

Functional Servicing Report for 1242, 1250, 1260 & 1270 Gordon Street and 9 Valley Road – Guelph ON

June 8, 2022

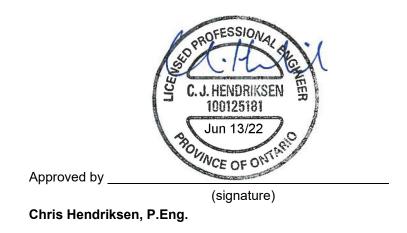
Prepared for:

Tricar Developments Inc.

Prepared by:

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### **Table of Contents**

1.0	INTRODUCTION AND BACKGROUND	1.1
1.1	OVERVIEW	1.1
1.2	BACKGROUND INFORMATION	1.1
1.3	EXISTING INFRASTRUCTURE	1.2
2.0	OVERALL GRADING AND DRAINAGE	2.2
2.1	DESIGN CONSTRAINTS AND PROCEDURES	2.2
2.2	PROPOSED ROAD PROFILES AND OVERALL SITE GRADING	2.3
3.0	SANITARY SERVICING	3.3
4.0	WATER DISTRIBUTION	4.3
5.0	STORMWATER MANAGEMENT (SWM) STRATEGY	5.4
5.1	STORMWATER MANAGEMENT CRITERIA	
	5.1.1 Hanlon Creek Watershed Plan (HCWP)	
	5.1.2 Torrance Creek Subwatershed Study (TCSS)	5.4
	5.1.3 City of Guelph Development Engineering Manual	
	5.1.4 Criteria for the Site	
5.2	SOILS INFORMATION	5.5
5.3	HYDROLOGIC MODELING	5.6
5.4	EXISTING CONDITIONS	5.6
5.5	PROPOSED CONDITIONS	5.7
5.6	STORMWATER MANAGEMENT	5.8
	5.6.1 Water Quantity Controls	5.8
	5.6.2 Infiltration Augmentation	5.8
	5.6.3 StormTech® Subsurface SWM Facility	5.8
	5.6.4 Hydrologic Modeling Results	
	5.6.5 Water Quality Controls	
5.7	SALT MANAGEMENT	5.10
6.0	CONCLUSIONS AND RECOMMENDATIONS	6.10

**APPENDIX A – PRELIMINARY CIVIL DRAWING PACKAGE** 

#### **APPENDIX B – DESIGN SHEETS**

#### APPENDIX C – EMAIL CORRESPONDENCE

#### APPENDIX D – SWM FIGURES, MODELS & SUPPORTING DATA

### **1.0 INTRODUCTION AND BACKGROUND**

### 1.1 OVERVIEW

This Functional Servicing Report has been prepared in support of the Zoning and Official Plan amendment and the Site Plan Application for the proposed development located at 1242, 1250, 1260 & 1270 Gordon Street and 9 Valley Road (Site) in the City of Guelph (City). The subject property is approximately 3.323 ha in size and is bounded to the northwest by existing residential subdivision, to the northeast by protected woodlot, to the southwest by Gordon Street, and to the southeast existing highdensity development.

The conceptual site plan for the proposed development that forms the basis of this servicing assessment includes two 10 story apartment buildings consisting of 325 units. The bulk of site parking will be achieved through underground and at/above grade enclosed parking.

This report outlines how the proposed development can be supplied with adequate services, including sanitary, domestic water, storm drainage and includes the preliminary design of the infiltration and water quality facilities proposed to provide the required water quality and quantity controls and the preliminary erosion and sediment control strategy to be implemented during construction.

### 1.2 BACKGROUND INFORMATION

A variety of sources have been referenced during the preparation of this report, and the following should be read in conjunction with this Report:

- Geotechnical Engineering Report, Two 12-Storey Apartment Buildings 1242, 1250, 1260 Gordon Street, Guelph, Ontario (CMT Engineering Inc, April 2018)
- Low Impact Development Stormwater Management Planning and Design Guide (Credit Valley Conservation Authority and Toronto and Region Conservation Authority, 2010)
- Erosion & Sediment Control Guideline for Urban Construction, (Greater Golden Horseshoe Area Conservation Authorities, December 2006)
- Stormwater Management Planning and Design Manual (SWMPD Manual), (Ontario Ministry of the Environment, March 2003)
- Development Engineering Manual, City of Guelph (City of Guelph Engineering and Transportation Services, January 2019)
- Groundwater Flow, Figure 14 of 1242, 1250, 1260 Gordon Street and 9 Valley Road Hydrogeological Assessment (Stantec Consulting Ltd., March 2020)

- Hanlon Creek Watershed Plan (Marshal Macklin Monaghan Ltd., LGL Ltd., October 1993)
- Torrance Creek Subwatershed Study- Management Strategy (Totten Sims Hubicki Associates, et al, September 1998)

### **1.3 EXISTING INFRASTRUCTURE**

A summary of the municipal infrastructure that currently exists near the Site is as follows:

- A 200mm sanitary sewer located on Gordon Street.
- A 400mm watermain on Gordon.
- A 575mm storm sewer on Gordon Street.

Fully constructed municipal roads include Gordon Street to the west and Valley Road to the north.

## 2.0 OVERALL GRADING AND DRAINAGE

### 2.1 DESIGN CONSTRAINTS AND PROCEDURES

Using existing topographic information provided by BSR&D limited (dated November 2014), the proposed Site grading will be designed to generally meet the following criteria:

- Match existing grades at all site boundaries.
- Match existing grades at existing tree driplines wherever possible to facilitate tree retention.
- Extension of Edinburgh Road and Valley Road to municipal standards and match into existing road grades of Gordon Street and Valley Road.
- Account for future urbanization of adjacent lands.
- Have consideration for future pedestrian connections north of the site towards Valley Road.
- Provide adequate cover over underground services.
- Ensure all building openings are protected from flooding.
- Comply with Municipal standards for minimum and maximum grades.
- Provide major overland flow routes for flows exceeding the storm sewer capacity.
- Maintain drainage from Gordon Street right-of-way and neighboring properties to the north and south.



### 2.2 PROPOSED ROAD PROFILES AND OVERALL SITE GRADING

Road profiles within the subject site were established based on the proposed street pattern to satisfy the constraints outlined in the previous Section 2.1. The road profiles have been designed to accommodate the constraints set out by the site layout and underground parking limits with grades ranging from 0.5% to 8.0% with 3:1 and 4:1 transition slopes or retaining walls utilized to accommodate the various grade changes within the site and at various perimeter locations. The proposed centerline road elevations for the extension Landsdown Drive and Edinburgh Road and lot grades are illustrated on the Grading plan as well as the plan and profile provided for these extensions (Drawing No. 5 of 8 and 4 of 8 respectively) included in Appendix A. Existing grades and cross sections of Gordon Street and Valley Road have been considered fixed constraints in the development of the preliminary grading. The extension of Landsdown Drive and Edinburgh Road will be 8.4m back of curb to back of curb as per City of Guelph's Linear Infrastructure Standard drawing SD-48a. Internal roads, consisting of 6.7m wide asphalt as the building has structured parking not subject to the standard 7.0m minimum width drive aisle.

### 3.0 SANITARY SERVICING

The City of Guelph is currently completing the Gordon Street Improvements EA and an overall Master Wastewater Servicing Plan that is considering an upgrade to the sanitary service capacity within Gordon Street fronting the site. Through correspondence with the City in 2019 through 2022, the proposed development will be incorporated in the design of the sanitary sewer upgrades. Confirmation of this has been received from Ike Umar via email on March 15, 2022 (see email correspondence attached in Appendix C). Staff have recommended that an H be applied to the property until such time as the sewer has been installed and the outlet is available however timing of the two projects may alleviate this requirement.

A 200mm extension of the municipal sanitary sewer east on the Edinburgh Road extension proposed as part of this redevelopment to provide service to the site. Sewers will be designed in accordance with the requirements of the Ontario Building Code and the City of Guelph. An illustration of the sanitary sewer layout can be found in the Sanitary Area Plan (Sheet No. 3 of 8) included in Appendix A.

### 4.0 WATER DISTRIBUTION

The existing water distribution system near the Site includes a 400mm watermain on Gordon Street. The primary source for the proposed development will be the Gordon Street watermain. It is anticipated that the following work to the existing municipal infrastructure will be made:

- Tapping sleeve and valve connection to the 400mm Gordon Street watermain (200mm connection).
- Extension of the municipal watermain along the Edinburgh Road extension to provide service to the Site.



