	3.16
.500	2.26	3.500	3.61	6.500	16.23	9.50	3.16
.583	2.26	3.583	3.61	6.583	7.21	9.58	3.16
.667	2.26	3.667	3.61	6.667	7.21	9.67	3.16
.750	2.26	3.750	3.61	6.750	7.21	9.75	3.16
.833	2.26	3.833	3.61	6.833	7.21	9.83	3.16
.917	2.26	3.917	3.61	6.917	7.21	9.92	3.16
1.000	2.26	4.000	3.61	7.000	7.21	10.00	3.16
1.083	2.26	4.083	5.41	7.083	5.41	10.08	1.80
1.167	2.26	4.167	5.41	7.167	5.41	10.17	1.80
1.250	2.26	4.250	5.41	7.250	5.41	10.25	1.80
1.333	2.26	4.333	5.41	7.333	5.41	10.33	1.80
1.417	2.26	4.417	5.41	7.417	5.41	10.42	1.80
1.500	2.26	4.500	5.41	7.500	5.41	10.50	1.80
1.583	2.26	4.583	7.21	7.583	5.41	10.58	1.80
1.667	2.26	4.667	7.21	7.667	5.41	10.67	1.80
1.750	2.26	4.750	7.21	7.750	5.41	10.75	1.80
1.833	2.26	4.833	7.21	7.833	5.41	10.83	1.80
1.917	2.26	4.917	7.21	7.917	5.41	10.92	1.80
2.000	2.26	5.000	7.21	8.000	5.41	11.00	1.80
2.083	2.70	5.083	10.82	8.083	3.16	11.08	1.80
2.167	2.70	5.167	10.82	8.167	3.16	11.17	1.80
2.250	2.70	5.250	10.82	8.250	3.16	11.25	1.80
2.333	2.70	5.333	10.82	8.333	3.16	11.33	1.80
2.417	2.70	5.417	10.82	8.417	3.16	11.42	1.80
2.500	2.70	5.500	10.82	8.500	3.16	11.50	1.80
2.583	2.70	5.583	43.29	8.583	3.16	11.58	1.80
2.667	2.70	5.667	43.29	8.667	3.16	11.67	1.80
2.750	2.70	5.750	43.29	8.750	3.16	11.75	1.80
2.833	2.70	5.833	119.04	8.833	3.16	11.83	1.80
2.917	2.70	5.917	119.04	8.917	3.16	11.92	1.80
3.000	2.70	6.000	119.04	9.000	3.16	12.00	1.80

Max. Eff. Inten. (mm/hr)= 119.04 111.85
over (min) 5.00 15.00

Hadati Creek watershed - Allowable

Storage Coeff. (min)=	1.88 (ii)	12.97 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.32	.08

PEAK FLOW (cms)=	.30	.04	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	.333 (iii)
RUNOFF VOLUME (mm)=	88.68	31.37	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT =	.98	.35	90.18
			.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0543)
 ID= 1 DT= 5.0 min

Area (ha)= 14.99
 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	11.99		3.00
Dep. Storage (mm)=	1.50		5.00
Average Slope (%)=	.55		.55
Length (m)=	200.00		40.00
Mannings n =	.013		.300

Max.Eff.Inten.(mm/hr)=	119.04	111.85
over (min)	5.00	20.00
Storage Coeff. (min)=	4.32 (ii)	15.41 (ii)
Unit Hyd. Tpeak (min)=	5.00	20.00
Unit Hyd. peak (cms)=	.23	.07

PEAK FLOW (cms)=	3.84	.48	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.17	4.164 (iii)
RUNOFF VOLUME (mm)=	88.68	31.37	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT =	.98	.35	90.18
			.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0542)
 ID= 1 DT= 5.0 min

Area (ha)= 25.25
 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	20.20		5.05
Dep. Storage (mm)=	1.50		5.00
Average Slope (%)=	.55		.55

Hadati Creek watershed - Allowable

Length (m)=	350.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	119.04	111.85
over (min)	5.00	20.00
Storage Coeff. (min)=	6.05 (ii)	17.13 (ii)
Unit Hyd. Tpeak (min)=	5.00	20.00
Unit Hyd. peak (cms)=	.19	.06

PEAK FLOW (cms)=	6.23	.77	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.17	6.749 (iii)
RUNOFF VOLUME (mm)=	88.68	31.37	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT =	.98	.35	90.18
			.85

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 16.00	
STANDHYD (0510)	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00
ID= 1 DT= 5.0 min		

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	12.80	3.20	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.50	.20	
Length (m)=	400.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	91.82	
over (min)	5.00	25.00	
Storage Coeff. (min)=	6.74 (ii)	22.99 (ii)	
Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	.18	.05	
PEAK FLOW (cms)=	3.88	.40	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.25	4.080 (iii)
RUNOFF VOLUME (mm)=	88.68	31.37	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT =	.98	.35	90.18
			.85

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 244.00	
STANDHYD (0500)	Total Imp(%)= 46.00	Dir. Conn.(%)= 26.00
ID= 1 DT= 5.0 min		

IMPERVIOUS PERVIOUS (i)

Hadati Creek watershed - Allowable

Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	150.55	
over (min)		10.00	25.00	
Storage Coeff. (min)=		11.73 (ii)	20.53 (ii)	
Unit Hyd. Tpeak (min)=		10.00	25.00	
Unit Hyd. peak (cms)=		.10	.05	
PEAK FLOW	(cms)=	15.54	24.76	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.25	34.262 (iii)
RUNOFF VOLUME	(mm)=	88.68	36.25	6.17
TOTAL RAINFALL	(mm)=	90.18	90.18	49.88
RUNOFF COEFFICIENT	=	.98	.40	90.18
				.55

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0540)				
ID= 1 DT= 5.0 min	Area (ha)= 4.63	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	111.85	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.64 (ii)	14.73 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.08	
PEAK FLOW	(cms)=	1.20	.16	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	1.339 (iii)
RUNOFF VOLUME	(mm)=	88.68	31.37	6.00
TOTAL RAINFALL	(mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT	=	.98	.35	90.18
				.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STANDHYD (0484)		Hadati Creek watershed - Allowable	
ID= 1 DT= 5.0 min	Area (ha)= 12.60	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.29	7.31	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.11 (ii)	12.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.08	
PEAK FLOW (cms)=	.83	1.92	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	2.550 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0565)		Area (ha)= 11.10	
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	4.66	6.44	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.11 (ii)	12.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.08	
PEAK FLOW (cms)=	.73	1.69	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	2.246 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek watershed - Allowable

CALIB
STANDHYD (0481)
ID= 1 DT= 5.0 min

Area (ha)= 5.90
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.48	3.42	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.11 (ii)	12.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.08	
PEAK FLOW (cms)=	.39	.90	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	1.194 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0410)
ID= 1 DT= 5.0 min

Area (ha)= 24.20
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	10.16	14.04	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	401.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.45 (ii)	11.16 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.23	.09	
PEAK FLOW (cms)=	1.64	3.90	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	5.204 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- Hadati Creek watershed - Allowable
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0415)
ID= 1 DT= 5.0 min

Area (ha)= 4.99
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.10	2.89	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.86	2.86	
Length (m)=	185.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.51 (ii)	8.54 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	.29	.12	
PEAK FLOW (cms)=	.35	.96	*TOTALS* 1.304 (iii)
TIME TO PEAK (hrs)=	6.00	6.00	6.00
RUNOFF VOLUME (mm)=	88.68	36.13	47.17
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0110)
ID= 1 DT= 5.0 min

Area (ha)= 19.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	7.98	11.02	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	365.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.21 (ii)	10.91 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.24	.09	
PEAK FLOW (cms)=	1.30	3.09	*TOTALS* 4.123 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	36.13	47.17
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.40	.52

Hadati Creek watershed - Allowable

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min		Area (ha)= 16.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.47	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	309.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.81 (ii)	10.51 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.09	
PEAK FLOW (cms)=		1.12	2.69	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	3.593 (iii)
RUNOFF VOLUME (mm)=		88.68	36.13	6.00
TOTAL RAINFALL (mm)=		90.18	90.18	47.17
RUNOFF COEFFICIENT =		.98	.40	90.18
				.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0102) ID= 1 DT= 5.0 min		Area (ha)= 14.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.01	8.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	287.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.64 (ii)	10.35 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.09	
PEAK FLOW (cms)=		.98	2.37	*TOTALS*
				3.171 (iii)

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TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	88.68	36.13	47.17
TOTAL RAINFALL	(mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT	=	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB					
STANDHYD (0105)					
ID= 1 DT= 5.0 min		Area (ha)= 51.32			
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00		
		IMPERVIOUS	PERVIOUS (i)		
Surface Area	(ha)=	21.55	29.77		
Dep. Storage	(mm)=	1.50	5.00		
Average Slope	(%)=	2.00	2.00		
Length	(m)=	550.00	40.00		
Mannings n	=	.013	.300		
Max.Eff.Inten.(mm/hr)=		119.04	149.56		
over (min)		5.00	15.00		
Storage Coeff. (min)=		5.38 (ii)	12.09 (ii)		
Unit Hyd. Tpeak (min)=		5.00	15.00		
Unit Hyd. peak (cms)=		.21	.09		
PEAK FLOW	(cms)=	3.42	8.01	*TOTALS*	
TIME TO PEAK	(hrs)=	6.00	6.08	10.668 (iii)	
RUNOFF VOLUME	(mm)=	88.68	36.13	6.00	
TOTAL RAINFALL	(mm)=	90.18	90.18	47.17	
RUNOFF COEFFICIENT	=	.98	.40	90.18	
				.52	

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0365)			
ID= 1 DT= 5.0 min		Area (ha)= 117.50	
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	49.35	68.15
Dep. Storage	(mm)=	1.50	5.00
Average slope	(%)=	2.00	2.00
Length	(m)=	885.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		119.04	149.56
over (min)		5.00	15.00
Storage Coeff. (min)=		7.16 (ii)	13.86 (ii)

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Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.17	.08	
PEAK FLOW (cms)=	7.49	17.25	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	22.881 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0355)	Area (ha)= 12.30		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.17	7.13	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.60	1.60	
Length (m)=	286.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)=	5.00	15.00	
Storage Coeff. (min)=	3.89 (ii)	11.05 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.25	.09	
PEAK FLOW (cms)=	.84	1.99	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	2.661 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0350)	Area (ha)= 16.30		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	6.85	9.45	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.00	1.00	
Length (m)=	330.00	40.00	
Mannings n =	.013	.300	

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Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.88 (ii)	13.13 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.08	
			TOTALS
PEAK FLOW (cms)=	1.10	2.45	3.299 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	36.13	47.17
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0360)	Area (ha)= 30.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 37.00	Dir. Conn.(%)= 19.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.10	18.90	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	447.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	140.44	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.75 (ii)	11.63 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.09	
			TOTALS
PEAK FLOW (cms)=	1.83	4.81	6.183 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	35.04	45.23
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.39	.50

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0395)	Area (ha)= 51.20		
ID= 1 DT= 5.0 min	Total Imp(%)= 10.00	Dir. Conn.(%)= 5.00	

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		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.12	46.08	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	112.64	
over (min)		5.00	15.00	
Storage Coeff. (min)=		7.23 (ii)	14.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.17	.08	
PEAK FLOW (cms)=		.78	8.19	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	8.631 (iii)
RUNOFF VOLUME (mm)=		88.68	31.49	6.08
TOTAL RAINFALL (mm)=		90.18	90.18	34.35
RUNOFF COEFFICIENT =		.98	.35	90.18
				.38

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0455)	Area (ha)= 12.70		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.92 (ii)	10.95 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.24	.09	
PEAK FLOW (cms)=		.87	2.06	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	2.756 (iii)
RUNOFF VOLUME (mm)=		88.68	36.13	6.00
TOTAL RAINFALL (mm)=		90.18	90.18	47.17
RUNOFF COEFFICIENT =		.98	.40	90.18
				.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0460)
ID= 1 DT= 5.0 min

Area (ha)= 36.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.84 (ii)	11.52 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.09	
				TOTALS
PEAK FLOW (cms)=		2.43	5.73	7.639 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		88.68	36.13	47.17
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	18.10	25.00	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		6.11 (ii)	12.82 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.19	.08	
				TOTALS
PEAK FLOW (cms)=		2.82	6.56	8.721 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		88.68	36.13	47.17
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.40	.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14

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- Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)	AREA (ha)=	.00
ID= 1 DT=****min	QPEAK (cms)=	.00
	TPEAK (hrs)=	.00
	VOLUME (mm)=	*****

DUHYD (0505)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
Inlet Cap.=9.000				
#of Inlets= 1				
Total(cms)= 9.0				
TOTAL HYD.(ID= 1):	244.00	34.26	6.17	49.88
MAJOR SYS.(ID= 2):	102.03	25.26	6.17	49.88
MINOR SYS.(ID= 3):	141.97	9.00	5.83	49.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0566)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0484):	12.60	2.550	6.00	47.17
+ ID2= 2 (0565):	11.10	2.246	6.00	47.17
ID = 3 (0566):	23.70	4.796	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0420)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0410):	24.20	5.204	6.00	47.17
+ ID2= 2 (0415):	4.99	1.304	6.00	47.17
ID = 3 (0420):	29.19	6.509	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min				
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000

AREA QPEAK TPEAK R.V.
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	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0110)	19.000	4.123	6.00	47.17
OUTFLOW: ID= 1 (0111)	19.000	.613	6.58	47.16

PEAK FLOW REDUCTION [Qout/Qin](%)= 14.87
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= .6478

ADD HYD (0103)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0101):	16.32	3.593	6.00	47.17
+ ID2= 2 (0102):	14.32	3.171	6.00	47.17
ID = 3 (0103):	30.64	6.763	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0106)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min	.0000	.0000	.5000	.4000
	.0100	.0100	6.6000	.8000
	.0260	.2300	.0000	.0000

**** WARNING : STORAGE-DISCHARGE TABLE WAS EXCEEDED.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	10.668	6.00	47.17
OUTFLOW: ID= 1 (0106)	51.320	7.689	6.17	47.16

PEAK FLOW REDUCTION [Qout/Qin](%)= 72.08
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= .8782

ROUTE CHN (0358)	Routing time step (min)'= 5.00
IN= 2---> OUT= 1	

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46

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.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0355)	12.30	2.66	6.00	47.17	.23	1.31
OUTFLOW:	ID= 1 (0358)	12.30	1.86	6.17	47.12	.20	1.23

ROUTE CHN (0353)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
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		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0350)	16.30	3.30	6.00	47.17	.26	1.34
OUTFLOW:	ID= 1 (0353)	16.30	2.44	6.17	47.13	.22	1.29

ROUTE CHN (0362)
IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0360)	30.00	6.18	6.00	45.23	.35	1.71
OUTFLOW:	ID= 1 (0362)	30.00	4.88	6.17	45.22	.31	1.63

ADD HYD (0465)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0455):	12.70	2.756	6.00	47.17
+ ID2= 2 (0460):	36.00	7.639	6.00	47.17
=====				
ID = 3 (0465):	48.70	10.395	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0515)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0510):	16.00	4.080	6.00	76.65
+ ID2= 2 (0505):	141.97	9.000	5.83	49.88
=====				
ID = 3 (0515):	157.97	13.080	6.00	52.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0564)	Routing time step (min)'= 5.00
IN= 2---> OUT= 1	

<----- DATA FOR SECTION (1.1) ----->				
Distance	Elevation	Manning		
.00	101.50	.0500		
1.00	100.70	.0500		
1.50	100.55	.0500 / .0300		Main Channel
2.00	99.50	.0300		Main Channel
3.50	99.60	.0300		Main Channel
4.50	100.65	.0300 / .0500		Main Channel
6.00	101.45	.0500		

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

<----- hydrograph ----->					<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0505)	102.03	25.26	6.17	49.88	1.80	1.37
OUTFLOW: ID= 1 (0564)	102.03	39.67	6.58	49.88	1.95	1.41

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

| IN= 2---> OUT= 1 | Hadati Creek Watershed - Allowable
Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->
 Distance Elevation Manning
 .00 1.00 .0350
 2.00 .50 .0350
 4.00 .00 .0350 / .0350 Main Channel
 4.50 .00 .0350 Main Channel
 5.00 .00 .0350 / .0350 Main Channel
 7.00 .50 .0350
 9.00 1.00 .0350

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .05 .05 .573E+01 .0 .67 2.23
 .11 .11 .135E+02 .1 .99 1.51
 .16 .16 .232E+02 .3 1.23 1.22
 .21 .21 .349E+02 .5 1.42 1.06
 .26 .26 .486E+02 .9 1.58 .95
 .32 .32 .643E+02 1.2 1.73 .87
 .37 .37 .820E+02 1.7 1.86 .81
 .42 .42 .102E+03 2.2 1.98 .76
 .47 .47 .123E+03 2.9 2.10 .71
 .53 .53 .147E+03 3.6 2.21 .68
 .58 .58 .173E+03 4.4 2.31 .65
 .63 .63 .200E+03 5.4 2.42 .62
 .68 .68 .230E+03 6.4 2.51 .60
 .74 .74 .262E+03 7.6 2.61 .58
 .79 .79 .295E+03 8.9 2.70 .56
 .84 .84 .331E+03 10.3 2.79 .54
 .89 .89 .369E+03 11.8 2.88 .52
 .95 .95 .408E+03 13.5 2.97 .51
 1.00 1.00 .450E+03 15.2 3.05 .49

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0566) 23.70 4.80 6.00 47.17 .60 2.35
 OUTFLOW: ID= 1 (0563) 23.70 4.63 6.08 47.17 .59 2.33

DUHYD (0425)
 Inlet Cap.=1.980
 #of Inlets= 1
 Total(cms)= 2.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	6.51	6.00	47.17
MAJOR SYS.(ID= 2):	10.15	4.53	6.00	47.17
MINOR SYS.(ID= 3):	19.04	1.98	5.83	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	.5000

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.0100	.0100	10.0000	.6000
.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	6.763	6.00	47.17
OUTFLOW: ID= 1 (0104)	30.640	7.048	6.08	47.16

PEAK FLOW REDUCTION [Qout/Qin] (%)=104.21
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .5855

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ADD HYD (0359) 1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0358):	12.30	1.856	6.17	47.12
+ ID2= 2 (0353):	16.30	2.435	6.17	47.13
=====				
ID = 3 (0359):	28.60	4.291	6.17	47.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0363) 1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0359):	28.60	4.291	6.17	47.13
+ ID2= 2 (0362):	30.00	4.880	6.17	45.22
=====				
ID = 3 (0363):	58.60	9.171	6.17	46.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0470) 1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0465):	48.70	10.395	6.00	47.17
+ ID2= 2 (0425):	10.15	4.529	6.00	47.17
=====				
ID = 3 (0470):	58.85	14.924	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0520) Inlet Cap.=3.050 #of Inlets= 1 Total(cms)= 3.0				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	157.97	13.08	6.00	52.60
=====				
MAJOR SYS.(ID= 2):	67.54	10.03	6.00	52.60

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 MINOR SYS.(ID= 3): 90.43 3.05 5.58 52.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0561)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 1.00 .0350
 2.00 .50 .0350
 4.00 .00 .0350 / .0350 Main Channel
 4.50 .00 .0350 Main Channel
 5.00 .00 .0350 / .0350 Main Channel
 7.00 .50 .0350
 9.00 1.00 .0350

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.319E+01	.1	.87	.95
.11	.11	.748E+01	.2	1.26	.66
.16	.16	.129E+02	.4	1.54	.54
.21	.21	.194E+02	.7	1.75	.48
.26	.26	.270E+02	1.0	1.93	.43
.32	.32	.357E+02	1.5	2.08	.40
.37	.37	.456E+02	2.0	2.22	.38
.42	.42	.565E+02	2.6	2.34	.36
.47	.47	.686E+02	3.4	2.46	.34
.53	.53	.817E+02	4.2	2.57	.32
.58	.58	.960E+02	5.1	2.68	.31
.63	.63	.111E+03	6.2	2.78	.30
.68	.68	.128E+03	7.3	2.87	.29
.74	.74	.145E+03	8.6	2.97	.28
.79	.79	.164E+03	10.0	3.06	.27
.84	.84	.184E+03	11.6	3.14	.27
.89	.89	.205E+03	13.2	3.23	.26
.95	.95	.227E+03	15.0	3.31	.25
1.00	1.00	.250E+03	17.0	3.40	.25

----- hydrograph -----> <--pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0563)	23.70	4.63	6.08	47.17	.55	2.62
OUTFLOW: ID= 1 (0561)	23.70	4.69	6.08	47.17	.55	2.63

ADD HYD (0114)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0111):	19.00	.613	6.58	47.16
+ ID2= 2 (0104):	30.64	7.048	6.08	47.16
ID = 3 (0114):	49.64	7.421	6.08	47.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0380)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0365):		117.50	22.881	6.00	47.17
+ ID2= 2 (0363):		58.60	9.171	6.17	46.15
ID = 3 (0380):		176.10	30.231	6.08	46.83

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)		Routing time step (min)'= 5.00
IN= 2--->	OUT= 1	

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	324.60	.0500
115.00	321.60	.0500
120.00	320.80	.0500 / .0300 Main Channel
122.00	320.80	.0300 / .0500 Main Channel
138.00	321.60	.0500
148.00	322.30	.0500
154.00	323.10	.0500
164.00	324.60	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

<---- hydrograph ---->				<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	MAX DEPTH
					(m)
INFLOW : ID= 2 (0470)	58.85	14.92	6.00	47.17	.78
OUTFLOW: ID= 1 (0475)	58.85	13.38	6.08	47.17	.74
					MAX VEL
					(m/s)

ADD HYD (0526)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3				

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	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0520):	67.54	10.030	6.00	52.60
+ ID2= 2 (0525):	.00	.001	.00	*****
<hr/>				
ID = 3 (0526):	67.54	10.030	6.00	52.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0561):		23.70	4.690	6.08	47.17
+ ID2= 2 (0481):		5.90	1.194	6.00	47.17
<hr/>					
ID = 3 (0492):		29.60	5.789	6.08	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0114):		49.64	7.421	6.08	47.16
+ ID2= 2 (0106):		51.32	7.689	6.17	47.16
<hr/>					
ID = 3 (0115):		100.96	14.393	6.08	47.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0390)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	1.3100	1.6000
		.7700	.2870	1.8600	23.2300
		1.2600	.9680	.0000	.0000
		<hr/>			
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0380)		176.100	30.231	6.08	46.83
OUTFLOW: ID= 1 (0390)		176.100	1.430	7.25	46.83

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.73
 TIME SHIFT OF PEAK FLOW (min)= 70.00
 MAXIMUM STORAGE USED (ha.m.)= 6.3304

ROUTE CHN (0527)		Routing time step (min)'= 5.00	
IN= 2---> OUT= 1			
<hr/>			
<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel

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141.50 310.80 .0300 Main Channel
142.00 312.40 .0300 / .0500 Main Channel
160.00 313.20 .0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	67.54	10.03	6.00	52.60	2.13	.74
OUTFLOW: ID= 1 (0527)	67.54	7.92	6.08	52.59	2.04	.76

RESERVOIR (0482)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	29.600	5.789	6.08	47.17
OUTFLOW: ID= 1 (0482)	29.600	3.997	6.25	47.17

PEAK FLOW REDUCTION [Qout/Qin](%)= 69.05
TIME SHIFT OF PEAK FLOW (min)= 10.00
MAXIMUM STORAGE USED (ha.m.)= .5994

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0390):	176.10	1.430	7.25	46.83

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+ ID2= 2 (0395):	51.20	8.631	6.08	34.35
ID = 3 (0400):	227.30	9.969	6.08	44.02

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0400)	227.30	9.97	6.08	44.02	.54	1.50
OUTFLOW: ID= 1 (0403)	227.30	6.22	6.25	44.02	.43	1.29

ADD HYD (0407)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0115):	100.96	14.393	6.08	47.16
+ ID2= 2 (0403):	227.30	6.216	6.25	44.02
ID = 3 (0407):	328.26	18.926	6.17	44.98

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek Watershed - Allowable

RESERVOIR (0113)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.6000	6.4000
1.1000	2.9000	9.1000	10.0000
1.3000	4.3000	12.0000	20.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	18.926	6.17	44.98
OUTFLOW: ID= 1 (0113)	328.260	1.552	12.50	44.98

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.20
TIME SHIFT OF PEAK FLOW (min)=380.00
MAXIMUM STORAGE USED (ha.m.)= 6.0640

ADD HYD (0430)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0425):	19.04	1.980	5.83	47.17
+ ID2= 2 (0113):	328.26	1.552	12.50	44.98
ID = 3 (0430):	347.30	3.000	6.33	45.10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning
100.00	325.40	.0600
120.00	324.60	.0600
126.00	323.90	.0600
130.00	323.00	.0600
140.00	322.30	.0600 / .0300
142.00	322.30	.0300 / .0600
150.00	323.90	.0600
155.00	324.60	.0600
160.00	325.40	.0600

Main Channel
Main Channel

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41

Hadati Creek watershed - Allowable					
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0430)	347.30	3.00	6.33	45.10	.38	1.33
OUTFLOW:	ID= 1 (0440)	347.30	2.86	6.42	45.10	.37	1.31

ADD HYD (0485)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0440):	347.30	2.860	6.42	45.10
+	ID2= 2 (0475):	58.85	13.381	6.08	47.17
=====					
ID =	3 (0485):	406.15	15.674	6.08	45.40

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0485):	406.15	15.674	6.08	45.40
+	ID2= 2 (0480):	43.10	8.721	6.00	47.17
=====					
ID =	3 (0490):	449.25	23.705	6.08	45.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0482):	29.60	3.997	6.25	47.17
+	ID2= 2 (0490):	449.25	23.705	6.08	45.57
=====					
ID =	3 (0491):	478.85	24.885	6.08	45.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)					
IN= 2----> OUT= 1					
DT= 5.0 min					
		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
		.0000	.0000	7.0800	2.4860

Hadati Creek watershed - Allowable

.2760	.0600	8.1000	3.3240
1.2000	.3400	9.7980	4.6420
2.0400	.6182	10.4940	7.4397
2.6400	1.1630	11.6850	10.3000
3.1200	1.7070	12.3480	11.4000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	478.850	24.885	6.08	45.67
OUTFLOW: ID= 1 (0483)	478.850	8.373	6.58	45.67

PEAK FLOW REDUCTION [Qout/Qin](%)= 33.65
TIME SHIFT OF PEAK FLOW (min)= 30.00
MAXIMUM STORAGE USED (ha.m.)= 3.5408

ADD HYD (0530)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0540):	4.63	1.339	6.00	76.65
+ ID2= 2 (0483):	478.85	8.373	6.58	45.67
ID = 3 (0530):	483.48	8.559	6.50	45.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0527):	67.54	7.924	6.08	52.59
+ ID2= 2 (0530):	483.48	8.559	6.50	45.97
ID = 3 (0545):	551.02	15.770	6.42	46.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0542):	25.25	6.749	6.00	76.65
+ ID2= 2 (0545):	551.02	15.770	6.42	46.78
ID = 3 (0546):	576.27	18.223	6.00	48.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0543):	14.99	4.164	6.00	76.65
+ ID2= 2 (0546):	576.27	18.223	6.00	48.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	6.35	3.25	12.70	6.25	23.11	9.25	52.83
.50	6.35	3.50	12.70	6.50	23.11	9.50	52.83
.75	6.35	3.75	12.70	6.75	23.11	9.75	52.83
1.00	6.35	4.00	12.70	7.00	23.11	10.00	52.83
1.25	4.32	4.25	16.76	7.25	12.70	10.25	37.85
1.50	4.32	4.50	16.76	7.50	12.70	10.50	37.85
1.75	4.32	4.75	16.76	7.75	12.70	10.75	37.85
2.00	4.32	5.00	16.76	8.00	12.70	11.00	37.85
2.25	6.35	5.25	12.70	8.25	12.70	11.25	12.70
2.50	6.35	5.50	12.70	8.50	12.70	11.50	12.70
2.75	6.35	5.75	12.70	8.75	12.70	11.75	12.70
3.00	6.35	6.00	12.70	9.00	12.70	12.00	12.70

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

Hadati Creek Watershed - Allowable							
.083	6.35	3.083	12.70	6.083	23.11	9.08	52.83
.167	6.35	3.167	12.70	6.167	23.11	9.17	52.83
.250	6.35	3.250	12.70	6.250	23.11	9.25	52.83
.333	6.35	3.333	12.70	6.333	23.11	9.33	52.83
.417	6.35	3.417	12.70	6.417	23.11	9.42	52.83
.500	6.35	3.500	12.70	6.500	23.11	9.50	52.83
.583	6.35	3.583	12.70	6.583	23.11	9.58	52.83
.667	6.35	3.667	12.70	6.667	23.11	9.67	52.83
.750	6.35	3.750	12.70	6.750	23.11	9.75	52.83
.833	6.35	3.833	12.70	6.833	23.11	9.83	52.83
.917	6.35	3.917	12.70	6.917	23.11	9.92	52.83
1.000	6.35	4.000	12.70	7.000	23.11	10.00	52.83
1.083	4.32	4.083	16.76	7.083	12.70	10.08	37.85
1.167	4.32	4.167	16.76	7.167	12.70	10.17	37.85
1.250	4.32	4.250	16.76	7.250	12.70	10.25	37.85
1.333	4.32	4.333	16.76	7.333	12.70	10.33	37.85
1.417	4.32	4.417	16.76	7.417	12.70	10.42	37.85
1.500	4.32	4.500	16.76	7.500	12.70	10.50	37.85
1.583	4.32	4.583	16.76	7.583	12.70	10.58	37.85
1.667	4.32	4.667	16.76	7.667	12.70	10.67	37.85
1.750	4.32	4.750	16.76	7.750	12.70	10.75	37.85
1.833	4.32	4.833	16.76	7.833	12.70	10.83	37.85
1.917	4.32	4.917	16.76	7.917	12.70	10.92	37.85
2.000	4.32	5.000	16.76	8.000	12.70	11.00	37.85
2.083	6.35	5.083	12.70	8.083	12.70	11.08	12.70
2.167	6.35	5.167	12.70	8.167	12.70	11.17	12.70
2.250	6.35	5.250	12.70	8.250	12.70	11.25	12.70
2.333	6.35	5.333	12.70	8.333	12.70	11.33	12.70
2.417	6.35	5.417	12.70	8.417	12.70	11.42	12.70
2.500	6.35	5.500	12.70	8.500	12.70	11.50	12.70
2.583	6.35	5.583	12.70	8.583	12.70	11.58	12.70
2.667	6.35	5.667	12.70	8.667	12.70	11.67	12.70
2.750	6.35	5.750	12.70	8.750	12.70	11.75	12.70
2.833	6.35	5.833	12.70	8.833	12.70	11.83	12.70
2.917	6.35	5.917	12.70	8.917	12.70	11.92	12.70
3.000	6.35	6.000	12.70	9.000	12.70	12.00	12.70

Max.Eff.Inten.(mm/hr)= 52.83 42.97
 over (min) 5.00 20.00
 Storage Coeff. (min)= 2.60 (ii) 18.86 (ii)
 Unit Hyd. Tpeak (min)= 5.00 20.00
 Unit Hyd. peak (cms)= .29 .06

PEAK FLOW (cms)= .13 .03
 TIME TO PEAK (hrs)= 9.67 10.00
 RUNOFF VOLUME (mm)= 209.57 81.35
 TOTAL RAINFALL (mm)= 211.07 211.07
 RUNOFF COEFFICIENT = .99 .39

TOTALS

.156 (iii)
 10.00
 182.64
 211.07
 .87

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 14.99
STANDHYD (0543)	Total Imp(%)= 80.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)= 79.00

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Hadati Creek Watershed - Allowable

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	11.99	3.00	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	200.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	42.97	
over (min)		5.00	25.00	
Storage Coeff. (min)=		5.98 (ii)	22.24 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.19	.05	
PEAK FLOW	(cms)=	1.74	.32	*TOTALS*
TIME TO PEAK	(hrs)=	10.00	10.08	2.054 (iii)
RUNOFF VOLUME	(mm)=	209.57	81.35	10.00
TOTAL RAINFALL	(mm)=	211.07	211.07	182.64
RUNOFF COEFFICIENT	=	.99	.39	211.07
				.87

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0542)	
ID= 1 DT= 5.0 min	
Area (ha)= 25.25	
Total Imp(%)= 80.00	
Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	20.20	5.05	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	350.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	42.97	
over (min)		10.00	25.00	
Storage Coeff. (min)=		8.37 (ii)	24.63 (ii)	
Unit Hyd. Tpeak (min)=		10.00	25.00	
Unit Hyd. peak (cms)=		.12	.05	
PEAK FLOW	(cms)=	2.92	.53	*TOTALS*
TIME TO PEAK	(hrs)=	10.00	10.17	3.443 (iii)
RUNOFF VOLUME	(mm)=	209.57	81.35	10.00
TOTAL RAINFALL	(mm)=	211.07	211.07	182.64
RUNOFF COEFFICIENT	=	.99	.39	211.07
				.87

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek Watershed - Allowable

CALIB
STANDHYD (0510)
ID= 1 DT= 5.0 min

Area (ha)= 16.00
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	42.97	
over (min)		10.00	35.00	
Storage Coeff. (min)=		9.33 (ii)	31.35 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.12	.03	
PEAK FLOW (cms)=		1.85	.31	*TOTALS* 2.134 (iii)
TIME TO PEAK (hrs)=		10.00	10.33	10.00
RUNOFF VOLUME (mm)=		209.57	81.35	182.64
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.39	.87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0500)
ID= 1 DT= 5.0 min

Area (ha)= 244.00
Total Imp(%)= 46.00 Dir. Conn.(%)= 26.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.90	
over (min)		15.00	30.00	
Storage Coeff. (min)=		16.24 (ii)	28.96 (ii)	
Unit Hyd. Tpeak (min)=		15.00	30.00	
Unit Hyd. peak (cms)=		.07	.04	
PEAK FLOW (cms)=		9.05	18.51	*TOTALS* 27.108 (iii)
TIME TO PEAK (hrs)=		10.00	10.25	10.08
RUNOFF VOLUME (mm)=		209.57	107.75	134.22
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.51	.64

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Hadati Creek watershed - Allowable

CALIB STANDHYD (0540) ID= 1 DT= 5.0 min		Area (ha)= 4.63 Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	42.97	
over (min)		5.00	25.00	
Storage Coeff. (min)=		5.03 (ii)	21.29 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.21	.05	
TOTALS				
PEAK FLOW	(cms)=	.54	.10	.636 (iii)
TIME TO PEAK	(hrs)=	10.00	10.08	10.00
RUNOFF VOLUME	(mm)=	209.57	81.35	182.64
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.39	.87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0484) ID= 1 DT= 5.0 min		Area (ha)= 12.60 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	5.29	7.31
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		52.83	59.46
over (min)		10.00	20.00
Storage Coeff. (min)=		8.46 (ii)	18.15 (ii)
Unit Hyd. Tpeak (min)=		10.00	20.00
Unit Hyd. peak (cms)=		.12	.06
TOTALS			
PEAK FLOW	(cms)=	.39	1.14
TIME TO PEAK	(hrs)=	10.00	10.00
RUNOFF VOLUME	(mm)=	209.57	107.20
TOTAL RAINFALL	(mm)=	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.51
			1.527 (iii)
			10.00
			128.70
			211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

Hadati Creek watershed - Allowable

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0565)
ID= 1 DT= 5.0 min

Area (ha)= 11.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	4.66	6.44	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.46 (ii)	18.15 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
PEAK FLOW (cms)=		.34	1.00	*TOTALS* 1.345 (iii)
TIME TO PEAK (hrs)=		10.00	10.00	10.00
RUNOFF VOLUME (mm)=		209.57	107.20	128.70
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0481)
ID= 1 DT= 5.0 min

Area (ha)= 5.90
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.48	3.42	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.46 (ii)	18.15 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
PEAK FLOW (cms)=		.18	.53	*TOTALS* .715 (iii)
TIME TO PEAK (hrs)=		10.00	10.00	10.00
RUNOFF VOLUME (mm)=		209.57	107.20	128.70
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.51	.61

Hadati Creek Watershed - Allowable

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0410) ID= 1 DT= 5.0 min	Area (ha)= 24.20 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	10.16	14.04	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	401.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.16 (ii)	15.86 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.19	.07	
PEAK FLOW (cms)=	.75	2.23	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	2.975 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT =	.99	.51	211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0415) ID= 1 DT= 5.0 min	Area (ha)= 4.99 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.10	2.89	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.86	2.86	
Length (m)=	185.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	15.00	
Storage Coeff. (min)=	3.48 (ii)	12.19 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.26	.09	
PEAK FLOW (cms)=	.15	.47	*TOTALS*
TIME TO PEAK (hrs)=	9.92	10.00	.626 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
			211.07

Hadati Creek watershed - Allowable
 RUNOFF COEFFICIENT = .99 .51 .61

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0110)	Area (ha)= 19.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	7.98	11.02	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	365.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	5.82 (ii)	15.52 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.20	.07	
			TOTALS
PEAK FLOW (cms)=	.59	1.75	2.340 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0101)	Area (ha)= 16.32		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.47	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	309.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.27 (ii)	14.96 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.21	.08	
			TOTALS

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PEAK FLOW	(cms)=	.50	1.52	2.027 (iii)
TIME TO PEAK	(hrs)=	10.00	10.00	10.00
RUNOFF VOLUME	(mm)=	209.57	107.20	128.70
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0102)	Area	(ha)=	14.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.01	8.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	287.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.04 (ii)	14.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
				TOTALS
PEAK FLOW	(cms)=	.44	1.34	1.780 (iii)
TIME TO PEAK	(hrs)=	10.00	10.00	10.00
RUNOFF VOLUME	(mm)=	209.57	107.20	128.70
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0105)	Area	(ha)=	51.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	21.55	29.77	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	550.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		7.45 (ii)	17.14 (ii)	

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Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.17	.06	
			TOTALS
PEAK FLOW (cms)=	1.58	4.68	6.260 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0365)	
ID= 1 DT= 5.0 min	
Area (ha)= 117.50	
Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	49.35		68.15	
Dep. Storage (mm)=	1.50		5.00	
Average Slope (%)=	2.00		2.00	
Length (m)=	885.00		40.00	
Mannings n =	.013		.300	
Max.Eff.Inten.(mm/hr)=	52.83		59.46	
over (min)	10.00		20.00	
Storage Coeff. (min)=	9.91 (ii)		19.60 (ii)	
Unit Hyd. Tpeak (min)=	10.00		20.00	
Unit Hyd. peak (cms)=	.11		.06	
				TOTALS
PEAK FLOW (cms)=	3.61		10.49	14.089 (iii)
TIME TO PEAK (hrs)=	10.00		10.08	10.00
RUNOFF VOLUME (mm)=	209.57		107.20	128.70
TOTAL RAINFALL (mm)=	211.07		211.07	211.07
RUNOFF COEFFICIENT =	.99		.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0355)	
ID= 1 DT= 5.0 min	
Area (ha)= 12.30	
Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.17		7.13	
Dep. Storage (mm)=	1.50		5.00	
Average Slope (%)=	1.60		1.60	
Length (m)=	286.00		40.00	
Mannings n =	.013		.300	

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Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	5.38 (ii)	15.74 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.21	.07	
			TOTALS
PEAK FLOW (cms)=	.38	1.13	1.513 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0350)	Area (ha)= 16.30		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.45	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.00	1.00	
Length (m)=	330.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.75 (ii)	18.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.18	.06	
			TOTALS
PEAK FLOW (cms)=	.50	1.47	1.968 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0360)	Area (ha)= 30.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 37.00	Dir. Conn.(%)= 19.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.10	18.90	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	

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Length (m)= 447.00 40.00
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 52.83 55.42
over (min) 5.00 20.00
Storage Coeff. (min)= 6.58 (ii) 16.55 (ii)
Unit Hyd. Tpeak (min)= 5.00 20.00
Unit Hyd. peak (cms)= .18 .06

PEAK FLOW (cms)= .84 2.78 *TOTALS*
TIME TO PEAK (hrs)= 10.00 10.00 3.618 (iii)
RUNOFF VOLUME (mm)= 209.57 101.80 122.28
TOTAL RAINFALL (mm)= 211.07 211.07 211.07
RUNOFF COEFFICIENT = .99 .48 .58

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0395)
ID= 1 DT= 5.0 min
Area (ha)= 51.20
Total Imp(%)= 10.00 Dir. Conn.(%)= 5.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 5.12 46.08
Dep. Storage (mm)= 1.50 5.00
Average Slope (%)= 2.00 2.00
Length (m)= 900.00 40.00
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 52.83 43.26
over (min) 10.00 25.00
Storage Coeff. (min)= 10.01 (ii) 21.02 (ii)
Unit Hyd. Tpeak (min)= 10.00 25.00
Unit Hyd. peak (cms)= .11 .05

PEAK FLOW (cms)= .37 5.03 *TOTALS*
TIME TO PEAK (hrs)= 10.00 10.08 5.388 (iii)
RUNOFF VOLUME (mm)= 209.57 81.91 88.29
TOTAL RAINFALL (mm)= 211.07 211.07 211.07
RUNOFF COEFFICIENT = .99 .39 .42

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB

STANDHYD (0455)		Hadati Creek watershed - Allowable	
ID= 1 DT= 5.0 min	Area (ha)= 12.70	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.33	7.37	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.71	1.71	
Length (m)=	300.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	5.43 (ii)	15.59 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.20	.07	
PEAK FLOW (cms)=	.39	1.17	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	1.564 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT =	.99	.51	211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0460)		Area (ha)= 36.00	
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	15.12	20.88	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.03	2.03	
Length (m)=	465.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.71 (ii)	16.36 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.18	.06	
PEAK FLOW (cms)=	1.11	3.30	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	4.413 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT =	.99	.51	211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

Max.Eff.Inten.(mm/hr)=	52.83	59.46
over (min)	10.00	20.00
Storage Coeff. (min)=	8.46 (ii)	18.15 (ii)
Unit Hyd. Tpeak (min)=	10.00	20.00
Unit Hyd. peak (cms)=	.12	.06

PEAK FLOW	(cms)=	1.33	3.90	*TOTALS*
TIME TO PEAK	(hrs)=	10.00	10.00	5.222 (iii)
RUNOFF VOLUME	(mm)=	209.57	107.20	10.00
TOTAL RAINFALL	(mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT	=	.99	.51	211.07
				.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)
ID= 1 DT=****min

AREA (ha)= .00
QPEAK (cms)= .00
TPEAK (hrs)= .00
VOLUME (mm)=*****

DUHYD (0505)
Inlet Cap.=9.000
#of Inlets= 1
Total(cms)= 9.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	27.11	10.08	134.22
MAJOR SYS.(ID= 2):	78.53	18.11	10.08	134.22
MINOR SYS.(ID= 3):	165.47	9.00	6.75	134.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0566)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0484):	12.60	1.527	10.00	128.70
+ ID2= 2 (0565):	11.10	1.345	10.00	128.70

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ID = 3 (0566): 23.70 2.872 10.00 128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0420)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0410):		24.20	2.975	10.00	128.70
+ ID2= 2 (0415):		4.99	.626	10.00	128.70
ID = 3 (0420):		29.19	3.602	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	1.0000	1.0000
		.0100	.0100	20.0000	1.1000
		.0120	.1000	.0000	.0000

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0110)	19.000	2.340	10.00	128.70
OUTFLOW: ID= 1 (0111)	19.000	2.069	10.50	128.68

PEAK FLOW REDUCTION [Qout/Qin] (%) = 88.39
 TIME SHIFT OF PEAK FLOW (min) = 30.00
 MAXIMUM STORAGE USED (ha.m.) = 1.0100

ADD HYD (0103)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0101):		16.32	2.027	10.00	128.70
+ ID2= 2 (0102):		14.32	1.780	10.00	128.70
ID = 3 (0103):		30.64	3.807	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0106)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	.5000	.4000
		.0100	.0100	6.6000	.8000
		.0260	.2300	.0000	.0000

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0105)	51.320	6.260	10.00	128.70
OUTFLOW: ID= 1 (0106)	51.320	5.997	10.08	128.69

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PEAK FLOW REDUCTION [Qout/Qin](%)= 95.79
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .7608

ROUTE CHN (0358) |
 IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .01 .01 .102E+02 .0 .17 109.52
 .03 .03 .409E+02 .0 .27 68.99
 .04 .04 .920E+02 .0 .35 52.65
 .05 .05 .163E+03 .1 .42 43.46
 .07 .07 .255E+03 .1 .49 37.45
 .08 .08 .368E+03 .2 .55 33.17
 .10 .10 .499E+03 .3 .64 28.86
 .11 .11 .634E+03 .4 .74 24.66
 .12 .12 .769E+03 .6 .84 21.72
 .14 .14 .904E+03 .8 .94 19.54
 .15 .15 .104E+04 1.0 1.03 17.84
 .16 .16 .119E+04 1.2 1.11 16.57
 .18 .18 .135E+04 1.4 1.17 15.71
 .19 .19 .154E+04 1.7 1.21 15.10
 .20 .20 .175E+04 2.0 1.25 14.65
 .22 .22 .198E+04 2.3 1.28 14.31
 .23 .23 .223E+04 2.6 1.31 14.04
 .25 .25 .250E+04 3.0 1.33 13.82
 .26 .26 .279E+04 3.4 1.34 13.65

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0355) 12.30 1.51 10.00 128.70 .18 1.18
 OUTFLOW: ID= 1 (0358) 12.30 1.44 10.08 128.64 .18 1.17

ROUTE CHN (0353) |
 IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel

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20.00 .26 .0300

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

			<---- hydrograph ---->			<-pipe / channel->		
			AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0350)			16.30	1.97	10.00	128.70	.20	1.25
OUTFLOW: ID= 1 (0353)			16.30	1.87	10.08	128.66	.20	1.24

ROUTE CHN (0362)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05

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.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0360)	30.00	3.62	10.00	122.28	.27	1.53
OUTFLOW:	ID= 1 (0362)	30.00	3.50	10.08	122.26	.27	1.52

ADD HYD (0465)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0455):	12.70	1.564	10.00	128.70
+	ID2= 2 (0460):	36.00	4.413	10.00	128.70
=====					
ID =	3 (0465):	48.70	5.977	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1=	1 (0510):	16.00	2.134	10.00	182.64
+	ID2= 2 (0505):	165.47	9.000	6.75	134.22
=====					
ID =	3 (0515):	181.47	11.134	10.00	138.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0564)		Routing time step (min)'= 5.00
IN= 2---> OUT= 1		

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
.00	101.50	.0500
1.00	100.70	.0500
1.50	100.55	.0500 / .0300
2.00	99.50	.0300
3.50	99.60	.0300
4.50	100.65	.0300 / .0500
6.00	101.45	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51

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.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

		<---- hydrograph ---->			<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0505)	78.53	18.11	10.08	134.22	1.92	1.40
OUTFLOW: ID= 1 (0564)	78.53	17.83	10.25	134.22	1.95	1.41

ROUTE CHN (0563)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.05	.05	.573E+01	.0	.67	2.23
.11	.11	.135E+02	.1	.99	1.51
.16	.16	.232E+02	.3	1.23	1.22
.21	.21	.349E+02	.5	1.42	1.06
.26	.26	.486E+02	.9	1.58	.95
.32	.32	.643E+02	1.2	1.73	.87
.37	.37	.820E+02	1.7	1.86	.81
.42	.42	.102E+03	2.2	1.98	.76
.47	.47	.123E+03	2.9	2.10	.71
.53	.53	.147E+03	3.6	2.21	.68
.58	.58	.173E+03	4.4	2.31	.65
.63	.63	.200E+03	5.4	2.42	.62
.68	.68	.230E+03	6.4	2.51	.60
.74	.74	.262E+03	7.6	2.61	.58
.79	.79	.295E+03	8.9	2.70	.56
.84	.84	.331E+03	10.3	2.79	.54
.89	.89	.369E+03	11.8	2.88	.52
.95	.95	.408E+03	13.5	2.97	.51
1.00	1.00	.450E+03	15.2	3.05	.49

	<---- hydrograph ---->			<-pipe / channel->	
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL

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		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0566)	23.70	2.87	10.00	128.70	.47	2.10
OUTFLOW:	ID= 1 (0563)	23.70	2.87	10.00	128.70	.47	2.10

DUHYD (0425)
Inlet Cap.=1.980
#of Inlets= 1
Total(cms)= 2.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	3.60	10.00	128.70
MAJOR SYS.(ID= 2):	4.95	1.62	10.00	128.70
MINOR SYS.(ID= 3):	24.24	1.98	9.33	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	.5000
.0100	.0100	10.0000	.6000
.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	3.807	10.00	128.70
OUTFLOW: ID= 1 (0104)	30.640	3.797	10.00	128.69

PEAK FLOW REDUCTION [Qout/Qin](%)= 99.73
TIME SHIFT OF PEAK FLOW (min)= .00
MAXIMUM STORAGE USED (ha.m.)= .5312

ADD HYD (0359)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0358):	12.30	1.436	10.08	128.64
+ ID2= 2 (0353):	16.30	1.875	10.08	128.66
ID = 3 (0359):	28.60	3.311	10.08	128.65

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0363)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0359):	28.60	3.311	10.08	128.65
+ ID2= 2 (0362):	30.00	3.504	10.08	122.26
ID = 3 (0363):	58.60	6.814	10.08	125.38

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0470)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0465):	48.70	5.977	10.00	128.70
+ ID2= 2 (0425):	4.95	1.622	10.00	128.70
=====				
ID = 3 (0470):	53.65	7.598	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0520)				
Inlet Cap.=3.050				
#of Inlets= 1				
Total(cms)= 3.0				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
TOTAL HYD.(ID= 1):	181.47	11.13	10.00	138.49
=====				
MAJOR SYS.(ID= 2):	98.04	8.08	10.00	138.49
MINOR SYS.(ID= 3):	83.43	3.05	4.25	138.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0561)					
IN= 2---> OUT= 1					
Routing time step (min)'= 5.00					

<----- DATA FOR SECTION (1.1) ----->					
Distance	Elevation Manning				
.00	1.00 .0350				
2.00	.50 .0350				
4.00	.00 .0350 / .0350 Main Channel				
4.50	.00 .0350 Main Channel				
5.00	.00 .0350 / .0350 Main Channel				
7.00	.50 .0350				
9.00	1.00 .0350				
<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.05	.05	.319E+01	.1	.87	.95
.11	.11	.748E+01	.2	1.26	.66
.16	.16	.129E+02	.4	1.54	.54
.21	.21	.194E+02	.7	1.75	.48
.26	.26	.270E+02	1.0	1.93	.43
.32	.32	.357E+02	1.5	2.08	.40
.37	.37	.456E+02	2.0	2.22	.38
.42	.42	.565E+02	2.6	2.34	.36
.47	.47	.686E+02	3.4	2.46	.34
.53	.53	.817E+02	4.2	2.57	.32
.58	.58	.960E+02	5.1	2.68	.31
.63	.63	.111E+03	6.2	2.78	.30
.68	.68	.128E+03	7.3	2.87	.29
.74	.74	.145E+03	8.6	2.97	.28
.79	.79	.164E+03	10.0	3.06	.27
.84	.84	.184E+03	11.6	3.14	.27
.89	.89	.205E+03	13.2	3.23	.26

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.95	.95	.227E+03	15.0	3.31	.25
1.00	1.00	.250E+03	17.0	3.40	.25

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0563)	23.70	2.87	10.00	128.70	.44	2.38
OUTFLOW: ID= 1 (0561)	23.70	2.87	10.00	128.70	.44	2.38

ADD HYD (0114)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0111):	19.00	2.069	10.50	128.68	
+ ID2= 2 (0104):	30.64	3.797	10.00	128.69	
=====					
ID = 3 (0114):	49.64	4.896	10.50	128.69	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0365):	117.50	14.089	10.00	128.70	
+ ID2= 2 (0363):	58.60	6.814	10.08	125.38	
=====					
ID = 3 (0380):	176.10	20.834	10.00	127.59	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)		
IN= 2---> OUT= 1		Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	324.60	.0500
115.00	321.60	.0500
120.00	320.80	.0500 / .0300
122.00	320.80	.0300 / .0500
138.00	321.60	.0500
148.00	322.30	.0500
154.00	323.10	.0500
164.00	324.60	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02

Hadati Creek Watershed - Allowable					
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

		<---- hydrograph ---->			<-pipe / channel->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0470)	53.65	7.60	10.00	128.70	.58	1.33
OUTFLOW: ID= 1 (0475)	53.65	7.51	10.00	128.70	.58	1.33

ADD HYD (0526)					
1 + 2 = 3					
ID1= 1 (0520):	98.04	8.084	10.00	138.49	
+ ID2= 2 (0525):	.00	.001	.00	*****	
ID = 3 (0526):	98.04	8.084	10.00	138.49	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)					
1 + 2 = 3					
ID1= 1 (0561):	23.70	2.867	10.00	128.70	
+ ID2= 2 (0481):	5.90	.715	10.00	128.70	
ID = 3 (0492):	29.60	3.582	10.00	128.70	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
ID1= 1 (0114):	49.64	4.896	10.50	128.69	
+ ID2= 2 (0106):	51.32	5.997	10.08	128.69	
ID = 3 (0115):	100.96	10.540	10.08	128.69	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0390)					
IN= 2---> OUT= 1					
DT= 5.0 min					
	OUTFLOW	STORAGE	OUTFLOW	STORAGE	

Hadati Creek Watershed - Allowable

(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	20.834	10.00	127.59
OUTFLOW: ID= 1 (0390)	176.100	1.714	12.33	127.59

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.23
 TIME SHIFT OF PEAK FLOW (min)=140.00
 MAXIMUM STORAGE USED (ha.m.)= 17.4981

ROUTE CHN (0527)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

<---- hydrograph ---->

<-pipe / channel->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	98.04	8.08	10.00	138.49	2.05	.76
OUTFLOW: ID= 1 (0527)	98.04	7.97	10.08	138.49	2.04	.76

RESERVOIR (0482)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW STORAGE | OUTFLOW STORAGE

Hadati Creek watershed - Allowable

(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	29.600	3.582	10.00	128.70
OUTFLOW: ID= 1 (0482)	29.600	3.550	10.08	128.69

PEAK FLOW REDUCTION [Qout/Qin] (%) = 99.13
 TIME SHIFT OF PEAK FLOW (min) = 5.00
 MAXIMUM STORAGE USED (ha.m.) = .5800

ADD HYD (0400)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0390):	176.10	1.714	12.33	127.59
+ ID2= 2 (0395):	51.20	5.388	10.08	88.29
=====				
ID = 3 (0400):	227.30	6.909	10.08	118.74

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13

Hadati Creek watershed - Allowable					
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0400)	227.30	6.91	10.08	118.74	.46	1.36
OUTFLOW:	ID= 1 (0403)	227.30	6.38	10.33	118.74	.44	1.30

```

-----
| ADD HYD (0407) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0115):  100.96  10.540  10.08  128.69
+ ID2= 2 (0403):  227.30   6.377  10.33  118.74
=====
ID = 3 (0407):  328.26  16.526  10.17  121.80

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0113) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
      OUTFLOW      STORAGE      OUTFLOW      STORAGE
      (cms)      (ha.m.)      (cms)      (ha.m.)
      .0000      .0000      1.6000      6.4000
      1.1000      2.9000      9.1000     10.0000
      1.3000      4.3000     12.0000     20.0000

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	16.526	10.17	121.80
OUTFLOW: ID= 1 (0113)	328.260	9.456	11.50	121.80

PEAK FLOW REDUCTION [Qout/Qin](%)= 57.22
 TIME SHIFT OF PEAK FLOW (min)= 80.00
 MAXIMUM STORAGE USED (ha.m.)= 11.2348

```

-----
| ADD HYD (0430) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0425):  24.24   1.980   9.33  128.70
+ ID2= 2 (0113):  328.26   9.456  11.50  121.80
=====
ID = 3 (0430):  352.50  11.349  11.08  122.27

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ROUTE CHN (0440) |
| IN= 2---> OUT= 1 |
-----
Routing time step (min)'= 5.00

```

<----- DATA FOR SECTION (1.1) ----->

Hadati Creek watershed - Allowable			
Distance	Elevation	Manning	
100.00	325.40	.0600	
120.00	324.60	.0600	
126.00	323.90	.0600	
130.00	323.00	.0600	
140.00	322.30	.0600 / .0300	Main Channel
142.00	322.30	.0300 / .0600	Main Channel
150.00	323.90	.0600	
155.00	324.60	.0600	
160.00	325.40	.0600	

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

<---- hydrograph ---->				<-pipe / channel-->		
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0430)	352.50	11.35	11.08	122.27	.72	1.73
OUTFLOW: ID= 1 (0440)	352.50	11.32	11.08	122.27	.71	1.73

ADD HYD (0485)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0440):	352.50	11.321	11.08	122.27	
+ ID2= 2 (0475):	53.65	7.511	10.00	128.70	
=====					
ID = 3 (0485):	406.15	16.120	10.75	123.12	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0485):	406.15	16.120	10.75	123.12	
+ ID2= 2 (0480):	43.10	5.222	10.00	128.70	
=====					

Hadati Creek Watershed - Allowable
ID = 3 (0490): 449.25 19.973 10.67 123.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)					
1 + 2 = 3					
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0482):		29.60	3.550	10.08	128.69
+ ID2= 2 (0490):		449.25	19.973	10.67	123.66
ID = 3 (0491):		478.85	23.211	10.17	123.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)				
IN= 2---> OUT= 1				
DT= 5.0 min				

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	7.0800	2.4860
	.2760	.0600	8.1000	3.3240
	1.2000	.3400	9.7980	4.6420
	2.0400	.6182	10.4940	7.4397
	2.6400	1.1630	11.6850	10.3000
	3.1200	1.7070	12.3480	11.4000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	478.850	23.211	10.17	123.97
OUTFLOW: ID= 1 (0483)	478.850	11.874	12.08	123.97
PEAK FLOW REDUCTION	[Qout/Qin] (%)= 51.15			
TIME SHIFT OF PEAK FLOW	(min)=115.00			
MAXIMUM STORAGE USED	(ha.m.)= 10.6135			

ADD HYD (0530)					
1 + 2 = 3					
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0540):		4.63	.636	10.00	182.64
+ ID2= 2 (0483):		478.85	11.874	12.08	123.97
ID = 3 (0530):		483.48	12.008	12.00	124.53

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)		AREA	QPEAK	TPEAK	R.V.
1 +	2 =	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0527):	98.04	7.968	10.08	138.49
+ ID2= 2	(0530):	483.48	12.008	12.00	124.53
ID = 3 (0545):		581.52	19.161	11.00	126.88

Hadati Creek Watershed - Allowable

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0542):	25.25	3.443	10.00	182.64	
+ ID2= 2 (0545):	581.52	19.161	11.00	126.88	
ID = 3 (0546):	606.77	21.671	10.08	129.20	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0543):	14.99	2.054	10.00	182.64	
+ ID2= 2 (0546):	606.77	21.671	10.08	129.20	
ID = 3 (0547):	621.76	23.685	10.00	130.49	

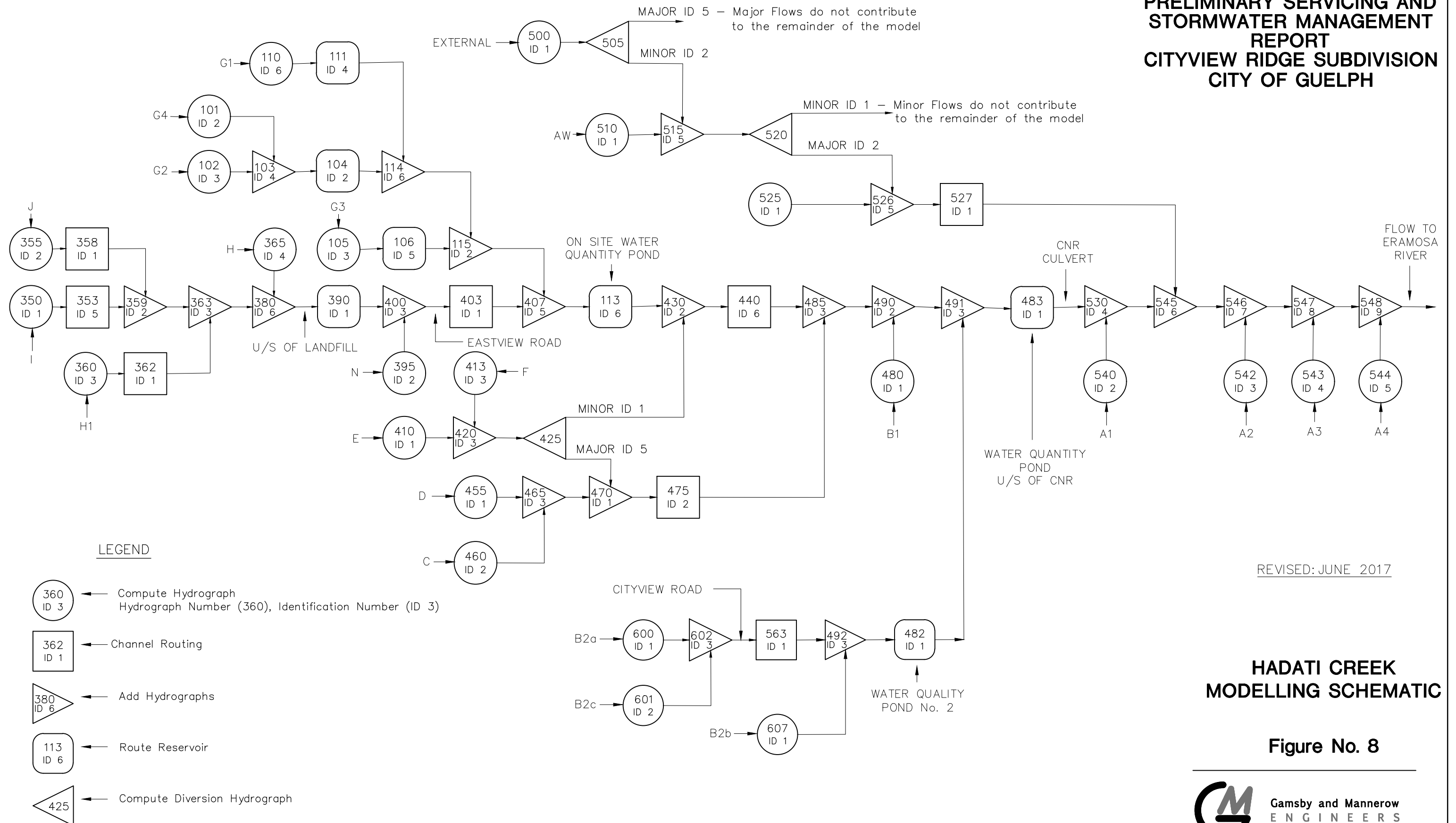
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0544):	1.13	.156	10.00	182.64	
+ ID2= 2 (0547):	621.76	23.685	10.00	130.49	
ID = 3 (0548):	622.89	23.841	10.00	130.59	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

PRELIMINARY SERVICING AND STORMWATER MANAGEMENT REPORT CITYVIEW RIDGE SUBDIVISION CITY OF GUELPH



REVISED: JUNE 2017

HADATI CREEK MODELLING SCHEMATIC

Figure No. 8



Hadati Creek Watershed - Post Development with Cityview Ridge

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V    V    I    SSSSS  U    U    A    L
V    V    I    SS     U    U    A A   L
V    V    I    SS     U    U    AAAAA L
V    V    I    SS     U    U    A    A L
  VV     I    SSSSS  UUUUU  A    A  LLLLL

  000    TTTT  TTTT  H    H  Y    Y  M    M    000
O    O    T    T    H    H  Y Y   MM MM  O    O
O    O    T    T    H    H  Y    M    M  O    O

  000    T    T    H    H  Y    M    M    000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 2.3.2\voim.dat

Output filename: Y:\SPrimmer\OTTHYMO\Cityview Ridge\Hadati Creek Watershed - Post Development with Cityview Ridge.out

Summary filename: Y:\SPrimmer\OTTHYMO\Cityview Ridge\Hadati Creek Watershed - Post Development with Cityview Ridge.sum

DATE: 3/30/2015

TIME: 3:05:13 PM

USER:

COMMENTS: _____

 ** SIMULATION NUMBER: 1 **

READ STORM
 Ptotal= 25.00 mm

Filename: Y:\SPrimmer\OTTHYMO\Ci
 tyview Ridge\25mm4hr.stm
 Comments: 25 mm - 4 hour - 10 Minute Time Step

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	.53	1.17	17.57	2.17	2.95	3.17	.76
.33	.71	1.33	61.55	2.33	2.19	3.33	.65
.50	.99	1.50	24.02	2.50	1.69	3.50	.57
.67	1.51	1.67	11.16	2.67	1.34	3.67	.49
.83	2.57	1.83	6.44	2.83	1.09	3.83	.44
1.00	5.31	2.00	4.20	3.00	.90	4.00	.38

Hadati Creek watershed - Post Development with Cityview Ridge

CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	.53	1.083	17.57	2.083	2.95	3.08	.76
.167	.53	1.167	17.57	2.167	2.95	3.17	.76
.250	.71	1.250	61.55	2.250	2.19	3.25	.65
.333	.71	1.333	61.55	2.333	2.19	3.33	.65
.417	.99	1.417	24.02	2.417	1.69	3.42	.57
.500	.99	1.500	24.02	2.500	1.69	3.50	.57
.583	1.51	1.583	11.16	2.583	1.34	3.58	.49
.667	1.51	1.667	11.16	2.667	1.34	3.67	.49
.750	2.57	1.750	6.44	2.750	1.09	3.75	.44
.833	2.57	1.833	6.44	2.833	1.09	3.83	.44
.917	5.31	1.917	4.20	2.917	.90	3.92	.38
1.000	5.31	2.000	4.20	3.000	.90	4.00	.38

Max. Eff. Inten. (mm/hr)=	61.55	7.05
over (min)	10.00	35.00
Storage Coeff. (min)=	7.96 (ii)	30.70 (ii)
Unit Hyd. Tpeak (min)=	10.00	35.00
Unit Hyd. peak (cms)=	.13	.04

PEAK FLOW (cms)=	1.09	.23	*TOTALS*
TIME TO PEAK (hrs)=	1.42	1.83	1.142 (iii)
RUNOFF VOLUME (mm)=	23.50	2.16	1.42
TOTAL RAINFALL (mm)=	25.00	25.00	6.64
RUNOFF COEFFICIENT =	.94	.09	25.00
			.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum. Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0415)
ID= 1 DT= 5.0 min

Area (ha)= 4.99
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	2.10	2.89
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.86	2.86
Length	(m)=	185.00	40.00

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Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 61.55 8.82
over (min) 5.00 25.00
Storage Coeff. (min)= 3.27 (ii) 21.96 (ii)
Unit Hyd. Tpeak (min)= 5.00 25.00
Unit Hyd. peak (cms)= .27 .05

PEAK FLOW (cms)= .17 .04 *TOTALS*
TIME TO PEAK (hrs)= 1.33 1.67 .179 (iii)
RUNOFF VOLUME (mm)= 23.50 2.16 1.33
TOTAL RAINFALL (mm)= 25.00 25.00 6.64
RUNOFF COEFFICIENT = .94 .09 25.00
.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0410)
ID= 1 DT= 5.0 min
Area (ha)= 24.20
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 10.16 14.04
Dep. Storage (mm)= 1.50 5.00
Average Slope (%)= 2.00 2.00
Length (m)= 401.00 40.00
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 61.55 7.05
over (min) 5.00 30.00
Storage Coeff. (min)= 5.80 (ii) 28.54 (ii)
Unit Hyd. Tpeak (min)= 5.00 30.00
Unit Hyd. peak (cms)= .20 .04

PEAK FLOW (cms)= .75 .14 *TOTALS*
TIME TO PEAK (hrs)= 1.33 1.75 .770 (iii)
RUNOFF VOLUME (mm)= 23.50 2.16 1.33
TOTAL RAINFALL (mm)= 25.00 25.00 6.64
RUNOFF COEFFICIENT = .94 .09 25.00
.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0460)
ID= 1 DT= 5.0 min
Area (ha)= 36.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

IMPERVIOUS PERVIOUS (i)

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Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		6.31 (ii)	28.95 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.19	.04	
				TOTALS
PEAK FLOW	(cms)=	1.09	.21	1.117 (iii)
TIME TO PEAK	(hrs)=	1.33	1.75	1.33
RUNOFF VOLUME	(mm)=	23.50	2.16	6.64
TOTAL RAINFALL	(mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT	=	.94	.09	.27

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0455)
ID= 1 DT= 5.0 min

Area (ha)= 12.70
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		5.11 (ii)	28.94 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.21	.04	
				TOTALS
PEAK FLOW	(cms)=	.41	.07	.417 (iii)
TIME TO PEAK	(hrs)=	1.33	1.75	1.33
RUNOFF VOLUME	(mm)=	23.50	2.16	6.64
TOTAL RAINFALL	(mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT	=	.94	.09	.27

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0395)

Area (ha)= 51.20

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 ID= 1 DT= 5.0 min | Total Imp(%)= 10.00 Dir. Conn.(%)= 5.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.12	46.08	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		10.00	230.00	
Storage Coeff. (min)=	9.42 (ii)		225.31 (ii)	
Unit Hyd. Tpeak (min)=	10.00		230.00	
Unit Hyd. peak (cms)=	.12		.00	
PEAK FLOW	(cms)=	.29	.00	*TOTALS*
TIME TO PEAK	(hrs)=	1.42	.00	.292 (iii)
RUNOFF VOLUME	(mm)=	23.50	.00	1.42
TOTAL RAINFALL	(mm)=	25.00	25.00	1.17
RUNOFF COEFFICIENT	=	.94	.00	25.00
				.05

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0360)
 ID= 1 DT= 5.0 min | Area (ha)= 30.00
 Total Imp(%)= 37.00 Dir. Conn.(%)= 19.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	11.10	18.90	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	447.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	2.81	
over (min)		5.00	40.00	
Storage Coeff. (min)=	6.19 (ii)		39.07 (ii)	
Unit Hyd. Tpeak (min)=	5.00		40.00	
Unit Hyd. peak (cms)=	.19		.03	
PEAK FLOW	(cms)=	.83	.08	*TOTALS*
TIME TO PEAK	(hrs)=	1.33	1.92	.834 (iii)
RUNOFF VOLUME	(mm)=	23.50	1.27	1.33
TOTAL RAINFALL	(mm)=	25.00	25.00	5.50
RUNOFF COEFFICIENT	=	.94	.05	25.00
				.22

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- Hadati Creek watershed - Post Development with Cityview Ridge
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0350) ID= 1 DT= 5.0 min		Area (ha)= 16.30	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.45	
Dep. Storage	(mm)=	1.50	5.00	
Average slope	(%)=	1.00	1.00	
Length	(m)=	330.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten. (mm/hr)=		61.55	5.04	
over (min)		5.00	40.00	
Storage Coeff. (min)=		6.35 (ii)	38.38 (ii)	
Unit Hyd. Tpeak (min)=		5.00	40.00	
Unit Hyd. peak (cms)=		.19	.03	
PEAK FLOW (cms)=		.49	.07	*TOTALS* .499 (iii)
TIME TO PEAK (hrs)=		1.33	1.92	1.33
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0355) ID= 1 DT= 5.0 min		Area (ha)= 12.30	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten. (mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		5.06 (ii)	29.38 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.21	.04	
PEAK FLOW (cms)=		.40	.07	*TOTALS* .405 (iii)
TIME TO PEAK (hrs)=		1.33	1.75	1.33
RUNOFF VOLUME (mm)=		23.50	2.16	6.64
TOTAL RAINFALL (mm)=		25.00	25.00	25.00
RUNOFF COEFFICIENT =		.94	.09	.27

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- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0365) ID= 1 DT= 5.0 min		Area (ha)= 117.50 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	49.35	68.15
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	885.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		61.55	7.05
over (min)		10.00	35.00
Storage Coeff. (min)=	9.32 (ii)		32.06 (ii)
Unit Hyd. Tpeak (min)=	10.00		35.00
Unit Hyd. peak (cms)=	.12		.03
PEAK FLOW (cms)=	2.82		.62
TIME TO PEAK (hrs)=	1.42		1.83
RUNOFF VOLUME (mm)=	23.50		2.16
TOTAL RAINFALL (mm)=	25.00		25.00
RUNOFF COEFFICIENT	=	.94	.09
		TOTALS	
		2.960 (iii)	
		1.42	
		6.64	
		25.00	
		.27	

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0105) ID= 1 DT= 5.0 min		Area (ha)= 51.32 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	21.55	29.77
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	550.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		61.55	7.05
over (min)		5.00	30.00
Storage Coeff. (min)=	7.01 (ii)		29.75 (ii)
Unit Hyd. Tpeak (min)=	5.00		30.00
Unit Hyd. peak (cms)=	.17		.04
PEAK FLOW (cms)=	1.50		.30
TIME TO PEAK (hrs)=	1.33		1.75
RUNOFF VOLUME (mm)=	23.50		2.16
TOTAL RAINFALL (mm)=	25.00		25.00
		TOTALS	
		1.538 (iii)	
		1.33	
		6.64	
		25.00	

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 RUNOFF COEFFICIENT = .94 .09 .27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0102) ID= 1 DT= 5.0 min		Area (ha)= 14.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.01	8.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	287.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		4.74 (ii)	27.48 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.22	.04	
PEAK FLOW (cms)=		.47	.09	*TOTALS*
TIME TO PEAK (hrs)=		1.33	1.75	.479 (iii)
RUNOFF VOLUME (mm)=		23.50	2.16	1.33
TOTAL RAINFALL (mm)=		25.00	25.00	6.64
RUNOFF COEFFICIENT =		.94	.09	25.00
				.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min		Area (ha)= 16.32		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.47	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	309.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	7.05	
over (min)		5.00	30.00	
Storage Coeff. (min)=		4.96 (ii)	27.70 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.22	.04	
				TOTALS

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PEAK FLOW	(cms)=	.53	.10	.540 (iii)
TIME TO PEAK	(hrs)=	1.33	1.75	1.33
RUNOFF VOLUME	(mm)=	23.50	2.16	6.64
TOTAL RAINFALL	(mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT	=	.94	.09	.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0110) ID= 1 DT= 5.0 min	Area (ha)= 19.00 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00	
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)= 7.98	11.02	
Dep. Storage	(mm)= 1.50	5.00	
Average Slope	(%)= 2.00	2.00	
Length	(m)= 365.00	40.00	
Mannings n	= .013	.300	
Max.Eff.Inten.(mm/hr)=	61.55	7.05	
over (min)	5.00	30.00	
Storage Coeff. (min)=	5.48 (ii)	28.22 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	.20	.04	
			TOTALS
PEAK FLOW	(cms)= .60	.11	.614 (iii)
TIME TO PEAK	(hrs)= 1.33	1.75	1.33
RUNOFF VOLUME	(mm)= 23.50	2.16	6.64
TOTAL RAINFALL	(mm)= 25.00	25.00	25.00
RUNOFF COEFFICIENT	= .94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0600) ID= 1 DT= 5.0 min	Area (ha)= 11.38 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00	
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)= 4.78	6.60	
Dep. Storage	(mm)= 1.50	5.00	
Average Slope	(%)= 2.00	2.00	
Length	(m)= 680.00	40.00	
Mannings n	= .013	.300	
Max.Eff.Inten.(mm/hr)=	61.55	7.05	
over (min)	10.00	35.00	

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Storage Coeff. (min)=	7.96 (ii)	30.70 (ii)	
Unit Hyd. Tpeak (min)=	10.00	35.00	
Unit Hyd. peak (cms)=	.13	.04	
			TOTALS
PEAK FLOW (cms)=	.29	.06	.301 (iii)
TIME TO PEAK (hrs)=	1.42	1.83	1.42
RUNOFF VOLUME (mm)=	23.50	2.16	6.64
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.09	.27

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0601)
 ID= 1 DT= 5.0 min

Area (ha)= 7.62
 Total Imp(%)= 46.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=		3.51	4.11
Dep. Storage (mm)=		1.50	5.00
Average Slope (%)=		2.00	2.00
Length (m)=		680.00	40.00
Mannings n =		.013	.300
Max.Eff.Inten.(mm/hr)=		61.55	13.97
over (min)		10.00	30.00
Storage Coeff. (min)=	7.96 (ii)		25.26 (ii)
Unit Hyd. Tpeak (min)=	10.00		30.00
Unit Hyd. peak (cms)=	.13		.04
			TOTALS
PEAK FLOW (cms)=	.19	.07	.212 (iii)
TIME TO PEAK (hrs)=	1.42	1.75	1.42
RUNOFF VOLUME (mm)=	23.50	3.18	7.45
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.13	.30

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0607)
 ID= 1 DT= 5.0 min

Area (ha)= 5.97
 Total Imp(%)= 42.00 Dir. Conn.(%)= 2.50

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=		2.51	3.46
Dep. Storage (mm)=		1.50	5.00
Average Slope (%)=		2.00	2.00
Length (m)=		680.00	40.00
Mannings n =		.013	.300

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Max.Eff.Inten.(mm/hr)=	61.55	33.18	
over (min)	10.00	25.00	
Storage Coeff. (min)=	7.96 (ii)	20.20 (ii)	
Unit Hyd. Tpeak (min)=	10.00	25.00	
Unit Hyd. peak (cms)=	.13	.05	
			TOTALS
PEAK FLOW (cms)=	.02	.13	.141 (iii)
TIME TO PEAK (hrs)=	1.42	1.67	1.67
RUNOFF VOLUME (mm)=	23.50	4.97	5.44
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.20	.22

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0540)	Area (ha)= 4.63		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	3.70	.93	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	150.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	61.55	.00	
over (min)	5.00	325.00	
Storage Coeff. (min)=	4.73 (ii)	322.74 (ii)	
Unit Hyd. Tpeak (min)=	5.00	325.00	
Unit Hyd. peak (cms)=	.22	.00	
			TOTALS
PEAK FLOW (cms)=	.57	.00	.569 (iii)
TIME TO PEAK (hrs)=	1.33	.00	1.33
RUNOFF VOLUME (mm)=	23.50	.00	18.56
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.00	.74

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0500)	Area (ha)= 244.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 46.00	Dir. Conn.(%)= 26.00	

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		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		42.79	5.28	
over (min)		20.00	55.00	
Storage Coeff. (min)=		17.67 (ii)	51.28 (ii)	
Unit Hyd. Tpeak (min)=		20.00	55.00	
Unit Hyd. peak (cms)=		.06	.02	
PEAK FLOW	(cms)=	5.07	.82	*TOTALS*
TIME TO PEAK	(hrs)=	1.58	2.17	5.342 (iii)
RUNOFF VOLUME	(mm)=	23.50	2.25	1.58
TOTAL RAINFALL	(mm)=	25.00	25.00	7.77
RUNOFF COEFFICIENT	=	.94	.09	25.00
				.31

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0510)	Area	(ha)=	16.00	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)=	79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		10.00	440.00	
Storage Coeff. (min)=		8.77 (ii)	439.54 (ii)	
Unit Hyd. Tpeak (min)=		10.00	440.00	
Unit Hyd. peak (cms)=		.12	.00	
PEAK FLOW	(cms)=	1.48	.00	*TOTALS*
TIME TO PEAK	(hrs)=	1.42	.00	1.475 (iii)
RUNOFF VOLUME	(mm)=	23.50	.00	1.42
TOTAL RAINFALL	(mm)=	25.00	25.00	18.56
RUNOFF COEFFICIENT	=	.94	.00	25.00
				.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB STANDHYD (0542) ID= 1 DT= 5.0 min		Area (ha)= 25.25 Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	20.20	5.05	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	350.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		10.00	330.00	
Storage Coeff. (min)=		7.87 (ii)	325.88 (ii)	
Unit Hyd. Tpeak (min)=		10.00	330.00	
Unit Hyd. peak (cms)=		.13	.00	
PEAK FLOW	(cms)=	2.41	.00	*TOTALS* 2.408 (iii)
TIME TO PEAK	(hrs)=	1.42	.00	1.42
RUNOFF VOLUME	(mm)=	23.50	.00	18.56
TOTAL RAINFALL	(mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT	=	.94	.00	.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0543) ID= 1 DT= 5.0 min		Area (ha)= 14.99 Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	11.99	3.00	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	200.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		61.55	.00	
over (min)		5.00	325.00	
Storage Coeff. (min)=		5.63 (ii)	323.64 (ii)	
Unit Hyd. Tpeak (min)=		5.00	325.00	
Unit Hyd. peak (cms)=		.20	.00	
PEAK FLOW	(cms)=	1.77	.00	*TOTALS* 1.767 (iii)
TIME TO PEAK	(hrs)=	1.33	.00	1.33
RUNOFF VOLUME	(mm)=	23.50	.00	18.56
TOTAL RAINFALL	(mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT	=	.94	.00	.74

***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

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- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0544)
ID= 1 DT= 5.0 min

Area (ha)= 1.13
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.90	.23
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	50.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	61.55	.00
over (min)	5.00	325.00
Storage Coeff. (min)=	2.45 (ii)	320.46 (ii)
Unit Hyd. Tpeak (min)=	5.00	325.00
Unit Hyd. peak (cms)=	.30	.00

			TOTALS
PEAK FLOW (cms)=	.15	.00	.151 (iii)
TIME TO PEAK (hrs)=	1.33	.00	1.33
RUNOFF VOLUME (mm)=	23.50	.00	18.56
TOTAL RAINFALL (mm)=	25.00	25.00	25.00
RUNOFF COEFFICIENT =	.94	.00	.74

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
***** WARNING: THE PERVIOUS AREA HAS NO FLOW .

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)
ID= 1 DT=****min

AREA (ha)= .00
QPEAK (cms)= .00
TPEAK (hrs)= .00
VOLUME (mm)=*****

ADD HYD (0420)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0415):	4.99	.179	1.33	6.64
+ ID2= 2 (0410):	24.20	.770	1.33	6.64
ID = 3 (0420):	29.19	.948	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0465)

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1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0460):	36.00	1.117	1.33	6.64
+ ID2= 2 (0455):	12.70	.417	1.33	6.64
<hr/>				
ID = 3 (0465):	48.70	1.534	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0362)
IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

<---- hydrograph ---->				<-pipe / channel->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
INFLOW : ID= 2 (0360)	30.00	.83	1.33	5.50	MAX DEPTH (m)
OUTFLOW: ID= 1 (0362)	30.00	.41	1.50	5.48	MAX VEL (m/s)
					.14
					.96
					.11
					.71

ROUTE CHN (0353)
IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel

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5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

		<---- hydrograph ---->			<-pipe / channel->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0350)	16.30	.50	1.33	6.64	.12	.78
OUTFLOW: ID= 1 (0353)	16.30	.22	1.58	6.60	.09	.57

ROUTE CHN (0358)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->					
Distance	Elevation	Manning			
.00	.26	.0300			
5.50	.15	.0300 / .0150	Main Channel		
5.51	.00	.0150	Main Channel		
10.00	.09	.0150	Main Channel		
14.49	.00	.0150	Main Channel		
14.50	.15	.0150 / .0300	Main Channel		
20.00	.26	.0300			

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72

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.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		<---- hydrograph ---->			<-pipe / channel-->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW : ID= 2 (0355)		12.30	.40	1.33	6.64	.11
OUTFLOW: ID= 1 (0358)		12.30	.15	1.58	6.59	.08

RESERVOIR (0106)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	1.538	1.33	6.64
OUTFLOW: ID= 1 (0106)	51.320	.155	2.42	6.63

PEAK FLOW REDUCTION [Qout/Qin] (%) = 10.08
TIME SHIFT OF PEAK FLOW (min) = 65.00
MAXIMUM STORAGE USED (ha.m.) = .2763

ADD HYD (0103)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):	14.32	.479	1.33	6.64
+ ID2= 2 (0101):	16.32	.540	1.33	6.64
ID = 3 (0103):	30.64	1.019	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	1.0000
.0100	.0100	20.0000	1.1000
.0120	.1000	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	.614	1.33	6.64

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 OUTFLOW: ID= 1 (0111) 19.000 .024 2.92 6.63

PEAK FLOW REDUCTION [Qout/Qin](%)= 3.93
 TIME SHIFT OF PEAK FLOW (min)= 95.00
 MAXIMUM STORAGE USED (ha.m.)= .1111

ADD HYD (0602)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0600):	11.38	.301	1.42	6.64
+ ID2= 2 (0601):	7.62	.212	1.42	7.45
ID = 3 (0602):	19.00	.514	1.42	6.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0505)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
Inlet Cap.=9.000				
#of Inlets= 1				
Total(cms)= 9.0				
TOTAL HYD.(ID= 1):	244.00	5.34	1.58	7.77
MAJOR SYS.(ID= 2):	.00	.00	.00	.00
MINOR SYS.(ID= 3):	244.00	5.34	1.58	7.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0505):	244.00	5.342	1.58	7.77
+ ID2= 2 (0510):	16.00	1.475	1.42	18.56
ID = 3 (0515):	260.00	6.307	1.58	8.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0425)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
Inlet Cap.=1.980				
#of Inlets= 1				
Total(cms)= 2.0				
TOTAL HYD.(ID= 1):	29.19	.95	1.33	6.64
MAJOR SYS.(ID= 2):	.00	.00	.00	.00
MINOR SYS.(ID= 3):	29.19	.95	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0470)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
*** W A R N I N G : HYDROGRAPH 0425 <ID= 1> IS DRY.					
*** W A R N I N G : HYDROGRAPH 0470 = HYDROGRAPH 0465					
*** W A R N I N G : HYDROGRAPH 0470 = HYDROGRAPH 0465					
ID1= 1 (0425):		.00	.000	.00	.00
+ ID2= 2 (0465):		48.70	1.534	1.33	6.64
ID = 3 (0470):		48.70	1.534	1.33	6.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0359)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0353):		16.30	.216	1.58	6.60
+ ID2= 2 (0358):		12.30	.153	1.58	6.59
ID = 3 (0359):		28.60	.369	1.58	6.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)		OUTFLOW		STORAGE	
IN= 2---> OUT= 1		(cms)		(ha.m.)	
DT= 5.0 min					
		.0000	.0000	1.0000	.5000
		.0100	.0100	10.0000	.6000
		.0150	.1332	.0000	.0000
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0103)		30.640	1.019	1.33	6.64
OUTFLOW: ID= 1 (0104)		30.640	.097	2.33	6.63
PEAK FLOW REDUCTION [Qout/Qin](%)= 9.52					
TIME SHIFT OF PEAK FLOW (min)= 60.00					
MAXIMUM STORAGE USED (ha.m.)= .1639					

ADD HYD (0114)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0104):		30.64	.097	2.33	6.63
+ ID2= 2 (0111):		19.00	.024	2.92	6.63
ID = 3 (0114):		49.64	.118	2.42	6.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0563)		Routing time step (min)'= 5.00
IN= 2---> OUT= 1		

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<----- DATA FOR SECTION (2.2) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.745E+01	.0	.64	3.06
.11	.11	.175E+02	.1	.96	2.03
.16	.16	.301E+02	.3	1.21	1.61
.21	.21	.454E+02	.6	1.42	1.37
.26	.26	.632E+02	.9	1.61	1.21
.32	.32	.836E+02	1.3	1.77	1.10
.37	.37	.107E+03	1.8	1.93	1.01
.42	.42	.132E+03	2.3	2.08	.94
.47	.47	.160E+03	3.0	2.22	.88
.53	.53	.191E+03	3.8	2.35	.83
.58	.58	.225E+03	4.8	2.48	.79
.63	.63	.261E+03	5.8	2.60	.75
.68	.68	.299E+03	7.0	2.72	.72
.74	.74	.340E+03	8.2	2.84	.69
.79	.79	.384E+03	9.7	2.95	.66
.84	.84	.430E+03	11.3	3.06	.64
.89	.89	.479E+03	13.0	3.17	.62
.95	.95	.531E+03	14.8	3.27	.60
1.00	1.00	.585E+03	16.9	3.38	.58

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0602)	19.00	.51	1.42	6.96	.20	1.38
OUTFLOW: ID= 1 (0563)	19.00	.53	1.42	6.96	.21	1.40

ROUTE CHN (0564)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	101.50	.0500	
1.00	100.70	.0500	
1.50	100.55	.0500 / .0300	Main Channel
2.00	99.50	.0300	Main Channel
3.50	99.60	.0300	Main Channel
4.50	100.65	.0300 / .0500	Main Channel
6.00	101.45	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51

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.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: INFLOW HYDROGRAPH IS DRY!!

DUHYD (0520)
Inlet Cap.=3.050
#of Inlets= 1
Total(cms)= 3.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	260.00	6.31	1.58	8.44
MAJOR SYS.(ID= 2):	59.59	3.26	1.58	8.44
MINOR SYS.(ID= 3):	200.41	3.05	1.33	8.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
100.00	324.60	.0500	
115.00	321.60	.0500	
120.00	320.80	.0500 / .0300	Main Channel
122.00	320.80	.0300 / .0500	Main Channel
138.00	321.60	.0500	
148.00	322.30	.0500	
154.00	323.10	.0500	
164.00	324.60	.0500	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29

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2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

		<---- hydrograph ---->			<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW : ID= 2 (0470)		48.70	1.53	1.33	6.64	.26
OUTFLOW: ID= 1 (0475)		48.70	1.10	1.42	6.64	.23
						MAX VEL (m/s)
						.91
						.87

ADD HYD (0363)					
1 + 2 = 3					
ID1= 1 (0362):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0359):		30.00	.406	1.50	5.48
		28.60	.369	1.58	6.60
ID = 3 (0363):		58.60	.769	1.50	6.03

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
ID1= 1 (0106):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0114):		51.32	.155	2.42	6.63
		49.64	.118	2.42	6.63
ID = 3 (0115):		100.96	.273	2.42	6.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)					
1 + 2 = 3					
ID1= 1 (0563):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0607):		19.00	.533	1.42	6.96
		5.97	.141	1.67	5.44
ID = 3 (0492):		24.97	.596	1.42	6.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0526)					
1 + 2 = 3					
ID1= 1 (0525):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID2= 2 (0520):		.00	.001	.00	*****
		59.59	3.257	1.58	8.44

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ID = 3 (0526): 59.59 3.257 1.58 8.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0363):	58.60	.769	1.50	6.03
+ ID2= 2 (0365):	117.50	2.960	1.42	6.64
<hr/>				
ID = 3 (0380):	176.10	3.653	1.42	6.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0482)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	.2910	.3795
	.2590	.0579	.2970	.4503
	.2660	.1180	1.6320	.5232
	.2720	.1802	4.1680	.5983
	.2790	.2445	7.5660	.6756
	.2850	.3109	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	24.970	.596	1.42	6.60
OUTFLOW: ID= 1 (0482)	24.970	.260	2.00	6.60
PEAK FLOW REDUCTION [Qout/Qin](%)= 43.68				
TIME SHIFT OF PEAK FLOW (min)= 35.00				
MAXIMUM STORAGE USED (ha.m.)= .0700				

ROUTE CHN (0527)					
IN= 2---> OUT= 1					
Routing time step (min)'= 5.00					

<----- DATA FOR SECTION (1.1) ----->					
Distance	Elevation Manning				
100.00	313.20 .0500				
140.00	312.40 .0500 / .0300 Main Channel				
140.50	310.80 .0300 Main Channel				
141.50	310.80 .0300 Main Channel				
142.00	312.40 .0300 / .0500 Main Channel				
160.00	313.20 .0500				
<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70

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.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

		<---- hydrograph ---->			<--pipe / channel-->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	59.59	3.26	1.58	8.44	1.66	1.16
OUTFLOW: ID= 1 (0527)	59.59	2.80	1.67	8.44	1.54	1.21

RESERVOIR (0390)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	3.653	1.42	6.44
OUTFLOW: ID= 1 (0390)	176.100	.982	2.25	6.43

PEAK FLOW REDUCTION [Qout/Qin] (%) = 26.88
TIME SHIFT OF PEAK FLOW (min) = 50.00
MAXIMUM STORAGE USED (ha.m.) = .5820

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0395):	51.20	.292	1.42	1.17
+ ID2= 2 (0390):	176.10	.982	2.25	6.43
ID = 3 (0400):	227.30	1.022	1.58	5.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	

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148.00 335.30 .0500
156.00 336.00 .0500
165.00 338.30 .0000

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

			<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0400)	AREA (ha) 227.30	1.02	1.58	5.25	.17	.73
OUTFLOW:	ID= 1 (0403)	227.30	.88	3.17	5.25	.16	.71

ADD HYD (0407)					
1 + 2 = 3					

ID1= 1 (0403):		AREA (ha) 227.30	QPEAK (cms) .881	TPEAK (hrs) 3.17	R.V. (mm) 5.25
+ ID2= 2 (0115):		100.96	.273	2.42	6.63
=====					
ID = 3 (0407):		328.26	1.112	2.83	5.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0113)					
IN= 2----> OUT= 1					
DT= 5.0 min					

		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
		.0000	.0000	1.6000	6.4000
		1.1000	2.9000	9.1000	10.0000
		1.3000	4.3000	12.0000	20.0000

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)		328.260	1.112	2.83	5.67
OUTFLOW: ID= 1 (0113)		328.260	.354	5.83	5.67

PEAK FLOW REDUCTION [Qout/Qin](%)= 31.88

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 TIME SHIFT OF PEAK FLOW (min)=180.00
 MAXIMUM STORAGE USED (ha.m.)= .9343

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-----
| ADD HYD (0430) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 (0113):  328.26      .354      5.83      5.67
+ ID2= 2 (0425):  29.19      .948      1.33      6.64
=====
ID = 3 (0430):  357.45      .951      1.33      5.75
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| ROUTE CHN (0440) |
| IN= 2----> OUT= 1 |
-----
      Routing time step (min)'= 5.00
  
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<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
100.00      325.40      .0600
120.00      324.60      .0600
126.00      323.90      .0600
130.00      323.00      .0600
140.00      322.30      .0600 / .0300 Main Channel
142.00      322.30      .0300 / .0600 Main Channel
150.00      323.90      .0600
155.00      324.60      .0600
160.00      325.40      .0600
  
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<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)      (m)      (cu.m.)      (cms)      (m/s)      (min)
.16      322.46      .233E+03      .6      .96      6.96
.33      322.63      .672E+03      2.1      1.26      5.27
.49      322.79      .132E+04      4.9      1.48      4.51
.65      322.95      .216E+04      9.0      1.66      4.03
.82      323.12      .319E+04      14.9      1.87      3.57
.98      323.28      .433E+04      22.5      2.08      3.21
1.14      323.44      .556E+04      31.6      2.27      2.93
1.31      323.61      .689E+04      42.3      2.45      2.72
1.47      323.77      .833E+04      54.6      2.62      2.54
1.63      323.93      .987E+04      68.3      2.77      2.41
1.79      324.09      .115E+05      82.8      2.87      2.33
1.96      324.26      .134E+05      99.2      2.96      2.25
2.12      324.42      .154E+05      117.9      3.06      2.18
2.28      324.58      .176E+05      138.8      3.15      2.11
2.45      324.75      .200E+05      157.4      3.14      2.12
2.61      324.91      .228E+05      179.6      3.15      2.11
2.77      325.07      .259E+05      205.8      3.18      2.09
2.94      325.24      .293E+05      236.1      3.23      2.07
3.10      325.40      .330E+05      270.6      3.28      2.03
  