Please refer to the Preliminary Servicing plan (Drawing No. 1 of 8) for an illustration of the watermain layout.

Based on building information currently available, a conservative fire flow requirement for the site is 150 L/s, based on typical OBC calculations as provided in Appendix B.

A 200 mm diameter watermain is proposed for the development with 200mm connections provided to each building. They are positioned as illustrated on the Preliminary Servicing plan (Drawing No. 1 of 8).

Fire protection will be provided via onsite hydrants, adequately spaced to ensure proper coverage to all buildings, in conjunction with standpipe connections for building sprinkler systems. The City of Guelph will confirm the pipe sizing proposed provides adequate pressure to meet MOE design criteria. No backflow prevention or pressure reducing valves (PRV) have been proposed for this development.

The City has advised that sufficient and adequate capacity is available in the City's existing water supply and distribution system to accommodate the proposed development and there are no water capacity constraints expected for most demand scenarios. However, there is potential for marginal water supply pressures in proposed development under certain conditions such as peak hour demand scenario at locations with elevation greater than 346 m height above mean sea level (AMSL) and average day demand scenario at locations with elevation greater than 339 m height AMSL in the existing water system.

### 5.0 STORMWATER MANAGEMENT (SWM) STRATEGY

### 5.1 STORMWATER MANAGEMENT CRITERIA

This site is covered by criteria from different documents. The documents and site criteria are discussed below.

#### 5.1.1 Hanlon Creek Watershed Plan (HCWP)

The HCWP states that for upper Hanlon Creek development no urban drainage will be permitted to the headwaters of Tributary E or F, except for lands that already have drainage outlets. All stormwater generated from the area must either infiltrate into the ground or evaporate (100-year infiltration and zero runoff). There is no discussion in the report on requirements for redeveloping lands within the existing development areas where this project is located.

#### 5.1.2 Torrance Creek Subwatershed Study (TCSS)

The TCSS states that for Zone 2, where this site is located, the requirement is to detain the postdevelopment flow to pre-development ratees for the 2- to 100-year events and to infiltrate 150 mm/yr.

#### 5.1.3 City of Guelph Development Engineering Manual

The specific SWM Criteria for the Site from the City of Guelph Development Engineering Manual (January 2019) is outlined below.

Water Quantity Control

• Based on City Guidelines, on-site stormwater control should be sized to attenuate postdevelopment peaks flows to the pre-development (existing) peak flows. This 'post-to-pre' control should be provided for the 2-year through to the 100-year storm events.

Water Quality Control

Based on City guidelines, the feasibility of on-site infiltration should be investigated. All developments are required to provide a minimum of Enhanced water quality level protection (i.e., 80% TSS removal). It is recommended for small development sites (approximately 2 ha) a treatment train approach be followed.

#### 5.1.4 Criteria for the Site

The HCWP appears to be more applicable to development in the upper Hanlon Creek areas, with drainage to Tributaries E and F. The project site is located in the 'existing development' area within the study and is not specifically addressed within the plan and drains to Tributary D.

Additionally, the GRCA mapping for the site shows a recharge of 122-199 mm/year and runoff of 118-207 mm/year while sites within the Upper Hanlon Creek area have a recharge of 315-371 mm/year and a runoff of 0 mm/year, showing that the flow regime for the two areas is obviously different.

Based on the above information, it was decided that applying the TCSS criteria to the site was a reasonable approach based on the information available. The SWM criteria for the site are as follows:

- Attenuate post-development peak flows to pre-development rates for the 2-year though 100-year storm events
- Maintain infiltration balance
- Minimum of Enhanced Water Quality Protection.

### 5.2 SOILS INFORMATION

Site soil properties were confirmed using the Geotechnical Investigation Report (XCG Consulting Ltd., April 2018), which outlined soil conditions for the site as per tested boreholes. It was confirmed that site soils can be expected to be sand – silt with traces of clay, with overall good drainage properties. For this analysis, site soils were classified as BC, which was deemed to be a conservative estimate.

Infiltration rates for the site were determined to be approximately 23 mm/hr for the south portion of the site and 32 mm/hr for the east portion of the site. These design rates were calculated by Stantec Consulting Ltd. (Stantec) based on test pit and infiltration testing completed in June 2021.

A hydrogeologic assessment of the Site was completed by Stantec, and is documented in the Hydrogeological Report, 1242, 1250, 1260 Gordon Street, and 9 Valley Road, City of Guelph (Stantec, 2020 and as amended). In the Site monitoring well MW5 – 18S a high water table elevation of 340.3 m was recorded. The groundwater flow follows a similar divide as surface water, with a portion flowing east as part of the Torrance Creek Watershed, and another portion flowing west as part of the Hanlon Creek Watershed.

### 5.3 HYDROLOGIC MODELING

A hydrologic model was prepared to simulate drainage conditions for the subject development. MIDUSS was used to predict flows for the existing and proposed development conditions and to design the SWM system to ensure the previously mentioned criteria were achieved.

To address the criteria, existing and post-development conditions were modeled for the 2 year, 5 year and 100 year 3-hour Chicago design storms, derived using the City of Guelph parameters as provided in Table 1.

Storm Event	а	b	C	Duration (hrs.)	Depth (mm)
2-year	743	6	0.798		34
5-year	1593	11	0.879	3	47
100-year	4688	17	0.925		87

Table 1: City of Guelph – Chicago Storm Parameters

### 5.4 EXISTING CONDITIONS

The proposed development encompasses 3.323 ha and 5 residential properties however this infill project is unique with a portion of the site being dedicated as municipal right-of-way with different controls and so for the purposes of the proposed site SWM design, the existing site is defined by lands outside the municipal right-of-way being 3.05 ha including 4 residential properties with gravel/asphalt driveways. A large portion of the site is a woodlot area, associated with the Torrance Creek Swamp (Provincially Significant Wetland), and generally has steep slopes (approximately 5 %). A portion of the properties drain to an existing storm sewer on Gordon Street. The drainage catchments are shown on Figure 1, attached, and are summarized below.

- Catchment 101 A 1.33 ha area that includes residential homes, with storm water out-letting to Gordon Street to the west.
- **Catchment 102** A 1.72 ha undeveloped area, which discharges as shallow overland flow to the woodlot to the east, part of the Torrance Creek Swamp

#### 5.5 **PROPOSED CONDITIONS**

The proposed site plan includes two 10-storey apartment buildings, with two levels of underground parking. The proposed drainage catchments are summarized in detail below and shown in Figure 2, attached. Generally, the proposed conditions will increase the area out-letting to Gordon Street to the west and will reduce the area out-letting to the Torrance watershed to the east. The development will also increase the impervious area and will produce an increase in stormwater flows to the downstream Gordon Street storm sewer.

- Catchment 201 A 0.09 ha building/landscaped area that will drain uncontrolled to Gordon Street to the west.
- Catchment 202 A 0.24 ha roof top area. Runoff from this area will be attenuated by a roof-top control system (Zurn Z105 Control-Flo Roof Drain, or approved equivalent), controlling 100-year storm event runoff to a rate of 42L/s/ha (industry standard). The first 25 mm of runoff will be directed to an infiltration chamber (StormTech® SC-310) while overflows will be directed to a subsurface stormwater detention facility (StormTech® M-3500) and ultimately the Gordon Street storm sewer.
- Catchment 203 A 0.24 ha rooftop area. Runoff from this area will be attenuated by a roof-top control system (Zurn Z105 Control-Flo Roof Drain, or approved equivalent), controlling 100-year storm event runoff to a rate of 42L/s/ha (industry standard). Rooftop runoff will discharge to a clearstone infiltration gallery designed to infiltrate the runoff from a 25 mm event, with overflows discharging overland the Torrance Creek Swamp.
- **Catchment 204** A 0.51 ha area, including the parking area, lane-way and small portions of landscape. Runoff will be collected by catchbasins and conveyed via a storm sewer system to a StormTech® infiltration chamber. Prior to discharging to the chamber, flows will be treated with an oil/grit-separator and StormTech® Isolator Row Plus, to minimize the potential for clogging. Flows exceeding that capacity of the infiltration chamber will discharge to an underground StormTech® stormwater detention facility (StormTech® M-3500) and ultimately the Gordon Street storm sewer.
- **Catchment 205** A 0.23 ha designated park area draining uncontrolled east to the Torrance Watershed.
- **Catchment 206** A 1.41 ha undeveloped woodlot area draining uncontrolled east to the Torrance Watershed.
- **Catchment 207** A 0.15 ha landscaped area that will outlet to the StormTech® subsurface stormwater detention facility.
- Catchment 208 A 0.06 ha amenity area, which will flow uncontrolled to the Gordon Street storm sewer.
- Catchment 209 A 0.12 ha parking area, with minor flows (up to the 5-year storm event) collected via parking lot structure roof drains and conveyed south to the StormTech® infiltration chamber (StormTech® SC-310) while overflows will be directed to a subsurface stormwater detention facility (StormTech® M-3500) and ultimately the Gordon Street storm sewer. Major flows (larger than the 5-year storm event) will outlet via overland flow to Street A and ultimately the Gordon Street storm sewer.



• **Catchment 210** – 0.11 ha of Street A right-of-way. Street A is a proposed municipal right-of-way not part of the proposed development. Based on discussions with the City of Guelph water quantity controls are not required for this portion of the site, and therefore has only been included in figures for completeness.

#### 5.6 STORMWATER MANAGEMENT

#### 5.6.1 Water Quantity Controls

Water Quantity controls for the subject site will be provided through the use of rooftop flow controls, infiltration chambers/galleries and a subsurface stormwater management facility.

#### 5.6.2 Infiltration Augmentation

Two infiltration facilities have been provided augment infiltration of site runoff.

The east infiltration gallery is a 7.5 m (W) x 10 m (L) x 1 m (D) clearstone infiltration gallery designed to infiltrate the runoff from Building 2 (easternmost building, Catchment 203) under the 25 mm storm event. Overflows from the gallery will discharge overland to the Torrance Creek Swamp east of the site. An infiltration rate of 32 mm/hr was assumed based on the Hydrogeological Report (Stantec, 2020 and as amended)

The south infiltration gallery has been designed to infiltrate the runoff from Catchment 202, 204 and 209 under the 25 mm storm event. The volume of the proposed chamber is 116 m<sup>3</sup> and is comprised of StormTech® SC-310 units (drawings attached). Overflows will discharge to a subsurface stormwater detention facility, prior to discharging to the Gordon Street Storm Sewer. An overflow weir with an elevation equal to the obvert of the infiltration chamber has been provided in MH6 direct flows to the gallery prior to overflow discharge to the downstream system. An infiltration rate of 23 mm/hr was assumed based on the Hydrogeological Report (Stantec, 2020 and as amended)

#### 5.6.3 StormTech® Subsurface SWM Facility

A StormTech® M-3500 subsurface SWM facility has been proposed in the southwest portion of the property to provide water quantity controls for runoff draining to Gordon Street. The proposed facility is 553 m<sup>3</sup> with outflows controlled through the use of a 75 mm diameter orifice provided in CBMH1.

#### 5.6.4 Hydrologic Modeling Results

	Existing Flow Ra	ates to Outlet (m³/s)
Storm Event	Gordon Street (101)	Torrance Creek Watershed (102)
2-yr	0.03	0.02
5-yr	0.04	0.04

Table 2 summarizes the pre- and post-development modeling results for the site.

100-yr	0.19	0.25			
	Proposed Flow Rates to Outlet (m <sup>3</sup> /s)				
Storm Event	Gordon Street (201, 202, 204, 207, 208, 209)	Torrance Creek Watershed (203,205, 206)			
2-yr	0.03	0.02			
5-yr	0.04	0.05			
100-yr	0.13	0.28			

#### **Torrance Creek Watershed**

As shown in Table 2, post-development flows to the Torrance Creek watershed are proposed to have a minor increase over the pre-development flow rates during the modeled storm events. Based on the hydrologic modeling the increase in flows is primarily a result of uncontrolled runoff from Catchments 205 (Future Park Block) and 206 (landscaped area on the east portion of the site) and the result of shorter flow paths than under pre-development conditions. It is noted that the Torrance Creek Swamp adjacent to the site is significantly larger than the subject site with an even larger contributing watershed. It is not expected that this minor increase in flows (30 L/s in the 100-year storm event) will have significant impact on the downstream Torrance Creek Swamp or downstream infrastructure (which will be buffered by the Torrance Creek Swamp).

#### **Gordon Street**

As shown in Table 2, the proposed SWM controls satisfy water quantity targets to Gordon Street.

#### 5.6.5 Water Quality Controls

#### **Torrance Creek**

Catchments contributing to the Torrance Creek watershed consist of rooftop runoff (Catchment 203), Park Block (Catchment 205) and Landscaped Area (Catchment 206). Runoff from these areas can be considered clean, and no additional water quantity controls are required.

#### **Gordon Street / Infiltration Chamber**

Water quality controls for the parking lot and driveway areas conveyed to the infiltration chamber and subsurface stormwater detention facility will be provided through a treatment train approach. An OGS (ADS FD-4HC or approved equivalent) has been sized to provide an enhanced level of water quality control upstream of the infiltration chamber. In addition, a StormTech Isolator Row Plus ® has been provided at the inlet of the chamber to filter out suspended solids prior to distribution throughout the facility, and alone exceeds the requirement TSS removal to provide an enhanced level of water quality control. Uncontrolled areas fronting Gordon Street are landscaped areas and can be considered clean.

Water quality calculations have been attached for reference.

#### Street A

An OGS (ADS FD-4HC or approved equivalent) has been provided for Street A, prior to discharging to the Gordon Street storm sewer. The OGS has been sized to provide an enhanced level of water quality treatment for the Street A right-of-way. Calculations have been attached for reference.

### 5.7 SALT MANAGEMENT

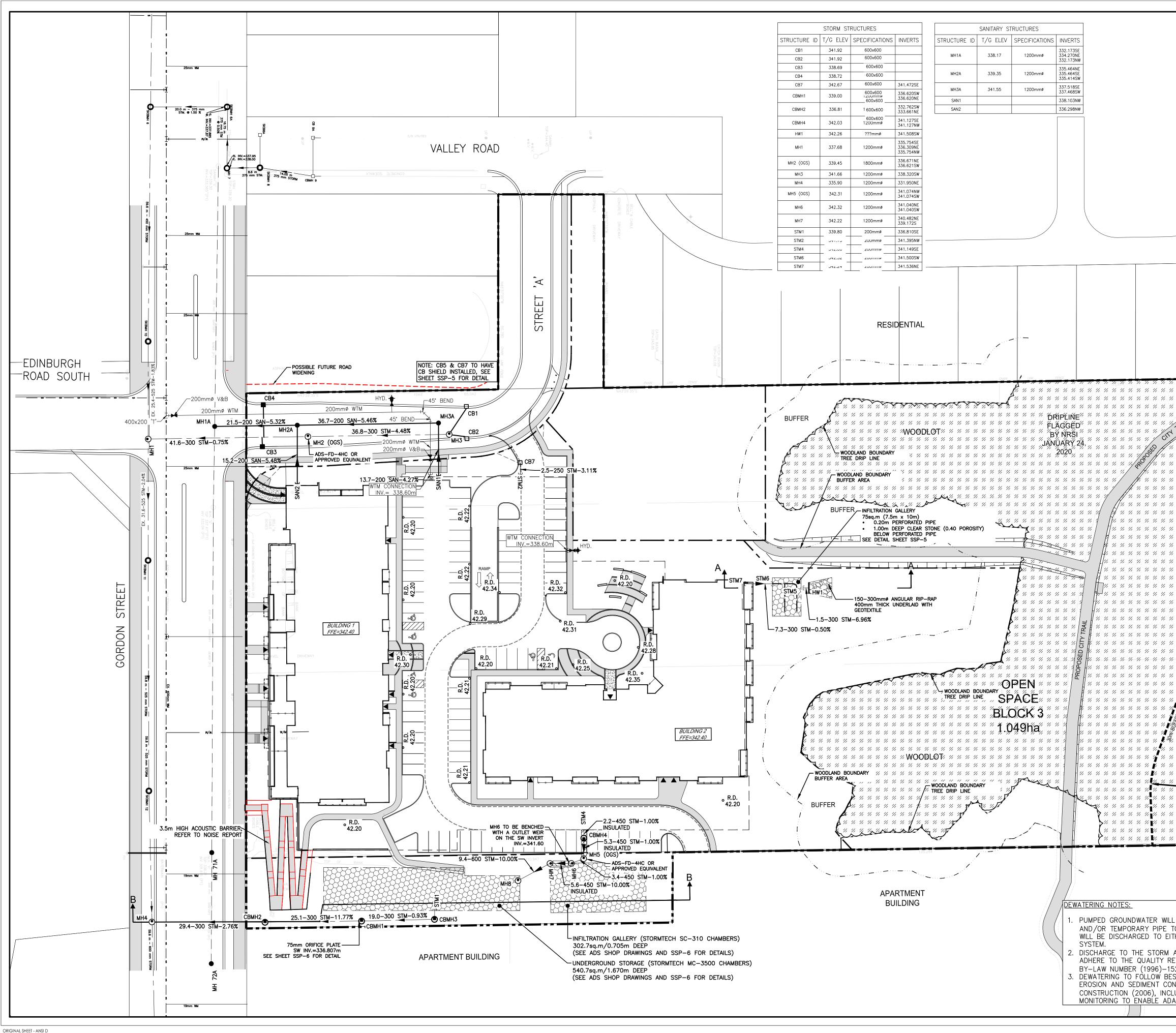
In order to meet water balance criteria, the infiltration of treated parking lot runoff was necessary. In order to mitigate the discharge of chloride laden water into the groundwater system, it is recommended that salt application for winter maintenance is prohibited and that site owners employ non-chloride salt alternatives.