```

```

<----- hydrograph ----->      <-pipe / channel->
      AREA      QPEAK      TPEAK      R.V.      MAX DEPTH      MAX VEL
      (ha)      (cms)      (hrs)      (mm)      (m)      (m/s)
INFLOW : ID= 2 (0430)  357.45      .95      1.33      5.75      .20      1.02
OUTFLOW: ID= 1 (0440)  357.45      .72      1.42      5.75      .18      .98
  
```

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ADD HYD (0485)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0475):	48.70	1.101	1.42	6.64
+ ID2= 2 (0440):	357.45	.720	1.42	5.75
=====				
ID = 3 (0485):	406.15	1.820	1.42	5.86

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0480):	43.10	1.142	1.42	6.64
+ ID2= 2 (0485):	406.15	1.820	1.42	5.86
=====				
ID = 3 (0490):	449.25	2.962	1.42	5.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0490):	449.25	2.962	1.42	5.93
+ ID2= 2 (0482):	24.97	.260	2.00	6.60
=====				
ID = 3 (0491):	474.22	3.086	1.42	5.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	7.0800	2.4860
	.2760	.0600	8.1000	3.3240
	1.2000	.3400	9.7980	4.6420
	2.0400	.6182	10.4940	7.4397
	2.6400	1.1630	11.6850	10.3000
	3.1200	1.7070	12.3480	11.4000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	474.220	3.086	1.42	5.97
OUTFLOW: ID= 1 (0483)	474.220	1.344	2.00	5.97

PEAK FLOW REDUCTION [Qout/Qin](%)= 43.57
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= .3886

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ADD HYD (0530)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0483):		474.22	1.344	2.00	5.97
+ ID2= 2 (0540):		4.63	.569	1.33	18.56
ID = 3 (0530):		478.85	1.391	2.00	6.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0530):		478.85	1.391	2.00	6.09
+ ID2= 2 (0527):		59.59	2.796	1.67	8.44
ID = 3 (0545):		538.44	4.086	1.67	6.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0545):		538.44	4.086	1.67	6.35
+ ID2= 2 (0542):		25.25	2.408	1.42	18.56
ID = 3 (0546):		563.69	5.474	1.58	6.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0546):		563.69	5.474	1.58	6.90
+ ID2= 2 (0543):		14.99	1.767	1.33	18.56
ID = 3 (0547):		578.68	6.159	1.50	7.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0547):		578.68	6.159	1.50	7.20
+ ID2= 2 (0544):		1.13	.151	1.33	18.56
ID = 3 (0548):		579.81	6.220	1.50	7.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek Watershed - Post Development with Cityview Ridge

 ** SIMULATION NUMBER: 2 **

 | READ STORM |
Ptotal= 53.41 mm

Filename: Y:\SPrimmer\OTTHYMO\Ci
 tyview Ridge\5yrSCS12hr.stm
 Comments: 5 year SCS Type II 12hour design storm

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.25	1.34	3.25	2.14	6.25	9.61	9.25	1.87
.50	1.34	3.50	2.14	6.50	9.61	9.50	1.87
.75	1.34	3.75	2.14	6.75	4.27	9.75	1.87
1.00	1.34	4.00	2.14	7.00	4.27	10.00	1.87
1.25	1.34	4.25	3.20	7.25	3.20	10.25	1.07
1.50	1.34	4.50	3.20	7.50	3.20	10.50	1.07
1.75	1.34	4.75	4.27	7.75	3.20	10.75	1.07
2.00	1.34	5.00	4.27	8.00	3.20	11.00	1.07
2.25	1.60	5.25	6.41	8.25	1.87	11.25	1.07
2.50	1.60	5.50	6.41	8.50	1.87	11.50	1.07
2.75	1.60	5.75	25.64	8.75	1.87	11.75	1.07
3.00	1.60	6.00	70.50	9.00	1.87	12.00	1.07

 | CALIB |
 | STANDHYD (0480) |
ID= 1 DT= 5.0 min

Area (ha)= 43.10
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	1.34	3.083	2.14	6.083	9.61	9.08	1.87
.167	1.34	3.167	2.14	6.167	9.61	9.17	1.87
.250	1.34	3.250	2.14	6.250	9.61	9.25	1.87
.333	1.34	3.333	2.14	6.333	9.61	9.33	1.87
.417	1.34	3.417	2.14	6.417	9.61	9.42	1.87
.500	1.34	3.500	2.14	6.500	9.61	9.50	1.87
.583	1.34	3.583	2.14	6.583	4.27	9.58	1.87
.667	1.34	3.667	2.14	6.667	4.27	9.67	1.87
.750	1.34	3.750	2.14	6.750	4.27	9.75	1.87
.833	1.34	3.833	2.14	6.833	4.27	9.83	1.87
.917	1.34	3.917	2.14	6.917	4.27	9.92	1.87
1.000	1.34	4.000	2.14	7.000	4.27	10.00	1.87
1.083	1.34	4.083	3.20	7.083	3.20	10.08	1.07
1.167	1.34	4.167	3.20	7.167	3.20	10.17	1.07
1.250	1.34	4.250	3.20	7.250	3.20	10.25	1.07
1.333	1.34	4.333	3.20	7.333	3.20	10.33	1.07
1.417	1.34	4.417	3.20	7.417	3.20	10.42	1.07

Hadati Creek watershed - Post Development with Cityview Ridge

1.500	1.34	4.500	3.20	7.500	3.20	10.50	1.07
1.583	1.34	4.583	4.27	7.583	3.20	10.58	1.07
1.667	1.34	4.667	4.27	7.667	3.20	10.67	1.07
1.750	1.34	4.750	4.27	7.750	3.20	10.75	1.07
1.833	1.34	4.833	4.27	7.833	3.20	10.83	1.07
1.917	1.34	4.917	4.27	7.917	3.20	10.92	1.07
2.000	1.34	5.000	4.27	8.000	3.20	11.00	1.07
2.083	1.60	5.083	6.41	8.083	1.87	11.08	1.07
2.167	1.60	5.167	6.41	8.167	1.87	11.17	1.07
2.250	1.60	5.250	6.41	8.250	1.87	11.25	1.07
2.333	1.60	5.333	6.41	8.333	1.87	11.33	1.07
2.417	1.60	5.417	6.41	8.417	1.87	11.42	1.07
2.500	1.60	5.500	6.41	8.500	1.87	11.50	1.07
2.583	1.60	5.583	25.64	8.583	1.87	11.58	1.07
2.667	1.60	5.667	25.64	8.667	1.87	11.67	1.07
2.750	1.60	5.750	25.64	8.750	1.87	11.75	1.07
2.833	1.60	5.833	70.50	8.833	1.87	11.83	1.07
2.917	1.60	5.917	70.50	8.917	1.87	11.92	1.07
3.000	1.60	6.000	70.50	9.000	1.87	12.00	1.07

Max.Eff.Inten.(mm/hr)= 70.50 81.70
over (min) 10.00 20.00
Storage Coeff. (min)= 7.54 (ii) 16.07 (ii)
Unit Hyd. Tpeak (min)= 10.00 20.00
Unit Hyd. peak (cms)= .13 .06

TOTALS

PEAK FLOW (cms)= 1.52 2.56 3.608 (iii)
TIME TO PEAK (hrs)= 6.00 6.17 6.08
RUNOFF VOLUME (mm)= 51.91 14.24 22.15
TOTAL RAINFALL (mm)= 53.41 53.41 53.41
RUNOFF COEFFICIENT = .97 .27 .41

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0415)
ID= 1 DT= 5.0 min

Area (ha)= 4.99
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.10 2.89
Dep. Storage (mm)= 1.50 5.00
Average Slope (%)= 2.86 2.86
Length (m)= 185.00 40.00
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 70.50 81.70
over (min) 5.00 15.00
Storage Coeff. (min)= 3.10 (ii) 10.77 (ii)
Unit Hyd. Tpeak (min)= 5.00 15.00
Unit Hyd. peak (cms)= .27 .09

TOTALS

PEAK FLOW (cms)= .20 .39 .532 (iii)
TIME TO PEAK (hrs)= 6.00 6.08 6.00
RUNOFF VOLUME (mm)= 51.91 14.24 22.15
TOTAL RAINFALL (mm)= 53.41 53.41 53.41

Hadati Creek Watershed - Post Development with Cityview Ridge
 RUNOFF COEFFICIENT = .97 .27 .41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0410) ID= 1 DT= 5.0 min		Area (ha)= 24.20		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	10.16	14.04	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	401.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.49 (ii)	14.03 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.20	.08	
PEAK FLOW (cms)=		.95	1.66	*TOTALS* 2.307 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0460) ID= 1 DT= 5.0 min		Area (ha)= 36.00		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.97 (ii)	14.47 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.19	.08	
PEAK FLOW (cms)=		.95	1.66	*TOTALS* 2.307 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

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PEAK FLOW	(cms)=	1.40	2.42	3.376 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	51.91	14.24	22.15
TOTAL RAINFALL	(mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT	=	.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0455)	Area	(ha)=	12.70	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=	4.84 (ii)		13.78 (ii)	
Unit Hyd. Tpeak (min)=	5.00		15.00	
Unit Hyd. peak (cms)=	.22		.08	
				TOTALS
PEAK FLOW	(cms)=	.51	.88	1.226 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	51.91	14.24	22.15
TOTAL RAINFALL	(mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT	=	.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 F_o (mm/hr)= 75.00 K (1/hr)= 4.14
 F_c (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0395)	Area	(ha)=	51.20	
ID= 1 DT= 5.0 min	Total Imp(%)=	10.00	Dir. Conn.(%)=	5.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.12	46.08	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	58.39	
over (min)		10.00	20.00	

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Storage Coeff. (min)= 8.92 (ii) 18.68 (ii)
 Unit Hyd. Tpeak (min)= 10.00 20.00
 Unit Hyd. peak (cms)= .12 .06

PEAK FLOW (cms)= .41 2.36
 TIME TO PEAK (hrs)= 6.00 6.25
 RUNOFF VOLUME (mm)= 51.91 9.64
 TOTAL RAINFALL (mm)= 53.41 53.41
 RUNOFF COEFFICIENT = .97 .18

TOTALS
 2.601 (iii)
 6.17
 11.75
 53.41
 .22

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0360)
 ID= 1 DT= 5.0 min

Area (ha)= 30.00
 Total Imp(%)= 37.00 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 11.10 18.90
 Dep. Storage (mm)= 1.50 5.00
 Average Slope (%)= 2.00 2.00
 Length (m)= 447.00 40.00
 Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 70.50 75.96
 over (min)= 5.00 15.00
 Storage Coeff. (min)= 5.86 (ii) 14.65 (ii)
 Unit Hyd. Tpeak (min)= 5.00 15.00
 Unit Hyd. peak (cms)= .20 .08

PEAK FLOW (cms)= 1.06 1.94
 TIME TO PEAK (hrs)= 6.00 6.08
 RUNOFF VOLUME (mm)= 51.91 13.31
 TOTAL RAINFALL (mm)= 53.41 53.41
 RUNOFF COEFFICIENT = .97 .25

TOTALS
 2.582 (iii)
 6.00
 20.64
 53.41
 .39

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0350)
 ID= 1 DT= 5.0 min

Area (ha)= 16.30
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

IMPERVIOUS PERVIOUS (i)
 Surface Area (ha)= 6.85 9.45

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Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.00	1.00	
Length	(m)=	330.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	77.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.01 (ii)	16.75 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.19	.06	
PEAK FLOW	(cms)=	.63	.95	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.17	1.186 (iii)
RUNOFF VOLUME	(mm)=	51.91	14.24	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	22.15
RUNOFF COEFFICIENT	=	.97	.27	53.41
				.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0355) ID= 1 DT= 5.0 min	Area (ha)= 12.30 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
---	---

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.79 (ii)	13.92 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.08	
PEAK FLOW	(cms)=	.49	.85	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	1.183 (iii)
RUNOFF VOLUME	(mm)=	51.91	14.24	6.00
TOTAL RAINFALL	(mm)=	53.41	53.41	22.15
RUNOFF COEFFICIENT	=	.97	.27	53.41
				.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0365)	Area (ha)= 117.50
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 ID= 1 DT= 5.0 min | Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.83 (ii)	17.37 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
				TOTALS
PEAK FLOW (cms)=		3.95	6.70	9.481 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.08
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0105)
 ID= 1 DT= 5.0 min | Area (ha)= 51.32
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	21.55	29.77	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	550.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.64 (ii)	15.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.18	.07	
				TOTALS
PEAK FLOW (cms)=		1.96	3.14	3.870 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.08
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB STANDHYD (0102) ID= 1 DT= 5.0 min		Area (ha)= 14.32	Dir. Conn.(%)= 21.00	
		Total Imp(%)= 42.00		
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.01	8.31	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	287.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.49 (ii)	13.03 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.23	.08	
				TOTALS
PEAK FLOW (cms)=		.58	1.02	1.415 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min		Area (ha)= 16.32	Dir. Conn.(%)= 21.00	
		Total Imp(%)= 42.00		
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.47	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	309.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.70 (ii)	13.23 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.08	
				TOTALS
PEAK FLOW (cms)=		.65	1.15	1.601 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- Hadati Creek Watershed - Post Development with Cityview Ridge
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0110)
ID= 1 DT= 5.0 min

Area (ha)= 19.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	7.98	11.02	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	365.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.19 (ii)	13.73 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
PEAK FLOW (cms)=		.75	1.32	*TOTALS* 1.831 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0600)
ID= 1 DT= 5.0 min

Area (ha)= 11.38
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	4.78	6.60	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	81.70	
over (min)		10.00	20.00	
Storage Coeff. (min)=		7.54 (ii)	16.07 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.13	.06	
PEAK FLOW (cms)=		.40	.68	*TOTALS* .953 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.08
RUNOFF VOLUME (mm)=		51.91	14.24	22.15
TOTAL RAINFALL (mm)=		53.41	53.41	53.41
RUNOFF COEFFICIENT =		.97	.27	.41

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- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0601)	Area (ha)=	7.62		
ID= 1 DT= 5.0 min	Total Imp(%)=	46.00	Dir. Conn.(%)=	21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	3.51	4.11	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	89.23	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.54 (ii)	15.78 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.07	
PEAK FLOW (cms)=	.27	.49	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.17	.679 (iii)
RUNOFF VOLUME (mm)=	51.91	15.62	6.08
TOTAL RAINFALL (mm)=	53.41	53.41	23.24
RUNOFF COEFFICIENT =	.97	.29	53.41
			.44

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0607)	Area (ha)=	5.97		
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	2.50

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.51	3.46	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	105.29	
over (min)	10.00	20.00	
Storage Coeff. (min)=	7.54 (ii)	15.25 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.07	
PEAK FLOW (cms)=	.03	.52	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.17	.534 (iii)
RUNOFF VOLUME (mm)=	51.91	17.87	6.17
TOTAL RAINFALL (mm)=	53.41	53.41	18.72
			53.41

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 RUNOFF COEFFICIENT = .97 .33 .35

***** WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0540) ID= 1 DT= 5.0 min		Area (ha)= 4.63	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.70	.93	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	30.06	
over (min)		5.00	25.00	
Storage Coeff. (min)=		4.48 (ii)	23.24 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.23	.05	
PEAK FLOW (cms)=		.70	.04	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.25	.713 (iii)
RUNOFF VOLUME (mm)=		51.91	9.54	6.00
TOTAL RAINFALL (mm)=		53.41	53.41	43.01
RUNOFF COEFFICIENT =		.97	.18	53.41
				.81

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0500) ID= 1 DT= 5.0 min		Area (ha)= 244.00	Total Imp(%)= 46.00	Dir. Conn.(%)= 26.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		70.50	78.43	
over (min)		15.00	30.00	
Storage Coeff. (min)=		14.47 (ii)	25.89 (ii)	
Unit Hyd. Tpeak (min)=		15.00	30.00	

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Unit Hyd. peak (cms)=	.08	.04	
			TOTALS
PEAK FLOW (cms)=	8.08	9.34	14.467 (iii)
TIME TO PEAK (hrs)=	6.08	6.33	6.25
RUNOFF VOLUME (mm)=	51.91	14.36	24.12
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.27	.45

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0510)	Area (ha)= 16.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	12.80		3.20	
Dep. Storage (mm)=	1.50		5.00	
Average Slope (%)=	.50		.20	
Length (m)=	400.00		40.00	
Mannings n =	.013		.300	
Max.Eff.Inten.(mm/hr)=	70.50		20.04	
over (min)	10.00		40.00	
Storage Coeff. (min)=	8.31 (ii)		38.19 (ii)	
Unit Hyd. Tpeak (min)=	10.00		40.00	
Unit Hyd. peak (cms)=	.13		.03	
				TOTALS
PEAK FLOW (cms)=	2.06		.09	2.080 (iii)
TIME TO PEAK (hrs)=	6.00		6.50	6.00
RUNOFF VOLUME (mm)=	51.91		9.54	43.01
TOTAL RAINFALL (mm)=	53.41		53.41	53.41
RUNOFF COEFFICIENT =	.97		.18	.81

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0542)	Area (ha)= 25.25		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	20.20		5.05
Dep. Storage (mm)=	1.50		5.00
Average Slope (%)=	.55		.55
Length (m)=	350.00		40.00
Mannings n =	.013		.300
Max.Eff.Inten.(mm/hr)=	70.50		30.06

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over (min)	5.00	30.00	
Storage Coeff. (min)=	7.45 (ii)	26.21 (ii)	
Unit Hyd. Tpeak (min)=	5.00	30.00	
Unit Hyd. peak (cms)=	.17	.04	
			TOTALS
PEAK FLOW (cms)=	3.56	.19	3.608 (iii)
TIME TO PEAK (hrs)=	6.00	6.33	6.00
RUNOFF VOLUME (mm)=	51.91	9.54	43.01
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.18	.81

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0543)	Area (ha)= 14.99		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	11.99	3.00	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	200.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	70.50	30.06	
over (min)	5.00	25.00	
Storage Coeff. (min)=	5.33 (ii)	24.09 (ii)	
Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	.21	.05	
			TOTALS
PEAK FLOW (cms)=	2.23	.12	2.271 (iii)
TIME TO PEAK (hrs)=	6.00	6.33	6.00
RUNOFF VOLUME (mm)=	51.91	9.54	43.01
TOTAL RAINFALL (mm)=	53.41	53.41	53.41
RUNOFF COEFFICIENT =	.97	.18	.81

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0544)	Area (ha)= 1.13		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.90	.23	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	50.00	40.00	

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Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 70.50 30.06
over (min) 5.00 25.00
Storage Coeff. (min)= 2.32 (ii) 21.08 (ii)
Unit Hyd. Tpeak (min)= 5.00 25.00
Unit Hyd. peak (cms)= .30 .05

PEAK FLOW (cms)= .17 .01 *TOTALS*
TIME TO PEAK (hrs)= 6.00 6.25 .178 (iii)
RUNOFF VOLUME (mm)= 51.91 9.54 6.00
TOTAL RAINFALL (mm)= 53.41 53.41 43.01
RUNOFF COEFFICIENT = .97 .18 53.41
.81

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525)	AREA (ha)= .00
ID= 1 DT=****min	QPEAK (cms)= .00
	TPEAK (hrs)= .00
	VOLUME (mm)=*****

ADD HYD (0420)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0415):	4.99	.532	6.00	22.15
+ ID2= 2 (0410):	24.20	2.307	6.00	22.15
ID = 3 (0420):	29.19	2.839	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0465)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0460):	36.00	3.376	6.00	22.15
+ ID2= 2 (0455):	12.70	1.226	6.00	22.15
ID = 3 (0465):	48.70	4.602	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0362)	Routing time step (min)'= 5.00
IN= 2---> OUT= 1	

<----- DATA FOR SECTION (1.1) ----->
Distance Elevation Manning

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.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0360)	30.00	2.58	6.00	20.64	.23	1.41
OUTFLOW: ID= 1 (0362)	30.00	2.01	6.17	20.63	.21	1.31

ROUTE CHN (0353)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24

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.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0350)	16.30	1.19	6.00	22.15	.16	1.10
OUTFLOW:	ID= 1 (0353)	16.30	.95	6.25	22.11	.15	1.02

ROUTE CHN (0358)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0355)	12.30	1.18	6.00	22.15	.16	1.10
OUTFLOW:	ID= 1 (0358)	12.30	.74	6.17	22.10	.13	.92

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RESERVOIR (0106)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	3.870	6.08	22.15
OUTFLOW: ID= 1 (0106)	51.320	2.731	6.33	22.14

PEAK FLOW REDUCTION [Qout/Qin](%)= 70.57
TIME SHIFT OF PEAK FLOW (min)= 15.00
MAXIMUM STORAGE USED (ha.m.)= .5507

ADD HYD (0103)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):	14.32	1.415	6.00	22.15
+ ID2= 2 (0101):	16.32	1.601	6.00	22.15
ID = 3 (0103):	30.64	3.016	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	1.0000
.0100	.0100	20.0000	1.1000
.0120	.1000	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	1.831	6.00	22.15
OUTFLOW: ID= 1 (0111)	19.000	.238	6.58	22.14

PEAK FLOW REDUCTION [Qout/Qin](%)= 12.98
TIME SHIFT OF PEAK FLOW (min)= 35.00
MAXIMUM STORAGE USED (ha.m.)= .3060

ADD HYD (0602)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0600):	11.38	.953	6.08	22.15
+ ID2= 2 (0601):	7.62	.679	6.08	23.24
ID = 3 (0602):	19.00	1.632	6.08	22.59

Hadati Creek watershed - Post Development with Cityview Ridge

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> DUHYD (0505) Inlet Cap.=9.000 #of Inlets= 1 Total(cms)= 9.0 </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	14.47	6.25	24.12
MAJOR SYS.(ID= 2):	33.53	5.47	6.25	24.12
MINOR SYS.(ID= 3):	210.47	9.00	6.00	24.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> ADD HYD (0515) 1 + 2 = 3 </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0505):	210.47	9.000	6.00	24.12
+ ID2= 2 (0510):	16.00	2.080	6.00	43.01
ID = 3 (0515):	226.47	11.080	6.00	25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> DUHYD (0425) Inlet Cap.=1.980 #of Inlets= 1 Total(cms)= 2.0 </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	2.84	6.00	22.15
MAJOR SYS.(ID= 2):	2.28	.86	6.00	22.15
MINOR SYS.(ID= 3):	26.91	1.98	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> ADD HYD (0470) 1 + 2 = 3 </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0425):	2.28	.859	6.00	22.15
+ ID2= 2 (0465):	48.70	4.602	6.00	22.15
ID = 3 (0470):	50.98	5.461	6.00	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<div> ADD HYD (0359) 1 + 2 = 3 </div>				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)

Hadati Creek watershed - Post Development with Cityview Ridge

ID1= 1 (0353):	16.30	.952	6.25	22.11
+ ID2= 2 (0358):	12.30	.744	6.17	22.10
<hr/>				
ID = 3 (0359):	28.60	1.680	6.25	22.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104) IN= 2---> OUT= 1 DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	1.0000	.5000
	.0100	.0100	10.0000	.6000
	.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	3.016	6.00	22.15
OUTFLOW: ID= 1 (0104)	30.640	.801	6.42	22.14

PEAK FLOW REDUCTION	[Qout/Qin](%)= 26.57
TIME SHIFT OF PEAK FLOW	(min)= 25.00
MAXIMUM STORAGE USED	(ha.m.)= .4263

ADD HYD (0114) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0104):	30.64	.801	6.42	22.14
+ ID2= 2 (0111):	19.00	.238	6.58	22.14
<hr/>				
ID = 3 (0114):	49.64	1.029	6.50	22.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0563) IN= 2---> OUT= 1	Routing time step (min)'= 5.00				
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<----- DATA FOR SECTION (2.2) ----->					
Distance	Elevation	Manning			
.00	1.00	.0350			
2.00	.50	.0350			
4.00	.00	.0350 / .0350	Main Channel		
4.50	.00	.0350	Main Channel		
5.00	.00	.0350 / .0350	Main Channel		
7.00	.50	.0350			
9.00	1.00	.0350			

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.745E+01	.0	.64	3.06
.11	.11	.175E+02	.1	.96	2.03
.16	.16	.301E+02	.3	1.21	1.61
.21	.21	.454E+02	.6	1.42	1.37
.26	.26	.632E+02	.9	1.61	1.21
.32	.32	.836E+02	1.3	1.77	1.10

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.37	.37	.107E+03	1.8	1.93	1.01
.42	.42	.132E+03	2.3	2.08	.94
.47	.47	.160E+03	3.0	2.22	.88
.53	.53	.191E+03	3.8	2.35	.83
.58	.58	.225E+03	4.8	2.48	.79
.63	.63	.261E+03	5.8	2.60	.75
.68	.68	.299E+03	7.0	2.72	.72
.74	.74	.340E+03	8.2	2.84	.69
.79	.79	.384E+03	9.7	2.95	.66
.84	.84	.430E+03	11.3	3.06	.64
.89	.89	.479E+03	13.0	3.17	.62
.95	.95	.531E+03	14.8	3.27	.60
1.00	1.00	.585E+03	16.9	3.38	.58

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0602)	19.00	1.63	6.08	22.59	.35	1.89
OUTFLOW:	ID= 1 (0563)	19.00	1.61	6.08	22.59	.35	1.88

ROUTE CHN (0564)
IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
.00	101.50	.0500
1.00	100.70	.0500
1.50	100.55	.0500 / .0300
2.00	99.50	.0300
3.50	99.60	.0300
4.50	100.65	.0300 / .0500
6.00	101.45	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0505)	33.53	5.47	6.25	24.12	1.58	1.28

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 OUTFLOW: ID= 1 (0564) 33.53 4.91 6.33 24.12 1.50 1.25

DUHYD (0520)
 Inlet Cap.=3.050
 #of Inlets= 1
 Total(cms)= 3.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	226.47	11.08	6.00	25.46
MAJOR SYS.(ID= 2):	88.85	8.03	6.00	25.46
MINOR SYS.(ID= 3):	137.62	3.05	5.75	25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	324.60	.0500	
115.00	321.60	.0500	
120.00	320.80	.0500 / .0300	Main Channel
122.00	320.80	.0300 / .0500	Main Channel
138.00	321.60	.0500	
148.00	322.30	.0500	
154.00	323.10	.0500	
164.00	324.60	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0470)	50.98	5.46	6.00	22.15	.49	1.23
OUTFLOW: ID= 1 (0475)	50.98	4.60	6.08	22.15	.45	1.19

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ADD HYD (0363)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0362):	30.00	2.013	6.17	20.63
+ ID2= 2	(0359):	28.60	1.680	6.25	22.11
ID = 3 (0363):		58.60	3.649	6.17	21.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0106):	51.32	2.731	6.33	22.14
+ ID2= 2	(0114):	49.64	1.029	6.50	22.14
ID = 3 (0115):		100.96	3.732	6.33	22.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0563):	19.00	1.610	6.08	22.59
+ ID2= 2	(0607):	5.97	.534	6.17	18.72
ID = 3 (0492):		24.97	2.115	6.08	21.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0526)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0525):	.00	.001	.00	*****
+ ID2= 2	(0520):	88.85	8.030	6.00	25.46
ID = 3 (0526):		88.85	8.030	6.00	25.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)					
1 + 2 = 3					
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0363):	58.60	3.649	6.17	21.35
+ ID2= 2	(0365):	117.50	9.481	6.08	22.15
ID = 3 (0380):		176.10	12.674	6.17	21.88

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 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0482)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.2910	.3795
.2590	.0579	.2970	.4503
.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	24.970	2.115	6.08	21.66
OUTFLOW: ID= 1 (0482)	24.970	.288	6.83	21.66

PEAK FLOW REDUCTION [Qout/Qin](%)= 13.60
 TIME SHIFT OF PEAK FLOW (min)= 45.00
 MAXIMUM STORAGE USED (ha.m.)= .3412

ROUTE CHN (0527)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
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		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0526)	88.85	8.03	6.00	25.46	2.05	.76
OUTFLOW:	ID= 1 (0527)	88.85	6.50	6.42	25.46	1.97	.79

RESERVOIR (0390)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW :	ID= 2 (0380)	176.100	12.674	6.17
OUTFLOW:	ID= 1 (0390)	176.100	1.333	7.08
				21.88

PEAK FLOW REDUCTION [Qout/Qin](%)= 10.52
TIME SHIFT OF PEAK FLOW (min)= 55.00
MAXIMUM STORAGE USED (ha.m.)= 2.5065

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0395):	51.20	2.601	6.17	11.75
+ ID2= 2 (0390):	176.10	1.333	7.08	21.88
ID = 3 (0400):	227.30	3.883	6.17	19.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02

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1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0400)	227.30	3.88	6.17	19.60	.34	1.13
OUTFLOW:	ID= 1 (0403)	227.30	2.23	6.42	19.60	.25	.89

ADD HYD (0407)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0403):	227.30	2.232	6.42	19.60
+ ID2= 2 (0115):	100.96	3.732	6.33	22.14
ID = 3 (0407):	328.26	5.857	6.33	20.38

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0113)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.6000	6.4000
1.1000	2.9000	9.1000	10.0000
1.3000	4.3000	12.0000	20.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	5.857	6.33	20.38
OUTFLOW: ID= 1 (0113)	328.260	1.137	12.67	20.38

PEAK FLOW REDUCTION [Qout/Qin](%)= 19.42
TIME SHIFT OF PEAK FLOW (min)=380.00
MAXIMUM STORAGE USED (ha.m.)= 3.1599

ADD HYD (0430)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0113):	328.26	1.137	12.67	20.38
+ ID2= 2 (0425):	26.91	1.980	6.00	22.15
ID = 3 (0430):	355.17	2.137	6.17	20.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek watershed - Post Development with Cityview Ridge

ROUTE CHN (0440)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 100.00 325.40 .0600
 120.00 324.60 .0600
 126.00 323.90 .0600
 130.00 323.00 .0600
 140.00 322.30 .0600 / .0300 Main Channel
 142.00 322.30 .0300 / .0600 Main Channel
 150.00 323.90 .0600
 155.00 324.60 .0600
 160.00 325.40 .0600

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .16 322.46 .233E+03 .6 .96 6.96
 .33 322.63 .672E+03 2.1 1.26 5.27
 .49 322.79 .132E+04 4.9 1.48 4.51
 .65 322.95 .216E+04 9.0 1.66 4.03
 .82 323.12 .319E+04 14.9 1.87 3.57
 .98 323.28 .433E+04 22.5 2.08 3.21
 1.14 323.44 .556E+04 31.6 2.27 2.93
 1.31 323.61 .689E+04 42.3 2.45 2.72
 1.47 323.77 .833E+04 54.6 2.62 2.54
 1.63 323.93 .987E+04 68.3 2.77 2.41
 1.79 324.09 .115E+05 82.8 2.87 2.33
 1.96 324.26 .134E+05 99.2 2.96 2.25
 2.12 324.42 .154E+05 117.9 3.06 2.18
 2.28 324.58 .176E+05 138.8 3.15 2.11
 2.45 324.75 .200E+05 157.4 3.14 2.12
 2.61 324.91 .228E+05 179.6 3.15 2.11
 2.77 325.07 .259E+05 205.8 3.18 2.09
 2.94 325.24 .293E+05 236.1 3.23 2.07
 3.10 325.40 .330E+05 270.6 3.28 2.03

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0430) 355.17 2.14 6.17 20.51 .33 1.26
 OUTFLOW: ID= 1 (0440) 355.17 2.11 6.17 20.51 .32 1.26

ADD HYD (0485)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0475):	50.98	4.600	6.08	22.15
+ ID2= 2 (0440):	355.17	2.113	6.17	20.51
ID = 3 (0485):	406.15	6.641	6.08	20.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0490)		AREA	QPEAK	TPEAK	R.V.
1	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0480):	43.10	3.608	6.08	22.15
+ ID2= 2	(0485):	406.15	6.641	6.08	20.72
ID = 3 (0490):		449.25	10.249	6.08	20.86

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)		AREA	QPEAK	TPEAK	R.V.
1	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0490):	449.25	10.249	6.08	20.86
+ ID2= 2	(0482):	24.97	.288	6.83	21.66
ID = 3 (0491):		474.22	10.516	6.08	20.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	7.0800	2.4860
		.2760	.0600	8.1000	3.3240
		1.2000	.3400	9.7980	4.6420
		2.0400	.6182	10.4940	7.4397
		2.6400	1.1630	11.6850	10.3000
		3.1200	1.7070	12.3480	11.4000
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0491)		474.220	10.516	6.08	20.90
OUTFLOW: ID= 1 (0483)		474.220	2.907	6.67	20.90

PEAK FLOW REDUCTION [Qout/Qin](%)= 27.65
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= 1.4680

ADD HYD (0530)		AREA	QPEAK	TPEAK	R.V.
1	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0483):	474.22	2.907	6.67	20.90
+ ID2= 2	(0540):	4.63	.713	6.00	43.01
ID = 3 (0530):		478.85	3.002	6.50	21.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)

Hadati Creek watershed - Post Development with Cityview Ridge					
1 + 2 = 3		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0530):		478.85	3.002	6.50	21.11
+ ID2= 2 (0527):		88.85	6.502	6.42	25.46
ID = 3 (0545):		567.70	9.482	6.50	21.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546) 1 + 2 = 3		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0545):		567.70	9.482	6.50	21.79
+ ID2= 2 (0542):		25.25	3.608	6.00	43.01
ID = 3 (0546):		592.95	10.345	6.00	22.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547) 1 + 2 = 3		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0546):		592.95	10.345	6.00	22.70
+ ID2= 2 (0543):		14.99	2.271	6.00	43.01
ID = 3 (0547):		607.94	12.615	6.00	23.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548) 1 + 2 = 3		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0547):		607.94	12.615	6.00	23.20
+ ID2= 2 (0544):		1.13	.178	6.00	43.01
ID = 3 (0548):		609.07	12.793	6.00	23.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 ** SIMULATION NUMBER: 3 **

READ STORM	Filename: Y:\SPrimmer\OTTHYMO\Ci
Ptotal= 73.56 mm	tyview Ridge\25yrSCS12hr.stm
	Comments: 25 year SCS Type II 12hr design storm

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.25	1.84	3.25	2.94	6.25	13.24	9.25	2.58
.50	1.84	3.50	2.94	6.50	13.24	9.50	2.58

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.75	1.84	3.75	2.94	6.75	5.89	9.75	2.58
1.00	1.84	4.00	2.94	7.00	5.89	10.00	2.58
1.25	1.84	4.25	4.41	7.25	4.41	10.25	1.47
1.50	1.84	4.50	4.41	7.50	4.41	10.50	1.47
1.75	1.84	4.75	5.89	7.75	4.41	10.75	1.47
2.00	1.84	5.00	5.89	8.00	4.41	11.00	1.47
2.25	2.21	5.25	8.83	8.25	2.58	11.25	1.47
2.50	2.21	5.50	8.83	8.50	2.58	11.50	1.47
2.75	2.21	5.75	35.31	8.75	2.58	11.75	1.47
3.00	2.21	6.00	97.10	9.00	2.58	12.00	1.47

CALIB
STANDHYD (0480)
ID= 1 DT= 5.0 min

Area (ha)= 43.10
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.84	3.083	2.94	6.083	13.24	9.08	2.58
.167	1.84	3.167	2.94	6.167	13.24	9.17	2.58
.250	1.84	3.250	2.94	6.250	13.24	9.25	2.58
.333	1.84	3.333	2.94	6.333	13.24	9.33	2.58
.417	1.84	3.417	2.94	6.417	13.24	9.42	2.58
.500	1.84	3.500	2.94	6.500	13.24	9.50	2.58
.583	1.84	3.583	2.94	6.583	5.89	9.58	2.58
.667	1.84	3.667	2.94	6.667	5.89	9.67	2.58
.750	1.84	3.750	2.94	6.750	5.89	9.75	2.58
.833	1.84	3.833	2.94	6.833	5.89	9.83	2.58
.917	1.84	3.917	2.94	6.917	5.89	9.92	2.58
1.000	1.84	4.000	2.94	7.000	5.88	10.00	2.58
1.083	1.84	4.083	4.41	7.083	4.41	10.08	1.47
1.167	1.84	4.167	4.41	7.167	4.41	10.17	1.47
1.250	1.84	4.250	4.41	7.250	4.41	10.25	1.47
1.333	1.84	4.333	4.41	7.333	4.41	10.33	1.47
1.417	1.84	4.417	4.41	7.417	4.41	10.42	1.47
1.500	1.84	4.500	4.41	7.500	4.41	10.50	1.47
1.583	1.84	4.583	5.88	7.583	4.41	10.58	1.47
1.667	1.84	4.667	5.89	7.667	4.41	10.67	1.47
1.750	1.84	4.750	5.89	7.750	4.41	10.75	1.47
1.833	1.84	4.833	5.89	7.833	4.41	10.83	1.47
1.917	1.84	4.917	5.89	7.917	4.41	10.92	1.47
2.000	1.84	5.000	5.89	8.000	4.41	11.00	1.47
2.083	2.21	5.083	8.83	8.083	2.58	11.08	1.47
2.167	2.21	5.167	8.83	8.167	2.58	11.17	1.47
2.250	2.21	5.250	8.83	8.250	2.58	11.25	1.47
2.333	2.21	5.333	8.83	8.333	2.58	11.33	1.47
2.417	2.21	5.417	8.83	8.417	2.58	11.42	1.47
2.500	2.21	5.500	8.83	8.500	2.58	11.50	1.47
2.583	2.21	5.583	35.31	8.583	2.58	11.58	1.47
2.667	2.21	5.667	35.31	8.667	2.58	11.67	1.47

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2.750	2.21	5.750	35.31	8.750	2.58	11.75	1.47
2.833	2.21	5.833	97.10	8.833	2.58	11.83	1.47
2.917	2.21	5.917	97.10	8.917	2.58	11.92	1.47
3.000	2.21	6.000	97.10	9.000	2.58	12.00	1.47

Max.Eff.Inten.(mm/hr)= 97.10 119.40
over (min) 5.00 15.00
Storage Coeff. (min)= 6.63 (ii) 13.97 (ii)
Unit Hyd. Tpeak (min)= 5.00 15.00
Unit Hyd. peak (cms)= .18 .08

PEAK FLOW (cms)= 2.27 4.88 *TOTALS* 6.559 (iii)
TIME TO PEAK (hrs)= 6.00 6.08 6.00
RUNOFF VOLUME (mm)= 72.06 26.53 36.09
TOTAL RAINFALL (mm)= 73.56 73.56 73.56
RUNOFF COEFFICIENT = .98 .36 .49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0415)
ID= 1 DT= 5.0 min
Area (ha)= 4.99
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.10 2.89
Dep. Storage (mm)= 1.50 5.00
Average Slope (%)= 2.86 2.86
Length (m)= 185.00 40.00
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)= 97.10 119.40
over (min) 5.00 10.00
Storage Coeff. (min)= 2.73 (ii) 9.32 (ii)
Unit Hyd. Tpeak (min)= 5.00 10.00
Unit Hyd. peak (cms)= .29 .12

PEAK FLOW (cms)= .28 .73 *TOTALS* 1.007 (iii)
TIME TO PEAK (hrs)= 6.00 6.00 6.00
RUNOFF VOLUME (mm)= 72.06 26.53 36.09
TOTAL RAINFALL (mm)= 73.56 73.56 73.56
RUNOFF COEFFICIENT = .98 .36 .49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0410)
Area (ha)= 24.20
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 ID= 1 DT= 5.0 min | Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	10.16	14.04	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	401.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.83 (ii)	12.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.22	.09	
				TOTALS
PEAK FLOW (cms)=		1.33	2.92	3.938 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		72.06	26.53	36.09
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0460)
 ID= 1 DT= 5.0 min | Area (ha)= 36.00
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.26 (ii)	12.56 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
				TOTALS
PEAK FLOW (cms)=		1.96	4.29	5.772 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		72.06	26.53	36.09
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0455)
ID= 1 DT= 5.0 min

Area (ha)= 12.70
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.33	7.37	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.71	1.71	
Length (m)=	300.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)=	5.00	15.00	
Storage Coeff. (min)=	4.25 (ii)	11.94 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.23	.09	
			TOTALS
PEAK FLOW (cms)=	.71	1.55	2.088 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0395)
ID= 1 DT= 5.0 min

Area (ha)= 51.20
Total Imp(%)= 10.00 Dir. Conn.(%)= 5.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.12	46.08	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	900.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	88.55	
over (min)=	10.00	20.00	
Storage Coeff. (min)=	7.85 (ii)	16.11 (ii)	
Unit Hyd. Tpeak (min)=	10.00	20.00	
Unit Hyd. peak (cms)=	.13	.06	
			TOTALS
PEAK FLOW (cms)=	.58	5.35	5.668 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.17
RUNOFF VOLUME (mm)=	72.06	21.36	23.89
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.29	.32

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

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Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0360)	Area (ha)=	30.00		
ID= 1 DT= 5.0 min	Total Imp(%)=	37.00	Dir. Conn.(%)=	19.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	11.10	18.90	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	447.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	111.81	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.16 (ii)	12.69 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
PEAK FLOW (cms)=		1.48	3.58	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.00	4.647 (iii)
RUNOFF VOLUME (mm)=		72.06	25.57	6.00
TOTAL RAINFALL (mm)=		73.56	73.56	34.40
RUNOFF COEFFICIENT	=	.98	.35	73.56
				.47

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0350)	Area (ha)=	16.30		
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.45	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.00	1.00	
Length	(m)=	330.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.29 (ii)	14.32 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
PEAK FLOW (cms)=		.89	1.82	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.00	2.485 (iii)
RUNOFF VOLUME (mm)=		72.06	26.53	6.00
				36.09

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TOTAL RAINFALL (mm)= 73.56 73.56 73.56
RUNOFF COEFFICIENT = .98 .36 .49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0355) ID= 1 DT= 5.0 min		Area (ha)= 12.30	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.22 (ii)	12.06 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.24	.09	
PEAK FLOW (cms)=		.68	1.49	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	2.015 (iii)
RUNOFF VOLUME (mm)=		72.06	26.53	6.00
TOTAL RAINFALL (mm)=		73.56	73.56	36.09
RUNOFF COEFFICIENT =		.98	.36	73.56
				.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0365) ID= 1 DT= 5.0 min		Area (ha)= 117.50	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		10.00	20.00	
Storage Coeff. (min)=		7.77 (ii)	15.10 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.13	.07	

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PEAK FLOW	(cms)=	5.65	11.98	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.17	16.238 (iii)
RUNOFF VOLUME	(mm)=	72.06	26.53	6.08
TOTAL RAINFALL	(mm)=	73.56	73.56	36.09
RUNOFF COEFFICIENT	=	.98	.36	73.56
				.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0105)	Area (ha)=	51.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	21.55	29.77	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	550.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	119.40	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.84 (ii)	13.17 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.20	.08	
				TOTALS
PEAK FLOW	(cms)=	2.76	5.98	8.044 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	72.06	26.53	36.09
TOTAL RAINFALL	(mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT	=	.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0102)	Area (ha)=	14.32	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	6.01	8.31
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	287.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		97.10	119.40
over (min)		5.00	15.00

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Storage Coeff. (min)=	3.95 (ii)	11.29 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.24	.09	
			TOTALS
PEAK FLOW (cms)=	.80	1.79	2.406 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0101) ID= 1 DT= 5.0 min	Area (ha)= 16.32 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.47	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	309.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.13 (ii)	11.47 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.24	.09	
			TOTALS
PEAK FLOW (cms)=	.91	2.02	2.725 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0110) ID= 1 DT= 5.0 min	Area (ha)= 19.00 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	7.98	11.02
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00

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Length (m)=	365.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.57 (ii)	11.90 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.23	.09	
			TOTALS
PEAK FLOW (cms)=	1.05	2.32	3.122 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0600) ID= 1 DT= 5.0 min

Area (ha)=	11.38	
Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	4.78	6.60	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	119.40	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.63 (ii)	13.97 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.18	.08	
			TOTALS
PEAK FLOW (cms)=	.60	1.29	1.732 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	72.06	26.53	36.09
TOTAL RAINFALL (mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT =	.98	.36	.49

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0601) ID= 1 DT= 5.0 min

Area (ha)=	7.62	
Total Imp(%)=	46.00	Dir. Conn.(%)= 21.00

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		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.51	4.11	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	129.34	
over (min)		5.00	15.00	
Storage Coeff. (min)=		6.63 (ii)	13.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.18	.08	
PEAK FLOW	(cms)=	.40	.89	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	1.186 (iii)
RUNOFF VOLUME	(mm)=	72.06	27.57	6.00
TOTAL RAINFALL	(mm)=	73.56	73.56	36.92
RUNOFF COEFFICIENT	=	.98	.37	73.56
				.50

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0607)
ID= 1 DT= 5.0 min

Area (ha)= 5.97
Total Imp(%)= 42.00 Dir. Conn.(%)= 2.50

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.51	3.46	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	150.66	
over (min)		5.00	15.00	
Storage Coeff. (min)=		6.63 (ii)	13.32 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.18	.08	
PEAK FLOW	(cms)=	.04	.90	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	.921 (iii)
RUNOFF VOLUME	(mm)=	72.06	29.58	6.08
TOTAL RAINFALL	(mm)=	73.56	73.56	30.64
RUNOFF COEFFICIENT	=	.98	.40	73.56
				.42

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB					
STANDHYD (0540)		Area (ha)= 4.63			
ID= 1 DT= 5.0 min		Total Imp(%)= 80.00		Dir. Conn.(%)= 79.00	
		IMPERVIOUS		PERVIOUS (i)	
Surface Area	(ha)=	3.70		.93	
Dep. Storage	(mm)=	1.50		5.00	
Average Slope	(%)=	.55		.55	
Length	(m)=	150.00		40.00	
Mannings n	=	.013		.300	
Max.Eff.Inten.(mm/hr)=		97.10		87.19	
over (min)		5.00		20.00	
Storage Coeff. (min)=		3.94 (ii)		16.20 (ii)	
Unit Hyd. Tpeak (min)=		5.00		20.00	
Unit Hyd. peak (cms)=		.24		.06	
				TOTALS	
PEAK FLOW	(cms)=	.97		.11	1.036 (iii)
TIME TO PEAK	(hrs)=	6.00		6.17	6.00
RUNOFF VOLUME	(mm)=	72.06		21.22	61.38
TOTAL RAINFALL	(mm)=	73.56		73.56	73.56
RUNOFF COEFFICIENT	=	.98		.29	.83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0500) ID= 1 DT= 5.0 min		Area (ha)= 244.00 Total Imp(%)= 46.00	Dir. Conn.(%)= 26.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	120.22	
over (min)		15.00	25.00	
Storage Coeff. (min)=		12.73 (ii)	22.36 (ii)	
Unit Hyd. Tpeak (min)=		15.00	25.00	
Unit Hyd. peak (cms)=		.08	.05	
PEAK FLOW	(cms)=	11.66	18.11	*TOTALS* 27.658 (iii)
TIME TO PEAK	(hrs)=	6.08	6.25	6.17
RUNOFF VOLUME	(mm)=	72.06	26.62	38.44
TOTAL RAINFALL	(mm)=	73.56	73.56	73.56
RUNOFF COEFFICIENT	=	.98	.36	.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

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 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> CALIB STANDHYD (0510) ID= 1 DT= 5.0 min </div>		Area (ha)= 16.00		
		Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	65.53	
over (min)		5.00	30.00	
Storage Coeff. (min)=		7.31 (ii)	25.92 (ii)	
Unit Hyd. Tpeak (min)=		5.00	30.00	
Unit Hyd. peak (cms)=		.17	.04	
				TOTALS
PEAK FLOW (cms)=		3.12	.25	3.209 (iii)
TIME TO PEAK (hrs)=		6.00	6.33	6.00
RUNOFF VOLUME (mm)=		72.06	21.22	61.38
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.29	.83

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> CALIB STANDHYD (0542) ID= 1 DT= 5.0 min </div>		Area (ha)= 25.25		
		Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	20.20	5.05	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	350.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		97.10	87.19	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.56 (ii)	18.81 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.18	.06	
				TOTALS
PEAK FLOW (cms)=		5.02	.53	5.333 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.00
RUNOFF VOLUME (mm)=		72.06	21.22	61.38
TOTAL RAINFALL (mm)=		73.56	73.56	73.56
RUNOFF COEFFICIENT =		.98	.29	.83

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

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Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0543) ID= 1 DT= 5.0 min	Area (ha)= 14.99 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.99	3.00	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	200.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	87.19	
over (min)=	5.00	20.00	
Storage Coeff. (min)=	4.69 (ii)	16.94 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.22	.06	
PEAK FLOW (cms)=	3.11	.34	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.17	3.310 (iii)
RUNOFF VOLUME (mm)=	72.06	21.22	6.00
TOTAL RAINFALL (mm)=	73.56	73.56	61.38
RUNOFF COEFFICIENT =	.98	.29	73.56
			.83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0544) ID= 1 DT= 5.0 min	Area (ha)= 1.13 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.90	.23	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	50.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	97.10	87.19	
over (min)=	5.00	15.00	
Storage Coeff. (min)=	2.04 (ii)	14.29 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.31	.08	
PEAK FLOW (cms)=	.24	.03	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	.266 (iii)
RUNOFF VOLUME (mm)=	72.06	21.22	6.00
TOTAL RAINFALL (mm)=	73.56	73.56	61.38
			73.56

Hadati Creek Watershed - Post Development with Cityview Ridge
 RUNOFF COEFFICIENT = .98 .29 .83

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| STORE HYD (0525) | AREA (ha)= .00
| ID= 1 DT=****min | QPEAK (cms)= .00
|                   | TPEAK (hrs)= .00
|                   | VOLUME (mm)=*****
-----

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-----
| ADD HYD (0420) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0415):	4.99	1.007	6.00	36.09
+ ID2= 2 (0410):	24.20	3.938	6.00	36.09
<hr/>				
ID = 3 (0420):	29.19	4.945	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| ADD HYD (0465) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0460):	36.00	5.772	6.00	36.09
+ ID2= 2 (0455):	12.70	2.088	6.00	36.09
<hr/>				
ID = 3 (0465):	48.70	7.859	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| ROUTE CHN (0362) |
| IN= 2---> OUT= 1 | Routing time step (min)'= 5.00
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<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
.00           .40           .0300
5.50          .15          .0300 / .0150 Main Channel
5.51          .00           .0150 Main Channel
10.00         .09           .0150 Main Channel
14.49         .00           .0150 Main Channel
14.50         .15          .0150 / .0300 Main Channel
20.00         .40           .0300

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)        (m)        (cu.m.)      (cms)          (m/s)         (min)
.02        .02        .176E+02      .0             .21           80.52

```

Hadati Creek watershed - Post Development with Cityview Ridge

.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0360)	30.00	4.65	6.00	34.40	.31	1.61
OUTFLOW: ID= 1 (0362)	30.00	3.64	6.17	34.39	.27	1.53

ROUTE CHN (0353) |
IN= 2----> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

Hadati Creek Watershed - Post Development with Cityview Ridge

		<---- hydrograph ---->			<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0350)	16.30	2.49	6.00	36.09	.23	1.29
OUTFLOW: ID= 1 (0353)	16.30	1.83	6.17	36.06	.20	1.23

ROUTE CHN (0358)
IN= 2----> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	
5.51	.00	.0150	
10.00	.09	.0150	
14.49	.00	.0150	
14.50	.15	.0150 / .0300	
20.00	.26	.0300	

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

		<---- hydrograph ---->			<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0355)	12.30	2.02	6.00	36.09	.21	1.25
OUTFLOW: ID= 1 (0358)	12.30	1.38	6.17	36.04	.17	1.15

RESERVOIR (0106)
IN= 2----> OUT= 1
DT= 5.0 min

OUTFLOW	STORAGE	OUTFLOW	STORAGE
(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

Hadati Creek watershed - Post Development with Cityview Ridge

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0105)	51.320	8.044	6.00	36.09
OUTFLOW: ID= 1 (0106)	51.320	5.545	6.17	36.09

PEAK FLOW REDUCTION	[Qout/Qin](%)= 68.94
TIME SHIFT OF PEAK FLOW	(min)= 10.00
MAXIMUM STORAGE USED	(ha.m.)= .7419

ADD HYD (0103)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0102):	14.32	2.406	6.00	36.09
+ ID2= 2 (0101):	16.32	2.725	6.00	36.09
=====				
ID = 3 (0103):	30.64	5.131	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0110)	19.000	3.122	6.00	36.09
OUTFLOW: ID= 1 (0111)	19.000	.447	6.58	36.08

PEAK FLOW REDUCTION	[Qout/Qin](%)= 14.31
TIME SHIFT OF PEAK FLOW	(min)= 35.00
MAXIMUM STORAGE USED	(ha.m.)= .4965

ADD HYD (0602)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0600):	11.38	1.732	6.00	36.09
+ ID2= 2 (0601):	7.62	1.186	6.00	36.92
=====				
ID = 3 (0602):	19.00	2.918	6.00	36.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0505)				
Inlet Cap.=9.000				
#of Inlets= 1				
Total(cms)= 9.0				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
TOTAL HYD.(ID= 1):	244.00	27.66	6.17	38.44

Hadati Creek Watershed - Post Development with Cityview Ridge
 MAJOR SYS.(ID= 2): 81.12 18.66 6.17 38.44
 MINOR SYS.(ID= 3): 162.88 9.00 5.92 38.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0505):	162.88	9.000	5.92	38.44
+ ID2= 2 (0510):	16.00	3.209	6.00	61.38
ID = 3 (0515):	178.88	12.209	6.00	40.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0425)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
Inlet Cap.=1.980				
#of Inlets= 1				
Total(cms)= 2.0				
TOTAL HYD.(ID= 1):	29.19	4.94	6.00	36.09
MAJOR SYS.(ID= 2):	7.51	2.96	6.00	36.09
MINOR SYS.(ID= 3):	21.68	1.98	5.83	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0470)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0425):	7.51	2.965	6.00	36.09
+ ID2= 2 (0465):	48.70	7.859	6.00	36.09
ID = 3 (0470):	56.21	10.824	6.00	36.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0359)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0353):	16.30	1.826	6.17	36.06
+ ID2= 2 (0358):	12.30	1.378	6.17	36.04
ID = 3 (0359):	28.60	3.204	6.17	36.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)	OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1				
DT= 5.0 min				

Hadati Creek watershed - Post Development with Cityview Ridge

	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	1.0000	.5000
	.0100	.0100	10.0000	.6000
	.0150	.1332	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	5.131	6.00	36.09
OUTFLOW: ID= 1 (0104)	30.640	4.550	6.17	36.08

PEAK FLOW REDUCTION [Qout/Qin](%)= 88.67
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= .5514

ADD HYD (0114)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0104):	30.64	4.550	6.17	36.08
+ ID2= 2 (0111):	19.00	.447	6.58	36.08
ID = 3 (0114):	49.64	4.877	6.17	36.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0563)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

TRAVEL TIME TABLE

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.745E+01	.0	.64	3.06
.11	.11	.175E+02	.1	.96	2.03
.16	.16	.301E+02	.3	1.21	1.61
.21	.21	.454E+02	.6	1.42	1.37
.26	.26	.632E+02	.9	1.61	1.21
.32	.32	.836E+02	1.3	1.77	1.10
.37	.37	.107E+03	1.8	1.93	1.01
.42	.42	.132E+03	2.3	2.08	.94
.47	.47	.160E+03	3.0	2.22	.88
.53	.53	.191E+03	3.8	2.35	.83
.58	.58	.225E+03	4.8	2.48	.79
.63	.63	.261E+03	5.8	2.60	.75
.68	.68	.299E+03	7.0	2.72	.72
.74	.74	.340E+03	8.2	2.84	.69
.79	.79	.384E+03	9.7	2.95	.66
.84	.84	.430E+03	11.3	3.06	.64
.89	.89	.479E+03	13.0	3.17	.62
.95	.95	.531E+03	14.8	3.27	.60

Hadati Creek watershed - Post Development with Cityview Ridge
 1.00 1.00 .585E+03 16.9 3.38 .58

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0602)	19.00	2.92	6.00	36.42	.46	2.19
OUTFLOW:	ID= 1 (0563)	19.00	2.87	6.08	36.42	.46	2.18

ROUTE CHN (0564)
 IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
.00	101.50	.0500
1.00	100.70	.0500
1.50	100.55	.0500 / .0300
2.00	99.50	.0300
3.50	99.60	.0300
4.50	100.65	.0300 / .0500
6.00	101.45	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0505)	81.12	18.66	6.17	38.44	1.72	1.34
OUTFLOW:	ID= 1 (0564)	81.12	28.30	6.50	38.44	1.95	1.41

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

DUHYD (0520)	AREA	QPEAK	TPEAK	R.V.
Inlet Cap.=3.050	(ha)	(cms)	(hrs)	(mm)
#of Inlets= 1				
Total(cms)= 3.0				

Hadati Creek Watershed - Post Development with Cityview Ridge
TOTAL HYD.(ID= 1): 178.88 12.21 6.00 40.49

MAJOR SYS.(ID= 2): 74.76 9.16 6.00 40.49
MINOR SYS.(ID= 3): 104.13 3.05 5.67 40.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)
IN= 2----> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
Distance Elevation Manning
100.00 324.60 .0500
115.00 321.60 .0500
120.00 320.80 .0500 / .0300 Main Channel
122.00 320.80 .0300 / .0500 Main Channel
138.00 321.60 .0500
148.00 322.30 .0500
154.00 323.10 .0500
164.00 324.60 .0500

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.20 321.00 .398E+03 .8 .84 8.53
.40 321.20 .125E+04 3.3 1.13 6.33
.60 321.40 .255E+04 8.1 1.36 5.27
.80 321.60 .430E+04 15.6 1.56 4.59
1.00 321.80 .644E+04 26.8 1.79 4.01
1.20 322.00 .892E+04 41.2 1.99 3.61
1.40 322.20 .117E+05 59.3 2.17 3.30
1.60 322.40 .148E+05 81.9 2.37 3.02
1.80 322.60 .182E+05 109.1 2.58 2.78
2.00 322.80 .218E+05 140.2 2.77 2.59
2.20 323.00 .256E+05 175.3 2.95 2.43
2.40 323.20 .296E+05 214.7 3.12 2.29
2.60 323.40 .338E+05 258.6 3.29 2.18
2.80 323.60 .382E+05 306.7 3.46 2.07
3.00 323.80 .428E+05 359.1 3.61 1.98
3.20 324.00 .476E+05 416.0 3.76 1.91
3.40 324.20 .526E+05 477.5 3.91 1.83
3.60 324.40 .578E+05 543.5 4.05 1.77
3.80 324.60 .632E+05 614.3 4.18 1.71

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0470) 56.21 10.82 6.00 36.09 .67 1.43
OUTFLOW: ID= 1 (0475) 56.21 9.54 6.08 36.09 .64 1.39

ADD HYD (0363)
1 + 2 = 3
ID1= 1 (0362): 30.00 3.642 6.17 34.39
+ ID2= 2 (0359): 28.60 3.204 6.17 36.05
ID = 3 (0363): 58.60 6.846 6.17 35.20

Hadati Creek watershed - Post Development with Cityview Ridge

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0106):	51.32	5.545	6.17	36.09
+ ID2= 2	(0114):	49.64	4.877	6.17	36.08
ID = 3 (0115):		100.96	10.422	6.17	36.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0563):	19.00	2.866	6.08	36.42
+ ID2= 2	(0607):	5.97	.921	6.08	30.64
ID = 3 (0492):		24.97	3.787	6.08	35.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0526)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0525):	.00	.001	.00	*****
+ ID2= 2	(0520):	74.76	9.159	6.00	40.49
ID = 3 (0526):		74.76	9.159	6.00	40.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0363):	58.60	6.846	6.17	35.20
+ ID2= 2	(0365):	117.50	16.238	6.08	36.09
ID = 3 (0380):		176.10	22.579	6.08	35.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0482)		OUTFLOW		STORAGE	
IN= 2---> OUT= 1		(cms)		(ha.m.)	
DT= 5.0 min					
		.0000	.0000	.2910	.3795
		.2590	.0579	.2970	.4503

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.2660	.1180	1.6320	.5232
.2720	.1802	4.1680	.5983
.2790	.2445	7.5660	.6756
.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	24.970	3.787	6.08	35.04
OUTFLOW: ID= 1 (0482)	24.970	1.351	6.42	35.04

PEAK FLOW REDUCTION [Qout/Qin](%)= 35.67
 TIME SHIFT OF PEAK FLOW (min)= 20.00
 MAXIMUM STORAGE USED (ha.m.)= .5079

ROUTE CHN (0527)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0526)	74.76	9.16	6.00	40.49	2.09	.74
OUTFLOW: ID= 1 (0527)	74.76	7.08	6.17	40.49	2.01	.77

RESERVOIR (0390)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW STORAGE | OUTFLOW STORAGE

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	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	1.3100	1.6000
	.7700	.2870	1.8600	23.2300
	1.2600	.9680	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	22.579	6.08	35.79
OUTFLOW: ID= 1 (0390)	176.100	1.387	7.17	35.79

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.14
TIME SHIFT OF PEAK FLOW (min)= 65.00
MAXIMUM STORAGE USED (ha.m.)= 4.6291

ADD HYD (0400)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0395):	51.20	5.668	6.17	23.89
+ ID2= 2 (0390):	176.10	1.387	7.17	35.79
ID = 3 (0400):	227.30	6.995	6.17	33.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20

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 3.00 338.30 .234E+06 561.0 4.56 6.95

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0400)	227.30	7.00	6.17	33.11	.46	1.36
OUTFLOW: ID= 1 (0403)	227.30	4.32	6.33	33.11	.36	1.16

ADD HYD (0407)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
ID1= 1 (0403):		227.30	4.324	6.33	33.11
+ ID2= 2 (0115):		100.96	10.422	6.17	36.08
ID = 3 (0407):		328.26	13.657	6.17	34.03

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0113)		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1					
DT= 5.0 min		.0000	.0000	1.6000	6.4000
		1.1000	2.9000	9.1000	10.0000
		1.3000	4.3000	12.0000	20.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	13.657	6.17	34.03
OUTFLOW: ID= 1 (0113)	328.260	1.367	15.17	34.02

PEAK FLOW REDUCTION [Qout/Qin] (%) = 10.01
 TIME SHIFT OF PEAK FLOW (min) = 540.00
 MAXIMUM STORAGE USED (ha.m.) = 4.7719

ADD HYD (0430)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
ID1= 1 (0113):		328.26	1.367	15.17	34.02
+ ID2= 2 (0425):		21.68	1.980	5.83	36.09
ID = 3 (0430):		349.94	2.494	6.25	34.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)		Routing time step (min)'= 5.00	
IN= 2---> OUT= 1			

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	325.40	.0600
120.00	324.60	.0600

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126.00	323.90	.0600	
130.00	323.00	.0600	
140.00	322.30	.0600 / .0300	Main Channel
142.00	322.30	.0300 / .0600	Main Channel
150.00	323.90	.0600	
155.00	324.60	.0600	
160.00	325.40	.0600	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

			<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0430)	AREA (ha)	2.49	6.25	34.15	.35	1.29
OUTFLOW:	ID= 1 (0440)	349.94	2.40	6.33	34.15	.34	1.28

ADD HYD (0485)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0475):	56.21	9.543	6.08	36.09
+ ID2= 2 (0440):	349.94	2.403	6.33	34.15
=====				
ID = 3 (0485):	406.15	11.718	6.08	34.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0480):	43.10	6.559	6.00	36.09
+ ID2= 2 (0485):	406.15	11.718	6.08	34.42
=====				
ID = 3 (0490):	449.25	17.844	6.08	34.58

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0491)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0490):	449.25	17.844	6.08	34.58	
+ ID2= 2 (0482):	24.97	1.351	6.42	35.04	
ID = 3 (0491):	474.22	18.128	6.08	34.60	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)					
IN= 2---> OUT= 1					
DT= 5.0 min					
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)	
	.0000	.0000	7.0800	2.4860	
	.2760	.0600	8.1000	3.3240	
	1.2000	.3400	9.7980	4.6420	
	2.0400	.6182	10.4940	7.4397	
	2.6400	1.1630	11.6850	10.3000	
	3.1200	1.7070	12.3480	11.4000	

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
INFLOW : ID= 2 (0491)	474.220	18.128	6.08	34.60	
OUTFLOW: ID= 1 (0483)	474.220	6.839	6.50	34.60	

PEAK FLOW REDUCTION [Qout/Qin](%)= 37.72
 TIME SHIFT OF PEAK FLOW (min)= 25.00
 MAXIMUM STORAGE USED (ha.m.)= 2.4478

ADD HYD (0530)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0483):	474.22	6.839	6.50	34.60	
+ ID2= 2 (0540):	4.63	1.036	6.00	61.38	
ID = 3 (0530):	478.85	7.014	6.50	34.86	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0530):	478.85	7.014	6.50	34.86	
+ ID2= 2 (0527):	74.76	7.076	6.17	40.49	
ID = 3 (0545):	553.61	13.871	6.50	35.62	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0546)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0545):	553.61	13.871	6.50	35.62
+ ID2= 2	(0542):	25.25	5.333	6.00	61.38
ID = 3 (0546):		578.86	14.994	6.00	36.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0546):	578.86	14.994	6.00	36.75
+ ID2= 2	(0543):	14.99	3.310	6.00	61.38
ID = 3 (0547):		593.85	18.304	6.00	37.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0547):	593.85	18.304	6.00	37.37
+ ID2= 2	(0544):	1.13	.266	6.00	61.38
ID = 3 (0548):		594.98	18.570	6.00	37.41

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 ** SIMULATION NUMBER: 4 **

READ STORM	Filename: Y:\SPrimmer\OTTHYMO\Ci
Ptotal= 90.18 mm	tyview Ridge\100yrSCS12hr.stm
	Comments: 100 year SCS Type II 12hr design storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	2.26	3.25	3.61	6.25	16.23	9.25	3.16
.50	2.26	3.50	3.61	6.50	16.23	9.50	3.16
.75	2.26	3.75	3.61	6.75	7.21	9.75	3.16
1.00	2.26	4.00	3.61	7.00	7.21	10.00	3.16
1.25	2.26	4.25	5.41	7.25	5.41	10.25	1.80
1.50	2.26	4.50	5.41	7.50	5.41	10.50	1.80
1.75	2.26	4.75	7.21	7.75	5.41	10.75	1.80
2.00	2.26	5.00	7.21	8.00	5.41	11.00	1.80
2.25	2.70	5.25	10.82	8.25	3.16	11.25	1.80
2.50	2.70	5.50	10.82	8.50	3.16	11.50	1.80
2.75	2.70	5.75	43.29	8.75	3.16	11.75	1.80
3.00	2.70	6.00	119.04	9.00	3.16	12.00	1.80

Hadati Creek watershed - Post Development with Cityview Ridge

CALIB					
STANDHYD (0480)		Area (ha)=	43.10		
ID= 1 DT= 5.0 min		Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	2.26	3.083	3.61	6.083	16.23	9.08	3.16
.167	2.26	3.167	3.61	6.167	16.23	9.17	3.16
.250	2.26	3.250	3.61	6.250	16.23	9.25	3.16
.333	2.26	3.333	3.61	6.333	16.23	9.33	3.16
.417	2.26	3.417	3.61	6.417	16.23	9.42	3.16
.500	2.26	3.500	3.61	6.500	16.23	9.50	3.16
.583	2.26	3.583	3.61	6.583	7.21	9.58	3.16
.667	2.26	3.667	3.61	6.667	7.21	9.67	3.16
.750	2.26	3.750	3.61	6.750	7.21	9.75	3.16
.833	2.26	3.833	3.61	6.833	7.21	9.83	3.16
.917	2.26	3.917	3.61	6.917	7.21	9.92	3.16
1.000	2.26	4.000	3.61	7.000	7.21	10.00	3.16
1.083	2.26	4.083	5.41	7.083	5.41	10.08	1.80
1.167	2.26	4.167	5.41	7.167	5.41	10.17	1.80
1.250	2.26	4.250	5.41	7.250	5.41	10.25	1.80
1.333	2.26	4.333	5.41	7.333	5.41	10.33	1.80
1.417	2.26	4.417	5.41	7.417	5.41	10.42	1.80
1.500	2.26	4.500	5.41	7.500	5.41	10.50	1.80
1.583	2.26	4.583	7.21	7.583	5.41	10.58	1.80
1.667	2.26	4.667	7.21	7.667	5.41	10.67	1.80
1.750	2.26	4.750	7.21	7.750	5.41	10.75	1.80
1.833	2.26	4.833	7.21	7.833	5.41	10.83	1.80
1.917	2.26	4.917	7.21	7.917	5.41	10.92	1.80
2.000	2.26	5.000	7.21	8.000	5.41	11.00	1.80
2.083	2.70	5.083	10.82	8.083	3.16	11.08	1.80
2.167	2.70	5.167	10.82	8.167	3.16	11.17	1.80
2.250	2.70	5.250	10.82	8.250	3.16	11.25	1.80
2.333	2.70	5.333	10.82	8.333	3.16	11.33	1.80
2.417	2.70	5.417	10.82	8.417	3.16	11.42	1.80
2.500	2.70	5.500	10.82	8.500	3.16	11.50	1.80
2.583	2.70	5.583	43.29	8.583	3.16	11.58	1.80
2.667	2.70	5.667	43.29	8.667	3.16	11.67	1.80
2.750	2.70	5.750	43.29	8.750	3.16	11.75	1.80
2.833	2.70	5.833	119.04	8.833	3.16	11.83	1.80
2.917	2.70	5.917	119.04	8.917	3.16	11.92	1.80
3.000	2.70	6.000	119.04	9.000	3.16	12.00	1.80

Max.Eff.Inten.(mm/hr)=	119.04	149.56
over (min)	5.00	15.00
Storage Coeff. (min)=	6.11 (ii)	12.82 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.19	.08

Hadati Creek watershed - Post Development with Cityview Ridge

PEAK FLOW	(cms)=	2.82	6.56	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	8.721 (iii)
RUNOFF VOLUME	(mm)=	88.68	36.13	6.00
TOTAL RAINFALL	(mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT	=	.98	.40	90.18
				.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0415)	Area (ha)=	4.99	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.10	2.89	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.86	2.86	
Length	(m)=	185.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.51 (ii)	8.54 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		.29	.12	
				TOTALS
PEAK FLOW	(cms)=	.35	.96	1.304 (iii)
TIME TO PEAK	(hrs)=	6.00	6.00	6.00
RUNOFF VOLUME	(mm)=	88.68	36.13	47.17
TOTAL RAINFALL	(mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT	=	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0410)	Area (ha)=	24.20	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	10.16	14.04
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	401.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		119.04	149.56

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over (min)	5.00	15.00	
Storage Coeff. (min)=	4.45 (ii)	11.16 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.23	.09	
			TOTALS
PEAK FLOW (cms)=	1.64	3.90	5.204 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	36.13	47.17
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0460)	Area (ha)= 36.00		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	15.12	20.88	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.03	2.03	
Length (m)=	465.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.84 (ii)	11.52 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.09	
			TOTALS
PEAK FLOW (cms)=	2.43	5.73	7.639 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	36.13	47.17
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0455)	Area (ha)= 12.70		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.33	7.37	
Dep. Storage (mm)=	1.50	5.00	

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Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.92 (ii)	10.95 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.24	.09	
PEAK FLOW (cms)=		.87	2.06	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	2.756 (iii)
RUNOFF VOLUME (mm)=		88.68	36.13	6.00
TOTAL RAINFALL (mm)=		90.18	90.18	47.17
RUNOFF COEFFICIENT	=	.98	.40	90.18
				.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0395)	Area (ha)=	51.20	
ID= 1 DT= 5.0 min	Total Imp(%)=	10.00	Dir. Conn.(%)= 5.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.12	46.08	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	900.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	112.64	
over (min)		5.00	15.00	
Storage Coeff. (min)=		7.23 (ii)	14.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.17	.08	
PEAK FLOW (cms)=		.78	8.19	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	8.631 (iii)
RUNOFF VOLUME (mm)=		88.68	31.49	6.08
TOTAL RAINFALL (mm)=		90.18	90.18	34.35
RUNOFF COEFFICIENT	=	.98	.35	90.18
				.38

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB

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STANDHYD (0360)	Area (ha)= 30.00
ID= 1 DT= 5.0 min	Total Imp(%)= 37.00 Dir. Conn.(%)= 19.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.10	18.90	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	447.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	140.44	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.75 (ii)	11.63 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.09	
PEAK FLOW (cms)=	1.83	4.81	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	6.183 (iii)
RUNOFF VOLUME (mm)=	88.68	35.04	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	45.23
RUNOFF COEFFICIENT =	.98	.39	90.18
			.50

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 ***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0350)	Area (ha)= 16.30
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.45	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.00	1.00	
Length (m)=	330.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	4.88 (ii)	13.13 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.22	.08	
PEAK FLOW (cms)=	1.10	2.45	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	3.299 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- Hadati Creek Watershed - Post Development with Cityview Ridge
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0355)
ID= 1 DT= 5.0 min

Area (ha)= 12.30
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.89 (ii)	11.05 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.09	
PEAK FLOW (cms)=		.84	1.99	*TOTALS* 2.661 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		88.68	36.13	47.17
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0365)
ID= 1 DT= 5.0 min

Area (ha)= 117.50
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		7.16 (ii)	13.86 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.17	.08	
PEAK FLOW (cms)=		7.49	17.25	*TOTALS* 22.881 (iii)
TIME TO PEAK (hrs)=		6.00	6.08	6.00
RUNOFF VOLUME (mm)=		88.68	36.13	47.17
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.40	.52

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- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0105) ID= 1 DT= 5.0 min	Area (ha)= 51.32 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	21.55	29.77	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	550.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.38 (ii)	12.09 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.21	.09	
PEAK FLOW (cms)=	3.42	8.01	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	10.668 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
TOTAL RAINFALL (mm)=	90.18	90.18	47.17
RUNOFF COEFFICIENT =	.98	.40	90.18
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0102) ID= 1 DT= 5.0 min	Area (ha)= 14.32 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.01	8.31	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	287.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	149.56	
over (min)	5.00	15.00	
Storage Coeff. (min)=	3.64 (ii)	10.35 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.25	.09	
PEAK FLOW (cms)=	.98	2.37	*TOTALS*
TIME TO PEAK (hrs)=	6.00	6.08	3.171 (iii)
RUNOFF VOLUME (mm)=	88.68	36.13	6.00
			47.17

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TOTAL RAINFALL (mm)= 90.18 90.18 90.18
RUNOFF COEFFICIENT = .98 .40 .52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0101)
ID= 1 DT= 5.0 min
Area (ha)= 16.32
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.47	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	309.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.81 (ii)	10.51 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.09	
PEAK FLOW (cms)=		1.12	2.69	*TOTALS*
TIME TO PEAK (hrs)=		6.00	6.08	3.593 (iii)
RUNOFF VOLUME (mm)=		88.68	36.13	6.00
TOTAL RAINFALL (mm)=		90.18	90.18	47.17
RUNOFF COEFFICIENT =		.98	.40	90.18
				.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0110)
ID= 1 DT= 5.0 min
Area (ha)= 19.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	7.98	11.02	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	365.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	149.56	
over (min)		5.00	15.00	
Storage Coeff. (min)=		4.21 (ii)	10.91 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	

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Unit Hyd. peak (cms)= .24 .09

				TOTALS
PEAK FLOW	(cms)=	1.30	3.09	4.123 (iii)
TIME TO PEAK	(hrs)=	6.00	6.08	6.00
RUNOFF VOLUME	(mm)=	88.68	36.13	47.17
TOTAL RAINFALL	(mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT	=	.98	.40	.52

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0600) ID= 1 DT= 5.0 min	Area (ha)= 11.38 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
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		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	4.78	6.60
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

Max.Eff.Inten.(mm/hr)=	119.04	149.56
over (min)	5.00	15.00
Storage Coeff. (min)=	6.11 (ii)	12.82 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.19	.08

			TOTALS
PEAK FLOW	(cms)=	.75	1.73
TIME TO PEAK	(hrs)=	6.00	6.08
RUNOFF VOLUME	(mm)=	88.68	36.13
TOTAL RAINFALL	(mm)=	90.18	90.18
RUNOFF COEFFICIENT	=	.98	.40
			.52

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0601) ID= 1 DT= 5.0 min	Area (ha)= 7.62 Total Imp(%)= 46.00 Dir. Conn.(%)= 21.00
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		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	3.51	4.11
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

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Max.Eff.Inten.(mm/hr)=	119.04	161.60	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.11 (ii)	12.61 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.08	
			TOTALS
PEAK FLOW (cms)=	.50	1.19	1.576 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	37.55	48.29
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.42	.54

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0607)	Area (ha)= 5.97		
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00	Dir. Conn.(%)= 2.50	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.51	3.46	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	680.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	187.59	
over (min)	5.00	15.00	
Storage Coeff. (min)=	6.11 (ii)	12.24 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.19	.09	
			TOTALS
PEAK FLOW (cms)=	.05	1.19	1.215 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.08
RUNOFF VOLUME (mm)=	88.68	39.89	41.11
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.44	.46

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0540)	Area (ha)= 4.63		
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00	

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	3.70	.93

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Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	150.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	111.85	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.64 (ii)	14.73 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.25	.08	
PEAK FLOW	(cms)=	1.20	.16	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.08	1.339 (iii)
RUNOFF VOLUME	(mm)=	88.68	31.37	6.00
TOTAL RAINFALL	(mm)=	90.18	90.18	76.65
RUNOFF COEFFICIENT	=	.98	.35	90.18
				.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0500)	Area	(ha)= 244.00	
ID= 1 DT= 5.0 min	Total Imp(%)=	46.00	Dir. Conn.(%)= 26.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	112.24	131.76	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.80	.80	
Length	(m)=	1275.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	150.55	
over (min)		10.00	25.00	
Storage Coeff. (min)=		11.73 (ii)	20.53 (ii)	
Unit Hyd. Tpeak (min)=		10.00	25.00	
Unit Hyd. peak (cms)=		.10	.05	
PEAK FLOW	(cms)=	15.54	24.76	*TOTALS*
TIME TO PEAK	(hrs)=	6.00	6.25	34.262 (iii)
RUNOFF VOLUME	(mm)=	88.68	36.25	6.17
TOTAL RAINFALL	(mm)=	90.18	90.18	49.88
RUNOFF COEFFICIENT	=	.98	.40	90.18
				.55

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		
STANDHYD (0510)	Area	(ha)= 16.00

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 ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	12.80	3.20	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.50	.20	
Length	(m)=	400.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	91.82	
over (min)		5.00	25.00	
Storage Coeff. (min)=		6.74 (ii)	22.99 (ii)	
Unit Hyd. Tpeak (min)=		5.00	25.00	
Unit Hyd. peak (cms)=		.18	.05	
				TOTALS
PEAK FLOW (cms)=		3.88	.40	4.080 (iii)
TIME TO PEAK (hrs)=		6.00	6.25	6.00
RUNOFF VOLUME (mm)=		88.68	31.37	76.65
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.35	.85

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
 STANDHYD (0542)
 ID= 1 DT= 5.0 min | Area (ha)= 25.25
 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	20.20	5.05	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	.55	.55	
Length	(m)=	350.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		119.04	111.85	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.05 (ii)	17.13 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.19	.06	
				TOTALS
PEAK FLOW (cms)=		6.23	.77	6.749 (iii)
TIME TO PEAK (hrs)=		6.00	6.17	6.00
RUNOFF VOLUME (mm)=		88.68	31.37	76.65
TOTAL RAINFALL (mm)=		90.18	90.18	90.18
RUNOFF COEFFICIENT =		.98	.35	.85

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0543)
ID= 1 DT= 5.0 min

Area (ha)= 14.99
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	11.99	3.00	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	200.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	111.85	
over (min)	5.00	20.00	
Storage Coeff. (min)=	4.32 (ii)	15.41 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.23	.07	
			TOTALS
PEAK FLOW (cms)=	3.84	.48	4.164 (iii)
TIME TO PEAK (hrs)=	6.00	6.17	6.00
RUNOFF VOLUME (mm)=	88.68	31.37	76.65
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.35	.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0544)
ID= 1 DT= 5.0 min

Area (ha)= 1.13
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.90	.23	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	50.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	119.04	111.85	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.88 (ii)	12.97 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.32	.08	
			TOTALS
PEAK FLOW (cms)=	.30	.04	.333 (iii)
TIME TO PEAK (hrs)=	6.00	6.08	6.00
RUNOFF VOLUME (mm)=	88.68	31.37	76.65
TOTAL RAINFALL (mm)=	90.18	90.18	90.18
RUNOFF COEFFICIENT =	.98	.35	.85

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

- Hadati Creek watershed - Post Development with Cityview Ridge
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| STORE HYD (0525) | AREA      (ha)= .00
| ID= 1 DT=****min | QPEAK    (cms)= .00
-----
|                   | TPEAK    (hrs)= .00
|                   | VOLUME   (mm)=*****
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-----
| ADD HYD   (0420) |
| 1 + 2 = 3       |
-----
| ID1= 1 (0415):   | AREA      (ha)   QPEAK  (cms)  TPEAK  (hrs)  R.V.  (mm)
| + ID2= 2 (0410): | 4.99      1.304   6.00   47.17
|                   | 24.20     5.204   6.00   47.17
|                   |-----|
| ID = 3 (0420):   | 29.19     6.509   6.00   47.17
|                   |-----|

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| ADD HYD   (0465) |
| 1 + 2 = 3       |
-----
| ID1= 1 (0460):   | AREA      (ha)   QPEAK  (cms)  TPEAK  (hrs)  R.V.  (mm)
| + ID2= 2 (0455): | 36.00     7.639   6.00   47.17
|                   | 12.70     2.756   6.00   47.17
|                   |-----|
| ID = 3 (0465):   | 48.70    10.395   6.00   47.17
|                   |-----|

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| ROUTE CHN (0362) |
| IN= 2----> OUT= 1 | Routing time step (min)'= 5.00
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<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
   .00         .40         .0300
   5.50        .15         .0300 / .0150 Main Channel
   5.51        .00         .0150 Main Channel
  10.00        .09         .0150 Main Channel
  14.49        .00         .0150 Main Channel
  14.50        .15         .0150 / .0300 Main Channel
  20.00        .40         .0300

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<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)         (m)      (cu.m.)      (cms)          (m/s)         (min)
.02         .02      .176E+02      .0             .21           80.52
.04         .04      .702E+02      .0             .33           50.72
.06         .06      .158E+03      .1             .43           38.71
.08         .08      .281E+03      .1             .52           31.95
.09         .09      .438E+03      .3             .62           26.84
.11         .11      .607E+03      .5             .77           21.66
.13         .13      .776E+03      .7             .90           18.45
.15         .15      .944E+03      1.0           1.03           16.22

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.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0360)	30.00	6.18	6.00	45.23	.35	1.71
OUTFLOW:	ID= 1 (0362)	30.00	4.88	6.17	45.22	.31	1.63

ROUTE CHN (0353)
IN= 2----> OUT= 1 | Routing time step (min)'= 5.00

Distance	Elevation	Manning	
.00	.26	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.26	.0300	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.929E+01	.0	.17	99.56
.03	.03	.372E+02	.0	.27	62.72
.04	.04	.836E+02	.0	.35	47.86
.05	.05	.149E+03	.1	.42	39.51
.07	.07	.232E+03	.1	.49	34.05
.08	.08	.334E+03	.2	.55	30.15
.10	.10	.454E+03	.3	.64	26.24
.11	.11	.576E+03	.4	.74	22.41
.12	.12	.699E+03	.6	.84	19.75
.14	.14	.822E+03	.8	.94	17.76
.15	.15	.944E+03	1.0	1.03	16.22
.16	.16	.108E+04	1.2	1.11	15.07
.18	.18	.123E+04	1.4	1.17	14.28
.19	.19	.140E+04	1.7	1.21	13.72
.20	.20	.159E+04	2.0	1.25	13.31
.22	.22	.180E+04	2.3	1.28	13.01
.23	.23	.203E+04	2.6	1.31	12.76
.25	.25	.227E+04	3.0	1.33	12.57
.26	.26	.254E+04	3.4	1.34	12.41

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0350)	16.30	3.30	6.00	47.17	.26	1.34
OUTFLOW:	ID= 1 (0353)	16.30	2.44	6.17	47.13	.22	1.29

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ROUTE CHN (0358)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .01 .01 .102E+02 .0 .17 109.52
 .03 .03 .409E+02 .0 .27 68.99
 .04 .04 .920E+02 .0 .35 52.65
 .05 .05 .163E+03 .1 .42 43.46
 .07 .07 .255E+03 .1 .49 37.45
 .08 .08 .368E+03 .2 .55 33.17
 .10 .10 .499E+03 .3 .64 28.86
 .11 .11 .634E+03 .4 .74 24.66
 .12 .12 .769E+03 .6 .84 21.72
 .14 .14 .904E+03 .8 .94 19.54
 .15 .15 .104E+04 1.0 1.03 17.84
 .16 .16 .119E+04 1.2 1.11 16.57
 .18 .18 .135E+04 1.4 1.17 15.71
 .19 .19 .154E+04 1.7 1.21 15.10
 .20 .20 .175E+04 2.0 1.25 14.65
 .22 .22 .198E+04 2.3 1.28 14.31
 .23 .23 .223E+04 2.6 1.31 14.04
 .25 .25 .250E+04 3.0 1.33 13.82
 .26 .26 .279E+04 3.4 1.34 13.65

<----- hydrograph -----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0355) 12.30 2.66 6.00 47.17 .23 1.31
 OUTFLOW: ID= 1 (0358) 12.30 1.86 6.17 47.12 .20 1.23

RESERVOIR (0106)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	10.668	6.00	47.17
OUTFLOW: ID= 1 (0106)	51.320	7.689	6.17	47.16

PEAK FLOW REDUCTION [Qout/Qin](%)= 72.08
 TIME SHIFT OF PEAK FLOW (min)= 10.00

Hadati Creek Watershed - Post Development with Cityview Ridge
 MAXIMUM STORAGE USED (ha.m.)= .8782

ADD HYD (0103)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):	14.32	3.171	6.00	47.17
+ ID2= 2 (0101):	16.32	3.593	6.00	47.17
ID = 3 (0103):	30.64	6.763	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0111)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	1.0000	1.0000
	.0100	.0100	20.0000	1.1000
	.0120	.1000	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	4.123	6.00	47.17
OUTFLOW: ID= 1 (0111)	19.000	.613	6.58	47.16

PEAK FLOW REDUCTION [Qout/Qin] (%)= 14.87
 TIME SHIFT OF PEAK FLOW (min)= 35.00
 MAXIMUM STORAGE USED (ha.m.)= .6478

ADD HYD (0602)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0600):	11.38	2.303	6.00	47.17
+ ID2= 2 (0601):	7.62	1.576	6.00	48.29
ID = 3 (0602):	19.00	3.878	6.00	47.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0505)				
Inlet Cap.=9.000				
#of Inlets= 1				
Total(cms)= 9.0				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	34.26	6.17	49.88
MAJOR SYS.(ID= 2):	102.03	25.26	6.17	49.88
MINOR SYS.(ID= 3):	141.97	9.00	5.83	49.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ADD HYD (0515)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0505):	141.97	9.000	5.83	49.88
+ ID2= 2 (0510):	16.00	4.080	6.00	76.65
=====				
ID = 3 (0515):	157.97	13.080	6.00	52.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0425)				
Inlet Cap.=1.980				
#of Inlets= 1				
Total(cms)= 2.0				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
TOTAL HYD.(ID= 1):	29.19	6.51	6.00	47.17
=====				
MAJOR SYS.(ID= 2):	10.15	4.53	6.00	47.17
MINOR SYS.(ID= 3):	19.04	1.98	5.83	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0470)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0425):	10.15	4.529	6.00	47.17
+ ID2= 2 (0465):	48.70	10.395	6.00	47.17
=====				
ID = 3 (0470):	58.85	14.924	6.00	47.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0359)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0353):	16.30	2.435	6.17	47.13
+ ID2= 2 (0358):	12.30	1.856	6.17	47.12
=====				
ID = 3 (0359):	28.60	4.291	6.17	47.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	.0000	.0000	1.0000	.5000
	.0100	.0100	10.0000	.6000
	.0150	.1332	.0000	.0000
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)

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 INFLOW : ID= 2 (0103) 30.640 6.763 6.00 47.17
 OUTFLOW: ID= 1 (0104) 30.640 7.048 6.08 47.16

PEAK FLOW REDUCTION [Qout/Qin] (%)=104.21
 TIME SHIFT OF PEAK FLOW (min)= 5.00
 MAXIMUM STORAGE USED (ha.m.)= .5855

**** WARNING : HYDROGRAPH PEAK WAS NOT REDUCED.
 CHECK OUTFLOW/STORAGE TABLE OR REDUCE DT.

ADD HYD	(0114)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0104):		30.64	7.048	6.08	47.16
+ ID2= 2 (0111):		19.00	.613	6.58	47.16
ID = 3 (0114):		49.64	7.421	6.08	47.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN	(0563)	Routing time step (min)'	= 5.00
IN= 2--->	OUT= 1		

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.05	.05	.745E+01	.0	.64	3.06
.11	.11	.175E+02	.1	.96	2.03
.16	.16	.301E+02	.3	1.21	1.61
.21	.21	.454E+02	.6	1.42	1.37
.26	.26	.632E+02	.9	1.61	1.21
.32	.32	.836E+02	1.3	1.77	1.10
.37	.37	.107E+03	1.8	1.93	1.01
.42	.42	.132E+03	2.3	2.08	.94
.47	.47	.160E+03	3.0	2.22	.88
.53	.53	.191E+03	3.8	2.35	.83
.58	.58	.225E+03	4.8	2.48	.79
.63	.63	.261E+03	5.8	2.60	.75
.68	.68	.299E+03	7.0	2.72	.72
.74	.74	.340E+03	8.2	2.84	.69
.79	.79	.384E+03	9.7	2.95	.66
.84	.84	.430E+03	11.3	3.06	.64
.89	.89	.479E+03	13.0	3.17	.62
.95	.95	.531E+03	14.8	3.27	.60
1.00	1.00	.585E+03	16.9	3.38	.58

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)

Hadati Creek watershed - Post Development with Cityview Ridge
 INFLOW : ID= 2 (0602) 19.00 3.88 6.00 47.62 .53 2.35
 OUTFLOW: ID= 1 (0563) 19.00 3.76 6.08 47.62 .52 2.33

ROUTE CHN (0564)
 IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 101.50 .0500
 1.00 100.70 .0500
 1.50 100.55 .0500 / .0300 Main Channel
 2.00 99.50 .0300 Main Channel
 3.50 99.60 .0300 Main Channel
 4.50 100.65 .0300 / .0500 Main Channel
 6.00 101.45 .0500

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<--pipe / channel--> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0505)	102.03	25.26	6.17	49.88	1.80	1.37
OUTFLOW: ID= 1 (0564)	102.03	39.67	6.58	49.88	1.95	1.41

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

DUHYD (0520)
 Inlet Cap.=3.050
 #of Inlets= 1
 Total(cms)= 3.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	157.97	13.08	6.00	52.60
MAJOR SYS.(ID= 2):	67.54	10.03	6.00	52.60
MINOR SYS.(ID= 3):	90.43	3.05	5.58	52.60

Hadati Creek Watershed - Post Development with Cityview Ridge
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 100.00 324.60 .0500
 115.00 321.60 .0500
 120.00 320.80 .0500 / .0300 Main Channel
 122.00 320.80 .0300 / .0500 Main Channel
 138.00 321.60 .0500
 148.00 322.30 .0500
 154.00 323.10 .0500
 164.00 324.60 .0500

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .20 321.00 .398E+03 .8 .84 8.53
 .40 321.20 .125E+04 3.3 1.13 6.33
 .60 321.40 .255E+04 8.1 1.36 5.27
 .80 321.60 .430E+04 15.6 1.56 4.59
 1.00 321.80 .644E+04 26.8 1.79 4.01
 1.20 322.00 .892E+04 41.2 1.99 3.61
 1.40 322.20 .117E+05 59.3 2.17 3.30
 1.60 322.40 .148E+05 81.9 2.37 3.02
 1.80 322.60 .182E+05 109.1 2.58 2.78
 2.00 322.80 .218E+05 140.2 2.77 2.59
 2.20 323.00 .256E+05 175.3 2.95 2.43
 2.40 323.20 .296E+05 214.7 3.12 2.29
 2.60 323.40 .338E+05 258.6 3.29 2.18
 2.80 323.60 .382E+05 306.7 3.46 2.07
 3.00 323.80 .428E+05 359.1 3.61 1.98
 3.20 324.00 .476E+05 416.0 3.76 1.91
 3.40 324.20 .526E+05 477.5 3.91 1.83
 3.60 324.40 .578E+05 543.5 4.05 1.77
 3.80 324.60 .632E+05 614.3 4.18 1.71

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0470) 58.85 14.92 6.00 47.17 .78 1.54
 OUTFLOW: ID= 1 (0475) 58.85 13.38 6.08 47.17 .74 1.49

ADD HYD (0363)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0362):	30.00	4.880	6.17	45.22
+ ID2= 2 (0359):	28.60	4.291	6.17	47.13
ID = 3 (0363):	58.60	9.171	6.17	46.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek Watershed - Post Development with Cityview Ridge

ADD HYD (0115)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0106):	51.32	7.689	6.17	47.16
+ ID2= 2	(0114):	49.64	7.421	6.08	47.16
ID = 3 (0115):		100.96	14.393	6.08	47.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0563):	19.00	3.758	6.08	47.62
+ ID2= 2	(0607):	5.97	1.215	6.08	41.11
ID = 3 (0492):		24.97	4.973	6.08	46.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0526)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0525):	.00	.001	.00	*****
+ ID2= 2	(0520):	67.54	10.030	6.00	52.60
ID = 3 (0526):		67.54	10.030	6.00	52.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1	(0363):	58.60	9.171	6.17	46.15
+ ID2= 2	(0365):	117.50	22.881	6.00	47.17
ID = 3 (0380):		176.10	30.231	6.08	46.83

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0482)		OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 1		(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min					
		.0000	.0000	.2910	.3795
		.2590	.0579	.2970	.4503
		.2660	.1180	1.6320	.5232
		.2720	.1802	4.1680	.5983
		.2790	.2445	7.5660	.6756
		.2850	.3109	.0000	.0000

Hadati Creek Watershed - Post Development with Cityview Ridge

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0492)	24.970	4.973	6.08	46.06
OUTFLOW: ID= 1 (0482)	24.970	3.025	6.25	46.06

PEAK FLOW REDUCTION [Qout/Qin](%)= 60.83
 TIME SHIFT OF PEAK FLOW (min)= 10.00
 MAXIMUM STORAGE USED (ha.m.)= .5657

ROUTE CHN (0527)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel
141.50	310.80	.0300	Main Channel
142.00	312.40	.0300 / .0500	Main Channel
160.00	313.20	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

<---- hydrograph ---->

	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0526)	67.54	10.03	6.00	52.60	2.13	.74
OUTFLOW: ID= 1 (0527)	67.54	7.92	6.08	52.59	2.04	.76

RESERVOIR (0390)
 IN= 2---> OUT= 1
 DT= 5.0 min

OUTFLOW	STORAGE	OUTFLOW	STORAGE
(cms)	(ha.m.)	(cms)	(ha.m.)
.0000	.0000	1.3100	1.6000
.7700	.2870	1.8600	23.2300
1.2600	.9680	.0000	.0000

Hadati Creek Watershed - Post Development with Cityview Ridge

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0380)	176.100	30.231	6.08	46.83
OUTFLOW: ID= 1 (0390)	176.100	1.430	7.25	46.83

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.73
 TIME SHIFT OF PEAK FLOW (min)= 70.00
 MAXIMUM STORAGE USED (ha.m.)= 6.3304

ADD HYD (0400)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0395):	51.20	8.631	6.08	34.35
+ ID2= 2 (0390):	176.10	1.430	7.25	46.83
ID = 3 (0400):	227.30	9.969	6.08	44.02

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)	
IN= 2---> OUT= 1	Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	338.30	.0500
110.00	336.80	.0500
135.00	336.00	.0300
142.00	335.30	.0500
148.00	335.30	.0500
156.00	336.00	.0500
165.00	338.30	.0000

Main Channel

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

<---- hydrograph ---->				<-pipe / channel->	
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)

Hadati Creek Watershed - Post Development with Cityview Ridge
 INFLOW : ID= 2 (0400) 227.30 9.97 6.08 44.02 .54 1.50
 OUTFLOW: ID= 1 (0403) 227.30 6.22 6.25 44.02 .43 1.29