### 6.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the preceding report, the following conclusions can be drawn:

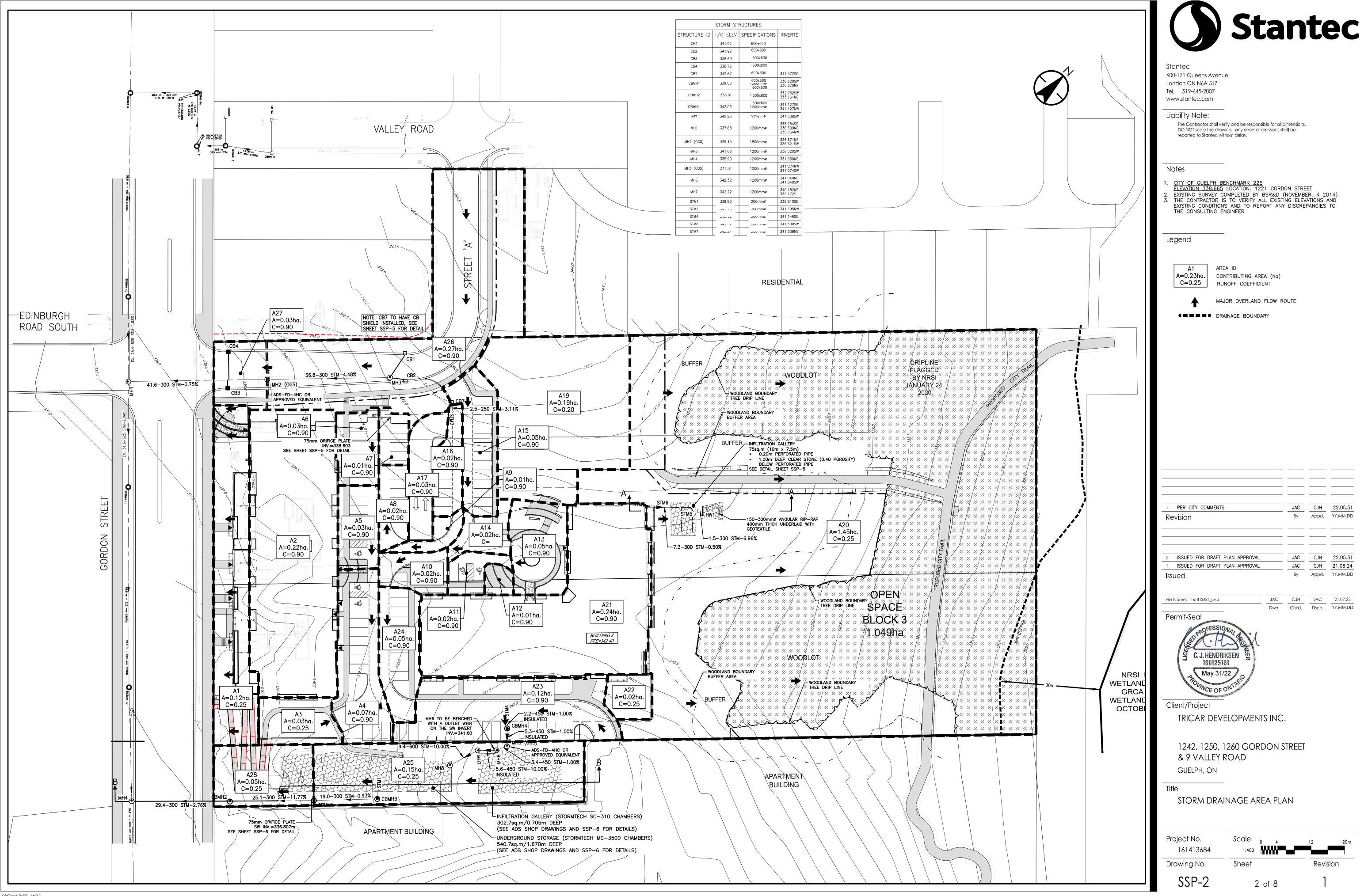
- Sanitary service is provided by the proposed upgrade to the municipal system located on Gordon Street just west of the site access.
- Water service is provided from the existing 400mm watermain on Gordon Street fronting this site.
- Enhanced (Level 1) water quality control will be provided for the parking lot and driveway runoff through the use of an OGS and Stormtech Isolator Row Plus® treatment train
- The proposed rooftop storage, infiltration chamber and subsurface stormwater detention facility provide water quantity controls prior to discharge to Gordon Street.