```

-----
| ADD HYD (0407) |
| 1 + 2 = 3 |
-----
                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
  ID1= 1 (0403): 227.30 6.216 6.25 44.02
+ ID2= 2 (0115): 100.96 14.393 6.08 47.16
=====
  ID = 3 (0407): 328.26 18.926 6.17 44.98
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR (0113) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
                OUTFLOW      STORAGE      OUTFLOW      STORAGE
                (cms)      (ha.m.)      (cms)      (ha.m.)
                .0000      .0000      1.6000      6.4000
                1.1000      2.9000      9.1000      10.0000
                1.3000      4.3000      12.0000      20.0000
  
```

```

                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
  INFLOW : ID= 2 (0407) 328.260 18.926 6.17 44.98
  OUTFLOW: ID= 1 (0113) 328.260 1.552 12.50 44.98
  
```

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.20
 TIME SHIFT OF PEAK FLOW (min)=380.00
 MAXIMUM STORAGE USED (ha.m.)= 6.0640

```

-----
| ADD HYD (0430) |
| 1 + 2 = 3 |
-----
                AREA      QPEAK      TPEAK      R.V.
                (ha)      (cms)      (hrs)      (mm)
  ID1= 1 (0113): 328.26 1.552 12.50 44.98
+ ID2= 2 (0425): 19.04 1.980 5.83 47.17
=====
  ID = 3 (0430): 347.30 3.000 6.33 45.10
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ROUTE CHN (0440) |
| IN= 2---> OUT= 1 |
-----
Routing time step (min)'= 5.00
  
```

```

<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
100.00      325.40      .0600
120.00      324.60      .0600
126.00      323.90      .0600
130.00      323.00      .0600
140.00      322.30      .0600 / .0300 Main Channel
142.00      322.30      .0300 / .0600 Main Channel
150.00      323.90      .0600
  
```

Hadati Creek Watershed - Post Development with Cityview Ridge

155.00 324.60 .0600
160.00 325.40 .0600

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18
2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

		<---- hydrograph ---->			<-pipe / channel->		
		AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0430)	347.30	3.00	6.33	45.10	.38	1.33
OUTFLOW:	ID= 1 (0440)	347.30	2.86	6.42	45.10	.37	1.31

ADD HYD (0485)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0475):	58.85	13.381	6.08	47.17	
+ ID2= 2 (0440):	347.30	2.860	6.42	45.10	
=====					
ID = 3 (0485):	406.15	15.674	6.08	45.40	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0480):	43.10	8.721	6.00	47.17	
+ ID2= 2 (0485):	406.15	15.674	6.08	45.40	
=====					
ID = 3 (0490):	449.25	23.705	6.08	45.57	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0491) |

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1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0490):	449.25	23.705	6.08	45.57
+ ID2= 2 (0482):	24.97	3.025	6.25	46.06
ID = 3 (0491):	474.22	24.000	6.08	45.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483) IN= 2---> OUT= 1 DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	7.0800	2.4860
	.2760	.0600	8.1000	3.3240
	1.2000	.3400	9.7980	4.6420
	2.0400	.6182	10.4940	7.4397
	2.6400	1.1630	11.6850	10.3000
	3.1200	1.7070	12.3480	11.4000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	474.220	24.000	6.08	45.60
OUTFLOW: ID= 1 (0483)	474.220	8.205	6.58	45.60

PEAK FLOW REDUCTION [Qout/Qin](%)= 34.19
TIME SHIFT OF PEAK FLOW (min)= 30.00
MAXIMUM STORAGE USED (ha.m.)= 3.4099

ADD HYD (0530) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0483):	474.22	8.205	6.58	45.60
+ ID2= 2 (0540):	4.63	1.339	6.00	76.65
ID = 3 (0530):	478.85	8.393	6.50	45.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0530):	478.85	8.393	6.50	45.90
+ ID2= 2 (0527):	67.54	7.924	6.08	52.59
ID = 3 (0545):	546.39	15.614	6.33	46.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
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Hadati Creek watershed - Post Development with Cityview Ridge

ID1= 1 (0545):	546.39	15.614	6.33	46.72
+ ID2= 2 (0542):	25.25	6.749	6.00	76.65
<hr/>				
ID = 3 (0546):	571.64	18.214	6.00	48.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0546):	571.64	18.214	6.00	48.05
+ ID2= 2 (0543):	14.99	4.164	6.00	76.65
<hr/>				
ID = 3 (0547):	586.63	22.378	6.00	48.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0548)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0547):	586.63	22.378	6.00	48.78
+ ID2= 2 (0544):	1.13	.333	6.00	76.65
<hr/>				
ID = 3 (0548):	587.76	22.711	6.00	48.83

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 ** SIMULATION NUMBER: 5 **

-----		Filename: Y:\SPrimmer\OTTHYMO\Ci	
READ STORM		tyview Ridge\RegSCS12hr.stm	
Ptotal=211.07 mm		Comments: Regional SCS Type II 12hr design storm	
<hr/>			
TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr
.25	6.35	3.25	12.70
.50	6.35	3.50	12.70
.75	6.35	3.75	12.70
1.00	6.35	4.00	12.70
1.25	4.32	4.25	16.76
1.50	4.32	4.50	16.76
1.75	4.32	4.75	16.76
2.00	4.32	5.00	16.76
2.25	6.35	5.25	12.70
2.50	6.35	5.50	12.70
2.75	6.35	5.75	12.70
3.00	6.35	6.00	12.70

 | CALIB |

Hadati Creek Watershed - Post Development with Cityview Ridge

STANDHYD (0480) | Area (ha)= 43.10
ID= 1 DT= 5.0 min | Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	18.10	25.00
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	680.00	40.00
Mannings n	=	.013	.300

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	6.35	3.083	12.70	6.083	23.11	9.08	52.83
.167	6.35	3.167	12.70	6.167	23.11	9.17	52.83
.250	6.35	3.250	12.70	6.250	23.11	9.25	52.83
.333	6.35	3.333	12.70	6.333	23.11	9.33	52.83
.417	6.35	3.417	12.70	6.417	23.11	9.42	52.83
.500	6.35	3.500	12.70	6.500	23.11	9.50	52.83
.583	6.35	3.583	12.70	6.583	23.11	9.58	52.83
.667	6.35	3.667	12.70	6.667	23.11	9.67	52.83
.750	6.35	3.750	12.70	6.750	23.11	9.75	52.83
.833	6.35	3.833	12.70	6.833	23.11	9.83	52.83
.917	6.35	3.917	12.70	6.917	23.11	9.92	52.83
1.000	6.35	4.000	12.70	7.000	23.11	10.00	52.83
1.083	4.32	4.083	16.76	7.083	12.70	10.08	37.85
1.167	4.32	4.167	16.76	7.167	12.70	10.17	37.85
1.250	4.32	4.250	16.76	7.250	12.70	10.25	37.85
1.333	4.32	4.333	16.76	7.333	12.70	10.33	37.85
1.417	4.32	4.417	16.76	7.417	12.70	10.42	37.85
1.500	4.32	4.500	16.76	7.500	12.70	10.50	37.85
1.583	4.32	4.583	16.76	7.583	12.70	10.58	37.85
1.667	4.32	4.667	16.76	7.667	12.70	10.67	37.85
1.750	4.32	4.750	16.76	7.750	12.70	10.75	37.85
1.833	4.32	4.833	16.76	7.833	12.70	10.83	37.85
1.917	4.32	4.917	16.76	7.917	12.70	10.92	37.85
2.000	4.32	5.000	16.76	8.000	12.70	11.00	37.85
2.083	6.35	5.083	12.70	8.083	12.70	11.08	12.70
2.167	6.35	5.167	12.70	8.167	12.70	11.17	12.70
2.250	6.35	5.250	12.70	8.250	12.70	11.25	12.70
2.333	6.35	5.333	12.70	8.333	12.70	11.33	12.70
2.417	6.35	5.417	12.70	8.417	12.70	11.42	12.70
2.500	6.35	5.500	12.70	8.500	12.70	11.50	12.70
2.583	6.35	5.583	12.70	8.583	12.70	11.58	12.70
2.667	6.35	5.667	12.70	8.667	12.70	11.67	12.70
2.750	6.35	5.750	12.70	8.750	12.70	11.75	12.70
2.833	6.35	5.833	12.70	8.833	12.70	11.83	12.70
2.917	6.35	5.917	12.70	8.917	12.70	11.92	12.70
3.000	6.35	6.000	12.70	9.000	12.70	12.00	12.70

Max.Eff.Inten.(mm/hr)=	52.83	59.46
over (min)	10.00	20.00
Storage Coeff. (min)=	8.46 (ii)	18.15 (ii)
Unit Hyd. Tpeak (min)=	10.00	20.00
Unit Hyd. peak (cms)=	.12	.06

PEAK FLOW (cms)=	1.33	3.90	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	5.222 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
			211.07

Hadati Creek Watershed - Post Development with Cityview Ridge
 RUNOFF COEFFICIENT = .99 .51 .61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0415) ID= 1 DT= 5.0 min		Area (ha)= 4.99		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	2.10	2.89	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.86	2.86	
Length	(m)=	185.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	15.00	
Storage Coeff. (min)=		3.48 (ii)	12.19 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.26	.09	
PEAK FLOW (cms)=		.15	.47	
TIME TO PEAK (hrs)=		9.92	10.00	
RUNOFF VOLUME (mm)=		209.57	107.20	
TOTAL RAINFALL (mm)=		211.07	211.07	
RUNOFF COEFFICIENT =		.99	.51	
			TOTALS .626 (iii)	

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0410) ID= 1 DT= 5.0 min		Area (ha)= 24.20		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	10.16	14.04	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	401.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.16 (ii)	15.86 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.19	.07	
			TOTALS	

Hadati Creek Watershed - Post Development with Cityview Ridge

PEAK FLOW	(cms)=	.75	2.23	2.975 (iii)
TIME TO PEAK	(hrs)=	10.00	10.00	10.00
RUNOFF VOLUME	(mm)=	209.57	107.20	128.70
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0460)	Area	(ha)=	36.00	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	15.12	20.88	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.03	2.03	
Length	(m)=	465.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		6.71 (ii)	16.36 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.18	.06	
				TOTALS
PEAK FLOW	(cms)=	1.11	3.30	4.413 (iii)
TIME TO PEAK	(hrs)=	10.00	10.00	10.00
RUNOFF VOLUME	(mm)=	209.57	107.20	128.70
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD (0455)	Area	(ha)=	12.70	
ID= 1 DT= 5.0 min	Total Imp(%)=	42.00	Dir. Conn.(%)=	21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.33	7.37	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.71	1.71	
Length	(m)=	300.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		5.43 (ii)	15.59 (ii)	

Hadati Creek watershed - Post Development with Cityview Ridge

Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.20	.07	
			TOTALS
PEAK FLOW (cms)=	.39	1.17	1.564 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0395) ID= 1 DT= 5.0 min	Area (ha)= 51.20 Total Imp(%)= 10.00 Dir. Conn.(%)= 5.00
---	--

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	5.12	46.08	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	900.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	43.26	
over (min)	10.00	25.00	
Storage Coeff. (min)=	10.01 (ii)	21.02 (ii)	
Unit Hyd. Tpeak (min)=	10.00	25.00	
Unit Hyd. peak (cms)=	.11	.05	
			TOTALS
PEAK FLOW (cms)=	.37	5.03	5.388 (iii)
TIME TO PEAK (hrs)=	10.00	10.08	10.08
RUNOFF VOLUME (mm)=	209.57	81.91	88.29
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.39	.42

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0360) ID= 1 DT= 5.0 min	Area (ha)= 30.00 Total Imp(%)= 37.00 Dir. Conn.(%)= 19.00
---	---

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	11.10	18.90
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	447.00	40.00

Hadati Creek watershed - Post Development with Cityview Ridge
Mannings n = .013 .300

Max.Eff.Inten.(mm/hr)=	52.83	55.42	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.58 (ii)	16.55 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.18	.06	
			TOTALS
PEAK FLOW (cms)=	.84	2.78	3.618 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	101.80	122.28
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.48	.58

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0350) ID= 1 DT= 5.0 min	Area (ha)= 16.30 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.85	9.45	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	1.00	1.00	
Length (m)=	330.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	6.75 (ii)	18.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.18	.06	
			TOTALS
PEAK FLOW (cms)=	.50	1.47	1.968 (iii)
TIME TO PEAK (hrs)=	10.00	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	107.20	128.70
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.51	.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0355) ID= 1 DT= 5.0 min	Area (ha)= 12.30 Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00
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Hadati Creek Watershed - Post Development with Cityview Ridge

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	5.17	7.13	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	1.60	1.60	
Length	(m)=	286.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		5.38 (ii)	15.74 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.21	.07	
PEAK FLOW	(cms)=	.38	1.13	*TOTALS*
TIME TO PEAK	(hrs)=	10.00	10.00	1.513 (iii)
RUNOFF VOLUME	(mm)=	209.57	107.20	10.00
TOTAL RAINFALL	(mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT	=	.99	.51	211.07
				.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0365)	
ID= 1 DT= 5.0 min	

Area (ha)= 117.50
 Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	49.35	68.15	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	885.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		10.00	20.00	
Storage Coeff. (min)=		9.91 (ii)	19.60 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.11	.06	
PEAK FLOW	(cms)=	3.61	10.49	*TOTALS*
TIME TO PEAK	(hrs)=	10.00	10.08	14.089 (iii)
RUNOFF VOLUME	(mm)=	209.57	107.20	10.00
TOTAL RAINFALL	(mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT	=	.99	.51	211.07
				.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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STANDHYD (0105)	Area (ha)= 51.32
ID= 1 DT= 5.0 min	Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	21.55	29.77	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	550.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	20.00	
Storage Coeff. (min)=	7.45 (ii)	17.14 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.17	.06	
PEAK FLOW (cms)=	1.58	4.68	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	6.260 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT =	.99	.51	211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 14.32
STANDHYD (0102)	Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00
ID= 1 DT= 5.0 min	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	6.01	8.31	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	287.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	59.46	
over (min)	5.00	15.00	
Storage Coeff. (min)=	5.04 (ii)	14.74 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	.21	.08	
PEAK FLOW (cms)=	.44	1.34	*TOTALS*
TIME TO PEAK (hrs)=	10.00	10.00	1.780 (iii)
RUNOFF VOLUME (mm)=	209.57	107.20	10.00
TOTAL RAINFALL (mm)=	211.07	211.07	128.70
RUNOFF COEFFICIENT =	.99	.51	211.07
			.61

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB
STANDHYD (0101)
ID= 1 DT= 5.0 min

Area (ha)= 16.32
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	6.85	9.47	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	309.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	15.00	
Storage Coeff. (min)=		5.27 (ii)	14.96 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		.21	.08	
				TOTALS
PEAK FLOW (cms)=		.50	1.52	2.027 (iii)
TIME TO PEAK (hrs)=		10.00	10.00	10.00
RUNOFF VOLUME (mm)=		209.57	107.20	128.70
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.51	.61

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0110)
ID= 1 DT= 5.0 min

Area (ha)= 19.00
Total Imp(%)= 42.00 Dir. Conn.(%)= 21.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	7.98	11.02	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	365.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		5.00	20.00	
Storage Coeff. (min)=		5.82 (ii)	15.52 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		.20	.07	
				TOTALS
PEAK FLOW (cms)=		.59	1.75	2.340 (iii)
TIME TO PEAK (hrs)=		10.00	10.00	10.00
RUNOFF VOLUME (mm)=		209.57	107.20	128.70
TOTAL RAINFALL (mm)=		211.07	211.07	211.07
RUNOFF COEFFICIENT =		.99	.51	.61

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

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 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> <div>CALIB</div> <div>STANDHYD (0600)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 11.38		
		Total Imp(%)= 42.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	4.78	6.60	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	59.46	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.46 (ii)	18.15 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
PEAK FLOW (cms)=		.35	1.03	*TOTALS*
TIME TO PEAK (hrs)=		10.00	10.00	1.379 (iii)
RUNOFF VOLUME (mm)=		209.57	107.20	10.00
TOTAL RAINFALL (mm)=		211.07	211.07	128.70
RUNOFF COEFFICIENT =		.99	.51	211.07
				.61

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<div> <div>CALIB</div> <div>STANDHYD (0601)</div> <div>ID= 1 DT= 5.0 min</div> </div>		Area (ha)= 7.62		
		Total Imp(%)= 46.00	Dir. Conn.(%)= 21.00	
		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	3.51	4.11	
Dep. Storage	(mm)=	1.50	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	680.00	40.00	
Mannings n	=	.013	.300	
Max.Eff.Inten.(mm/hr)=		52.83	64.79	
over (min)		10.00	20.00	
Storage Coeff. (min)=		8.46 (ii)	17.83 (ii)	
Unit Hyd. Tpeak (min)=		10.00	20.00	
Unit Hyd. peak (cms)=		.12	.06	
PEAK FLOW (cms)=		.23	.70	*TOTALS*
TIME TO PEAK (hrs)=		10.00	10.00	.936 (iii)
RUNOFF VOLUME (mm)=		209.57	113.39	10.00
TOTAL RAINFALL (mm)=		211.07	211.07	133.59
RUNOFF COEFFICIENT =		.99	.54	211.07
				.63

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

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Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0607)
ID= 1 DT= 5.0 min

Area (ha)= 5.97
Total Imp(%)= 42.00 Dir. Conn.(%)= 2.50

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.51	3.46
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	680.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	52.83	76.31
over (min)	10.00	20.00
Storage Coeff. (min)=	8.46 (ii)	17.23 (ii)
Unit Hyd. Tpeak (min)=	10.00	20.00
Unit Hyd. peak (cms)=	.12	.06

		TOTALS
PEAK FLOW (cms)=	.02	.721 (iii)
TIME TO PEAK (hrs)=	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	126.19
TOTAL RAINFALL (mm)=	211.07	211.07
RUNOFF COEFFICIENT =	.99	.60

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:

Fo (mm/hr)= 75.00 K (1/hr)= 4.14

Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0540)
ID= 1 DT= 5.0 min

Area (ha)= 4.63
Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	3.70	.93
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	150.00	40.00
Mannings n =	.013	.300

Max.Eff.Inten.(mm/hr)=	52.83	42.97
over (min)	5.00	25.00
Storage Coeff. (min)=	5.03 (ii)	21.29 (ii)
Unit Hyd. Tpeak (min)=	5.00	25.00
Unit Hyd. peak (cms)=	.21	.05

		TOTALS
PEAK FLOW (cms)=	.54	.636 (iii)
TIME TO PEAK (hrs)=	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	182.64

Hadati Creek watershed - Post Development with Cityview Ridge
TOTAL RAINFALL (mm)= 211.07 211.07 211.07
RUNOFF COEFFICIENT = .99 .39 .87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0500) ID= 1 DT= 5.0 min		Area (ha)= 244.00 Total Imp(%)= 46.00	Dir. Conn.(%)= 26.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	112.24	131.76
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	.80	.80
Length	(m)=	1275.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		52.83	59.90
over (min)		15.00	30.00
Storage Coeff. (min)=		16.24 (ii)	28.96 (ii)
Unit Hyd. Tpeak (min)=		15.00	30.00
Unit Hyd. peak (cms)=		.07	.04
PEAK FLOW (cms)=		9.05	18.51
TIME TO PEAK (hrs)=		10.00	10.25
RUNOFF VOLUME (mm)=		209.57	107.75
TOTAL RAINFALL (mm)=		211.07	211.07
RUNOFF COEFFICIENT =		.99	.51
			TOTALS
			27.108 (iii)
			10.08
			134.22
			211.07
			.64

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
Fo (mm/hr)= 75.00 K (1/hr)= 4.14
Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0510) ID= 1 DT= 5.0 min		Area (ha)= 16.00 Total Imp(%)= 80.00	Dir. Conn.(%)= 79.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	12.80	3.20
Dep. Storage	(mm)=	1.50	5.00
Average Slope	(%)=	.50	.20
Length	(m)=	400.00	40.00
Mannings n	=	.013	.300
Max.Eff.Inten.(mm/hr)=		52.83	42.97
over (min)		10.00	35.00
Storage Coeff. (min)=		9.33 (ii)	31.35 (ii)
Unit Hyd. Tpeak (min)=		10.00	35.00
Unit Hyd. peak (cms)=		.12	.03
			TOTALS

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PEAK FLOW	(cms)=	1.85	.31	2.134 (iii)
TIME TO PEAK	(hrs)=	10.00	10.33	10.00
RUNOFF VOLUME	(mm)=	209.57	81.35	182.64
TOTAL RAINFALL	(mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT	=	.99	.39	.87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0542) ID= 1 DT= 5.0 min	Area (ha)= 25.25 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	20.20	5.05	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	350.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	42.97	
over (min)	10.00	25.00	
Storage Coeff. (min)=	8.37 (ii)	24.63 (ii)	
Unit Hyd. Tpeak (min)=	10.00	25.00	
Unit Hyd. peak (cms)=	.12	.05	
			TOTALS
PEAK FLOW (cms)=	2.92	.53	3.443 (iii)
TIME TO PEAK (hrs)=	10.00	10.17	10.00
RUNOFF VOLUME (mm)=	209.57	81.35	182.64
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.39	.87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0543) ID= 1 DT= 5.0 min	Area (ha)= 14.99 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00
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	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	11.99	3.00
Dep. Storage (mm)=	1.50	5.00
Average Slope (%)=	.55	.55
Length (m)=	200.00	40.00
Mannings n =	.013	.300
Max.Eff.Inten.(mm/hr)=	52.83	42.97
over (min)	5.00	25.00
Storage Coeff. (min)=	5.98 (ii)	22.24 (ii)

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Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	.19	.05	
			TOTALS
PEAK FLOW (cms)=	1.74	.32	2.054 (iii)
TIME TO PEAK (hrs)=	10.00	10.08	10.00
RUNOFF VOLUME (mm)=	209.57	81.35	182.64
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.39	.87

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0544) ID= 1 DT= 5.0 min	Area (ha)= 1.13 Total Imp(%)= 80.00 Dir. Conn.(%)= 79.00
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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.90	.23	
Dep. Storage (mm)=	1.50	5.00	
Average Slope (%)=	.55	.55	
Length (m)=	50.00	40.00	
Mannings n =	.013	.300	
Max.Eff.Inten.(mm/hr)=	52.83	42.97	
over (min)=	5.00	20.00	
Storage Coeff. (min)=	2.60 (ii)	18.86 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	.29	.06	
			TOTALS
PEAK FLOW (cms)=	.13	.03	.156 (iii)
TIME TO PEAK (hrs)=	9.67	10.00	10.00
RUNOFF VOLUME (mm)=	209.57	81.35	182.64
TOTAL RAINFALL (mm)=	211.07	211.07	211.07
RUNOFF COEFFICIENT =	.99	.39	.87

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) HORTONS EQUATION SELECTED FOR PERVIOUS LOSSES:
 Fo (mm/hr)= 75.00 K (1/hr)= 4.14
 Fc (mm/hr)= 12.50 Cum.Inf. (mm)= .00
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

STORE HYD (0525) ID= 1 DT=****min	AREA (ha)= .00 QPEAK (cms)= .00 TPEAK (hrs)= .00 VOLUME (mm)=*****
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ADD HYD (0420) 1 + 2 = 3	AREA QPEAK TPEAK R.V.
-----------------------------	-----------------------

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	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0415):	4.99	.626	10.00	128.70
+ ID2= 2 (0410):	24.20	2.975	10.00	128.70
<hr/>				
ID = 3 (0420):	29.19	3.602	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0465)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0460):	36.00	4.413	10.00	128.70
+ ID2= 2 (0455):	12.70	1.564	10.00	128.70
<hr/>				
ID = 3 (0465):	48.70	5.977	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0362)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
.00	.40	.0300	
5.50	.15	.0300 / .0150	Main Channel
5.51	.00	.0150	Main Channel
10.00	.09	.0150	Main Channel
14.49	.00	.0150	Main Channel
14.50	.15	.0150 / .0300	Main Channel
20.00	.40	.0300	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.02	.02	.176E+02	.0	.21	80.52
.04	.04	.702E+02	.0	.33	50.72
.06	.06	.158E+03	.1	.43	38.71
.08	.08	.281E+03	.1	.52	31.95
.09	.09	.438E+03	.3	.62	26.84
.11	.11	.607E+03	.5	.77	21.66
.13	.13	.776E+03	.7	.90	18.45
.15	.15	.944E+03	1.0	1.03	16.22
.17	.17	.116E+04	1.3	1.16	14.36
.20	.20	.140E+04	1.8	1.27	13.13
.22	.22	.166E+04	2.3	1.36	12.24
.24	.24	.194E+04	2.8	1.44	11.58
.26	.26	.225E+04	3.4	1.51	11.05
.29	.29	.258E+04	4.0	1.57	10.63
.31	.31	.293E+04	4.8	1.62	10.27
.33	.33	.331E+04	5.5	1.67	9.97
.35	.35	.371E+04	6.4	1.72	9.71
.38	.38	.413E+04	7.3	1.76	9.48
.40	.40	.457E+04	8.2	1.80	9.28

<---- hydrograph ---->				<-pipe / channel->	
INFLOW : ID= 2 (0360)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
	30.00	3.62	10.00	122.28	.27
					MAX VEL (m/s)
					1.53

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 OUTFLOW: ID= 1 (0362) 30.00 3.50 10.08 122.26 .27 1.52

ROUTE CHN (0353)
 IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 .01 .01 .929E+01 .0 .17 99.56
 .03 .03 .372E+02 .0 .27 62.72
 .04 .04 .836E+02 .0 .35 47.86
 .05 .05 .149E+03 .1 .42 39.51
 .07 .07 .232E+03 .1 .49 34.05
 .08 .08 .334E+03 .2 .55 30.15
 .10 .10 .454E+03 .3 .64 26.24
 .11 .11 .576E+03 .4 .74 22.41
 .12 .12 .699E+03 .6 .84 19.75
 .14 .14 .822E+03 .8 .94 17.76
 .15 .15 .944E+03 1.0 1.03 16.22
 .16 .16 .108E+04 1.2 1.11 15.07
 .18 .18 .123E+04 1.4 1.17 14.28
 .19 .19 .140E+04 1.7 1.21 13.72
 .20 .20 .159E+04 2.0 1.25 13.31
 .22 .22 .180E+04 2.3 1.28 13.01
 .23 .23 .203E+04 2.6 1.31 12.76
 .25 .25 .227E+04 3.0 1.33 12.57
 .26 .26 .254E+04 3.4 1.34 12.41

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0350) 16.30 1.97 10.00 128.70 .20 1.25
 OUTFLOW: ID= 1 (0353) 16.30 1.87 10.08 128.66 .20 1.24

ROUTE CHN (0358)
 IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 .00 .26 .0300
 5.50 .15 .0300 / .0150 Main Channel
 5.51 .00 .0150 Main Channel
 10.00 .09 .0150 Main Channel
 14.49 .00 .0150 Main Channel
 14.50 .15 .0150 / .0300 Main Channel
 20.00 .26 .0300

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----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.01	.01	.102E+02	.0	.17	109.52
.03	.03	.409E+02	.0	.27	68.99
.04	.04	.920E+02	.0	.35	52.65
.05	.05	.163E+03	.1	.42	43.46
.07	.07	.255E+03	.1	.49	37.45
.08	.08	.368E+03	.2	.55	33.17
.10	.10	.499E+03	.3	.64	28.86
.11	.11	.634E+03	.4	.74	24.66
.12	.12	.769E+03	.6	.84	21.72
.14	.14	.904E+03	.8	.94	19.54
.15	.15	.104E+04	1.0	1.03	17.84
.16	.16	.119E+04	1.2	1.11	16.57
.18	.18	.135E+04	1.4	1.17	15.71
.19	.19	.154E+04	1.7	1.21	15.10
.20	.20	.175E+04	2.0	1.25	14.65
.22	.22	.198E+04	2.3	1.28	14.31
.23	.23	.223E+04	2.6	1.31	14.04
.25	.25	.250E+04	3.0	1.33	13.82
.26	.26	.279E+04	3.4	1.34	13.65

<---- hydrograph ---->

<-pipe / channel-->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0355)	12.30	1.51	10.00	128.70	.18	1.18
OUTFLOW: ID= 1 (0358)	12.30	1.44	10.08	128.64	.18	1.17

RESERVOIR (0106)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	.5000	.4000
.0100	.0100	6.6000	.8000
.0260	.2300	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0105)	51.320	6.260	10.00	128.70
OUTFLOW: ID= 1 (0106)	51.320	5.997	10.08	128.69

PEAK FLOW REDUCTION [Qout/Qin](%)= 95.79
TIME SHIFT OF PEAK FLOW (min)= 5.00
MAXIMUM STORAGE USED (ha.m.)= .7608

ADD HYD (0103)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):	14.32	1.780	10.00	128.70
+ ID2= 2 (0101):	16.32	2.027	10.00	128.70
ID = 3 (0103):	30.64	3.807	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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RESERVOIR (0111)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.0000	1.0000
.0100	.0100	20.0000	1.1000
.0120	.1000	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0110)	19.000	2.340	10.00	128.70
OUTFLOW: ID= 1 (0111)	19.000	2.069	10.50	128.68

PEAK FLOW REDUCTION [Qout/Qin](%)= 88.39
TIME SHIFT OF PEAK FLOW (min)= 30.00
MAXIMUM STORAGE USED (ha.m.)= 1.0100

ADD HYD (0602)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0600):	11.38	1.379	10.00	128.70
+ ID2= 2 (0601):	7.62	.936	10.00	133.59
ID = 3 (0602):	19.00	2.315	10.00	130.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0505)
Inlet Cap.=9.000
#of Inlets= 1
Total(cms)= 9.0

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	244.00	27.11	10.08	134.22
MAJOR SYS.(ID= 2):	78.53	18.11	10.08	134.22
MINOR SYS.(ID= 3):	165.47	9.00	6.75	134.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0515)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0505):	165.47	9.000	6.75	134.22
+ ID2= 2 (0510):	16.00	2.134	10.00	182.64
ID = 3 (0515):	181.47	11.134	10.00	138.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DUHYD (0425)
Inlet Cap.=1.980
#of Inlets= 1

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Total(cms)= 2.0	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
TOTAL HYD.(ID= 1):	29.19	3.60	10.00	128.70
MAJOR SYS.(ID= 2):	4.95	1.62	10.00	128.70
MINOR SYS.(ID= 3):	24.24	1.98	9.33	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0470) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0425):	4.95	1.622	10.00	128.70
+ ID2= 2 (0465):	48.70	5.977	10.00	128.70
ID = 3 (0470):	53.65	7.598	10.00	128.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0359) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0353):	16.30	1.875	10.08	128.66
+ ID2= 2 (0358):	12.30	1.436	10.08	128.64
ID = 3 (0359):	28.60	3.311	10.08	128.65

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0104) IN= 2---> OUT= 1 DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.0000	.0000	1.0000	.5000
	.0100	.0100	10.0000	.6000
	.0150	.1332	.0000	.0000
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0103)	30.640	3.807	10.00	128.70
OUTFLOW: ID= 1 (0104)	30.640	3.797	10.00	128.69

PEAK FLOW REDUCTION [Qout/Qin](%)= 99.73
TIME SHIFT OF PEAK FLOW (min)= .00
MAXIMUM STORAGE USED (ha.m.)= .5312

ADD HYD (0114) 1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0104):	30.64	3.797	10.00	128.69
+ ID2= 2 (0111):	19.00	2.069	10.50	128.68

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ID = 3 (0114): 49.64 4.896 10.50 128.69

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0563)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (2.2) ----->

Distance	Elevation	Manning	
.00	1.00	.0350	
2.00	.50	.0350	
4.00	.00	.0350 / .0350	Main Channel
4.50	.00	.0350	Main Channel
5.00	.00	.0350 / .0350	Main Channel
7.00	.50	.0350	
9.00	1.00	.0350	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.05	.05	.745E+01	.0	.64	3.06
.11	.11	.175E+02	.1	.96	2.03
.16	.16	.301E+02	.3	1.21	1.61
.21	.21	.454E+02	.6	1.42	1.37
.26	.26	.632E+02	.9	1.61	1.21
.32	.32	.836E+02	1.3	1.77	1.10
.37	.37	.107E+03	1.8	1.93	1.01
.42	.42	.132E+03	2.3	2.08	.94
.47	.47	.160E+03	3.0	2.22	.88
.53	.53	.191E+03	3.8	2.35	.83
.58	.58	.225E+03	4.8	2.48	.79
.63	.63	.261E+03	5.8	2.60	.75
.68	.68	.299E+03	7.0	2.72	.72
.74	.74	.340E+03	8.2	2.84	.69
.79	.79	.384E+03	9.7	2.95	.66
.84	.84	.430E+03	11.3	3.06	.64
.89	.89	.479E+03	13.0	3.17	.62
.95	.95	.531E+03	14.8	3.27	.60
1.00	1.00	.585E+03	16.9	3.38	.58

<---- hydrograph ---->

<-pipe / channel->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0602)	19.00	2.31	10.00	130.66	.42	2.07
OUTFLOW: ID= 1 (0563)	19.00	2.31	10.00	130.66	.42	2.07

ROUTE CHN (0564)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
.00	101.50	.0500	
1.00	100.70	.0500	
1.50	100.55	.0500 / .0300	Main Channel
2.00	99.50	.0300	Main Channel
3.50	99.60	.0300	Main Channel
4.50	100.65	.0300 / .0500	Main Channel
6.00	101.45	.0500	

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<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	99.60	.353E+02	.0	.19	43.69
.19	99.69	.112E+03	.1	.37	22.76
.29	99.79	.195E+03	.2	.49	17.03
.38	99.88	.285E+03	.3	.59	14.23
.48	99.98	.381E+03	.5	.67	12.51
.57	100.07	.484E+03	.7	.74	11.32
.67	100.17	.594E+03	.9	.80	10.43
.76	100.26	.710E+03	1.2	.86	9.74
.86	100.36	.832E+03	1.5	.91	9.18
.95	100.45	.961E+03	1.8	.96	8.72
1.05	100.55	.110E+04	2.2	1.00	8.32
1.16	100.66	.127E+04	2.7	1.07	7.80
1.28	100.78	.148E+04	3.4	1.14	7.31
1.39	100.89	.170E+04	4.1	1.20	6.94
1.50	101.00	.195E+04	4.9	1.25	6.65
1.61	101.11	.221E+04	5.8	1.30	6.41
1.72	101.22	.250E+04	6.7	1.34	6.22
1.84	101.34	.280E+04	7.7	1.38	6.04
1.95	101.45	.313E+04	8.8	1.41	5.90

**** WARNING: TRAVEL TIME TABLE EXCEEDED

<---- hydrograph ---->					<-pipe / channel->	
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0505)	78.53	18.11	10.08	134.22	1.92	1.40
OUTFLOW: ID= 1 (0564)	78.53	17.83	10.25	134.22	1.95	1.41

DUHYD (0520)					
Inlet Cap.=3.050					
#of Inlets= 1					
Total(cms)= 3.0					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
TOTAL HYD.(ID= 1):	181.47	11.13	10.00	138.49	
=====					
MAJOR SYS.(ID= 2):	98.04	8.08	10.00	138.49	
MINOR SYS.(ID= 3):	83.43	3.05	4.25	138.49	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0475)		Routing time step (min)'= 5.00
IN= 2--->	OUT= 1	

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
100.00	324.60	.0500
115.00	321.60	.0500
120.00	320.80	.0500 / .0300
122.00	320.80	.0300 / .0500
138.00	321.60	.0500
148.00	322.30	.0500
154.00	323.10	.0500
164.00	324.60	.0500

<----- TRAVEL TIME TABLE ----->
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DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.20	321.00	.398E+03	.8	.84	8.53
.40	321.20	.125E+04	3.3	1.13	6.33
.60	321.40	.255E+04	8.1	1.36	5.27
.80	321.60	.430E+04	15.6	1.56	4.59
1.00	321.80	.644E+04	26.8	1.79	4.01
1.20	322.00	.892E+04	41.2	1.99	3.61
1.40	322.20	.117E+05	59.3	2.17	3.30
1.60	322.40	.148E+05	81.9	2.37	3.02
1.80	322.60	.182E+05	109.1	2.58	2.78
2.00	322.80	.218E+05	140.2	2.77	2.59
2.20	323.00	.256E+05	175.3	2.95	2.43
2.40	323.20	.296E+05	214.7	3.12	2.29
2.60	323.40	.338E+05	258.6	3.29	2.18
2.80	323.60	.382E+05	306.7	3.46	2.07
3.00	323.80	.428E+05	359.1	3.61	1.98
3.20	324.00	.476E+05	416.0	3.76	1.91
3.40	324.20	.526E+05	477.5	3.91	1.83
3.60	324.40	.578E+05	543.5	4.05	1.77
3.80	324.60	.632E+05	614.3	4.18	1.71

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0470)	53.65	7.60	10.00	128.70	.58	1.33
OUTFLOW: ID= 1 (0475)	53.65	7.51	10.00	128.70	.58	1.33

ADD HYD (0363)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0362):	30.00	3.504	10.08	122.26
+ ID2= 2 (0359):	28.60	3.311	10.08	128.65
ID = 3 (0363):	58.60	6.814	10.08	125.38

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0115)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0106):	51.32	5.997	10.08	128.69
+ ID2= 2 (0114):	49.64	4.896	10.50	128.69
ID = 3 (0115):	100.96	10.540	10.08	128.69

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0492)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0563):	19.00	2.311	10.00	130.66
+ ID2= 2 (0607):	5.97	.721	10.00	126.19

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ID = 3 (0492): 24.97 3.032 10.00 129.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0526)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0525):	.00	.001	.00	*****
+ ID2= 2 (0520):	98.04	8.084	10.00	138.49
ID = 3 (0526):	98.04	8.084	10.00	138.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0380)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0363):	58.60	6.814	10.08	125.38
+ ID2= 2 (0365):	117.50	14.089	10.00	128.70
ID = 3 (0380):	176.10	20.834	10.00	127.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0482)	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
IN= 2---> OUT= 1				
DT= 5.0 min	.0000	.0000	.2910	.3795
	.2590	.0579	.2970	.4503
	.2660	.1180	1.6320	.5232
	.2720	.1802	4.1680	.5983
	.2790	.2445	7.5660	.6756
	.2850	.3109	.0000	.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0492)	24.970	3.032	10.00	129.59
OUTFLOW: ID= 1 (0482)	24.970	3.007	10.08	129.59

PEAK FLOW REDUCTION	[Qout/Qin] (%)= 99.18
TIME SHIFT OF PEAK FLOW	(min)= 5.00
MAXIMUM STORAGE USED	(ha.m.)= .5640

ROUTE CHN (0527)	Routing time step (min)'= 5.00
IN= 2---> OUT= 1	

Distance	Elevation	Manning	
100.00	313.20	.0500	
140.00	312.40	.0500 / .0300	Main Channel
140.50	310.80	.0300	Main Channel

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 141.50 310.80 .0300 Main Channel
 142.00 312.40 .0300 / .0500 Main Channel
 160.00 313.20 .0500

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	310.92	.575E+02	.1	.40	18.86
.25	311.05	.119E+03	.2	.57	13.13
.37	311.17	.185E+03	.3	.69	10.87
.49	311.29	.256E+03	.4	.78	9.61
.62	311.42	.330E+03	.6	.86	8.77
.74	311.54	.409E+03	.8	.92	8.17
.86	311.66	.492E+03	1.1	.97	7.70
.98	311.78	.579E+03	1.3	1.02	7.32
1.11	311.91	.671E+03	1.6	1.07	7.01
1.23	312.03	.767E+03	1.9	1.11	6.74
1.35	312.15	.867E+03	2.2	1.15	6.50
1.48	312.28	.971E+03	2.6	1.19	6.29
1.60	312.40	.108E+04	2.9	1.23	6.11
1.73	312.53	.149E+04	3.6	1.10	6.85
1.87	312.67	.248E+04	4.9	.88	8.52
2.00	312.80	.405E+04	6.9	.77	9.74
2.13	312.93	.620E+04	10.1	.73	10.21
2.27	313.07	.893E+04	14.6	.74	10.17
2.40	313.20	.122E+05	20.7	.76	9.85

		<---- hydrograph ---->			<-pipe / channel->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
INFLOW :	ID= 2 (0526)	98.04	8.08	10.00	138.49	2.05
OUTFLOW:	ID= 1 (0527)	98.04	7.97	10.08	138.49	2.04
						MAX VEL (m/s)
						.76
						.76

RESERVOIR (0390)
 IN= 2---> OUT= 1
 DT= 5.0 min

		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
		.0000	.0000	1.3100	1.6000
		.7700	.2870	1.8600	23.2300
		1.2600	.9680	.0000	.0000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW :	ID= 2 (0380)	176.100	20.834	10.00	127.59
OUTFLOW:	ID= 1 (0390)	176.100	1.714	12.33	127.59

PEAK FLOW REDUCTION [Qout/Qin](%)= 8.23
 TIME SHIFT OF PEAK FLOW (min)=140.00
 MAXIMUM STORAGE USED (ha.m.)= 17.4981

ADD HYD (0400)
 1 + 2 = 3

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0395):		51.20	5.388	10.08	88.29
+ ID2= 2 (0390):		176.10	1.714	12.33	127.59
=====					
ID = 3 (0400):		227.30	6.909	10.08	118.74

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0403)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
100.00	338.30	.0500	
110.00	336.80	.0500	
135.00	336.00	.0300	Main Channel
142.00	335.30	.0500	
148.00	335.30	.0500	
156.00	336.00	.0500	
165.00	338.30	.0000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	335.46	.231E+04	.9	.71	44.52
.32	335.62	.563E+04	3.2	1.09	29.11
.47	335.77	.997E+04	7.3	1.39	22.72
.63	335.93	.153E+05	13.4	1.66	19.04
.79	336.09	.218E+05	22.7	1.97	16.04
.95	336.25	.299E+05	35.3	2.25	14.10
1.11	336.41	.396E+05	51.2	2.46	12.89
1.26	336.56	.510E+05	70.7	2.63	12.02
1.42	336.72	.641E+05	94.1	2.79	11.35
1.58	336.88	.787E+05	122.4	2.96	10.71
1.74	337.04	.939E+05	155.6	3.15	10.06
1.89	337.19	.110E+06	192.8	3.34	9.48
2.05	337.35	.126E+06	233.9	3.53	8.97
2.21	337.51	.143E+06	278.9	3.71	8.53
2.37	337.67	.160E+06	327.7	3.89	8.13
2.53	337.83	.178E+06	380.3	4.07	7.79
2.68	337.98	.196E+06	436.7	4.23	7.48
2.84	338.14	.215E+06	496.9	4.40	7.20
3.00	338.30	.234E+06	561.0	4.56	6.95

<----- hydrograph ----->

<-pipe / channel->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0400)	227.30	6.91	10.08	118.74	.46	1.36
OUTFLOW: ID= 1 (0403)	227.30	6.38	10.33	118.74	.44	1.30

ADD HYD (0407)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0403):	227.30	6.377	10.33	118.74
+ ID2= 2 (0115):	100.96	10.540	10.08	128.69
ID = 3 (0407):	328.26	16.526	10.17	121.80

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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RESERVOIR (0113)
IN= 2---> OUT= 1
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.0000	.0000	1.6000	6.4000
1.1000	2.9000	9.1000	10.0000
1.3000	4.3000	12.0000	20.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0407)	328.260	16.526	10.17	121.80
OUTFLOW: ID= 1 (0113)	328.260	9.456	11.50	121.80

PEAK FLOW REDUCTION [Qout/Qin](%)= 57.22
TIME SHIFT OF PEAK FLOW (min)= 80.00
MAXIMUM STORAGE USED (ha.m.)= 11.2348

ADD HYD (0430)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0113):	328.26	9.456	11.50	121.80
+ ID2= 2 (0425):	24.24	1.980	9.33	128.70
ID = 3 (0430):	352.50	11.349	11.08	122.27

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0440)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning
100.00	325.40	.0600
120.00	324.60	.0600
126.00	323.90	.0600
130.00	323.00	.0600
140.00	322.30	.0600 / .0300
142.00	322.30	.0300 / .0600
150.00	323.90	.0600
155.00	324.60	.0600
160.00	325.40	.0600

Main Channel
Main Channel

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.16	322.46	.233E+03	.6	.96	6.96
.33	322.63	.672E+03	2.1	1.26	5.27
.49	322.79	.132E+04	4.9	1.48	4.51
.65	322.95	.216E+04	9.0	1.66	4.03
.82	323.12	.319E+04	14.9	1.87	3.57
.98	323.28	.433E+04	22.5	2.08	3.21
1.14	323.44	.556E+04	31.6	2.27	2.93
1.31	323.61	.689E+04	42.3	2.45	2.72
1.47	323.77	.833E+04	54.6	2.62	2.54
1.63	323.93	.987E+04	68.3	2.77	2.41
1.79	324.09	.115E+05	82.8	2.87	2.33
1.96	324.26	.134E+05	99.2	2.96	2.25
2.12	324.42	.154E+05	117.9	3.06	2.18

Hadati Creek Watershed - Post Development with Cityview Ridge

2.28	324.58	.176E+05	138.8	3.15	2.11
2.45	324.75	.200E+05	157.4	3.14	2.12
2.61	324.91	.228E+05	179.6	3.15	2.11
2.77	325.07	.259E+05	205.8	3.18	2.09
2.94	325.24	.293E+05	236.1	3.23	2.07
3.10	325.40	.330E+05	270.6	3.28	2.03

			<---- hydrograph ---->			<-pipe / channel->		
			AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0430)			352.50	11.35	11.08	122.27	.72	1.73
OUTFLOW: ID= 1 (0440)			352.50	11.32	11.08	122.27	.71	1.73

ADD HYD (0485)					
1 + 2 = 3					
ID1= 1 (0475):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		53.65	7.511	10.00	128.70
+ ID2= 2 (0440):		352.50	11.321	11.08	122.27
ID = 3 (0485):		406.15	16.120	10.75	123.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0490)					
1 + 2 = 3					
ID1= 1 (0480):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		43.10	5.222	10.00	128.70
+ ID2= 2 (0485):		406.15	16.120	10.75	123.12
ID = 3 (0490):		449.25	19.973	10.67	123.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0491)					
1 + 2 = 3					
ID1= 1 (0490):		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		449.25	19.973	10.67	123.66
+ ID2= 2 (0482):		24.97	3.007	10.08	129.59
ID = 3 (0491):		474.22	22.680	10.17	123.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0483)					
IN= 2---> OUT= 1					
DT= 5.0 min					
		OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
		.0000	.0000	7.0800	2.4860
		.2760	.0600	8.1000	3.3240
		1.2000	.3400	9.7980	4.6420
		2.0400	.6182	10.4940	7.4397

Hadati Creek watershed - Post Development with Cityview Ridge

2.6400	1.1630		11.6850	10.3000
3.1200	1.7070		12.3480	11.4000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0491)	474.220	22.680	10.17	123.97
OUTFLOW: ID= 1 (0483)	474.220	11.709	12.08	123.97

PEAK FLOW REDUCTION [Qout/Qin](%)= 51.63
 TIME SHIFT OF PEAK FLOW (min)=115.00
 MAXIMUM STORAGE USED (ha.m.)= 10.3422

ADD HYD (0530)				
1 + 2 = 3				

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0483):	474.22	11.709	12.08	123.97
+ ID2= 2 (0540):	4.63	.636	10.00	182.64
=====				
ID = 3 (0530):	478.85	11.843	12.00	124.54

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0545)				
1 + 2 = 3				

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0530):	478.85	11.843	12.00	124.54
+ ID2= 2 (0527):	98.04	7.968	10.08	138.49
=====				
ID = 3 (0545):	576.89	19.057	11.00	126.91

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0546)				
1 + 2 = 3				

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0545):	576.89	19.057	11.00	126.91
+ ID2= 2 (0542):	25.25	3.443	10.00	182.64
=====				
ID = 3 (0546):	602.14	21.640	10.08	129.24

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0547)				
1 + 2 = 3				

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0546):	602.14	21.640	10.08	129.24
+ ID2= 2 (0543):	14.99	2.054	10.00	182.64
=====				
ID = 3 (0547):	617.13	23.544	10.00	130.54

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Hadati Creek watershed - Post Development with Cityview Ridge

ADD HYD (0548)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (0547):	617.13	23.544	10.00	130.54	
+ ID2= 2 (0544):	1.13	.156	10.00	182.64	
=====					
ID = 3 (0548):	618.26	23.700	10.00	130.64	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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"                                     105172_POST_2yr UC
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        w:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                    105172_POST_2yr UC.out"
" Licensee name:                      gmbp"
" Company                            Hewlett-Packard Company"
" Date & Time last used:              6/2/2016 at 3:21:13 PM"
31 TIME PARAMETERS"
" 5.000 Time Step"
" 170.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
32 STORM Chicago storm"
" 1 Chicago storm"
" 743.000 Coefficient A"
" 6.000 Constant B"
" 0.799 Exponent C"
" 0.400 Fraction R"
" 170.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                    105.606 mm/hr"
" Total depth                          33.816 mm"
" 6 002hyd Hydrograph extension used in this file"
33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clythe Creeek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 0.496 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 22.189 2.170 2.858 minutes"
" Time to Centroid 93.436 84.151 84.470 minutes"
" Rainfall depth 33.816 33.816 33.816 mm"
" Rainfall volume 403.59 749.53 1153.12 c.m"
" Rainfall losses 31.713 1.985 12.390 mm"
" Runoff depth 2.103 31.830 21.426 mm"
" Runoff volume 25.10 705.52 730.63 c.m"
" Runoff coefficient 0.062 0.941 0.634 "
" Maximum flow 0.017 0.496 0.496 c.m/sec"
40 HYDROGRAPH Add Runoff "

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"          105172_POST_2yr UC
"          4  Add Runoff "
"              0.496      0.496      0.000      0.000"
" 33  CATCHMENT 202"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      202 Catchment 202 - To Clythe Creek"
"      25.000 % Impervious"
"      0.740 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      0.555 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      0.185 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"              0.041      0.496      0.000      0.000 c.m/sec"
"      Catchment 202      Pervious      Impervious      Total Area "
"      Surface Area      0.555      0.185      0.740      hectare"
"      Time of concentration      22.189      2.170      5.482      minutes"
"      Time to Centroid      93.436      84.151      85.688      minutes"
"      Rainfall depth      33.816      33.816      33.816      mm"
"      Rainfall volume      187.68      62.56      250.24      c.m"
"      Rainfall losses      31.713      1.985      24.281      mm"
"      Runoff depth      2.103      31.830      9.535      mm"
"      Runoff volume      11.67      58.89      70.56      c.m"
"      Runoff coefficient      0.062      0.941      0.282      "
"      Maximum flow      0.008      0.041      0.041      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"              0.041      0.537      0.000      0.000"
" 33  CATCHMENT 300"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      300 Catchment 300 - To Clythe Creek"
"      0.000 % Impervious"
"      6.480 Total Area"
"      45.000 Flow length"
"      2.000 Overland Slope"
"      6.480 Pervious Area"
"      45.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"

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"                                105172_POST_2yr UC
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      0.073      0.537      0.000      0.000 c.m/sec"
" Catchment 300 Pervious Impervious Total Area "
" Surface Area 6.480 0.000 6.480 hectare"
" Time of concentration 28.300 2.768 28.300 minutes"
" Time to Centroid 98.613 85.041 98.613 minutes"
" Rainfall depth 33.816 33.816 33.816 mm"
" Rainfall volume 2191.27 0.00 2191.27 c.m"
" Rainfall losses 31.709 2.082 31.709 mm"
" Runoff depth 2.107 31.734 2.107 mm"
" Runoff volume 136.54 0.00 136.55 c.m"
" Runoff coefficient 0.062 0.000 0.062 "
" Maximum flow 0.073 0.000 0.073 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      0.073      0.538      0.000      0.000"
" 64 SHOW TABLE"
" 2 Flow hydrograph"
" 4 Inflow Hydrograph"
" Maximum flow 0.538 c.m/sec"
" Hydrograph volume 937.732 c.m"
" 38 START/RE-START TOTALS 300"
" 3 Runoff Totals on EXIT"
" Total Catchment area 10.630 hectare"
" Total Impervious area 2.402 hectare"
" Total % impervious 22.592"
" 19 EXIT"

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"                                105172_POST_5yr UC
"                                ----->"
"                                MIDUSS Output
"                                MIDUSS version                      Version 2.25 rev. 473"
"                                MIDUSS created                      Sunday, February 07, 2010"
"                                10 Units used:                      ie METRIC"
"                                Job folder:                        W:\Guelph\105-2005\105172\Design Data\
"                                Modelling Files\MIDUSS\2016 Revisions"
"                                Output filename:                  105172_POST_5yr UC.out"
"                                Licensee name:                    gmbp"
"                                Company                            Hewlett-Packard Company"
"                                Date & Time last used:            6/2/2016 at 3:28:36 PM"
" 31 TIME PARAMETERS"
"      5.000 Time Step"
"      170.000 Max. Storm length"
"      1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
"      1 Chicago storm"
"      1593.000 Coefficient A"
"      11.000 Constant B"
"      0.879 Exponent C"
"      0.400 Fraction R"
"      170.000 Duration"
"      1.000 Time step multiplier"
"      Maximum intensity          134.894 mm/hr"
"      Total depth                46.775 mm"
"      6 005hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
"      1 Triangular scs"
"      1 Equal length"
"      2 Horton equation"
"      201 Catchment 201 - To Clythe Creeek"
"      65.000 % Impervious"
"      3.410 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      1.194 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      2.217 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"      0.675 0.000 0.000 0.000 c.m/sec"
"      Catchment 201 Pervious Impervious Total Area "
"      Surface Area 1.194 2.217 3.410 hectare"
"      Time of concentration 15.360 1.968 3.517 minutes"
"      Time to Centroid 88.710 82.363 83.097 minutes"
"      Rainfall depth 46.775 46.775 46.775 mm"
"      Rainfall volume 558.26 1036.77 1595.03 c.m"
"      Rainfall losses 35.929 2.131 13.960 mm"
"      Runoff depth 10.846 44.644 32.815 mm"
"      Runoff volume 129.45 989.54 1118.99 c.m"
"      Runoff coefficient 0.232 0.954 0.702 "
"      Maximum flow 0.099 0.665 0.675 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"          105172_POST_5yr UC
"      4  Add Runoff "
"          0.675      0.675      0.000      0.000"
33  CATCHMENT 202"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      202  Catchment 202 - To Clythe Creek"
"      25.000  % Impervious"
"      0.740  Total Area"
"      30.000  Flow length"
"      2.000  Overland Slope"
"      0.555  Pervious Area"
"      30.000  Pervious length"
"      2.000  Pervious slope"
"      0.185  Impervious Area"
"      30.000  Impervious length"
"      2.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      75.000  Pervious Max.infiltration"
"      12.500  Pervious Min.infiltration"
"      0.250  Pervious Lag constant (hours)"
"      5.000  Pervious Depression storage"
"      0.015  Impervious Manning 'n'"
"      0.000  Impervious Max.infiltration"
"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"          0.069      0.675      0.000      0.000 c.m/sec"
"      Catchment 202      Pervious      Impervious      Total Area "
"      Surface Area      0.555      0.185      0.740      hectare"
"      Time of concentration      15.360      1.968      7.614      minutes"
"      Time to Centroid      88.710      82.363      85.039      minutes"
"      Rainfall depth      46.775      46.775      46.775      mm"
"      Rainfall volume      259.60      86.53      346.14      c.m"
"      Rainfall losses      35.929      2.131      27.479      mm"
"      Runoff depth      10.846      44.644      19.296      mm"
"      Runoff volume      60.20      82.59      142.79      c.m"
"      Runoff coefficient      0.232      0.954      0.413      "
"      Maximum flow      0.046      0.055      0.069      c.m/sec"
40  HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"          0.069      0.735      0.000      0.000"
33  CATCHMENT 300"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      300  Catchment 300 - To Clythe Creek"
"      0.000  % Impervious"
"      6.480  Total Area"
"      45.000  Flow length"
"      2.000  Overland Slope"
"      6.480  Pervious Area"
"      45.000  Pervious length"
"      2.000  Pervious slope"
"      0.000  Impervious Area"
"      45.000  Impervious length"
"      2.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      75.000  Pervious Max.infiltration"
"      12.500  Pervious Min.infiltration"
"      0.250  Pervious Lag constant (hours)"
"      5.000  Pervious Depression storage"
"      0.015  Impervious Manning 'n'"