# APPENDIX A – PRELIMINARY CIVIL DRAWING PACKAGE

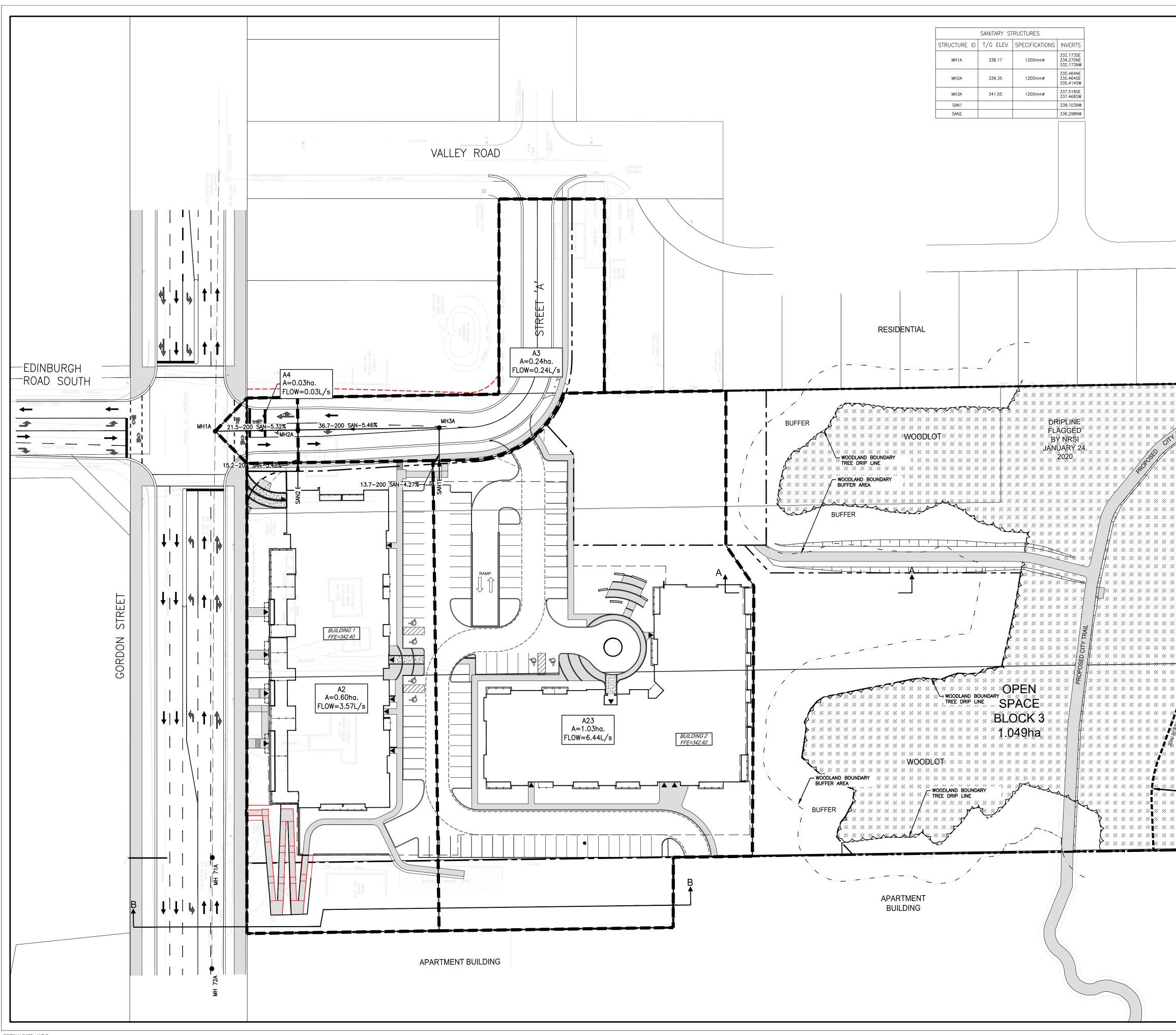


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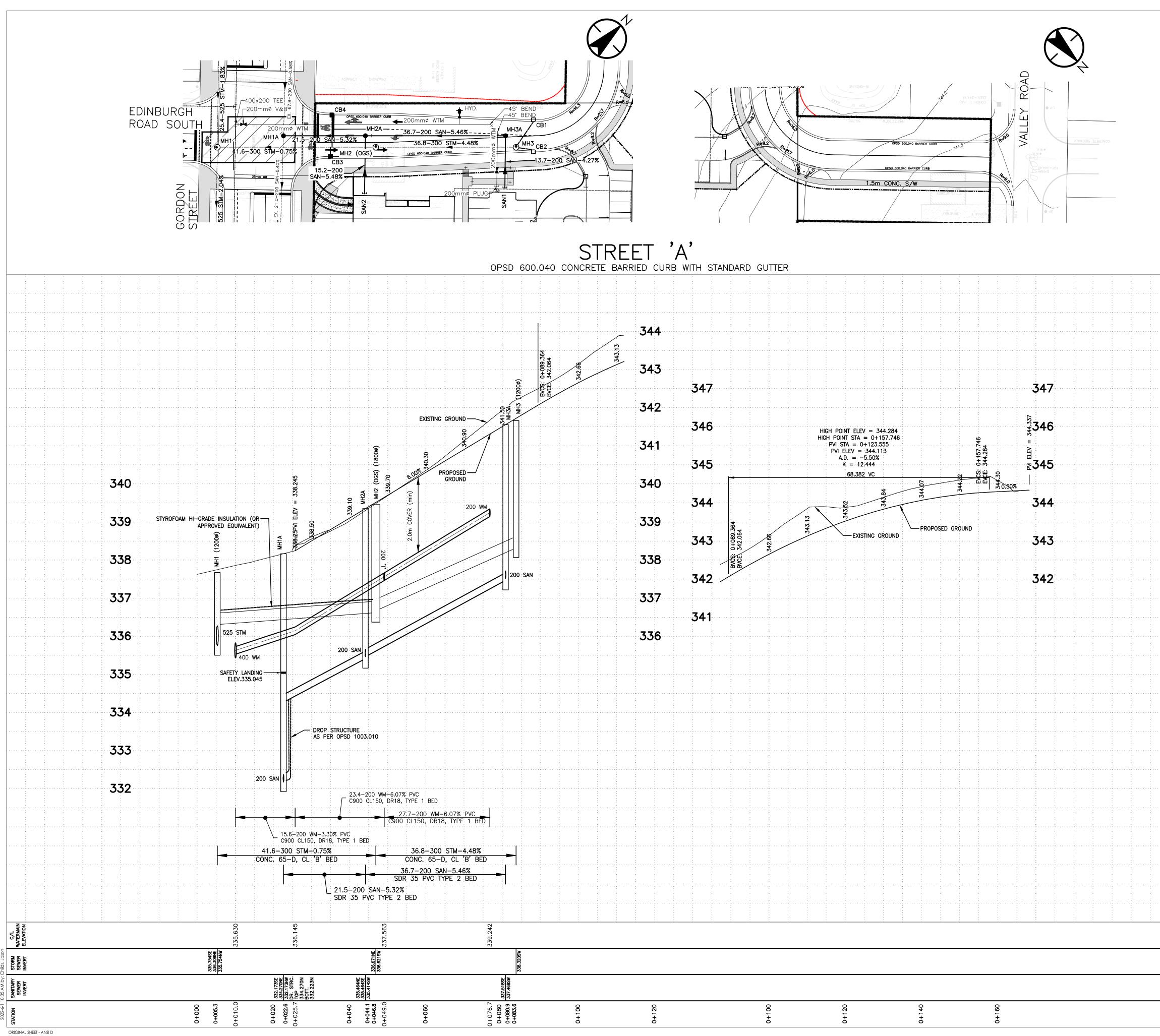
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Notes

- <u>CITY OF GUELPH BENCHMARK 225</u> <u>ELEVATION 338.665</u> LOCATION: 1221 GORDON STREET
   EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014)
   THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER

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<b>→</b>	PROPOSED 3- C/W STORZ (			ANT
	EX. WATERMAI			
	PROPOSED W		N	
EX. CB	EX. CATCHBAS	SIN		
EX. MH	EX. MANHOLE			
CB or CICB	PROPOSED CA	TCHBAS	N	
CBMH1	PROPOSED CA	TCHBAS	IN MANH	OLE
● R2	PROPOSED ST	ORM MA	NHOLE	
• S2	PROPOSED SA	NITARY	MANHOLE	Ξ
	PROPOSED SA	NITARY	SEWER	
	EX. SANITARY	SEWER		
	PROPOSED ST	ORM SE	WER	
	EX. STORM S	EWER		



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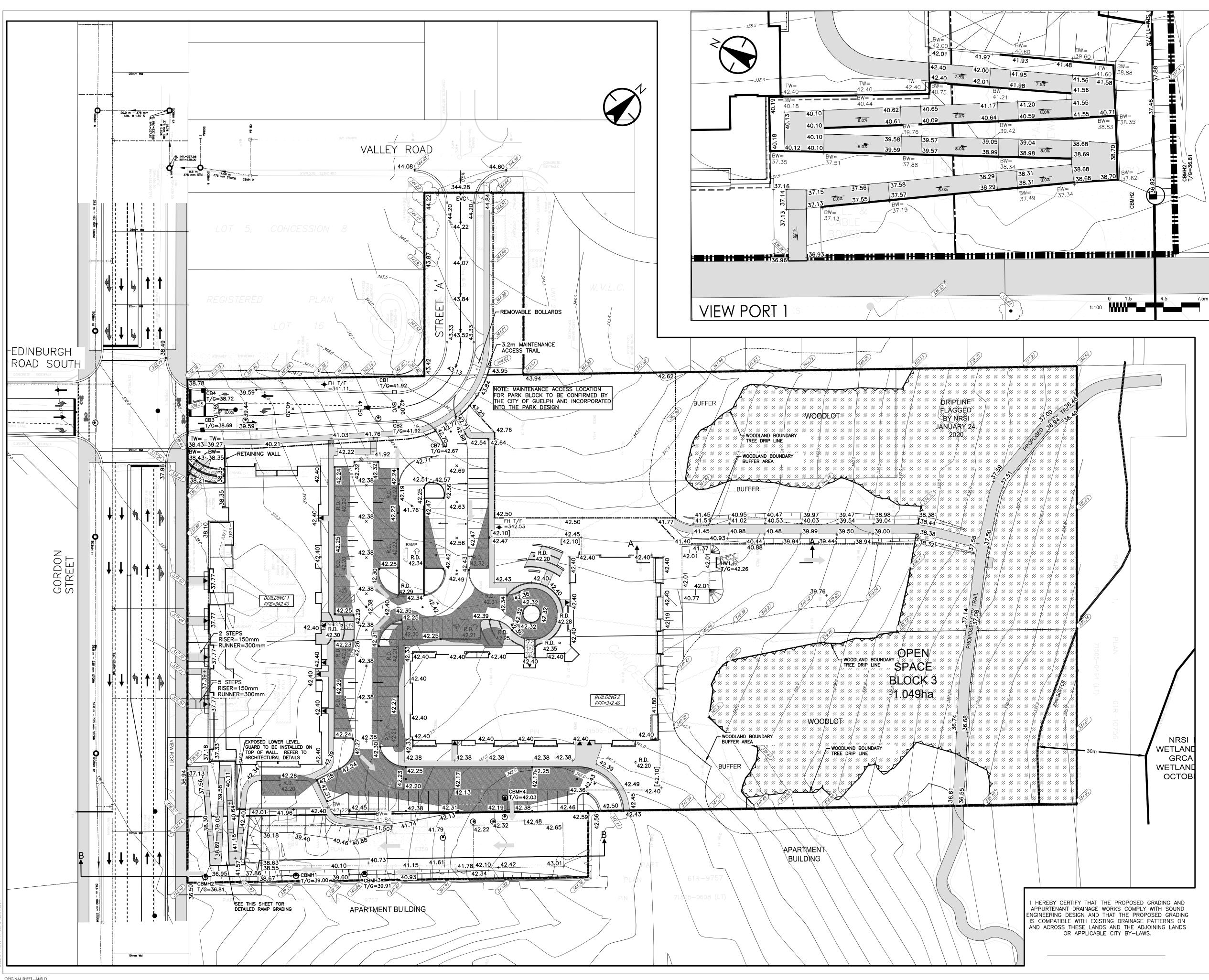
1242, 1250, 1260 GORDON STREET & 9 VALLEY ROAD GUELPH, ON