```

```

"                                105172_POST_5yr UC
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      0.444      0.735      0.000      0.000 c.m/sec"
" Catchment 300 Pervious Impervious Total Area "
" Surface Area 6.480 0.000 6.480 hectare"
" Time of concentration 19.590 2.510 19.590 minutes"
" Time to Centroid 92.382 83.161 92.382 minutes"
" Rainfall depth 46.775 46.775 46.775 mm"
" Rainfall volume 3031.02 0.00 3031.02 c.m"
" Rainfall losses 35.903 2.312 35.903 mm"
" Runoff depth 10.872 44.463 10.872 mm"
" Runoff volume 704.50 0.00 704.50 c.m"
" Runoff coefficient 0.232 0.000 0.232 "
" Maximum flow 0.444 0.000 0.444 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      0.444      0.868      0.000      0.000"
" 64 SHOW TABLE"
" 2 Flow hydrograph"
" 4 Inflow Hydrograph"
" Maximum flow 0.868 c.m/sec"
" Hydrograph volume 1966.276 c.m"
" 38 START/RE-START TOTALS 300"
" 3 Runoff Totals on EXIT"
" Total Catchment area 10.630 hectare"
" Total Impervious area 2.402 hectare"
" Total % impervious 22.592"
" 19 EXIT"

```

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"                                     105172_POST_25yr UC
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" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        w:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                   105172_POST_25yr UC.out"
" Licensee name:                     gmbp"
" Company                           Hewlett-Packard Company"
" Date & Time last used:             6/2/2016 at 3:30:00 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 210.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 3158.000 Coefficient A"
" 15.000 Constant B"
" 0.936 Exponent C"
" 0.400 Fraction R"
" 210.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                  169.546 mm/hr"
" Total depth                       69.476 mm"
" 6 025hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clyde Creek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.074 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 11.267 1.796 3.566 minutes"
" Time to Centroid 102.758 98.258 99.099 minutes"
" Rainfall depth 69.476 69.476 69.476 mm"
" Rainfall volume 829.20 1539.94 2369.15 c.m"
" Rainfall losses 40.822 2.348 15.814 mm"
" Runoff depth 28.654 67.128 53.663 mm"
" Runoff volume 341.99 1487.90 1829.89 c.m"
" Runoff coefficient 0.412 0.966 0.772 "
" Maximum flow 0.258 0.912 1.074 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"          105172_POST_25yr UC
"          4  Add Runoff "
"              1.074      1.074      0.000      0.000"
" 33  CATCHMENT 202"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      202 Catchment 202 - To Clythe Creek"
"      25.000 % Impervious"
"      0.740 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      0.555 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      0.185 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"              0.169      1.074      0.000      0.000 c.m/sec"
"      Catchment 202      Pervious      Impervious      Total Area "
"      Surface Area      0.555      0.185      0.740      hectare"
"      Time of concentration      11.267      1.796      7.114      minutes"
"      Time to Centroid      102.758      98.258      100.785      minutes"
"      Rainfall depth      69.476      69.476      69.476      mm"
"      Rainfall volume      385.59      128.53      514.13      c.m"
"      Rainfall losses      40.822      2.348      31.204      mm"
"      Runoff depth      28.654      67.128      38.273      mm"
"      Runoff volume      159.03      124.19      283.22      c.m"
"      Runoff coefficient      0.412      0.966      0.551      "
"      Maximum flow      0.120      0.076      0.169      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"              0.169      1.226      0.000      0.000"
" 33  CATCHMENT 300"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      300 Catchment 300 - To Clythe Creek"
"      0.000 % Impervious"
"      6.480 Total Area"
"      45.000 Flow length"
"      2.000 Overland Slope"
"      6.480 Pervious Area"
"      45.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"

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"      105172_POST_25yr UC
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      1.261      1.226      0.000      0.000 c.m/sec"
"      Catchment 300      Pervious      Impervious      Total Area "
"      Surface Area      6.480      0.000      6.480      hectare"
"      Time of concentration      14.371      2.291      14.371      minutes"
"      Time to Centroid      105.688      98.958      105.688      minutes"
"      Rainfall depth      69.476      69.476      69.476      mm"
"      Rainfall volume      4502.07      0.00      4502.07      c.m"
"      Rainfall losses      40.830      2.498      40.830      mm"
"      Runoff depth      28.647      66.978      28.647      mm"
"      Runoff volume      1856.30      0.00      1856.30      c.m"
"      Runoff coefficient      0.412      0.000      0.412      "
"      Maximum flow      1.261      0.000      1.261      c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      1.261      2.156      0.000      0.000"
" 64 SHOW TABLE"
" 2 Flow hydrograph"
" 4 Inflow Hydrograph"
"      Maximum flow      2.156      c.m/sec"
"      Hydrograph volume      3969.412      c.m"
" 38 START/RE-START TOTALS 300"
" 3 Runoff Totals on EXIT"
"      Total Catchment area      10.630      hectare"
"      Total Impervious area      2.402      hectare"
"      Total % impervious      22.592"
" 19 EXIT"

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"                                     105172_POST_100yr UC
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        w:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                    105172_POST_100yr UC.out"
" Licensee name:                      gmbp"
" Company                            Hewlett-Packard Company"
" Date & Time last used:              6/2/2016 at 3:31:23 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 210.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 4688.000 Coefficient A"
" 17.000 Constant B"
" 0.962 Exponent C"
" 0.400 Fraction R"
" 210.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                    213.574 mm/hr"
" Total depth                        88.830 mm"
" 6 100hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
" 1 Triangular scs"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clythe Creeek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.469 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 9.306 1.638 3.326 minutes"
" Time to Centroid 102.153 97.460 98.493 minutes"
" Rainfall depth 88.830 88.830 88.830 mm"
" Rainfall volume 1060.18 1968.91 3029.10 c.m"
" Rainfall losses 43.655 2.647 17.000 mm"
" Runoff depth 45.175 86.183 71.830 mm"
" Runoff volume 539.17 1910.24 2449.40 c.m"
" Runoff coefficient 0.509 0.970 0.809 "
" Maximum flow 0.418 1.149 1.469 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"          4  Add Runoff " 105172_POST_100yr UC
"          1.469 1.469 0.000 0.000"
" 33  CATCHMENT 202"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      202  Catchment 202 - To Clythe Creek"
"      25.000 % Impervious"
"      0.740 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      0.555 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      0.185 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"          0.256 1.469 0.000 0.000 c.m/sec"
"      Catchment 202 Pervious Impervious Total Area "
"      Surface Area 0.555 0.185 0.740 hectare"
"      Time of concentration 9.306 1.638 6.325 minutes"
"      Time to Centroid 102.153 97.460 100.328 minutes"
"      Rainfall depth 88.830 88.830 88.830 mm"
"      Rainfall volume 493.01 164.34 657.34 c.m"
"      Rainfall losses 43.655 2.647 33.403 mm"
"      Runoff depth 45.175 86.183 55.427 mm"
"      Runoff volume 250.72 159.44 410.16 c.m"
"      Runoff coefficient 0.509 0.970 0.624 "
"      Maximum flow 0.195 0.096 0.256 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"          0.256 1.714 0.000 0.000"
" 33  CATCHMENT 300"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      300  Catchment 300 - To Clythe Creek"
"      0.000 % Impervious"
"      6.480 Total Area"
"      45.000 Flow length"
"      2.000 Overland Slope"
"      6.480 Pervious Area"
"      45.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"

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"      105172_POST_100yr UC
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"      1.971 1.714 0.000 0.000 c.m/sec"
"      Catchment 300 Pervious Impervious Total Area "
"      Surface Area 6.480 0.000 6.480 hectare"
"      Time of concentration 11.869 2.089 11.869 minutes"
"      Time to Centroid 104.828 98.071 104.828 minutes"
"      Rainfall depth 88.830 88.830 88.830 mm"
"      Rainfall volume 5756.17 0.01 5756.17 c.m"
"      Rainfall losses 43.360 2.670 43.360 mm"
"      Runoff depth 45.470 86.160 45.470 mm"
"      Runoff volume 2946.46 0.01 2946.46 c.m"
"      Runoff coefficient 0.512 0.000 0.512 "
"      Maximum flow 1.971 0.000 1.971 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      1.971 3.386 0.000 0.000"
" 64 SHOW TABLE"
"      2 Flow hydrograph"
"      4 Inflow Hydrograph"
"      Maximum flow 3.386 c.m/sec"
"      Hydrograph volume 5806.026 c.m"
" 38 START/RE-START TOTALS 300"
"      3 Runoff Totals on EXIT"
"      Total Catchment area 10.630 hectare"
"      Total Impervious area 2.402 hectare"
"      Total % impervious 22.592"
" 19 EXIT"

```


105172_POST_Regional UC

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"      MIDUSS Output ----->"
"      MIDUSS version          Version 2.25 rev. 473"
"      MIDUSS created          Sunday, February 07, 2010"
"      10 Units used:          ie METRIC"
"      Job folder:             w:\Guelph\105-2005\105172\Design Data\
"                                Modelling Files\MIDUSS\2016 Revisions"
"      Output filename:        105172_POST_Regional UC.out"
"      Licensee name:          gmbp"
"      Company                 Hewlett-Packard Company"
"      Date & Time last used:   6/2/2016 at 3:36:32 PM"
" 31      TIME PARAMETERS"
"      60.000 Time Step"
"      2880.000 Max. Storm length"
"      3600.000 Max. Hydrograph"
" 32      STORM Historic"
"      5 Historic"
"      2880.000 Duration"
"      48.000 Rainfall intensity values"
"              2.028      2.028      2.028      2.028      2.028"
"              2.028      2.028      2.028      2.028      2.028"
"              2.028      2.028      2.028      2.028      2.028"
"              2.028      2.028      2.028      2.028      2.028"
"              2.028      2.028      2.028      2.028      2.028"
"              2.028      2.026      2.026      2.026      2.028"
"              2.026      6.000      4.000      6.000      13.000"
"              17.000     13.000     23.000     13.000     13.000"
"              53.000     38.000     13.000"
"      Maximum intensity          53.000 mm/hr"
"      Total depth                285.000 mm"
" 33      6 000hyd Hydrograph extension used in this file"
"      CATCHMENT 201"
"      1 Triangular scs"
"      1 Equal length"
"      2 Horton equation"
"      201 Catchment 201 - To Clythe Creeek"
"      65.000 % Impervious"
"      3.410 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      1.194 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      2.217 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"              0.376      0.000      0.000      0.000 c.m/sec"
"      Catchment 201      Pervious      Impervious      Total Area "
"      Surface Area      1.194      2.217      3.410      hectare"
"      Time of concentration      17.225      2.860      4.946      minutes"
"      Time to Centroid      2775.198      2251.465      2327.523      minutes"
"      Rainfall depth      285.000      285.000      285.000      mm"
"      Rainfall volume      3401.48      6317.02      9718.50      c.m"

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		105172_POST_Regional UC				
"		Rainfall losses	207.571	39.596	98.387	mm"
"		Runoff depth	77.429	245.404	186.613	mm"
"		Runoff volume	924.12	5439.38	6363.50	c.m"
"		Runoff coefficient	0.272	0.861	0.655	"
"		Maximum flow	0.094	0.282	0.376	c.m/sec"
" 40		HYDROGRAPH Add Runoff "				
"	4	Add Runoff "	0.376	0.000	0.000"	
" 33		CATCHMENT 202"				
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	202	Catchment 202 - To Clythe Creek"				
"	25.000	% Impervious"				
"	0.740	Total Area"				
"	30.000	Flow length"				
"	2.000	Overland Slope"				
"	0.555	Pervious Area"				
"	30.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.185	Impervious Area"				
"	30.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		0.067	0.376	0.000	0.000	c.m/sec"
"		Catchment 202	Pervious	Impervious	Total Area	"
"		Surface Area	0.555	0.185	0.740	hectare"
"		Time of concentration	17.225	2.860	9.845	minutes"
"		Time to Centroid	2775.197	2251.465	2506.141	minutes"
"		Rainfall depth	285.000	285.000	285.000	mm"
"		Rainfall volume	1581.75	527.25	2109.00	c.m"
"		Rainfall losses	207.571	39.596	165.577	mm"
"		Runoff depth	77.429	245.404	119.423	mm"
"		Runoff volume	429.73	454.00	883.73	c.m"
"		Runoff coefficient	0.272	0.861	0.419	"
"		Maximum flow	0.044	0.024	0.067	c.m/sec"
" 40		HYDROGRAPH Add Runoff "				
"	4	Add Runoff "	0.067	0.443	0.000	0.000"
" 33		CATCHMENT 300"				
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	300	Catchment 300 - To Clythe Creek"				
"	0.000	% Impervious"				
"	6.480	Total Area"				
"	45.000	Flow length"				
"	2.000	Overland Slope"				
"	6.480	Pervious Area"				
"	45.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.000	Impervious Area"				
"	45.000	Impervious length"				
"	2.000	Impervious slope"				

```

"          105172_POST_Regional UC
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"          0.538      0.443      0.000      0.000 c.m/sec"
" Catchment 300 Pervious Impervious Total Area "
" Surface Area 6.480 0.000 6.480 hectare"
" Time of concentration 21.969 3.647 21.969 minutes"
" Time to Centroid 2780.244 2236.986 2780.242 minutes"
" Rainfall depth 285.000 285.000 285.000 mm"
" Rainfall volume 1.8468 0.0000 1.8468 ha-m"
" Rainfall losses 206.992 38.537 206.992 mm"
" Runoff depth 78.008 246.463 78.008 mm"
" Runoff volume 5054.92 0.02 5054.94 c.m"
" Runoff coefficient 0.274 0.000 0.274 "
" Maximum flow 0.538 0.000 0.538 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"          0.538      0.911      0.000      0.000"
" 64 SHOW TABLE"
" 2 Flow hydrograph"
" 4 Inflow Hydrograph"
" Maximum flow 0.911 c.m/sec"
" Hydrograph volume 12302.162 c.m"
" 38 START/RE-START TOTALS 300"
" 3 Runoff Totals on EXIT"
" Total Catchment area 10.630 hectare"
" Total Impervious area 2.402 hectare"
" Total % impervious 22.592"
" 19 EXIT"

```

Cityview Ridge Subdivision (Formerly P.T. Valeriotte Property)
City of Guelph
Our File: 105-172
June 2016

Catchment 201 - Proposed Stormwater Management Facility

STORAGE VOLUME CALCULATIONS						
Elevation	Depth	Surface Area	Permanent Pool Volume	Accumulated Perm. Pool Volume	Incremental Storage Volume	Accum. Inc. Storage Volume
(m)	(m)	(m ²)	(m ³)	(m ³)	(m ³)	(m ³)
339.35	0.00	1486.7	0.0	0.0		Bottom of Pond
339.45	0.10	1618.7	155.3	155.3		
339.55	0.20	1779.1	169.9	325.2		
339.65	0.30	1941.5	186.0	511.2		
339.75	0.40	2092.1	201.7	712.9	0.0	0.0
339.85	0.50	2253.8			217.3	217.3
339.95	0.60	2417.1			233.5	450.8
340.05	0.70	2581.7			249.9	700.8
340.15	0.80	2748.8			266.5	967.3
340.25	0.90	2918.6			283.4	1250.7
340.35	1.00	3090.9			300.5	1551.1
340.45	1.10	3265.6			317.8	1869.0
340.55	1.20	3442.9			335.4	2204.4
340.65	1.30	3622.9			353.3	2557.7
340.75	1.40	3805.4			371.4	2929.1
340.85	1.50	3990.6			389.8	3318.9
340.95	1.60	4178.4			408.4	3727.4
341.05	1.70	4335.3			425.7	4153.0
341.15	1.80	4497.0			441.6	4594.6
						Weir Elevation
						Top of Bank

CB Lip Elevation

Cityview Ridge Subdivision (Formerly P.T. Valeriotte Property)
City of Guelph
Our File: 105-172
June 2016

Catchment 201 - Proposed Stormwater Management Facility (continued)

WEIR CALCULATIONS

ORIFICE CALCULATIONS
 375 mm Diameter Outlet Pipe
 Invert Elevation = 338.20 m

ORIFICE CALCULATIONS
 90 mm Diameter Knockout
 Invert Elevation = 339.75 m

d1 =	1.80	m	Q =	0.470	m ³ /s	Q =	0.011	m ³ /s
h =	1.60	m	Cd =	0.6		Cd =	0.6	
H =	0.20	m	H =	2.763	m	H =	0.455	m
2g =	19.62		2g =	19.62		2g =	19.62	
L =	10	m	A =	0.110	m ²	A =	0.006	m ²
			D =	0.375	m	D =	0.090	m
Q =	1.2482	cu m/s	D/2	0.188		D/2	0.045	m

STAGE/STORAGE/DISCHARGE TABLE

Elevation (m)	Stage (m)	Storage (m ³)	Orifice Control 90 mm	Orifice Control 375 mm	Weir	Discharge (m ³ /s)	
339.75	0.00	0.0	0.000	0.00	0.00	0.000	Top of Permanent Pool
339.85	0.10	217.3	0.004	0.00	0.00	0.004	
339.95	0.20	450.8	0.007	0.00	0.00	0.007	
340.05	0.30	700.8	0.009	0.00	0.00	0.009	
340.15	0.40	967.3	0.010	0.00	0.00	0.010	
340.25	0.50	1250.7	0.011	0.00	0.00	0.011	CB Lip Elevation
340.35	0.60	1551.1	0.000	0.411	0.00	0.411	
340.45	0.70	1869.0	0.000	0.422	0.00	0.422	
340.55	0.80	2204.4	0.000	0.432	0.00	0.432	
340.65	0.90	2557.7	0.000	0.442	0.00	0.442	
340.75	1.00	2929.1	0.000	0.451	0.00	0.451	
340.85	1.10	3318.9	0.000	0.461	0.00	0.461	
340.95	1.20	3727.4	0.000	0.470	0.00	0.470	Weir Elevation
341.05	1.30	4153.0	0.000	0.479	0.4353	0.914	
341.15	1.40	4594.6	0.000	0.488	1.2482	1.736	Top of Bank

Cityview Ridge Subdivision (Formerly P.T. Valeriote Property)
City of Guelph
Our File: 105-172
June 2016

Catchment 202 - Energy Dissipation/Dispersion Structure

STORAGE VOLUME TABLE				
Elevation (m)	Depth (m)	Surface Area (m ²)	Increm. Storage (m ³)	Total Storage (m ³)
336.00	0.00	130.00	0.00	0.00
336.10	0.10	130.00	4.33	4.33
336.20	0.20	130.00	4.33	8.67
336.30	0.30	130.00	4.33	13.00
336.40	0.40	130.00	4.33	17.33
336.50	0.50	130.00	4.33	21.67
336.60	0.60	130.00	4.33	26.00
336.70	0.70	130.00	4.33	30.33
336.80	0.80	130.00	4.33	34.67
336.90	0.90	130.00	7.20	41.87
337.00	1.00	130.00	8.20	50.07
337.10	1.10	130.00	9.20	59.27
				Top of Stone / Weir Overflow

Cityview Ridge Subdivision (Formerly P.T. Valeriot Property)
City of Guelph
Our File: 105-172
June 2016

Catchment 202 - Energy Dissipation/Dispersion Structure (continued)

BOTTOM		SIDES		OVERFLOW WEIR	
L(dw) =	m	L(dw) =	m	d1 =	m
W(dw) =	m			h =	m
D(dw) =	m	D(dw) =	m	H =	m
				2g =	19.62
A(c) =	m ²	A(c) =	sq m	L =	48.50
VOL(dw) =	m ³				
VOL(st) =	m ³			Q =	2.1290
K =	cm/s	K =	cm/s		m ³ /s
	1.00E-04		1.00E-04		

STORAGE VOLUME TABLE

Elevation (m)	Stage (m)	Storage (m³)	Infiltration		Weir		Total	
			Discharge (m³/s)	(m³/s)	Discharge (m³/s)	(m³/s)	Discharge (m³/s)	(m³/s)
336.00	0.00	0.0	0.0000	0.0000	0.0000	0.0000	0.0000	Bottom of Stone
336.10	0.10	4.3	0.0001	0.0000	0.0000	0.0001	0.0001	
336.20	0.20	8.7	0.0002	0.0000	0.0000	0.0002	0.0002	
336.30	0.30	13.0	0.0002	0.0000	0.0000	0.0002	0.0002	
336.40	0.40	17.3	0.0002	0.0000	0.0000	0.0002	0.0002	
336.50	0.50	21.7	0.0002	0.0000	0.0000	0.0002	0.0002	
336.60	0.60	26.0	0.0002	0.0000	0.0000	0.0002	0.0002	
336.70	0.70	30.3	0.0002	0.0000	0.0000	0.0002	0.0002	
336.80	0.80	34.7	0.0002	0.0000	0.0000	0.0002	0.0002	
336.90	0.90	41.9	0.0002	0.0000	0.0000	0.0002	0.0002	
337.00	1.00	50.1	0.0003	0.0000	0.0000	0.0003	0.0003	Top of Stone / Weir
337.10	1.10	59.3	0.0003	0.0000	2.1290	2.1292	2.1292	Overflow

Cityview Ridge Subdivision (Formerly P.T. Valeriote Property)
City of Guelph
Our File: 105-172
June 2016

Catchment B2a: Existing Stormwater Quality Pond No. 2

Elevation	Stage Storage Discharge Calculations				
	Stage	Surface Area	Incremental Storage Volume	Accumulated Storage Volume	
(m)	(m)	(m²)	(m³)	(m³)	
321.50	0.00	5,688.0	0.00	0.00	Pond Bottom
321.60	0.10	5,900.0	579.40	579.40	
321.70	0.20	6,110.0	600.50	1,179.90	
321.80	0.30	6,323.0	621.65	1,801.55	
321.90	0.40	6,537.0	643.00	2,444.55	
322.00	0.50	6,752.0	664.45	3,109.00	
322.10	0.60	6,967.0	685.95	3,794.95	
322.20	0.70	7,184.0	707.55	4,502.50	Weir
322.30	0.80	7,401.0	729.25	5,231.75	
322.40	0.90	7,619.0	751.00	5,982.75	
322.50	1.00	7,839.0	772.90	6,755.65	Overflow

Cityview Ridge Subdivision (Formerly P.T. Valeriote Property)
City of Guelph
Our File: 105-172
June 2016

Catchment B2a: Existing Stormwater Quality Pond No. 2 (continued)

OUTLET #1

300 mm diameter orifice (pipe inv. = 319.55)

OVERFLOW WEIR

Q =	0.303	m ³ /s	d1 =	1.00	m
Cd =	0.6		h =	0.70	m
H =	2.60	m	H =	0.30	m
2g =	19.62		2g =	19.62	
A =	0.071	m ²	L =	30.00	m
D =	0.300	m	Q =	7.251	m ³ /s
D/2	0.150				

Stage/Storage/Discharge Table

Elevation	Stage	Storage	Outlet #1 1050 mm dia. pipe	Overflow Weir	Total Discharge
(m)	(m)	(m ³)	(m ³ /s)	(m ³ /s)	(m ³ /s)
321.50	0.00	0.00	0.000	0.000	0.000
321.60	0.10	579.40	0.259	0.000	0.259
321.70	0.20	1,179.90	0.266	0.000	0.266
321.80	0.30	1,801.55	0.272	0.000	0.272
321.90	0.40	2,444.55	0.279	0.000	0.279
322.00	0.50	3,109.00	0.285	0.000	0.285
322.10	0.60	3,794.95	0.291	0.000	0.291
322.20	0.70	4,502.50	0.297	0.000	0.297
322.30	0.80	5,231.75	0.303	1.329	1.632
322.40	0.90	5,982.75	0.309	3.860	4.168
322.50	1.00	6,755.65	0.314	7.251	7.566
					Pond Bottom
					Weir
					Overflow

```

"                                     105172_POST_2yr
"
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        w:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                    105172_POST_2yr.out"
" Licensee name:                      gmbp"
" Company                            Hewlett-Packard Company"
" Date & Time last used:              6/2/2016 at 4:05:28 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 170.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 743.000 Coefficient A"
" 6.000 Constant B"
" 0.799 Exponent C"
" 0.400 Fraction R"
" 170.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                    105.606 mm/hr"
" Total depth                        33.816 mm"
" 6 002hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clyde Creek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 0.496 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 22.189 2.170 2.858 minutes"
" Time to Centroid 93.436 84.151 84.470 minutes"
" Rainfall depth 33.816 33.816 33.816 mm"
" Rainfall volume 403.59 749.53 1153.12 c.m"
" Rainfall losses 31.713 1.985 12.390 mm"
" Runoff depth 2.103 31.830 21.426 mm"
" Runoff volume 25.10 705.52 730.63 c.m"
" Runoff coefficient 0.062 0.941 0.634 "
" Maximum flow 0.017 0.496 0.496 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

```

```

"                                     105172_POST_2yr
"
"      4  Add Runoff "
"      0.496      0.496      0.000      0.000"
" 54  POND DESIGN"
"      0.496  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      730.6  Hydrograph volume      c.m"
"      15.    Number of stages"
"      0.000  Minimum water level      metre"
"      3.000  Maximum water level      metre"
"      0.000  Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      Volume"
"      339.750      0.000      0.000"
"      339.850      0.00400      217.300"
"      339.950      0.00700      450.800"
"      340.050      0.00900      700.800"
"      340.150      0.01000      967.300"
"      340.250      0.01100      1250.700"
"      340.350      0.4110      1551.100"
"      340.450      0.4220      1869.000"
"      340.550      0.4320      2204.400"
"      340.650      0.4420      2557.700"
"      340.750      0.4510      2929.100"
"      340.850      0.4610      3318.900"
"      340.950      0.4700      3727.400"
"      341.050      0.9140      4153.000"
"      341.150      1.736      4594.600"
"      Peak outflow      0.009      c.m/sec"
"      Maximum level      340.039      metre"
"      Maximum storage      673.523      c.m"
"      Centroidal lag      17.512      hours"
"      0.496      0.496      0.009      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.496      0.009      0.009      0.000"
" 51  PIPE DESIGN"
"      0.009  Current peak flow      c.m/sec"
"      0.013  Manning 'n'"
"      0.450  Diameter      metre"
"      4.420  Gradient      %"
"      Depth of flow      0.038      metre"
"      Velocity      1.359      m/sec"
"      Pipe capacity      0.599      c.m/sec"
"      Critical depth      0.063      metre"
" 53  ROUTE      Pipe Route 19"
"      19.20      Pipe Route 19 Reach length      ( metre)"
"      0.488      x-factor <= 0.5"
"      10.600      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      x-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.500      Beta weighting factor"
"      10.714      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      0.009      c.m/sec"
"      0.496      0.009      0.009      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.496      0.009      0.009      0.000"
" 54  POND DESIGN"
"      0.009  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      540.4  Hydrograph volume      c.m"

```

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"                                     105172_POST_2yr
"
" 12. Number of stages"
" 0.000 Minimum water level      metre"
" 3.000 Maximum water level      metre"
" 0.000 Starting water level     metre"
" 0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      Volume"
"      336.000      0.000      0.000"
"      336.100      1.00E-05      4.300"
"      336.200      2.00E-05      8.700"
"      336.300      3.00E-05      13.000"
"      336.400      4.00E-05      17.300"
"      336.500      5.00E-05      21.700"
"      336.600      6.00E-05      26.000"
"      336.700      7.00E-05      30.300"
"      336.800      8.00E-05      34.700"
"      336.900      9.00E-05      41.900"
"      337.000      1.00E-04      50.100"
"      337.100      2.129      59.300"
"      Peak outflow      0.009      c.m/sec"
"      Maximum level      337.000      metre"
"      Maximum storage      50.138      c.m"
"      Centroidal lag      13.761      hours"
"      0.496      0.009      0.009      0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
"      0.496      0.009      0.009      0.000"
52 CHANNEL DESIGN"
" 0.009 Current peak flow      c.m/sec"
" 0.065 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 65.000 Basewidth      metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 0.100 Channel depth      metre"
" 18.000 Gradient      %"
"      Depth of flow      0.002      metre"
"      Velocity      0.088      m/sec"
"      Channel capacity      9.152      c.m/sec"
"      Critical depth      0.001      metre"
53 ROUTE channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.500 X-factor <= 0.5"
" 212.649 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
"      Peak outflow      0.009      c.m/sec"
"      0.496      0.009      0.009      0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
"      0.496      0.009      0.009      0.000"
33 CATCHMENT 202"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 202 Catchment 202 - To Clythe Creeek"
" 25.000 % Impervious"
" 0.740 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"

```

105172_POST_2yr

"	0.555	Pervious Area"				
"	30.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.185	Impervious Area"				
"	30.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		0.041 0.009 0.009 0.000 c.m/sec"				
"		Catchment 202 Pervious Impervious Total Area "				
"		Surface Area 0.555 0.185 0.740 hectare"				
"		Time of concentration 22.189 2.170 5.482 minutes"				
"		Time to Centroid 93.436 84.151 85.688 minutes"				
"		Rainfall depth 33.816 33.816 33.816 mm"				
"		Rainfall volume 187.68 62.56 250.24 c.m"				
"		Rainfall losses 31.713 1.985 24.281 mm"				
"		Runoff depth 2.103 31.830 9.535 mm"				
"		Runoff volume 11.67 58.89 70.56 c.m"				
"		Runoff coefficient 0.062 0.941 0.282 "				
"		Maximum flow 0.008 0.041 0.041 c.m/sec"				
40		HYDROGRAPH Add Runoff "				
"	4	Add Runoff "				
"		0.041 0.041 0.009 0.000"				
33		CATCHMENT 300"				
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	300	Catchment 300 - To Clyde Creek"				
"	0.000	% Impervious"				
"	6.480	Total Area"				
"	45.000	Flow length"				
"	2.000	overland Slope"				
"	6.480	Pervious Area"				
"	45.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.000	Impervious Area"				
"	45.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		0.073 0.041 0.009 0.000 c.m/sec"				
"		Catchment 300 Pervious Impervious Total Area "				
"		Surface Area 6.480 0.000 6.480 hectare"				
"		Time of concentration 28.300 2.768 28.300 minutes"				
"		Time to Centroid 98.613 85.041 98.613 minutes"				
"		Rainfall depth 33.816 33.816 33.816 mm"				
"		Rainfall volume 2191.27 0.00 2191.27 c.m"				

		105172_POST_2yr			
"	Rainfall losses	31.709	2.082	31.709	mm"
"	Runoff depth	2.107	31.734	2.107	mm"
"	Runoff volume	136.54	0.00	136.55	c.m"
"	Runoff coefficient	0.062	0.000	0.062	"
"	Maximum flow	0.073	0.000	0.073	c.m/sec"
" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.073	0.086	0.009	0.000"
" 64	SHOW TABLE"				
"	2 Flow hydrograph"				
"	4 Inflow Hydrograph"				
"	Maximum flow		0.086	c.m/sec"	
"	Hydrograph volume		695.173	c.m"	
" 38	START/RE-START TOTALS 300"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area			10.630	hectare"
"	Total Impervious area			2.402	hectare"
"	Total % impervious			22.592"	
" 19	EXIT"				

```

"                                     105172_POST_5yr
"
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        W:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                    105172_POST_5yr.out"
" Licensee name:                      gmbp"
" Company                            Hewlett-Packard Company"
" Date & Time last used:              6/2/2016 at 4:08:30 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 170.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 1593.000 Coefficient A"
" 11.000 Constant B"
" 0.879 Exponent C"
" 0.400 Fraction R"
" 170.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                  134.894 mm/hr"
" Total depth                       46.775 mm"
" 6 005hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clyde Creek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 0.675 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 15.360 1.968 3.517 minutes"
" Time to Centroid 88.710 82.363 83.097 minutes"
" Rainfall depth 46.775 46.775 46.775 mm"
" Rainfall volume 558.26 1036.77 1595.03 c.m"
" Rainfall losses 35.929 2.131 13.960 mm"
" Runoff depth 10.846 44.644 32.815 mm"
" Runoff volume 129.45 989.54 1118.99 c.m"
" Runoff coefficient 0.232 0.954 0.702 "
" Maximum flow 0.099 0.665 0.675 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

```

```

"                                     105172_POST_5yr
"      4  Add Runoff "
"      0.675      0.675      0.000      0.000"
" 54  POND DESIGN"
"      0.675  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      1119.0  Hydrograph volume      c.m"
"      15.    Number of stages"
"      0.000  Minimum water level      metre"
"      3.000  Maximum water level      metre"
"      0.000  Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      Volume"
"      339.750      0.000      0.000"
"      339.850      0.00400      217.300"
"      339.950      0.00700      450.800"
"      340.050      0.00900      700.800"
"      340.150      0.01000      967.300"
"      340.250      0.01100      1250.700"
"      340.350      0.4110      1551.100"
"      340.450      0.4220      1869.000"
"      340.550      0.4320      2204.400"
"      340.650      0.4420      2557.700"
"      340.750      0.4510      2929.100"
"      340.850      0.4610      3318.900"
"      340.950      0.4700      3727.400"
"      341.050      0.9140      4153.000"
"      341.150      1.736      4594.600"
"      Peak outflow      0.010      c.m/sec"
"      Maximum level      340.179      metre"
"      Maximum storage      1049.820      c.m"
"      Centroidal lag      20.307      hours"
"      0.675      0.675      0.010      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.675      0.010      0.010      0.000"
" 51  PIPE DESIGN"
"      0.010  Current peak flow      c.m/sec"
"      0.013  Manning 'n'"
"      0.450  Diameter      metre"
"      4.420  Gradient      %"
"      Depth of flow      0.041      metre"
"      Velocity      1.425      m/sec"
"      Pipe capacity      0.599      c.m/sec"
"      Critical depth      0.068      metre"
" 53  ROUTE      Pipe Route 19"
"      19.20      Pipe Route 19 Reach length      ( metre)"
"      0.487      X-factor <= 0.5"
"      10.104      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.500      Beta weighting factor"
"      10.345      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      0.010      c.m/sec"
"      0.675      0.010      0.010      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.675      0.010      0.010      0.000"
" 54  POND DESIGN"
"      0.010  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      743.2  Hydrograph volume      c.m"

```



```

105172_POST_5yr
"      12.  Number of stages"
"      0.000  Minimum water level      metre"
"      3.000  Maximum water level      metre"
"      0.000  Starting water level     metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"      Level Discharge  Volume"
"      336.000      0.000      0.000"
"      336.100      1.00E-05      4.300"
"      336.200      2.00E-05      8.700"
"      336.300      3.00E-05      13.000"
"      336.400      4.00E-05      17.300"
"      336.500      5.00E-05      21.700"
"      336.600      6.00E-05      26.000"
"      336.700      7.00E-05      30.300"
"      336.800      8.00E-05      34.700"
"      336.900      9.00E-05      41.900"
"      337.000      1.00E-04      50.100"
"      337.100      2.129      59.300"
"      Peak outflow      0.010      c.m/sec"
"      Maximum level      337.000      metre"
"      Maximum storage      50.144      c.m"
"      Centroidal lag      13.776      hours"
"      0.675      0.010      0.010      0.000 c.m/sec"
40      HYDROGRAPH Next link "
"      5      Next link "
"      0.675      0.010      0.010      0.000"
52      CHANNEL DESIGN"
"      0.010      Current peak flow      c.m/sec"
"      0.065      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; 1=general"
"      65.000      Basewidth      metre"
"      3.000      Left bank slope"
"      3.000      Right bank slope"
"      0.100      channel depth      metre"
"      18.000      Gradient      %"
"      Depth of flow      0.002      metre"
"      Velocity      0.092      m/sec"
"      Channel capacity      9.152      c.m/sec"
"      Critical depth      0.001      metre"
53      ROUTE      Channel Route 50"
"      50.00      Channel Route 50 Reach length      ( metre)"
"      0.500      X-factor <= 0.5"
"      203.874      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.500      Beta weighting factor"
"      300.000      Routing time step      ( seconds)"
"      2      No. of sub-reaches"
"      Peak outflow      0.010      c.m/sec"
"      0.675      0.010      0.010      0.000 c.m/sec"
40      HYDROGRAPH Next link "
"      5      Next link "
"      0.675      0.010      0.010      0.000"
33      CATCHMENT 202"
"      1      Triangular scs"
"      1      Equal length"
"      2      Horton equation"
"      202      Catchment 202 - To Clythe Creeek"
"      25.000      % Impervious"
"      0.740      Total Area"
"      30.000      Flow length"
"      2.000      Overland Slope"

```

105172_POST_5yr

"	0.555	Pervious Area"			
"	30.000	Pervious length"			
"	2.000	Pervious slope"			
"	0.185	Impervious Area"			
"	30.000	Impervious length"			
"	2.000	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious Max.infiltration"			
"	12.500	Pervious Min.infiltration"			
"	0.250	Pervious Lag constant (hours)"			
"	5.000	Pervious Depression storage"			
"	0.015	Impervious Manning 'n'"			
"	0.000	Impervious Max.infiltration"			
"	0.000	Impervious Min.infiltration"			
"	0.050	Impervious Lag constant (hours)"			
"	1.500	Impervious Depression storage"			
"		0.069 0.010 0.010 0.000 c.m/sec"			
"		Catchment 202 Pervious Impervious Total Area "			
"		Surface Area 0.555 0.185 0.740 hectare"			
"		Time of concentration 15.360 1.968 7.614 minutes"			
"		Time to Centroid 88.710 82.363 85.039 minutes"			
"		Rainfall depth 46.775 46.775 46.775 mm"			
"		Rainfall volume 259.60 86.53 346.14 c.m"			
"		Rainfall losses 35.929 2.131 27.479 mm"			
"		Runoff depth 10.846 44.644 19.296 mm"			
"		Runoff volume 60.20 82.59 142.79 c.m"			
"		Runoff coefficient 0.232 0.954 0.413 "			
"		Maximum flow 0.046 0.055 0.069 c.m/sec"			
40		HYDROGRAPH Add Runoff "			
"	4	Add Runoff "			
"		0.069 0.069 0.010 0.000"			
33		CATCHMENT 300"			
"	1	Triangular SCS"			
"	1	Equal length"			
"	2	Horton equation"			
"	300	Catchment 300 - To Clyde Creek"			
"	0.000	% Impervious"			
"	6.480	Total Area"			
"	45.000	Flow length"			
"	2.000	overland Slope"			
"	6.480	Pervious Area"			
"	45.000	Pervious length"			
"	2.000	Pervious slope"			
"	0.000	Impervious Area"			
"	45.000	Impervious length"			
"	2.000	Impervious slope"			
"	0.250	Pervious Manning 'n'"			
"	75.000	Pervious Max.infiltration"			
"	12.500	Pervious Min.infiltration"			
"	0.250	Pervious Lag constant (hours)"			
"	5.000	Pervious Depression storage"			
"	0.015	Impervious Manning 'n'"			
"	0.000	Impervious Max.infiltration"			
"	0.000	Impervious Min.infiltration"			
"	0.050	Impervious Lag constant (hours)"			
"	1.500	Impervious Depression storage"			
"		0.444 0.069 0.010 0.000 c.m/sec"			
"		Catchment 300 Pervious Impervious Total Area "			
"		Surface Area 6.480 0.000 6.480 hectare"			
"		Time of concentration 19.590 2.510 19.590 minutes"			
"		Time to Centroid 92.382 83.161 92.382 minutes"			
"		Rainfall depth 46.775 46.775 46.775 mm"			
"		Rainfall volume 3031.02 0.00 3031.02 c.m"			

		105172_POST_5yr			
"	Rainfall losses	35.903	2.312	35.903	mm"
"	Runoff depth	10.872	44.463	10.872	mm"
"	Runoff volume	704.50	0.00	704.50	c.m"
"	Runoff coefficient	0.232	0.000	0.232	"
"	Maximum flow	0.444	0.000	0.444	c.m/sec"
" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.444	0.507	0.010	0.000"
" 64	SHOW TABLE"				
"	2 Flow hydrograph"				
"	4 Inflow Hydrograph"				
"	Maximum flow		0.507	c.m/sec"	
"	Hydrograph volume		1538.107	c.m"	
" 38	START/RE-START TOTALS 300"				
"	3 Runoff Totals on EXIT"				
"	Total Catchment area			10.630	hectare"
"	Total Impervious area			2.402	hectare"
"	Total % impervious			22.592"	
" 19	EXIT"				

```

"                                     105172_POST_25yr
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        W:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                    105172_POST_25yr.out"
" Licensee name:                      gmbp"
" Company                            Hewlett-Packard Company"
" Date & Time last used:              6/2/2016 at 4:10:20 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 210.000 Max. Storm length"
" 1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 3158.000 Coefficient A"
" 15.000 Constant B"
" 0.936 Exponent C"
" 0.400 Fraction R"
" 210.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity                    169.546 mm/hr"
" Total depth                          69.476 mm"
" 6 025hyd Hydrograph extension used in this file"
" 33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clythe Creeek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
" 1.074 0.000 0.000 0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area 1.194 2.217 3.410 hectare"
" Time of concentration 11.267 2.796 3.566 minutes"
" Time to Centroid 102.758 98.258 99.099 minutes"
" Rainfall depth 69.476 69.476 69.476 mm"
" Rainfall volume 829.20 1539.94 2369.15 c.m"
" Rainfall losses 40.822 2.348 15.814 mm"
" Runoff depth 28.654 67.128 53.663 mm"
" Runoff volume 341.99 1487.90 1829.89 c.m"
" Runoff coefficient 0.412 0.966 0.772 "
" Maximum flow 0.258 0.912 1.074 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"                                105172_POST_25yr
"      4  Add Runoff "
"      1.074      1.074      0.000      0.000"
" 54  POND DESIGN"
"      1.074 Current peak flow      c.m/sec"
"      0.171 Target outflow      c.m/sec"
"      1829.9 Hydrograph volume      c.m"
"      15. Number of stages"
"      0.000 Minimum water level      metre"
"      3.000 Maximum water level      metre"
"      0.000 Starting water level      metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      Volume"
"      339.750      0.000      0.000"
"      339.850      0.00400      217.300"
"      339.950      0.00700      450.800"
"      340.050      0.00900      700.800"
"      340.150      0.01000      967.300"
"      340.250      0.01100      1250.700"
"      340.350      0.4110      1551.100"
"      340.450      0.4220      1869.000"
"      340.550      0.4320      2204.400"
"      340.650      0.4420      2557.700"
"      340.750      0.4510      2929.100"
"      340.850      0.4610      3318.900"
"      340.950      0.4700      3727.400"
"      341.050      0.9140      4153.000"
"      341.150      1.736      4594.600"
"      Peak outflow      0.196      c.m/sec"
"      Maximum level      340.296      metre"
"      Maximum storage      1390.030      c.m"
"      Centroidal lag      17.013      hours"
"      1.074      1.074      0.196      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link "
"      1.074      0.196      0.196      0.000"
" 51  PIPE DESIGN"
"      0.196 Current peak flow      c.m/sec"
"      0.013 Manning 'n'"
"      0.450 Diameter      metre"
"      4.420 Gradient      %"
"      Depth of flow      0.177      metre"
"      Velocity      3.375      m/sec"
"      Pipe capacity      0.599      c.m/sec"
"      Critical depth      0.312      metre"
" 53  ROUTE Pipe Route 19"
"      19.20 Pipe Route 19 Reach length (metre)"
"      0.441 X-factor <= 0.5"
"      4.267 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      4.762 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.196      c.m/sec"
"      1.074      0.196      0.196      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link "
"      1.074      0.196      0.196      0.000"
" 54  POND DESIGN"
"      0.196 Current peak flow      c.m/sec"
"      0.171 Target outflow      c.m/sec"
"      1306.6 Hydrograph volume      c.m"

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"                                     105172_POST_25yr
"
" 12. Number of stages"
" 0.000 Minimum water level      metre"
" 3.000 Maximum water level      metre"
" 0.000 Starting water level     metre"
" 0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      Volume"
"      336.000      0.000      0.000"
"      336.100      1.00E-05      4.300"
"      336.200      2.00E-05      8.700"
"      336.300      3.00E-05      13.000"
"      336.400      4.00E-05      17.300"
"      336.500      5.00E-05      21.700"
"      336.600      6.00E-05      26.000"
"      336.700      7.00E-05      30.300"
"      336.800      8.00E-05      34.700"
"      336.900      9.00E-05      41.900"
"      337.000      1.00E-04      50.100"
"      337.100      2.129      59.300"
"      Peak outflow      0.196      c.m/sec"
"      Maximum level      337.009      metre"
"      Maximum storage      50.948      c.m"
"      Centroidal lag      9.663      hours"
"      1.074      0.196      0.196      0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
"      1.074      0.196      0.196      0.000"
52 CHANNEL DESIGN"
" 0.196 Current peak flow      c.m/sec"
" 0.065 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 65.000 Basewidth      metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 0.100 channel depth      metre"
" 18.000 Gradient      %"
"      Depth of flow      0.010      metre"
"      Velocity      0.302      m/sec"
"      Channel capacity      9.152      c.m/sec"
"      Critical depth      0.010      metre"
53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.500 x-factor <= 0.5"
" 124.059 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 x-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
"      Peak outflow      0.192      c.m/sec"
"      1.074      0.196      0.192      0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
"      1.074      0.192      0.192      0.000"
33 CATCHMENT 202"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 202 Catchment 202 - To Clythe Creeek"
" 25.000 % Impervious"
" 0.740 Total Area"
" 30.000 Flow length"
" 2.000 overland Slope"

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105172_POST_25yr

"	0.555	Pervious Area"				
"	30.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.185	Impervious Area"				
"	30.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		0.169	0.192	0.192	0.000 c.m/sec"	
"		Catchment 202	Pervious	Impervious	Total Area	"
"		Surface Area	0.555	0.185	0.740	hectare"
"		Time of concentration	11.267	1.796	7.114	minutes"
"		Time to Centroid	102.758	98.258	100.785	minutes"
"		Rainfall depth	69.476	69.476	69.476	mm"
"		Rainfall volume	385.59	128.53	514.13	c.m"
"		Rainfall losses	40.822	2.348	31.204	mm"
"		Runoff depth	28.654	67.128	38.273	mm"
"		Runoff volume	159.03	124.19	283.22	c.m"
"		Runoff coefficient	0.412	0.966	0.551	"
"		Maximum flow	0.120	0.076	0.169	c.m/sec"
40		HYDROGRAPH Add Runoff "				
"	4	Add Runoff "				
"		0.169	0.229	0.192	0.000"	
33		CATCHMENT 300"				
"	1	Triangular SCS"				
"	1	Equal length"				
"	2	Horton equation"				
"	300	Catchment 300 - To Clythe Creek"				
"	0.000	% Impervious"				
"	6.480	Total Area"				
"	45.000	Flow length"				
"	2.000	Overland Slope"				
"	6.480	Pervious Area"				
"	45.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.000	Impervious Area"				
"	45.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		1.261	0.229	0.192	0.000 c.m/sec"	
"		Catchment 300	Pervious	Impervious	Total Area	"
"		Surface Area	6.480	0.000	6.480	hectare"
"		Time of concentration	14.371	2.291	14.371	minutes"
"		Time to Centroid	105.688	98.958	105.688	minutes"
"		Rainfall depth	69.476	69.476	69.476	mm"
"		Rainfall volume	4502.07	0.00	4502.07	c.m"

		105172_POST_25yr		
"	Rainfall losses	40.830	2.498	40.830 mm"
"	Runoff depth	28.647	66.978	28.647 mm"
"	Runoff volume	1856.30	0.00	1856.30 c.m"
"	Runoff coefficient	0.412	0.000	0.412 "
"	Maximum flow	1.261	0.000	1.261 c.m/sec"
" 40	HYDROGRAPH Add Runoff "			
"	4 Add Runoff "			
"		1.261	1.400	0.192 0.000"
" 64	SHOW TABLE"			
"	2 Flow hydrograph"			
"	4 Inflow Hydrograph"			
"	Maximum flow	1.400		c.m/sec"
"	Hydrograph volume	3394.234		c.m"
" 38	START/RE-START TOTALS 300"			
"	3 Runoff Totals on EXIT"			
"	Total Catchment area		10.630	hectare"
"	Total Impervious area		2.402	hectare"
"	Total % impervious		22.592"	
" 19	EXIT"			


```

"                                105172_POST_100yr
"                                MIDUSS Output ----->"
"                                MIDUSS version                Version 2.25 rev. 473"
"                                MIDUSS created                Sunday, February 07, 2010"
"                                10 Units used:                ie METRIC"
"                                Job folder:                    w:\Guelph\105-2005\105172\Design Data\
"                                                                Modelling Files\MIDUSS\2016 Revisions"
"                                Output filename:                105172_POST_100yr.out"
"                                Licensee name:                gmbp"
"                                Company                        Hewlett-Packard Company"
"                                Date & Time last used:        6/2/2016 at 4:14:14 PM"
" 31 TIME PARAMETERS"
"      5.000 Time Step"
"     210.000 Max. Storm length"
"    1500.000 Max. Hydrograph"
" 32 STORM Chicago storm"
"      1 Chicago storm"
"    4688.000 Coefficient A"
"      17.000 Constant B"
"       0.962 Exponent C"
"       0.400 Fraction R"
"     210.000 Duration"
"      1.000 Time step multiplier"
"      Maximum intensity                213.574 mm/hr"
"      Total depth                      88.830 mm"
" 33 6 100hyd Hydrograph extension used in this file"
"    CATCHMENT 201"
"      1 Triangular SCS"
"      1 Equal length"
"      2 Horton equation"
"     201 Catchment 201 - To Clythe Creeek"
"    65.000 % Impervious"
"     3.410 Total Area"
"    30.000 Flow length"
"     2.000 Overland Slope"
"     1.194 Pervious Area"
"    30.000 Pervious length"
"     2.000 Pervious slope"
"     2.217 Impervious Area"
"    30.000 Impervious length"
"     2.000 Impervious slope"
"     0.250 Pervious Manning 'n'"
"    75.000 Pervious Max.infiltration"
"    12.500 Pervious Min.infiltration"
"     0.250 Pervious Lag constant (hours)"
"     5.000 Pervious Depression storage"
"     0.015 Impervious Manning 'n'"
"     0.000 Impervious Max.infiltration"
"     0.000 Impervious Min.infiltration"
"     0.050 Impervious Lag constant (hours)"
"     1.500 Impervious Depression storage"
"           1.469 0.000 0.000 0.000 c.m/sec"
"    Catchment 201 Pervious Impervious Total Area "
"    Surface Area 1.194 2.217 3.410 hectare"
"    Time of concentration 9.306 1.638 3.326 minutes"
"    Time to Centroid 102.153 97.460 98.493 minutes"
"    Rainfall depth 88.830 88.830 88.830 mm"
"    Rainfall volume 1060.18 1968.91 3029.10 c.m"
"    Rainfall losses 43.655 2.647 17.000 mm"
"    Runoff depth 45.175 86.183 71.830 mm"
"    Runoff volume 539.17 1910.24 2449.40 c.m"
"    Runoff coefficient 0.509 0.970 0.809 "
"    Maximum flow 0.418 1.149 1.469 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"          105172_POST_100yr
"          4  Add Runoff "
"          1.469      1.469      0.000      0.000"
" 54  POND DESIGN"
"      1.469  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      2449.4  Hydrograph volume      c.m"
"      15.    Number of stages"
"      0.000  Minimum water level      metre"
"      3.000  Maximum water level      metre"
"      0.000  Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"          339.750      0.000      0.000"
"          339.850      0.00400      217.300"
"          339.950      0.00700      450.800"
"          340.050      0.00900      700.800"
"          340.150      0.01000      967.300"
"          340.250      0.01100      1250.700"
"          340.350      0.4110      1551.100"
"          340.450      0.4220      1869.000"
"          340.550      0.4320      2204.400"
"          340.650      0.4420      2557.700"
"          340.750      0.4510      2929.100"
"          340.850      0.4610      3318.900"
"          340.950      0.4700      3727.400"
"          341.050      0.9140      4153.000"
"          341.150      1.736      4594.600"
"          Peak outflow      0.413      c.m/sec"
"          Maximum level      340.373      metre"
"          Maximum storage      1624.434      c.m"
"          Centroidal lag      13.176      hours"
"          1.469      1.469      0.413      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"          1.469      0.413      0.413      0.000"
" 51  PIPE DESIGN"
"      0.413  Current peak flow      c.m/sec"
"      0.013  Manning 'n'"
"      0.450  Diameter      metre"
"      4.420  Gradient      %"
"          Depth of flow      0.275      metre"
"          Velocity      4.065      m/sec"
"          Pipe capacity      0.599      c.m/sec"
"          Critical depth      0.423      metre"
" 53  ROUTE      Pipe Route 19"
"      19.20  Pipe Route 19 Reach length      ( metre)"
"      0.392  X-factor <= 0.5"
"      3.543  K-lag      ( seconds)"
"      0.000  Default(0) or user spec.(1) values used"
"      0.500  X-factor <= 0.5"
"      30.000  K-lag      ( seconds)"
"      0.500  Beta weighting factor"
"      4.286  Routing time step      ( seconds)"
"          1  No. of sub-reaches"
"          Peak outflow      0.413      c.m/sec"
"          1.469      0.413      0.413      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"          1.469      0.413      0.413      0.000"
" 54  POND DESIGN"
"      0.413  Current peak flow      c.m/sec"
"      0.171  Target outflow      c.m/sec"
"      1927.7  Hydrograph volume      c.m"

```

```

105172_POST_100yr
"      12.  Number of stages"
"      0.000 Minimum water level   metre"
"      3.000 Maximum water level   metre"
"      0.000 Starting water level  metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge   Volume"
"          336.000      0.000      0.000"
"          336.100      1.00E-05      4.300"
"          336.200      2.00E-05      8.700"
"          336.300      3.00E-05     13.000"
"          336.400      4.00E-05     17.300"
"          336.500      5.00E-05     21.700"
"          336.600      6.00E-05     26.000"
"          336.700      7.00E-05     30.300"
"          336.800      8.00E-05     34.700"
"          336.900      9.00E-05     41.900"
"          337.000      1.00E-04     50.100"
"          337.100      2.129      59.300"
"          Peak outflow      0.413      c.m/sec"
"          Maximum level      337.019      metre"
"          Maximum storage      51.886      c.m"
"          Centroidal lag      7.142      hours"
"          1.469      0.413      0.413      0.000 c.m/sec"
" 40      HYDROGRAPH Next link "
"          5      Next link "
"          1.469      0.413      0.413      0.000"
" 52      CHANNEL DESIGN"
"          0.413      Current peak flow      c.m/sec"
"          0.065      Manning 'n'"
"          0.      Cross-section type: 0=trapezoidal; 1=general"
"          65.000      Basewidth      metre"
"          3.000      Left bank slope"
"          3.000      Right bank slope"
"          0.100      Channel depth      metre"
"          18.000      Gradient      %"
"          Depth of flow      0.016      metre"
"          Velocity      0.407      m/sec"
"          Channel capacity      9.152      c.m/sec"
"          Critical depth      0.016      metre"
" 53      ROUTE      Channel Route 50"
"          50.00      Channel Route 50 Reach length      ( metre)"
"          0.499      X-factor <= 0.5"
"          92.097      K-lag      ( seconds)"
"          0.000      Default(0) or user spec.(1) values used"
"          0.500      X-factor <= 0.5"
"          30.000      K-lag      ( seconds)"
"          0.500      Beta weighting factor"
"          75.000      Routing time step      ( seconds)"
"          1      No. of sub-reaches"
"          Peak outflow      0.413      c.m/sec"
"          1.469      0.413      0.413      0.000 c.m/sec"
" 40      HYDROGRAPH Next link "
"          5      Next link "
"          1.469      0.413      0.413      0.000"
" 33      CATCHMENT 202"
"          1      Triangular SCS"
"          1      Equal length"
"          2      Horton equation"
"          202      Catchment 202 - To clythe Creeek"
"          25.000      % Impervious"
"          0.740      Total Area"
"          30.000      Flow length"
"          2.000      Overland Slope"

```

105172_POST_100yr

"	0.555	Pervious Area"				
"	30.000	Pervious length"				
"	2.000	Pervious slope"				
"	0.185	Impervious Area"				
"	30.000	Impervious length"				
"	2.000	Impervious slope"				
"	0.250	Pervious Manning 'n'"				
"	75.000	Pervious Max.infiltration"				
"	12.500	Pervious Min.infiltration"				
"	0.250	Pervious Lag constant (hours)"				
"	5.000	Pervious Depression storage"				
"	0.015	Impervious Manning 'n'"				
"	0.000	Impervious Max.infiltration"				
"	0.000	Impervious Min.infiltration"				
"	0.050	Impervious Lag constant (hours)"				
"	1.500	Impervious Depression storage"				
"		0.256	0.413	0.413	0.000 c.m/sec"	
"		Catchment 202	Pervious	Impervious	Total Area	"
"		Surface Area	0.555	0.185	0.740	hectare"
"		Time of concentration	9.306	1.638	6.325	minutes"
"		Time to Centroid	102.153	97.460	100.328	minutes"
"		Rainfall depth	88.830	88.830	88.830	mm"
"		Rainfall volume	493.01	164.34	657.34	c.m"
"		Rainfall losses	43.655	2.647	33.403	mm"
"		Runoff depth	45.175	86.183	55.427	mm"
"		Runoff volume	250.72	159.44	410.16	c.m"
"		Runoff coefficient	0.509	0.970	0.624	"
"		Maximum flow	0.195	0.096	0.256	c.m/sec"
"	40	HYDROGRAPH Add Runoff "				
"		4 Add Runoff "				
"		0.256	0.527	0.413	0.000"	
"	33	CATCHMENT 300"				
"		1 Triangular SCS"				
"		1 Equal length"				
"		2 Horton equation"				
"		300 Catchment 300 - To Clythe Creek"				
"		0.000 % Impervious"				
"		6.480 Total Area"				
"		45.000 Flow length"				
"		2.000 Overland Slope"				
"		6.480 Pervious Area"				
"		45.000 Pervious length"				
"		2.000 Pervious slope"				
"		0.000 Impervious Area"				
"		45.000 Impervious length"				
"		2.000 Impervious slope"				
"		0.250 Pervious Manning 'n'"				
"		75.000 Pervious Max.infiltration"				
"		12.500 Pervious Min.infiltration"				
"		0.250 Pervious Lag constant (hours)"				
"		5.000 Pervious Depression storage"				
"		0.015 Impervious Manning 'n'"				
"		0.000 Impervious Max.infiltration"				
"		0.000 Impervious Min.infiltration"				
"		0.050 Impervious Lag constant (hours)"				
"		1.500 Impervious Depression storage"				
"		1.971	0.527	0.413	0.000 c.m/sec"	
"		Catchment 300	Pervious	Impervious	Total Area	"
"		Surface Area	6.480	0.000	6.480	hectare"
"		Time of concentration	11.869	2.089	11.869	minutes"
"		Time to Centroid	104.828	98.071	104.828	minutes"
"		Rainfall depth	88.830	88.830	88.830	mm"
"		Rainfall volume	5756.17	0.01	5756.17	c.m"

		105172_POST_100yr				
"		Rainfall losses	43.360	2.670	43.360	mm"
"		Runoff depth	45.470	86.160	45.470	mm"
"		Runoff volume	2946.46	0.01	2946.46	c.m"
"		Runoff coefficient	0.512	0.000	0.512	"
"		Maximum flow	1.971	0.000	1.971	c.m/sec"
" 40		HYDROGRAPH Add Runoff "				
"	4	Add Runoff "				
"		1.971	2.362	0.413	0.000"	
" 64		SHOW TABLE"				
"	2	Flow hydrograph"				
"	4	Inflow Hydrograph"				
"		Maximum flow	2.362	c.m/sec"		
"		Hydrograph volume	5236.133	c.m"		
" 38		START/RE-START TOTALS 300"				
"	3	Runoff Totals on EXIT"				
"		Total Catchment area		10.630	hectare"	
"		Total Impervious area		2.402	hectare"	
"		Total % impervious		22.592"		
" 19		EXIT"				

```

"                                     105172_POST_Regional
" MIDUSS Output ----->"
" MIDUSS version                      Version 2.25 rev. 473"
" MIDUSS created                      Sunday, February 07, 2010"
" 10 Units used:                      ie METRIC"
" Job folder:                        w:\Guelph\105-2005\105172\Design Data\
"                                     Modelling Files\MIDUSS\2016 Revisions"
" Output filename:                   105172_POST_Regional.out"
" Licensee name:                     gmbp"
" Company                           Hewlett-Packard Company"
" Date & Time last used:             6/2/2016 at 4:15:52 PM"
31 TIME PARAMETERS"
" 60.000 Time Step"
" 2880.000 Max. Storm length"
" 3600.000 Max. Hydrograph"
32 STORM Historic"
" 5 Historic"
" 2880.000 Duration"
" 48.000 Rainfall intensity values"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.028      2.028      2.028      2.028"
"      2.028      2.026      2.026      2.026      2.028"
"      2.026      6.000      4.000      6.000      13.000"
"      17.000     13.000     23.000     13.000     13.000"
"      53.000     38.000     13.000"
" Maximum intensity                    53.000 mm/hr"
" Total depth                        285.000 mm"
" 6 000hyd Hydrograph extension used in this file"
33 CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 2 Horton equation"
" 201 Catchment 201 - To Clythe Creeek"
" 65.000 % Impervious"
" 3.410 Total Area"
" 30.000 Flow length"
" 2.000 Overland Slope"
" 1.194 Pervious Area"
" 30.000 Pervious length"
" 2.000 Pervious slope"
" 2.217 Impervious Area"
" 30.000 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
" 0.250 Pervious Lag constant (hours)"
" 5.000 Pervious Depression storage"
" 0.015 Impervious Manning 'n'"
" 0.000 Impervious Max.infiltration"
" 0.000 Impervious Min.infiltration"
" 0.050 Impervious Lag constant (hours)"
" 1.500 Impervious Depression storage"
"      0.376      0.000      0.000      0.000 c.m/sec"
" Catchment 201 Pervious Impervious Total Area "
" Surface Area      1.194      2.217      3.410 hectare"
" Time of concentration 17.225      2.860      4.946 minutes"
" Time to Centroid 2775.198      2251.465      2327.523 minutes"
" Rainfall depth      285.000      285.000      285.000 mm"
" Rainfall volume      3401.48      6317.02      9718.50 c.m"

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"                               105172_POST_Regional
" Rainfall losses                207.571    39.596    98.387    mm"
" Runoff depth                   77.429     245.404   186.613   mm"
" Runoff volume                  924.12     5439.38   6363.50   c.m"
" Runoff coefficient             0.272      0.861     0.655     "
" Maximum flow                   0.094      0.282     0.376     c.m/sec"
40 HYDROGRAPH Add Runoff "
"   4 Add Runoff "
"       0.376    0.376    0.000    0.000"
54 POND DESIGN"
"   0.376 Current peak flow    c.m/sec"
"   0.171 Target outflow      c.m/sec"
" 6363.5 Hydrograph volume    c.m"
"   15. Number of stages"
"   0.000 Minimum water level  metre"
"   3.000 Maximum water level  metre"
"   0.000 Starting water level metre"
"   0 Keep Design Data: 1 = True; 0 = False"
"       Level Discharge    Volume"
"       339.750    0.000    0.000"
"       339.850    0.00400  217.300"
"       339.950    0.00700  450.800"
"       340.050    0.00900  700.800"
"       340.150    0.01000  967.300"
"       340.250    0.01100 1250.700"
"       340.350    0.4110  1551.100"
"       340.450    0.4220  1869.000"
"       340.550    0.4320  2204.400"
"       340.650    0.4420  2557.700"
"       340.750    0.4510  2929.100"
"       340.850    0.4610  3318.900"
"       340.950    0.4700  3727.400"
"       341.050    0.9140  4153.000"
"       341.150    1.736  4594.600"
"       Peak outflow                0.312    c.m/sec"
"       Maximum level                340.335  metre"
"       Maximum storage              1507.016  c.m"
"       Centroidal lag               47.728  hours"
"       0.376    0.376    0.312    0.000 c.m/sec"
40 HYDROGRAPH Next link "
"   5 Next link "
"       0.376    0.312    0.312    0.000"
51 PIPE DESIGN"
"   0.312 Current peak flow    c.m/sec"
"   0.013 Manning 'n'"
"   0.450 Diameter    metre"
"   4.420 Gradient    %"
"       Depth of flow                0.230  metre"
"       Velocity                    3.807  m/sec"
"       Pipe capacity                0.599  c.m/sec"
"       Critical depth              0.387  metre"
53 ROUTE Pipe Route 19"
"   19.20 Pipe Route 19 Reach length (metre)"
"   0.419 X-factor <= 0.5"
"   3.783 K-lag (seconds)"
"   0.000 Default(0) or user spec.(1) values used"
"   0.500 X-factor <= 0.5"
"  30.000 K-lag (seconds)"
"   0.500 Beta weighting factor"
"   4.390 Routing time step (seconds)"
"   1 No. of sub-reaches"
"       Peak outflow                0.312    c.m/sec"
"       0.376    0.312    0.312    0.000 c.m/sec"
40 HYDROGRAPH Next link "

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"                                     105172_POST_Regional
"      5  Next link "
"      0.376      0.312      0.312      0.000"
" 54  POND DESIGN"
"      0.312      Current peak flow      c.m/sec"
"      0.171      Target outflow      c.m/sec"
"      5475.3      Hydrograph volume      c.m"
"      12.      Number of stages"
"      0.000      Minimum water level      metre"
"      3.000      Maximum water level      metre"
"      0.000      Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"      Level Discharge      volume"
"      336.000      0.000      0.000"
"      336.100      1.00E-05      4.300"
"      336.200      2.00E-05      8.700"
"      336.300      3.00E-05      13.000"
"      336.400      4.00E-05      17.300"
"      336.500      5.00E-05      21.700"
"      336.600      6.00E-05      26.000"
"      336.700      7.00E-05      30.300"
"      336.800      8.00E-05      34.700"
"      336.900      9.00E-05      41.900"
"      337.000      1.00E-04      50.100"
"      337.100      2.129      59.300"
"      Peak outflow      0.312      c.m/sec"
"      Maximum level      337.015      metre"
"      Maximum storage      51.448      c.m"
"      Centroidal lag      43.394      hours"
"      0.376      0.312      0.312      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.376      0.312      0.312      0.000"
" 52  CHANNEL DESIGN"
"      0.312      Current peak flow      c.m/sec"
"      0.065      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; 1=general"
"      65.000      Basewidth      metre"
"      3.000      Left bank slope"
"      3.000      Right bank slope"
"      0.100      Channel depth      metre"
"      18.000      Gradient      %"
"      Depth of flow      0.013      metre"
"      Velocity      0.364      m/sec"
"      Channel capacity      9.152      c.m/sec"
"      Critical depth      0.013      metre"
" 53  ROUTE      Channel Route 50"
"      50.00      Channel Route 50 Reach length      ( metre)"
"      0.500      X-factor <= 0.5"
"      103.020      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.500      Beta weighting factor"
"      102.857      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      0.312      c.m/sec"
"      0.376      0.312      0.312      0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5  Next link "
"      0.376      0.312      0.312      0.000"
" 33  CATCHMENT 202"
"      1      Triangular SCS"
"      1      Equal length"

```



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105172_POST_Regional
"      2 Horton equation"
"      202 Catchment 202 - To Clythe Creek"
"      25.000 % Impervious"
"      0.740 Total Area"
"      30.000 Flow length"
"      2.000 Overland Slope"
"      0.555 Pervious Area"
"      30.000 Pervious length"
"      2.000 Pervious slope"
"      0.185 Impervious Area"
"      30.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"      0.067 0.312 0.312 0.000 c.m/sec"
"      Catchment 202 Pervious Impervious Total Area "
"      Surface Area 0.555 0.185 0.740 hectare"
"      Time of concentration 17.225 2.860 9.845 minutes"
"      Time to Centroid 2775.197 2251.465 2506.141 minutes"
"      Rainfall depth 285.000 285.000 285.000 mm"
"      Rainfall volume 1581.75 527.25 2109.00 c.m"
"      Rainfall losses 207.571 39.596 165.577 mm"
"      Runoff depth 77.429 245.404 119.423 mm"
"      Runoff volume 429.73 454.00 883.73 c.m"
"      Runoff coefficient 0.272 0.861 0.419 "
"      Maximum flow 0.044 0.024 0.067 c.m/sec"
40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.067 0.373 0.312 0.000"
33 CATCHMENT 300"
"      1 Triangular SCS"
"      1 Equal length"
"      2 Horton equation"
"      300 Catchment 300 - To Clythe Creek"
"      0.000 % Impervious"
"      6.480 Total Area"
"      45.000 Flow length"
"      2.000 Overland Slope"
"      6.480 Pervious Area"
"      45.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      75.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"      0.538 0.373 0.312 0.000 c.m/sec"

```

```

"                               105172_POST_Regional
" Catchment 300
" Surface Area                Pervious    Impervious Total Area "
"                               6.480      0.000      6.480    hectare"
" Time of concentration       21.969      3.647      21.969    minutes"
" Time to Centroid            2780.244    2236.986    2780.242  minutes"
" Rainfall depth              285.000      285.000      285.000    mm"
" Rainfall volume              1.8468      0.0000      1.8468    ha-m"
" Rainfall losses              206.992      38.537      206.992    mm"
" Runoff depth                 78.008      246.463      78.008    mm"
" Runoff volume                5054.92      0.02      5054.94    c.m"
" Runoff coefficient           0.274      0.000      0.274      "
" Maximum flow                 0.538      0.000      0.538    c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4   Add Runoff "
"       0.538      0.911      0.312      0.000"
" 64 SHOW TABLE"
" 2   Flow hydrograph"
" 4   Inflow Hydrograph"
"       Maximum flow                0.911      c.m/sec"
"       Hydrograph volume           11368.914    c.m"
" 38 START/RE-START TOTALS 300"
" 3   Runoff Totals on EXIT"
"       Total Catchment area                10.630    hectare"
"       Total Impervious area                2.402    hectare"
"       Total % impervious                22.592"
" 19 EXIT"

```

105172 - Cityview Ridge Subdivision**Cooling Trench Sizing Calculations (Energy Dissipation/Dispersion Structure)****Assumptions:**

$T_{in} = 36\text{ }^{\circ}\text{C}$
 $= 309\text{ K}$

 $T_{out} = 24\text{ }^{\circ}\text{C}$
 $= 297\text{ K}$

 $T_{avg} = 30\text{ }^{\circ}\text{C}$
 $= 303\text{ K}$

 $T_{stone} = 21\text{ }^{\circ}\text{C}$
 $= 294\text{ K}$

 $L = 65\text{ m}$
 $W = 2\text{ m}$
 $D = 1\text{ m}$

 $Diam. = 0.02\text{ m}$

Knowns:

$Rho = 998\text{ kg/m}^3$
 $C_p = 4181\text{ J/kg}^{\circ}\text{K}$
 $Pr_f = 6.62$
 $Gamma = 1.04\text{E-}06\text{ m}^3/\text{s}$
 $k_f = 2.79\text{ J/m}^2\text{K}^{\circ}\text{s}$

 $Q_{2yr} = 0.009\text{ m}^3/\text{s}$
 $Q_{5yr} = 0.010\text{ m}^3/\text{s}$
 $Q_{25yr} = 0.176\text{ m}^3/\text{s}$
 $Q_{100yr} = 0.412\text{ m}^3/\text{s}$
 $Q_{Regional} = 0.307\text{ m}^3/\text{s}$

Storm	qr (J/s)	As m^2	Af m^2	Vf (m/s)	hs $\text{J/m}^2\text{K}^{\circ}\text{s}$	qa (J/s)	SF (%)
2	450,645	20420	27.9	0.0003	655	120,399,575	26617%
5	500,717	20420	27.9	0.0004	678	124,540,667	24772%
25	8,812,611	20420	27.9	0.0063	2,081	382,385,866	4239%
100	20,629,522	20420	27.9	0.0148	3,057	561,814,119	2623%
Regional	15,371,998	20420	27.9	0.0110	2,671	490,965,210	3094%

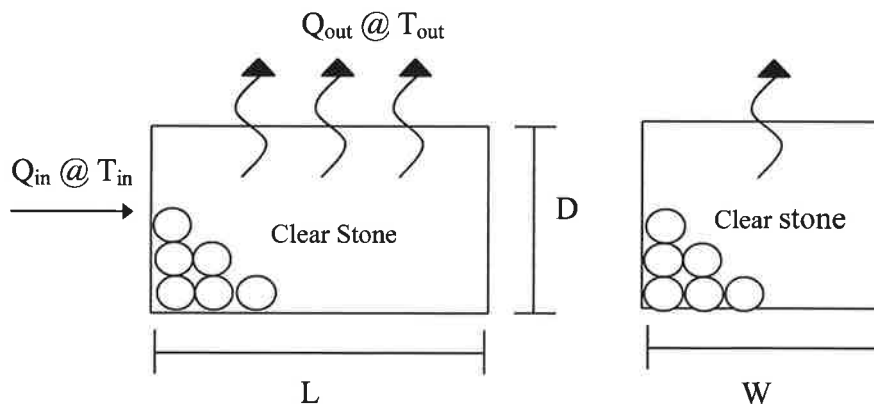
**Cityview Ridge Subdivision
City of Guelph
G&M File: 105-172**

**Cooling Trench Details
Sample Calculation**

Assumptions:

- Cooling trench is treated as a “black box”, therefore the specific design of the trench is ignored.
- Solid media (clear stone) in trench is isothermal (ie. at a constant temperature).
- Temperature of fluid moving through trench is assumed to be constant.
- Temperature of fluid moving through trench is approximated as the average inlet and outlet temperature.
- Each trench section is rectangular with spherical particles.
- Thermal conductivity of granite is approximate to the thermal conductivity of clear stone.

Schematic:



Design Variables:

Q = flowrate through trench (m^3/s)
= $0.009 \text{ m}^3/\text{s}$ for 2 year design storm event.

T_{in} = temperature of fluid at inlet (K)
= 36°C
= 309 K

T_{out} = temperature of fluid at outlet (K)
= 24°C
= 297 K

T_{avg} = average temperature of inflow and outflow (K)
= 30°C
= 303 K

T_{stone} = average temperature of clear stone (K)
= 21°C
= 294 K

L = length of trench (m)
= 65 m

W = width of trench (m)
= 2.0 m

D = depth of trench (m)
= 1.0 m

Dia. = diameter of clear stone (m)
= 0.020 m

Physical Properties:

ρ = fluid density
= 998 kg/m^3 for water at 295 K
(Incropera, DeWitt, p. 846)

C_p = specific heat of fluid
= 4181 J/kg.K for water at 295 K
(Incropera, DeWitt, p. 846)

P_{rf} = Prandtl number of fluid
= 6.62 for water (dimensionless)
(Incropera, DeWitt, p. 846)

γ_f = kinetic viscosity of fluid
= $1.04 \times 10^{-6} \text{ m}^2/\text{s}$ for water at 295 K
(Roberson, Crowe, p. A-24)

k_f = thermal conductivity of solid
= 2.79 W/m.K for granite
(Incropera, DeWitt, p.838)

Note: temperature measured in Kelvins (K) is calculated as follows:

$$K = (^\circ\text{C} + 273.15)$$

$$\text{i.e. } 295\text{K} = 21.85^\circ\text{C}$$

Analysis:

Calculate the required heat transfer rate (q_r) using the following equation:

$$\begin{aligned} q_r &= \dot{m} C_p \Delta T \\ q_r &= Q \rho C_p (T_{in} - T_{out}) \end{aligned} \quad \text{Eq. 1}$$

Where:

\dot{m} = mass flow rate (kg/s)

ρ = fluid density (kg/m³)

C_p = fluid specific heat (J/kg.K)

$$q_r = \left(0.007 \frac{m^3}{s} \right) \left(998 \frac{kg}{m^3} \right) \left(4181 \frac{J}{kg \cdot K} \right) (309 K - 297 K)$$

$$q_r = 450,645 \text{ J/s}$$

$$q_r = 450,645 \text{ W}$$

Therefore the heat transfer rate required to reduce the temperature of water to 297 K (24°C) from 309 K (36°C) is 350,502 W.