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STREET 'A' PLAN & PROFILE

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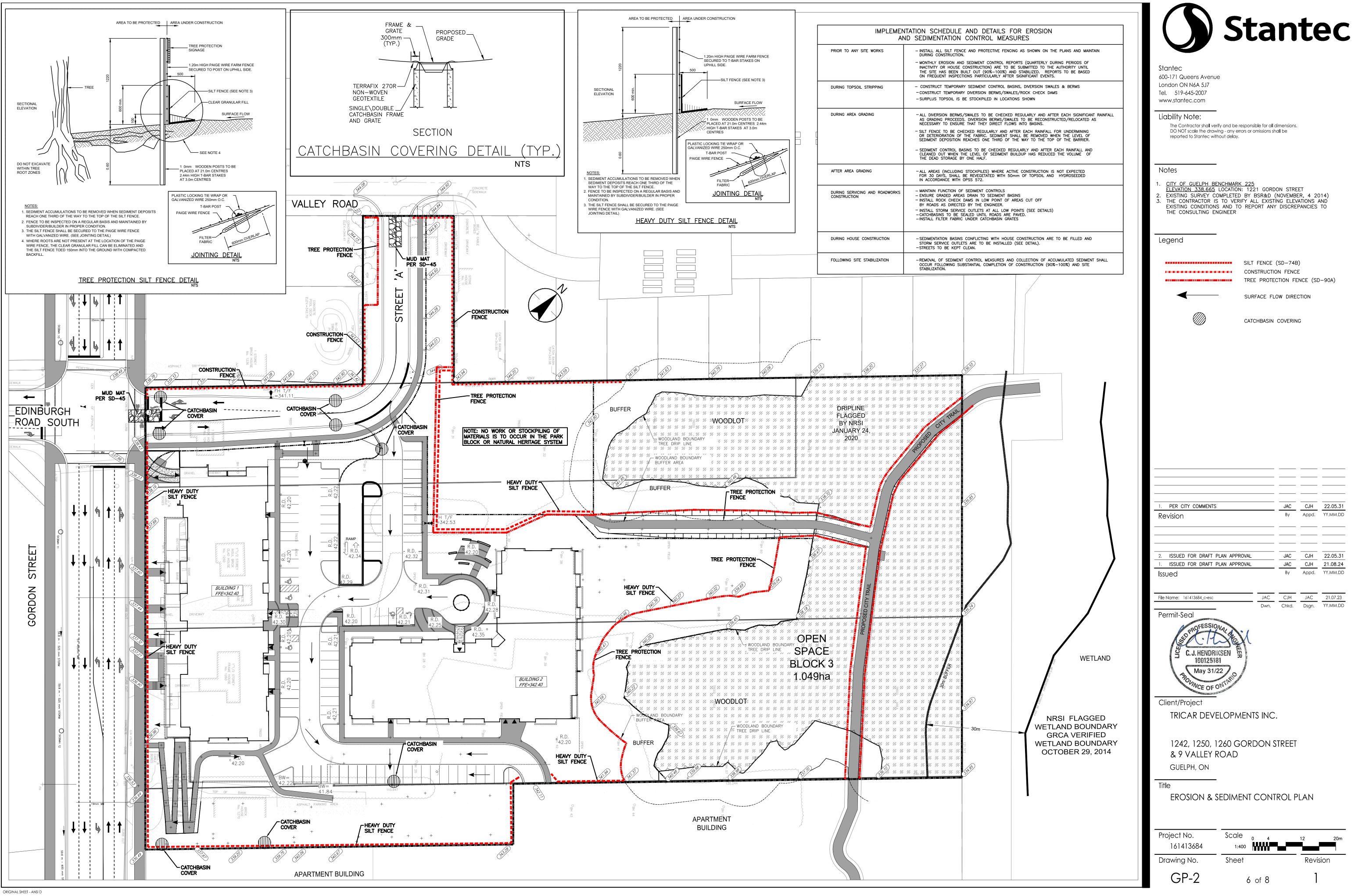
Notes

- CITY OF GUELPH BENCHMARK 225 ELEVATION 338.665 LOCATION: 1221 GORDON STREET EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014) THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER

Legend	PROPOSED SWALE
Θ	PROPOSED STORM MANHOLE
Õ	PROPOSED STORM CATCH BASIN MANHOLE
•	PROPOSED SANITARY MANHOLE
Õ	EX. STORM MANHOLE
lacksquare	EX. SANITARY MANHOLE
	PROPOSED CATCH BASIN
	EX. CATCH BASIN
• 75.95	PROPOSED GRADES
• 75.95 (SP)	PROPOSED OVERLAND FLOW SPILL POINT
75.95	EXISTING GRADES
	MAJOR OVERLAND FLOW ROUTE
	SITE BOUNDARY
• 71.77 • (SW)	PROPOSED SWALE GRADE
	EXISTING CONTOURS
-	FLOW DIRECTION
	HYDRANTS
Ψ	

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1. PER CITY COMMENTS		JAC	CJH	22.05.31
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### NOTES AND SPECIFICATIONS:

#### A. GENERAL:

- 1. BUILDINGS ARE NOT TO BE SITED WITH THIS DRAWING. THIS DRAWING TO BE READ IN CONJUNCTION WITH THE SITE SERVICING PLANS (SSP SERIES)
- & THE GRADING PLAN (GP SERIES) PREPARED BY STANTEC CONSULTING. HESE PLANS FOR CONSTRUCTION ONLY WHEN APPROVED BY THE CITY OF GUELPH AND
- SEALED BY THE ENGINEER. 3. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS; OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING
- SERVICES BEFORE PROCEEDING WITH ANY WORK. 4. ALL WORK WITHIN THE RIGHTS-OF-WAY OR CITY EASEMENTS ARE TO BE INSTALLED BY
- CITY OF GUELPH AT THE OWNER'S EXPENSE UNLESS OTHERWISE NOTED. ANY PROPOSED CHANGES SHALL BE APPROVED BY THE ENGINEER AND CITY OF GUELPH. ALL UNDERGROUND SERVICING TO BE INSPECTED BY STANTEC CONSULTING LTD. AND
- ALL ONDERGROUND SERVICING TO BE INSPECTED BY STATEC COORDINATE WITH STANTEC CERTIFIED FOR THE CITY OF GUELPH. CONTRACTOR SHALL COORDINATE WITH STANTEC AND SHALL CONTACT SAME AT LEAST 48 HOURS PRIOR TO INSTALLATION OF SERVICES.
   CONTRACTOR SHALL COORDINATE WITH STANTEC AND SHALL CONTACT SAME AT LEAST 48 HOURS PRIOR TO INSTALLATION OF SERVICES.
   ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE COORDINATE WITH STANTEC AND CONTRACT AND CONTRACT SAME AT LEAST 48
- REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR
- CONSTRUCTION PROJECTS (LATEST EDITION). THE PROPERTY OWNER IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY TO CITY OF GUELPH
- STANDARDS. 10. IF, FOR UNFORESEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENCROACH ONTO PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO THE DEVELOPMENT & TECHNICAL SERVICES – ENGINEERING DEVELOPMENT DIVISION, PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.