Calculate the available heat transfer rate (q_a) using the following equation:

$$q_a = h_s A_s (T_{avg} - T_{stone}) \quad \text{Eq. 2}$$

Where:

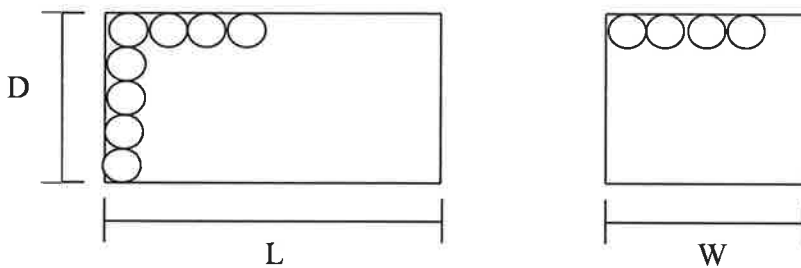
h_s = convective heat transfer coefficient $\left(\frac{W}{m^2 \cdot K} \right)$ for clear stone

A_s = surface area of clear stone particles (m^2)

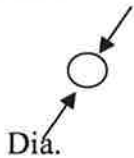
Step 1: Estimate the available surface area of the clear stone particles using the following equation:

$$A = (\pi \times Dia.^2) \times \left(\frac{L}{Dia.} \times \frac{W}{Dia.} \times \frac{H}{Dia.} \right) \quad \text{Eq. 3}$$

$$A = \pi \times \frac{L \times W \times D}{Dia.}$$



Where:



Dia: = diameter of spherical particles (m)

= diameter of "clear stone" particles (m)

A = available surface area (m^2)

= (area of one "clear stone" particle) * (Estimate of the total number of clear stone particles)

$$A = \pi \times \left(\frac{65m \times 2m \times 1.0m}{0.020m} \right)$$

$$A = 20,420 m^2$$

Therefore the available surface area of the clear stone particles is estimated to be 20,420 m^2 .

Step 2: Estimate the heat transfer coefficient of the clear stone particles using the equation:

$$h_s = \left(0.97 + 0.68 \left(\frac{\nu_f \text{Dia.}}{\gamma_f} \right)^{0.5} \right) \frac{k_f P_{rf}^{0.3}}{\text{Dia.}} \quad \text{Eq. 4}$$

Note: The equation used to estimate the heat transfer coefficient (h_g) utilizes Kramer's correlation for flow of liquids past spheres, for which ($1 < Re_{Dia} < 2000$). The scenario under analysis is very close to the lower limit acceptable for use with Kramer's correlation for the convective heat transfer coefficient.

Where:

ν_f = velocity of fluid through trench (m/s)

γ_f = kinematic viscosity of fluid (m²/s)

k_f = thermal conductivity of solid $\left(\frac{W}{m \cdot K} \right)$

P_{rf} = Prandtl number (dimensionless)

Calculate ν_f using the following equation:

$$\nu_f = \frac{Q}{A_{flow}} \quad \text{Eq. 5}$$

Where:

Q = flow rate through trench (m³/s)

A_{flow} = available flow area through trench (m²)

Calculate A_{flow} using the following equation:

A_{flow} = Cross-sectional area of trench - Cross-sectional area of particles

$$A_{flow} = (L \times W) - \left(\frac{\pi \times \text{Dia.}^2}{4} \right) \times \left(\frac{L}{D} \times \frac{W}{D} \right) \quad \text{Eq. 6}$$

Overall section area Cross-sectional area of a single sphere Estimate of number of spheres in section

$$A_{flow} = L \times W \left(1 - \frac{\pi}{4} \right)$$

Substitute equation for A_{flow} (Eq. 6) into the equation for ν_f (Eq. 5) and solve

$$\begin{aligned} \nu_f &= \frac{Q}{L \times W \left(1 - \frac{\pi}{4}\right)} \\ \nu_f &= \frac{0.009 \frac{m^3}{s}}{(65m \times 2m) \times \left(1 - \frac{\pi}{4}\right)} \\ \nu_f &= 0.0003 \frac{m}{s} \end{aligned} \quad \text{Eq. 7}$$

Therefore the velocity of fluid through the trench is $0.0003 \frac{m}{s}$.

Calculate the heat transfer coefficient (h_s) using the following equation:

$$\begin{aligned} h_s &= \left(0.97 + 0.68 \left(\frac{\nu_f \text{Dia.}}{\gamma_f} \right)^{0.5} \right) \frac{k_f P_{ef}^{0.3}}{\text{Dia.}} \\ h_s &= \left(0.97 + 0.68 \left(\frac{0.0003 \frac{m^2}{s} \times 0.020m}{1.04 \times 10^{-6} \frac{m^3}{s}} \right)^{0.5} \right) \frac{2.79 \frac{W}{m \cdot K} \times 6.62^{0.3}}{0.020m} \\ h_s &= 655 \frac{W}{m^2 \cdot K} \end{aligned} \quad \text{Eq. 4}$$

Therefore the heat transfer coefficient (h_s) for clear stone particles is $655 \frac{W}{m^2 \cdot K}$

Calculate the available heat transfer rate (q_a) using the following equation:

$$q_a = h_s A_s (T_{avg} - T_{stone}) \quad \text{Eq. 2}$$

$$q_a = \left(655 \frac{W}{m^2 \cdot K} \right) (20,420 m^2) (303 K - 294 K)$$
$$q_a = 120,399,575 \text{ W}$$

Therefore the available heat transfer rate to reduce the temperature of water to 297 K (24°C) from 309 K (36°C) is 120,399,575 W.

Calculate the Safety Factor (SF) using the following equation:

$$SF = \frac{q_a - q_r}{q_r} \times 100\% \quad \text{Eq. 8}$$
$$SF = \frac{120,399,575 \text{ W} - 450,645 \text{ W}}{450,645 \text{ W}} \times 100\%$$
$$SF = 26,617\%$$

Therefore the Safety Factor for the cooling trench is 26,617% based on the assumptions used in the calculations.

Therefore since the available heat transfer rate (q_a) of 120,399.575 W is greater than the required heat transfer rate (q_r) of 450,645 W, we conclude that in our opinion a cooling trench 65 m long by 2 m wide by 1 m deep, constructed with 0.020 m diameter clear stone, has the ability to reduce the temperature of the inflow from 309 K (36°C) to 297 K (24°C).

Cityview Ridge Subdivision
City of Guelph
G&M File: 105-172
Revised: June 2016

Stormwater Management Facility - Forebay (Catchment 201)

Forebay Length =	42.0 m	(Dist)
Forebay Width =	7.0 m	
Forebay Depth =	1.0 m	(d)
Forebay Bottom Width =	1.0 m	
Approximate Permanent Forebay Pool Volume =	168.0 cu m	
Length Width Ratio =	6 :1	(r)
2 Year Storm Peak Flowrate =	0.086 cu m/s	(Qp)
5 Year Storm Inflow Rate =	0.663 cu m/s	(Q5)
Desired Forebay Velocity =	0.500 m/s	(Vf)
Desired Settling Velocity (recommended) =	0.0003 m/s	(Vs)

Settling Length

$$\text{Dist} = ((r \times Q_p) / V_s)^{.5} = 41.5 \text{ m}$$

Forebay length (42m) exceeds the settling length (41.5).

Dispersion Length

$$\text{Dist} = (8 \times Q_5) / (d \times V_f) = 10.6 \text{ m}$$

Forebay length (45m) exceeds dispersion length (10.6m).

Flow Velocity in Forebay

$$\begin{aligned} \text{Cross-sectional Area} &= 4 \text{ sq m} \\ Q_5 &= 0.663 \text{ cu m/s} \end{aligned}$$

$$\text{Velocity} = Q_5 / A = 0.17 \text{ m/s}$$

The average flow velocity through the forebay is less than the allowable velocity of 0.5 m/s.



Stormceptor Design Summary

PCSWMM for Stormceptor

Project Information

Date	3/27/2015
Project Name	Cityview Ridge Subdivision
Project Number	105172
Location	City of Guelph

Designer Information

Company	N/A
Contact	N/A

Notes

N/A

Drainage Area

Total Area (ha)	7.62
Imperviousness (%)	65

The Stormceptor System model STC 14000 removes 78% TSS for a Fine (organics, silts and sand) particle size distribution and 92% runoff volume.

Rainfall

Name	TORONTO CENTRAL
State	ON
ID	100
Years of Records	1982 to 1999
Latitude	45°30'N
Longitude	90°30'W

Water Quality Objective

TSS Removal (%)	80
Runoff Volume (%)	90

Upstream Storage

Storage (ha-m)	Discharge (L/s)
0	0

Stormceptor Sizing Summary

Stormceptor Model	TSS Removal	Runoff Volume
	%	%
STC 300	36	30
STC 750	48	50
STC 1000	49	50
STC 1500	50	50
STC 2000	57	64
STC 3000	58	64
STC 4000	65	77
STC 5000	65	77
STC 6000	70	83
STC 9000	74	88
STC 10000	74	88
STC 14000	78	92



Particle Size Distribution

Removing silt particles from runoff ensures that the majority of the pollutants, such as hydrocarbons and heavy metals that adhere to fine particles, are not discharged into our natural water courses. The table below lists the particle size distribution used to define the annual TSS removal.

Fine (organics, silts and sand)								
Particle Size μm	Distribution %	Specific Gravity	Settling Velocity m/s		Particle Size μm	Distribution %	Specific Gravity	Settling Velocity m/s
20	20	1.3	0.0004					
60	20	1.8	0.0016					
150	20	2.2	0.0108					
400	20	2.65	0.0647					
2000	20	2.65	0.2870					

Stormceptor Design Notes


- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor version 1.0
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal.
- Only the STC 300 is adaptable to function with a catch basin inlet and/or inline pipes.
- Only the Stormceptor models STC 750 to STC 6000 may accommodate multiple inlet pipes.
- Inlet and outlet invert elevation differences are as follows:

Inlet and Outlet Pipe Invert Elevations Differences

Inlet Pipe Configuration	STC 300	STC 750 to STC 6000	STC 9000 to STC 14000
Single inlet pipe	75 mm	25 mm	75 mm
Multiple inlet pipes	75 mm	75 mm	Only one inlet pipe.

- Design estimates are based on stable site conditions only, after construction is completed.
- Design estimates assume that the storm drain is not submerged during zero flows. For submerged applications, please contact your local Stormceptor representative.
- Design estimates may be modified for specific spills controls. Please contact your local Stormceptor representative for further assistance.
- For pricing inquiries or assistance, please contact Imbrium Systems Inc., 1-800-565-4801.

United States Patent No. 5,753,115 • 5,849,181 • 6,068,765 • 6,371,690 • 7,582,216 • 7,666,303 | Australia Patent No. 693,164 • 707,133 • 729,096 • 779,401 • 299,647 • 2006,279 378 • 2008,286,900 | Canadian Patent No. 2,009,280 • 2,137,942 • 2,175,272 • 2,180,305 • 2,180,383 • 2,206,338 • 2,327,765 | Indonesian Patent No. 007055 | Japan Patent No. 3581233 • 9-11476 | Korea Patent No. 10-1451593 • 0519212 | Malaysia Patent No. 116657 | New Zealand Patent No. 314,648 • 583,583 • 583,008 | South African Patent No. 2010/00683 • 2010/01796 |

 imbrium® <small>WWW.IMBRIUMSYSTEMS.COM</small> 805 GLOBAL WAY, SUITE 113, LINTHICUM, MD 21231	STC 14000 STANDARD MODEL ####		REV #	DATE	REVISION DESCRIPTION	BY	SHEET NUMBER 1 OF 1
USA 888-279-8826 CA 800-565-4801 INTL +1-410-960-9900			DATE: #####	SCALE: 100	PROJECT No.: #####	DRAWN: ###	CHECKED: ###

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “F”

FLOODPLAIN ANALYSIS

Comparison of Pre and Post-Development Flood Levels

Cityview Ridge Subdivision (Formerly th P.T. Valeriot Property)
City of Guelph
Our File: 105-172
July 17, 2012

Comparison of Pre and Post-Development Flood Levels

Sec No.	Design Storm	Flow (cu m/s)			W.S. Elevation (m)			Tope Width (m)		
		POST	PRE	Difference	POST	PRE	Difference	POST	PRE	Difference
1	5 Year	3.99	3.99	0	316.29	316.29	0	34.52	34.52	0
1	25 Year	19.70	19.70	0	316.51	316.51	0	41.05	41.05	0
1	100 Year	34.10	34.10	0	316.66	316.66	0	45.22	45.22	0
1	Regional	38.60	38.60	0	316.70	316.70	0	46.40	46.40	0
2	5 Year	3.99	3.99	0	316.77	316.77	0	9.22	9.22	0
2	25 Year	19.70	19.70	0	317.84	317.84	0	28.11	28.11	0
2	100 Year	34.10	34.10	0	318.56	318.56	0	43.67	43.67	0
2	Regional	38.60	38.60	0	318.76	318.76	0	52.31	52.31	0
3	5 Year	3.99	3.99	0	317.26	317.26	0	21.89	21.89	0
3	25 Year	19.70	19.70	0	319.16	319.16	0	69.40	69.40	0
3	100 Year	34.10	34.10	0	319.74	319.74	0	141.61	141.61	0
3	Regional	38.60	38.60	0	320.43	320.43	0	154.38	154.38	0
4	5 Year	3.99	3.99	0	317.51	317.51	0	28.81	28.81	0
4	25 Year	19.70	19.70	0	319.16	319.16	0	69.44	69.44	0
4	100 Year	34.10	34.10	0	319.74	319.74	0	141.74	141.74	0
4	Regional	38.60	38.60	0	320.43	320.43	0	154.39	154.39	0
5	5 Year	3.99	3.99	0	317.51	317.51	0	28.83	28.83	0
5	25 Year	19.70	19.70	0	319.16	319.16	0	69.45	69.45	0
5	100 Year	34.10	34.10	0	319.74	319.74	0	141.75	141.75	0
5	Regional	38.60	38.60	0	320.43	320.43	0	154.39	154.39	0
6	5 Year	3.99	3.99	0	317.61	317.61	0	2.70	2.70	0
6	25 Year	19.70	19.70	0	319.15	319.15	0	47.90	47.90	0
6	100 Year	34.10	34.10	0	319.73	319.73	0	70.63	70.63	0
6	Regional	38.60	38.60	0	320.43	320.43	0	111.99	111.99	0
7	5 Year	3.99	3.99	0	317.92	317.92	0	2.70	2.70	0
7	25 Year	19.70	19.70	0	321.90	321.90	0	217.71	217.71	0
7	100 Year	34.10	34.10	0	322.84	322.84	0	256.71	256.71	0
7	Regional	38.60	38.60	0	322.92	322.92	0	257.16	257.16	0
7.1	5 Year	3.88	3.88	0	318.29	318.29	0	9.93	9.93	0
7.1	25 Year	19.10	19.10	0	321.90	321.90	0	87.25	87.25	0
7.1	100 Year	33.20	33.20	0	322.84	322.84	0	108.01	108.01	0
7.1	Regional	37.50	37.50	0	322.92	322.92	0	108.76	108.76	0

Sec No.	Design Storm	Flow (cu m/s)			W.S. Elevation (m)			Tope Width (m)		
		POST	PRE	Difference	POST	PRE	Difference	POST	PRE	Difference
7.2	5 Year	3.88	3.88	0	318.46	318.46	0	17.77	17.77	0
7.2	25 Year	19.10	19.10	0	321.90	321.90	0	102.47	102.47	0
7.2	100 Year	33.20	33.20	0	322.84	322.84	0	143.19	143.19	0
7.2	Regional	37.50	37.50	0	322.92	322.92	0	147.12	147.12	0
7.4	5 Year	3.88	3.88	0	318.49	318.49	0	20.75	20.75	0
7.4	25 Year	19.10	19.10	0	321.90	321.90	0	115.51	115.51	0
7.4	100 Year	33.20	33.20	0	322.84	322.84	0	164.21	164.21	0
7.4	Regional	37.50	37.50	0	322.92	322.92	0	167.36	167.36	0
7.6	5 Year	3.88	3.88	0	318.50	318.50	0	23.07	23.07	0
7.6	25 Year	19.10	19.10	0	321.90	321.90	0	135.91	135.91	0
7.6	100 Year	33.20	33.20	0	322.84	322.84	0	171.13	171.13	0
7.6	Regional	37.50	37.50	0	322.92	322.92	0	173.49	173.49	0
7.8	5 Year	3.88	3.88	0	318.52	318.52	0	24.59	24.59	0
7.8	25 Year	19.10	19.10	0	321.90	321.90	0	86.10	86.10	0
7.8	100 Year	33.20	33.20	0	322.84	322.84	0	167.67	167.67	0
7.8	Regional	37.50	37.50	0	322.92	322.92	0	172.11	172.11	0
8	5 Year	3.88	3.88	0	318.53	318.53	0	27.37	27.37	0
8	25 Year	19.10	19.10	0	321.90	321.90	0	71.51	71.51	0
8	100 Year	33.20	33.20	0	322.84	322.84	0	124.61	124.61	0
8	Regional	37.50	37.50	0	322.92	322.92	0	148.81	148.81	0
8.2	5 Year	3.88	3.88	0	318.54	318.54	0	25.89	25.89	0
8.2	25 Year	19.10	19.10	0	321.90	321.90	0	68.91	68.91	0
8.2	100 Year	33.20	33.20	0	322.84	322.84	0	80.54	80.54	0
8.2	Regional	37.50	37.50	0	322.92	322.92	0	81.53	81.53	0
8.4	5 Year	3.88	3.88	0	318.56	318.56	0	26.08	26.08	0
8.4	25 Year	19.10	19.10	0	321.90	321.90	0	67.40	67.40	0
8.4	100 Year	33.20	33.20	0	322.84	322.84	0	79.88	79.88	0
8.4	Regional	37.50	37.50	0	322.92	322.92	0	81.30	81.30	0
8.6	5 Year	3.88	3.88	0	318.68	318.68	0	18.51	18.51	0
8.6	25 Year	19.10	19.10	0	321.90	321.90	0	72.10	72.10	0
8.6	100 Year	33.20	33.20	0	322.84	322.84	0	83.91	83.91	0
8.6	Regional	37.50	37.50	0	322.92	322.92	0	85.08	85.08	0
8.8	5 Year	3.88	3.88	0	318.85	318.85	0	29.43	29.43	0
8.8	25 Year	19.10	19.10	0	321.91	321.91	0	76.87	76.87	0
8.8	100 Year	33.20	33.20	0	322.84	322.84	0	94.39	94.39	0
8.8	Regional	37.50	37.50	0	322.92	322.92	0	96.47	96.47	0
9	5 Year	3.88	3.88	0	318.89	318.89	0	19.97	19.97	0
9	25 Year	19.10	19.10	0	321.91	321.91	0	79.78	79.78	0
9	100 Year	33.20	33.20	0	322.84	322.84	0	93.77	93.77	0
9	Regional	37.50	37.50	0	322.92	322.92	0	95.54	95.54	0

Sec No.	Design Storm	Flow (cu m/s)			W.S. Elevation (m)			Tope Width (m)		
		POST	PRE	Difference	POST	PRE	Difference	POST	PRE	Difference
9.2	5 Year	3.88	3.88	0	319.17	319.17	0	27.90	27.90	0
9.2	25 Year	19.10	19.10	0	321.91	321.91	0	80.39	80.39	0
9.2	100 Year	33.20	33.20	0	322.84	322.84	0	98.70	98.70	0
9.2	Regional	37.50	37.50	0	322.92	322.92	0	102.83	102.83	0
9.4	5 Year	3.88	3.88	0	319.29	319.29	0	26.48	26.48	0
9.4	25 Year	19.10	19.10	0	321.91	321.91	0	90.30	90.30	0
9.4	100 Year	33.20	33.20	0	322.84	322.84	0	114.82	114.82	0
9.4	Regional	37.50	37.50	0	322.92	322.92	0	116.91	116.91	0
9.6	5 Year	3.88	3.88	0	319.33	319.33	0	22.08	22.08	0
9.6	25 Year	19.10	19.10	0	321.91	321.91	0	99.68	99.68	0
9.6	100 Year	33.20	33.20	0	322.84	322.84	0	117.49	117.49	0
9.6	Regional	37.50	37.50	0	322.92	322.92	0	119.01	119.01	0
9.7	5 Year	3.88	3.88	0	319.57	319.57	0	23.64	23.64	0
9.7	25 Year	19.10	19.10	0	321.91	321.91	0	101.41	101.41	0
9.7	100 Year	33.20	33.20	0	322.84	322.84	0	126.95	126.95	0
9.7	Regional	37.50	37.50	0	322.92	322.92	0	128.23	128.23	0
9.8	5 Year	3.88	3.88	0	319.77	319.77	0	25.74	25.74	0
9.8	25 Year	19.10	19.10	0	321.91	321.91	0	92.21	92.21	0
9.8	100 Year	33.20	33.20	0	322.84	322.84	0	127.80	136.09	8.29
9.8	Regional	37.50	37.50	0	322.92	322.92	0	128.37	139.38	11.01
9.9	5 Year	3.88	3.88	0	320.09	320.09	0	30.93	30.93	0
9.9	25 Year	19.10	19.10	0	321.90	321.90	0	81.14	81.14	0
9.9	100 Year	33.20	33.20	0	322.84	322.84	0	99.50	99.50	0
9.9	Regional	37.50	37.50	0	322.92	322.92	0	101.27	101.27	0
10	5 Year	3.88	3.88	0	320.14	320.14	0	44.86	44.86	0
10	25 Year	19.10	19.10	0	321.91	321.91	0	83.79	83.79	0
10	100 Year	33.20	33.20	0	322.84	322.84	0	102.95	102.95	0
10	Regional	37.50	37.50	0	322.92	322.92	0	104.59	104.59	0
11	5 Year	3.88	3.88	0	321.11	321.11	0	40.43	40.43	0
11	25 Year	19.10	19.10	0	322.72	322.72	0	87.53	87.53	0
11	100 Year	33.20	33.20	0	323.08	323.08	0	97.09	97.09	0
11	Regional	37.50	37.50	0	323.15	323.15	0	98.83	98.83	0
12	5 Year	3.88	3.88	0	321.14	321.14	0	47.28	47.28	0
12	25 Year	19.10	19.10	0	322.72	322.72	0	116.46	116.46	0
12	100 Year	33.20	33.20	0	323.09	323.09	0	125.46	125.46	0
12	Regional	37.50	37.50	0	323.15	323.15	0	127.11	127.11	0
13	5 Year	3.88	3.88	0	321.21	321.21	0	22.30	22.30	0
13	25 Year	19.10	19.10	0	322.73	322.73	0	58.71	58.71	0
13	100 Year	33.20	33.20	0	323.09	323.09	0	110.98	110.98	0
13	Regional	37.50	37.50	0	323.16	323.16	0	114.67	114.67	0

Sec No.	Design Storm	Flow (cu m/s)			W.S. Elevation (m)			Tope Width (m)		
		POST	PRE	Difference	POST	PRE	Difference	POST	PRE	Difference
14	5 Year	3.88	3.88	0	321.80	321.80	0	10.32	10.32	0
14	25 Year	19.10	19.10	0	322.72	322.72	0	64.91	64.91	0
14	100 Year	33.20	33.20	0	323.14	323.14	0	117.03	117.03	0
14	Regional	37.50	37.50	0	323.22	323.22	0	118.73	118.73	0
15	5 Year	3.69	3.69	0	322.84	322.84	0	26.55	26.55	0
15	25 Year	18.20	18.20	0	323.37	323.37	0	53.68	53.68	0
15	100 Year	31.60	31.60	0	323.65	323.65	0	76.40	76.40	0
15	Regional	35.80	35.80	0	323.72	323.72	0	84.70	84.70	0
16	5 Year	3.69	3.69	0	322.92	322.92	0	28.44	28.44	0
16	25 Year	18.20	18.20	0	323.43	323.43	0	41.85	41.85	0
16	100 Year	31.60	31.60	0	323.70	323.70	0	75.16	75.16	0
16	Regional	35.80	35.80	0	323.78	323.78	0	86.70	86.70	0
17	5 Year	3.69	3.69	0	324.97	324.97	0	328.35	328.35	0
17	25 Year	18.20	18.20	0	325.82	325.82	0	383.09	383.09	0
17	100 Year	31.60	31.60	0	325.90	325.90	0	387.87	387.87	0
17	Regional	35.80	35.80	0	325.92	325.92	0	389.45	389.45	0
18	5 Year	6.09	6.09	0	325.06	325.06	0	229.43	229.43	0
18	25 Year	19.30	19.30	0	325.82	325.82	0	279.50	279.50	0
18	100 Year	32.10	32.10	0	325.90	325.90	0	284.38	284.38	0
18	Regional	35.80	35.80	0	325.92	325.92	0	285.99	285.99	0
19	5 Year	6.09	6.09	0	325.06	325.06	0	206.06	206.06	0
19	25 Year	19.30	19.30	0	325.82	325.82	0	224.41	224.41	0
19	100 Year	32.10	32.10	0	325.90	325.90	0	225.63	225.63	0
19	Regional	35.80	35.80	0	325.92	325.92	0	226.04	226.04	0
20	5 Year	5.78	5.78	0	325.06	325.06	0	97.36	97.36	0
20	25 Year	18.30	18.30	0	325.82	325.82	0	108.08	108.08	0
20	100 Year	30.10	30.10	0	325.90	325.90	0	109.14	109.14	0
20	Regional	33.10	33.10	0	325.92	325.92	0	109.49	109.49	0
21	5 Year	5.78	5.78	0	325.06	325.06	0	122.56	122.56	0
21	25 Year	18.30	18.30	0	325.83	325.83	0	140.66	140.66	0
21	100 Year	30.10	30.10	0	325.90	325.90	0	142.72	142.72	0
21	Regional	33.10	33.10	0	325.93	325.93	0	143.40	143.40	0

**PRELIMINARY SERVICING &
STORMWATER MANAGEMENT REPORT
CITYVIEW RIDGE SUBDIVISION
CITY OF GUELPH
Revised: June 2017**

APPENDIX “G”

**Rip Rap Protection Calculations, Monthly Water Balance,
Monthly Enhanced Infiltration for Block 125**

105172 - 600mm Outlet

Riprap Outlet Protection Design Calculations

Assumptions:

- pipe discharges onto a relatively flat surface
- there is no well defined channel immediately downstream
- minimum tailwater conditions apply
- outlet pipe is flowing full

Given:

pipe diameter (D_o) =	0.6	m
=	24	inches
pipe slope =	0.5	%
maximum flow =	1.61	m ³ /s
=	56.86	ft ³ /s
outlet slope =	2.9	%

From Figure 7.45 (Erosion and Sediment Control Handbook, 1986)

Rip Rap Depth (d) =	30	in
=	0.76	m

Apron Length (L_a) =	22.00	ft
=	6.71	m

Median Stone Size (d_{50}) =	0.75	ft
=	0.23	m
=	229	mm

Upstream Apron Width (W_u) =	3 x D_o	
=	70.87	inches
=	1.80	m

Downstream Apron Width (W_d) =	$D_o + L_a$	
=	23.97	ft
=	7.31	m

Definition of Median Stone Size (d_{50}) :

50 percent by weight of a rock mixture is greater than or less than the d_{50} size.

Conclusions:

The actual depth of rip-rap (0.76m) is equal to the required rip-rap depth (0.76m)

The median stone size required for the rip rap of 229 mm is less than the specified mean size of 250 mm.

The required Upstream and Downstream Apron Width (W_u and W_d) of 1.80 m and 7.31 m, respectively are less than the specified width of 8.0m.

The required Apron Length (L_a) of 6.71m, is less than the specified length of 7.0m.

References:

Goldman, Steven J., Jackson, Katharine, and Bursztynsky, Taras A., 1986. Erosion and Sediment Control Handbook. New York: McGraw-Hill Incorporated.

Cityview Ridge Subdivision
City of Guelph
Monthly Water Balance (Thorntwaite and Mather Method)
Date: June 21, 2017

EXISTING CONDITIONS

Contributing Catchments:	10, 20 & 30	Soil Type: Guelph Loam - 76% Till; 24% Sand and Gravel	Impervious Area =	0.56	ha	Percent of Total Area	Runoff Factor =	0.43
Contributing Area =	18.28 ha	Vegetation: Shallow-rooted unkept vegetation	Pervious Till Area =	13.34	ha	3%	Evapotranspiration	
Percent Impervious =	3.0%	Root Zone Depth = 0.50m	Pervious S&G Area =	4.38	ha	73%	Factor for Impervious	
		Soil Moisture Retention Capacity = 75mm	Total Area =	18.28	ha	24%	Surfaces =	0.36
						100%		

Month	Daily Average Temperature	Monthly Heat Index (I)	Unadjusted Daily Potential Evapotranspiration	Correction Factors	Adjusted Potential Evapotranspiration (PE)	Average Precipitation (P)	P-PE	Accum. Pot. Water Loss	Storage (ST)	ΔS	Pervious ET	Actual Evapotranspiration (AE)	Pervious ET - Actual ET	Moisture Deficit (D)	Moisture Surplus (S)	Water Runoff (RO)	Snow Melt Runoff	Total Recharge and Runoff	Actual Runoff	Runoff Volume	Recharge Volume
	(°C)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(m³)	(m³)
Jan	-7.6	0.0	0.0	24.3	0.0	56.4	56.4		209.1	0.0		0.0	0.0	0.0	0.0	9.8	0.0	9.8	4.3	781	1,016
Feb	-6.9	0.0	0.0	24.6	0.0	50.8	50.8		259.9	0.0		0.0	0.0	0.0	0.0	4.9	0.0	4.9	2.1	390	508
Mar	-1.3	0.0	0.0	30.6	0.0	72.1	72.1		332.0	0.0		0.0	0.0	0.0	0.0	2.5	0.0	2.5	1.1	195	254
Apr	5.9	1.3	0.9	33.6	30.2	78.3	48.1		75.0	0.0	30.2	29.7	0.6	0.6	48.6	25.5	25.7	51.2	22.3	4,069	5,294
May	12.3	3.9	2.0	37.8	75.6	79.9	4.3		75.0	0.0	75.6	74.1	1.5	1.5	5.8	15.6	115.7	131.3	57.1	10,430	13,569
Jun	16.9	6.3	2.8	38.4	107.5	76.0	-31.5	-31.5	48.0	-27.0	103.0	101.0	2.0	6.5	2.0	8.8	57.8	66.6	29.0	5,294	6,887
Jul	19.7	8.0	3.3	38.7	127.7	88.5	-39.2	-70.7	28.0	-20.0	108.5	106.4	2.1	21.3	2.1	5.4	28.9	34.4	14.9	2,730	3,551
Aug	18.6	7.3	3.1	36.0	111.6	95.9	-15.7	-86.4	23.0	-5.0	100.9	99.0	1.9	12.6	1.9	3.7	14.5	18.1	7.9	1,442	1,876
Sep	14.1	4.8	2.3	31.2	71.8	92.1	20.3		43.3	20.3	71.8	70.4	1.4	1.4	1.4	2.5	7.5	10.0	4.4	797	1,037
Oct	7.9	2.0	1.3	28.5	37.1	69.2	32.2		75.0	31.7	37.1	36.3	0.7	0.7	1.2	1.9	3.9	5.8	2.5	458	596
Nov	2.4	0.3	0.4	24.3	9.7	86.3	76.6		75.0	0.0	9.7	9.5	0.2	0.2	76.8	39.3	2.0	41.3	18.0	3,282	4,270
Dec	-4.0	0.0	0.0	23.1	0.0	77.7	77.7		152.7	0.0		0.0	0.0	0.0	0.0	19.7	1.1	20.8	9.0	1,649	2,146
Total		33.9				923.2	352.0					526.5	10.3	44.7	139.7	139.7	257.0	396.7	172.4	31,518	41,003

POST-DEVELOPMENT CONDITIONS

Contributing Catchments:	B2c, 201, 202 & 300	Soil Type: Guelph Loam - 76% Till; 24% Sand and Gravel	Impervious Area =	5.91	ha	Percent of Total Area	Runoff Factor =	0.71
Contributing Area =	17.60 ha	Vegetation: Urban lawns	Pervious Till Area =	7.99	ha	34%	Evapotranspiration	
Percent Impervious =	32.0%	Root Zone Depth = 0.5m	Pervious S&G Area =	3.7	ha	45%	Factor for Impervious	
		Soil Moisture Retention Capacity = 75mm	Total Area =	17.6	ha	21%	Surfaces =	0.36
						100%		

Month	Daily Average Temperature	Monthly Heat Index	Unadjusted Daily Potential Evapotranspiration	Correction Factors	Adjusted Potential Evapotranspiration	Average Precipitation	P-PE	Accum. Pot. Water Loss	Storage	ΔS	Pervious ET	Actual Evapotranspiration	Pervious ET - Actual ET	Moisture Deficit	Moisture Surplus	Water Runoff	Snow Melt Runoff	Total Recharge & Runoff	Actual Runoff	Runoff Volume	Recharge Volume	Enhanced Recharge
	(°C)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(m³)	(m³)	(m³)
Jan	-7.6	0.0	0.0	24.3	0.0	56.4	56.4		209.1	0.0		0.0	0.0	0.0	0.0	11.6	0.0	11.6	8.2	1,500	590	55
Feb	-6.9	0.0	0.0	24.6	0.0	50.8	50.8		259.9	0.0		0.0	0.0	0.0	0.0	5.8	0.0	5.8	4.1	750	295	28
Mar	-1.3	0.0	0.0	30.6	0.0	72.1	72.1		332.0	0.0		0.0	0.0	0.0	0.0	2.9	0.0	2.9	2.1	375	147	14
Apr	5.9	1.3	0.9	33.6	30.2	78.3	48.1		75.0	0.0	30.2	20.9	9.4	9.4	57.4	30.2	25.7	55.9	39.7	7,249	2,851	246
May	12.3	3.9	2.0	37.8	75.6	79.9	4.3		75.0	0.0	75.6	52.2	23.4	23.4	27.7	28.9	115.7	144.6	102.6	18,763	7,379	646
Jun	16.9	6.3	2.8	38.4	107.5	76.0	-31.5	-31.5	48.0	-27.0	103.0	101.0	2.0	6.5	2.0	15.4	57.8	73.3	52.0	9,510	3,740	323
Jul	19.7	8.0	3.3	38.7	127.7	88.5	-39.2	-70.7	28.0	-20.0	108.5	106.4	2.1	21.3	2.1	8.8	28.9	37.7	26.8	4,890	1,923	161
Aug	18.6	7.3	3.1	36.0	111.6	95.9	-15.7	-86.4	23.0	-5.0	100.9	99.0	1.9	12.6	1.9	5.4	14.5	19.8	14.1	2,571	1,011	81
Sep	14.1	4.8	2.3	31.2	71.8	92.1	20.3		43.3	20.3	71.8	49.6	22.2	22.2	22.2	13.8	7.5	21.3	15.1	2,761	1,086	141
Oct	7.9	2.0	1.3	28.5	37.1	69.2	32.2		75.0	31.7	37.1	25.6	11.5	11.5	11.9	12.9	3.9	16.8	11.9	2,175	855	124
Nov	2.4	0.3	0.4	24.3	9.7	86.3	76.6		75.0	0.0	9.7	6.7	3.0	3.0	79.6	46.2	2.0	48.2	34.2	6,259	2,461	228
Dec	-4.0	0.0	0.0	23.1	0.0	77.7	77.7		152.7	0.0		0.0	0.0	0.0	0.0	23.1	1.1	24.2	17.2	3,142	1,236	114
Total		33.9				923.3	352.0					461.4	75.4	109.8	204.8	204.8	257.0	461.9	327.9	59,944	23,573	2,161
																				Total Recharge		25,734

Notes: Precipitation and Temperature data from Environment Canada Climate Normals 1971-200 for the Guelph Arboretum
Monthly water balance strategy as outlined in the document *Instructions and Tables for Computing Potential Evapotranspiration and the Water Balance (Thorntwaite and Mather, 1957)*
Evaporation Factor for Impervious Surfaces = Average Annual Evapotranspiration for Impervious Surfaces (200mm/year) / Average Annual Evapotranspiration for Pervious Till Surfaces (555mm/year) = 0.36
Runoff Factor = [(Impervious Percentage of Site x Average Annual Runoff for Impervious Surfaces (725mm/year)) + (Pervious Till Percentage of Site x Average Annual Runoff for Pervious Till Surfaces (190 mm/year)) + (Pervious Sand & Gravel Percentage of Site x Average Annual Runoff for Pervious S & G Surfaces (50 mm/year))] / Total Annual Recharge & Runoff

Cityview Ridge Subdivision
City of Guelph
Monthly Water Balance (Thornthwaite and Mather Method)
Date: June 21, 2017

EXISTING CONDITIONS

Contributing Catchments:	Block 125	Soil Type: 100% Sand and Gravel	Impervious Area =	0	ha	Percent of Total Area	Runoff Factor =	0.12
Contributing Area =	0.65 ha	Vegetation: Shallow-rooted unkept vegetation	Pervious Till Area =	0.00	ha	0%		
Percent Impervious =	0.0%	Root Zone Depth = 0.50m	Pervious S&G Area =	0.65	ha	100%	Evapotranspiration Factor for Impervious Surfaces =	0.36
		Soil Moisture Retention Capacity = 75mm	Total Area =	0.65	ha	100%		

Month	Daily Average Temperature	Monthly Heat Index (I)	Unadjusted Daily Potential Evapotranspiration	Correction Factors	Adjusted Potential Evapotranspiration (PE)	Average Precipitation (P)	P-PE	Accum. Pot. Water Loss	Storage (ST)	ΔS	Pervious ET	Actual Evapotranspiration (AE)	Pervious ET - Actual ET	Moisture Deficit (D)	Moisture Surplus (S)	Water Runoff (RO)	Snow Melt Runoff	Total Recharge and Runoff	Actual Runoff	Runoff Volume	Recharge Volume
	(°C)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(m³)	(m³)
Jan	-7.6	0.0	0.0	24.3	0.0	56.4	56.4		209.1	0.0		0.0	0.0	0.0	0.0	9.7	0.0	9.7	1.2	8	55
Feb	-6.9	0.0	0.0	24.6	0.0	50.8	50.8		259.9	0.0		0.0	0.0	0.0	0.0	4.8	0.0	4.8	0.6	4	28
Mar	-1.3	0.0	0.0	30.6	0.0	72.1	72.1		332.0	0.0		0.0	0.0	0.0	0.0	2.4	0.0	2.4	0.3	2	14
Apr	5.9	1.3	0.9	33.6	30.2	78.3	48.1		75.0	0.0	30.2	30.2	0.0	0.0	48.1	25.2	25.7	50.9	6.1	40	291
May	12.3	3.9	2.0	37.8	75.6	79.9	4.3		75.0	0.0	75.6	75.6	0.0	0.0	4.3	14.8	115.7	130.4	15.6	102	746
Jun	16.9	6.3	2.8	38.4	107.5	76.0	-31.5	-31.5	48.0	-27.0	103.0	103.0	0.0	4.5	0.0	7.4	57.8	65.2	7.8	51	373
Jul	19.7	8.0	3.3	38.7	127.7	88.5	-39.2	-70.7	28.0	-20.0	108.5	108.5	0.0	19.2	0.0	3.7	28.9	32.6	3.9	25	186
Aug	18.6	7.3	3.1	36.0	111.6	95.9	-15.7	-86.4	23.0	-5.0	100.9	100.9	0.0	10.7	0.0	1.8	14.5	16.3	2.0	13	93
Sep	14.1	4.8	2.3	31.2	71.8	92.1	20.3		43.3	20.3	71.8	71.8	0.0	0.0	0.0	0.9	7.5	8.4	1.0	7	48
Oct	7.9	2.0	1.3	28.5	37.1	69.2	32.2		75.0	31.7	37.1	37.1	0.0	0.0	0.5	0.7	3.9	4.6	0.6	4	26
Nov	2.4	0.3	0.4	24.3	9.7	86.3	76.6		75.0	0.0	9.7	9.7	0.0	0.0	76.6	38.6	2.0	40.6	4.9	32	232
Dec	-4.0	0.0	0.0	23.1	0.0	77.7	77.7		152.7	0.0		0.0	0.0	0.0	0.0	19.3	1.1	20.4	2.5	16	117
Total		33.9				923.2	352.0					536.8	0.0	34.4	129.4	129.4	257.0	386.5	46.4	301	2,211

POST-DEVELOPMENT CONDITIONS

Contributing Catchments:	Block 125	Soil Type: 100% Sand and Gravel	Impervious Area =	0.46	ha	Percent of Total Area	Runoff Factor =	0.74
Contributing Area =	0.65 ha	Vegetation: Urban lawns	Pervious Till Area =	0.00	ha	0%		
Percent Impervious =	70.0%	Root Zone Depth = 0.5m	Pervious S&G Area =	0.20	ha	30%	Evapotranspiration Factor for Impervious Surfaces =	0.36
		Soil Moisture Retention Capacity = 75mm	Total Area =	0.65	ha	100%		

Month	Daily Average Temperature	Monthly Heat Index	Unadjusted Daily Potential Evapotranspiration	Correction Factors	Adjusted Potential Evapotranspiration	Average Precipitation	P-PE	Accum. Pot. Water Loss	Storage	ΔS	Pervious ET	Actual Evapotranspiration	Pervious ET - Actual ET	Moisture Deficit	Moisture Surplus	Water Runoff	Snow Melt Runoff	Total Recharge & Runoff	Actual Runoff	Runoff Volume	Recharge Volume	Enhanced Recharge Volume
	(°C)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)		(mm)		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(m³)	(m³)	(m³)
Jan	-7.6	0.0	0.0	24.3	0.0	56.4	56.4		209.1	0.0		0.0	0.0	0.0	0.0	13.8	0.0	13.8	10.2	66	24	55
Feb	-6.9	0.0	0.0	24.6	0.0	50.8	50.8		259.9	0.0		0.0	0.0	0.0	0.0	6.9	0.0	6.9	5.1	33	12	28
Mar	-1.3	0.0	0.0	30.6	0.0	72.1	72.1		332.0	0.0		0.0	0.0	0.0	0.0	3.5	0.0	3.5	2.5	17	6	14
Apr	5.9	1.3	0.9	33.6	30.2	78.3	48.1		75.0	0.0	30.2	9.1	21.2	21.2	69.2	36.1	25.7	61.8	45.5	295	106	246
May	12.3	3.9	2.0	37.8	75.6	79.9	4.3		75.0	0.0	75.6	22.7	52.9	52.9	57.2	46.6	115.7	162.3	119.4	776	278	646
Jun	16.9	6.3	2.8	38.4	107.5	76.0	-31.5	-31.5	48.0	-27.0	103.0	103.0	0.0	4.5	0.0	23.3	57.8	81.1	59.7	388	139	323
Jul	19.7	8.0	3.3	38.7	127.7	88.5	-39.2	-70.7	28.0	-20.0	108.5	108.5	0.0	19.2	0.0	11.7	28.9	40.6	29.9	194	70	161
Aug	18.6	7.3	3.1	36.0	111.6	95.9	-15.7	-86.4	23.0	-5.0	100.9	100.9	0.0	10.7	0.0	5.8	14.5	20.3	14.9	97	35	81
Sep	14.1	4.8	2.3	31.2	71.8	92.1	20.3		43.3	20.3	71.8	21.5	50.2	50.2	50.2	28.0	7.5	35.5	26.2	170	61	141
Oct	7.9	2.0	1.3	28.5	37.1	69.2	32.2		75.0	31.7	37.1	11.1	25.9	25.9	26.4	27.2	3.9	31.1	22.9	149	53	124
Nov	2.4	0.3	0.4	24.3	9.7	86.3	76.6		75.0	0.0	9.7	2.9	6.8	6.8	83.4	55.3	2.0	57.3	42.2	274	98	228
Dec	-4.0	0.0	0.0	23.1	0.0	77.7	77.7		152.7	0.0		0.0	0.0	0.0	0.0	27.7	1.1	28.8	21.2	138	49	114
Total		33.9				923.3	352.0					379.7	157.1	191.5	286.5	285.9	257.0	543.0	399.6	2,598	932	2,161

Notes: Precipitation and Temperature data from Environment Canada Climate Normals 1971-200 for the Guelph Arboretum

Monthly water balance strategy as outlined in the document *Instructions and Tables for Computing Potential Evapotranspiration and the Water Balance (Thornthwaite and Mather, 1957)*

Evaporation Factor for Impervious Surfaces = Average Annual Evapotranspiration for Impervious Surfaces (200mm/year) / Average Annual Evapotranspiration for Pervious Till Surfaces (555mm/year) = 0.36

Runoff Factor = 1-[(Pervious Sand & Gravel Percentage of Site x Average Annual Infiltration for Pervious S & G Surfaces (380 mm/year))] / Total Annual Recharge & Runoff

Total Recharge Volume3,093

Runoff Volume After Enhancement437

Pre-Runoff - Post-Runoff-135

**Cityview Ridge Subdivision
City of Guelph
Monthly Enhanced Infiltration at Block 125**

Enhanced Infiltration Structure - Catchment 100

Structure Length = 20.00 m
Structure Width = 9.00
Structure Depth = 1.00

Area of Stone = 9.00 sq m

Volume of Stone = 180.00 cu m
Stone Porosity = 0.33333

Storage Volume of Stone = 60.00 cu m

A = contact area of structure = 180.00 sq m
V = runoff volume to be infiltrated = 60.00 cu m
P = percolation rate of native soils = 15.00000 mm/hr
n = porosity of storage media (weighted) = 0.33
T = retention time = Solve for T

$T = (1000 \times V) / (P \times n \times A) = 67.34 \text{ hours or } 2.8 \text{ day draindown period}$

Contributing Area 0.398 ha (Area to Infiltration Gallery)
Recharge Time 67.34 hours / 2.81 days
Recharge Volume Potential 60.00 m³

Month	Total Recharge & Runoff	No. of days	Max Potential Recharge	Available Recharge	Enhanced Recharge
	(mm)		(m ³)	(m ³)	(m ³)
Jan	13.8	31	663	55	55
Feb	6.9	28	599	28	28
Mar	3.5	31	663	14	14
Apr	61.8	30	642	246	246
May	162.3	31	663	646	646
Jun	81.1	30	642	323	323
Jul	40.6	31	663	161	161
Aug	20.3	31	663	81	81
Sep	35.5	30	642	141	141
Oct	31.1	31	663	124	124
Nov	57.3	30	642	228	228
Dec	28.8	31	663	114	114
Total	543.0	365	7,805	2,161	2,161