### B. UNDERGROUND SERVICES:

- CONTRACTOR SHALL VERIFY ELEVATION AND LOCATION OF EXISTING SANITARY AND STORM SEWERS AND WATERMAINS PRIOR TO COMMENCING SITE WORK AND SHALL NOTIFY THE ENGINEER OF ANY CONFLICTS BETWEEN EXISTING AND PROPOSED SERVICES.
- THE CONTRACTOR TO MAKE CONNECTIONS TO SERVICES AT STUB LOCATION FOR SANITARY, STORM SEWERS, WATERMAIN AND TO RESTORE ALL OFF-SITE AFFECTED PROPERTY TO
- 3. ON-SITE SERVICING SHALL NOT BE UNDERTAKEN PRIOR TO COMPLETION OF
- SERVICE CONNECTIONS WITHIN THE ROAD R.O.W.'S. 4. ALL UNDERGROUND SERVICES TO BE IN COMPLIANCE WITH THE LATEST REVISED BUILDING CODE, CITY OF GUELPH ENGINEERING STANDARDS, ONTARIO PROVINCIAL STANDARDS (OPSS, OPSD) AND WITH THE LATEST REGULATIONS OF THE ONTARIO PLUMBING CODE AND SUPPLEMENT SPECIFICATION FOR MUNICIPAL SERVICES (DGSSMS) AND INSPECTED BY
- CITY STAFF/CONSULTANT PRIOR TO BACKFILLING. 5. UNDERGROUND SERVICES TO TERMINATE 1.5m FROM BUILDING LINE, PLUGGED OR
- ONDERVICES TO TERMINATE TO THOM BUILDING LINE, PLUGGED OR CAPPED C/W MARKER EXTENDING FROM INVERT TO 1.0M ABOVE FINISHED GRADE.
   ALL BEDDING TO BE AS NOTED BELOW. TRENCH BACKFILL TO BE APPROVED NATIVE MATERIAL COMPACTED IN 200mm MAX. LIFTS TO 95% STANDARD PROCTOR DENSITY.
   ALL SERVICES SHALL BE TESTED AS SPECIFIED IN THE APPLICABLE OPSS (OPSS
- ALL SERVICES SHALL BE TESTED AS SPECIFIED IN THE AT LICADLE OF 35 (0135) 410 & 441).
  ALL SERVICES, UTILITIES AND CATCHBASIN LEADS ARE TO BE SUPPORTED AS PER OPSD 1007.01 DURING TRENCHING ACTIVITIES. THE CONTRACTOR IS RESPONSIBLE FOR LOCATING AND PROTECTING ALL EXISTING UTILITIES PRIOR TO AND DURING CONSTRUCTION. LOCATION OF EXISTING UTILITIES TO BE VERIFIED IN THE FIELD.
  ANY UTILITY RELOCATION DUE TO THIS DEVELOPMENT TO BE UNDERTAKEN AT THE EVENCE OF THE OWNED (DEED)
- EXPENSE OF THE OWNER/DEVELOPER.
- C. SEWERS/APPURTENANCES:
- 4. STORM SEWERS:
  LESS THAN 200mmø PVC DR–28 200mmø TO 375mmø – PVC DR-35
- PVC RIBBED PIPE (ULTRA-RIB OR EQUIVALENT) - CI - 3 CONCRETE • 450mmø TO 600mmø – PVC RIBBED PIPE (ULTRA-RIB OR EQUIVALENT)
- 65D CONCRETE 450mmø TO 600mmø – 65D CONCRETE
- 5. SANITARY SEWERS:
- LESS THAN 200mmø PVC DR-28 200mmø OR LARGER PVC DR-35 2.5m MINIMUM COVER FOR SANITARY SEWERS.
- 3. SEWER BEDDING: CITY OF GUELPH SD-29
- 150mm (MIN) GRAN 'A' TO 98% S.P.D.
  4. STORM MANHOLES: OPSD 701.010 (1200mmø) OPSD 701.011 (1500mmø) OPSD 701.012 (1800mmø) OPSD 701.013 (2400mmø) OPSD 701.014 (3000mmø
- 6. SANITARY MAINTENANCE HOLE:
  OPSD 701.010 (1200mmø) 7. MAINTENANCE HOLE BENCHING
- CITY OF GUELPH SD-44 • CBMH'S WITH AN OUTLET PIPE GREATER THAN 450mmø SHOULD BE BENCHED. 450mmø OR LESS SHALL BE PROVIDED WITH A 600mm SUMP. 8. CATCHBASINS/CATCHBASIN LEADS:
- OPSD 705.01 (SINGLE) OPSD 705.02 (DOUBLÉ)
- OPSD 705.03 (DITCH INLET 3:1 SLOPE)
   MINIMUM LEAD DIAMETER. 200mmø FOR SINGLE, 300mmø FOR DOUBLE CATCHBASINS.
- 9. FRAMES AND GRATES/COVERS: OPSD 400.10 (CB'S & CBMH'S)

- D. WATER SERVICES/APPURTENANCES:
- 1. WATERMAIN WALEKMAIN 100mmø TO 300mmø – AWWA C–900 PVC SDR–18 350mmø TO 600mmø – AWWA C905 PVC SDR–25 2.0m MINIMUM COVER FITTINGS TO AWWA C–907
- WHERE CONFLICT ARISES AT WATERMAIN/SERVICE CROSSING OTHER UNDERGROUND SERVICES, WATERMAIN/SERVICES SHALL BE LOWERED TO MAINTAIN 0.50m VERTICAL
- SEPARATION.
- 2. PIPE BEDDING: CITY OF GUELPH SD-29
- 150mm (MIN) GRANULAR 'A' 98% S.P.D. 5. THRUST BLOCKING:
- CITY OF GUELPH SD-27
   TRACER WIRE:
   CITY OF GUELPH SD-54A
   CITY OF GUELPH SD-54A

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5. HYDRANTS: CITY OF GUELPH SD-25A (OPEN RIGHT)

- 6. VALVES:
  ALL VALVES TO OPEN COUNTER-CLOCKWISE AND COMPLY WITH A.W.W.A. SPEC.
  CITY OF GUELPH SD-24 WATER SERVICES
- 25mmø TYPE K COPPER PIPING WET TAPPED TO PVC WATERMAIN WITH APPROVED SADDLE CITY OF GUELPH SD-54B 8. WATER METERS:
- BUILDING UNITS TO HAVE INDIVIDUAL WATER METERS TO THE SATISFACTION OF CITY OF GUELPH WATERWORKS DEPARTMENT
   MAINTAIN SPATIAL SEPARATION FOR SITE SERVICES PER BUILDING CODE PART 7.3.5.6
- 1. ALL NEW WATER PIPING INSTALLATIONS AS PER AWAR C651-05 1. CATHODIC PROTECTION IN ACCORDANCE WITH CITY OF GUELPH STANDARDS. 12. A WATERMAIN COMMISSIONING PLAN IN ACCORDANCE WITH DGSSMS WILL BE REQUIRED.

#### E. GRADING:

- 1. COMPLETE ALL EXCAVATION, GRADING, TRIMMING AND COMPACTION AS REQUIRED TO FACILITATE THE WORK, ALL SUBGRADE AREAS SHALL BE PROOF ROLLED TO 98% S.D.P.
- PRIOR TO GRANULAR SUBBASE PLACEMENT. DISPOSE OF ALL SURPLUS AND UNSUITABLE MATERIAL OFFSITE. SAWCUT ASPHALT IN NEAT LINES AT ALL MATCH LINES. MATCH EXISTING GRADES AT ADJACENT PROPERTY LINES. 5. TRANSITION SLOPES TO BE MAXIMUM 3:1 (HORIZONTAL TO VERTICAL) UNLESS OTHERWISE
- NOTED
- . SURFACE WORKS: 1. CURBS:
- OPSD 600.040 (CONCRETE BARRIER CURB WITH STANDARD GUTTER) OPSD 600.070 (CONCRETE BARRIER CURB WITH STANDARD GUTTER, TWO STAGE CONSTRUCTION)
- OPSD 600.080 (CONCRETE BARRIER CURB WITH NARROW GUTTER) OPSD 600.110 (CONCRETE BARRIER CURB)
   ASPHALT PAVEMENT: (PARKING AREA)
- 40mm HL 3 (SURFACE ASPHALT) 97% MARSHALL 50mm HL4 (BASE ASPHALT) 97% S.P.D. 100% S.P.D.
- 150mm GRANULAR 'A' BASE 300mm GRANULAR 'B' SUB-BASE 100% S.P.D. 3. ASPHALT PAVEMENT: (ABOVE PARKING GARAGE)
- CONCRETE DECK ROOFING MEMBRANE
- PROTECTION BOARD 40MM HL 3 (SURFACE ASPHALT) 97% MARSHALL
- 50MM HL4 (BASE ASPHALT) 97% S.P.D. 4. PAVEMENT: (HEAVY DUTY/FIRE ROUTE) 50mm HL-3 SURFACE ASPHALT 97% MARSHALL – (WHERE IN PLACE)
- 60mm HL-4 BASE ASPHALT 97% MARSHALL 150mm GRANULAR 'A' 100% S.P.D.
- 400mm GRANULAR 'B' 100% S.P.D. SAW CUT CLEAN EDGES AT ALL MATCH LINES AND APPLY TACK COAT. 5. CONCRETE SIDEWALKS:
- CITY OF GUELPH SD-2, 1.5m WIDE (CONCRETE SIDEWALK)
- CITY OF GUELPH SD-4 (SIDEWALK RAMPS)
   SITE AREAS DISTURBED BY CONSTRUCTION AND NOT INDICATED FOR REMOVAL TO BE RESTORED TO ORIGINAL CONDITIONS.
- G. EROSION CONTROL:

- ALL SILT FENCING TO BE INSTALLED PRIOR TO COMMENCEMENT OF ANY AREA GRADING, EXCAVATION OR DEMOLITION.
   EROSION CONTROL FENCE TO BE PLACED AROUND THE BASE OF ALL STOCKPILES. ALL STOCKPILES TO BE KEPT A MINIMUM OF 2.5m FROM ALL PROPERTY LINES.
   P-250 FILTER FABRIC UNDERLYING CONSTRUCTION VEHICLE ENTRANCE TO CONSIST OF CLEANED OR REPLACED 200mm THICK, 50mmø STONE. STONE TO BE TAKEN UP AND UNIVEL MODIMUM ATALOR 2017 ENTRANCE (SEE DETAIL)
- WHEN ACCUMULATIONS COVER 50% OF TOP OF STONE (SEE DETAIL). 4. EROSION PROTECTION TO BE PROVIDED AROUND ALL STORM AND SANITARY MANHOLES
- EROSION PROTECTION TO BE PROVIDED AROUND ALL STORM AND SANTIART MAINFOLES AND/OR CATCHBASINS.
   ADDITIONAL EROSION CONTROL MEASURES MAY BE REQUIRED AS SITE DEVELOPMENT PROGRESSES, CONTRACTOR TO PROVIDE ALL ADDITIONAL EROSION CONTROL STRUCTURES.
   EROSION CONTROL STRUCTURES TO BE MONITORED REGULARLY BY STANTEC CONSULTING LTD. AND ANY DAMAGE REPAIRED IMMEDIATELY. SEDIMENTS TO BE REMOVED WHEN
- ACCUMULATIONS REACH A MAXIMUM OF ONE THIRD (1/2) THE HEIGHT OF THE SILT
- ALL EROSION CONTROL STRUCTURES TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN RE-STABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER.
- 8. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED UNLESS APPROVED BY STANTEC CONSULTING LTD. AND THE CITY OF GUELPH'S WORKS EPARTMENT
- 9. THE CONTRACTOR IS RESPONSIBLE FOR REMOVING SEDIMENTS FROM THE MUNICIPAL ROAD AND SIDEWALKS AT THE END OF EACH WORK DAY. 10. MUD MATS TO BE PROVIDED ON SITE AT ALL LOCATIONS WHERE CONSTRUCTION VEHICLES EXIT THE SITE. MUD MATS SHALL BE A MINIMUM OF 3.0m WIDE, 15.0m LONG (LENGTH MAY VARY DEPENDING ON SITE LAYOUT) AND 0.3m DEEP AND SHALL CONSIST OF 20mm CLEAR STONE MATERIAL OR APPROVED EQUIVALENT. CONTRACTOR TO ENSURE ALL
- VEHICLES LEAVE THE SITE VIA THE MUD MAT AND THAT THE MAT IS MAINTAINED IN A MANNER TO MAXIMIZE ITS EFFECTIVENESS AT ALL TIMES. I1. STANTEC CONSULTING LTD. TO MONITOR THE SITE DEVELOPMENT TO ENSURE ALL EROSION CONTROLS ARE INSTALLED AND MAINTAINED TO CITY REQUIREMENTS. CONTRACTOR TO COMPLY WITH THE ENGINEER'S INSTRUCTIONS TO INSTALL, MODIFY, OR MAINTAIN EROSION CONTROL WORKS.

### H. RETAINING WALLS:

- 1. RETAINING WALL TO BE CONSTRUCTED AS DESIGNED BY OTHERS. APPROPRIATE OPSD 400.10 (CB<sup>5</sup>s & CBMH'S)
  OPSD 401.01 TYPE 'A' (SANITARY AND STORM MH'S)
  CITY OF GUELPH SD-15 (RLCB'S)
  CITY OF GUELPH SD-9 (SAFETY GRATE FOR MH'S)
  ALL FRAMES ON STRUCTURES TO BE SET USING PRECAST CONCRETE ADJUSTMENT UNITS
  MATER SERVICES (ADDULTENANCES)

  - I. DEWATERING NOTES:
  - 1. PUMPED GROUNDWATER WILL BE DIRECTED OFFSITE VIA SWALE AND/OR TEMPORARY PIPE OP OPPY DRIVE EAST, WHERE THE WATER WILL BE DISCHARGED TO EITHER THE STORM OR SANITARY SEWER SYSTEM.
  - 2. DISCHARGE TO THE STORM AND/OR SANITARY SEWER SYSTEM MUST ADHERE TO THE QUALITY REQUIREMENTS AS PER CITY OF GUELPH BY-LAW NUMBER (1996)-15202.

### J. MISCELLANEOUS:

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- WHERE COVER OVER SEWERS IS LESS THAN 1.2m IN PAVED AREAS, OR LESS THAN 0.90m IN GRASSED AREAS INSTALL INSULATION AS PER DETAIL. INSULATION TO BE 60mm THICK × 1800mm WIDE UNLESS OTHERWISE NOTED. INSTALL LONGITUDINALLY OVER OCHTERIN IN CONTROL ADDITION OF THE ADDITION OF THE
- CENTERLINE OF PIPE WITH OVERLAPPING JOINTS. 2. IT IS THE SITE OWNERS' RESPONSIBILITY TO ENSURE THAT ALL SEDIMENT CONTROLS ARE IMPLEMENTED AND MAINTAINED IN ACCORDANCE WITH THE ABOVE CRITERIA.

300mm AMMENDED SOIL -

INV.=341.536m

PROPOSED GROUND -

INSULATION OR APPROVED EQUIVALENT

300 STM SEWER

300x200 REDUCER -

EXISTING GROUND ----

HIGH GROUND WATER ----339.510m

NILEX 4545 FILTER FABRIC, OR

APPROVED EQUIVALENT, LINES -

TOP, BOTTOM AND SIDES OF

DRY WELL (OVERLAP 300MM

AT SEAMS)

√.=341.5*°* 

INV.=340.510/

STYROFOAM HI-BRAND -

- 1 PRIOR TO INSTALLATION
- · LAYDOWN OR STOCKPILE LOCATIONS; • EQUIPMENT STORAGE;
- TRAFFIC FLOW OR SITE ACCESS.

# 2 INSTALLATION

- PROTECTED IN THE EVENT OF RAIN.
- AT THE MINIMUM OVERLAP
- NOT TO BE USED.

3 MAINTENANCI

1 INSTALLATION

2 MAINTENANCE

### UNDERGROUND STORAGE AND INFILTRATION TRENCHES

• EFFORTS SHOULD BE MADE TO AVOID COMPACTION BY NOT USING THE FACILITY LOCATION AS:

• MATERIAL TO BE USED IN THE CONSTRUCTION OF THE FACILITY SHOULD NOT BE BROUGHT ON SITE PRIOR TO IT BEING NEEDED. IF THIS MATERIAL IS ON SITE PRIOR TO FINAL PLACEMENT, IT SHALL BE STOCKPILED SEPARATELY FROM ANY OTHER CONSTRUCTION MATERIALS AND ADEQUATELY PROTECTED (AS DIRECTED BY THE LID INSPECTOR).

• TRENCH FLOOR TO BE SCARIFIED TO A DEPTH OF 0.15M UNLESS THE LID INSPECTOR DIRECTS GREATER DEPTHS OF SCARIFICATION. • ONCE THE AREA IS SCARIFIED, AT LEAST 2 LOCATIONS IN EACH FACILITY ARE TO BE TESTED FOR IN-SITU INFILTRATION RATE. ADDITIONAL SCARIFICATION MAY BE REQUIRED FOLLOWING THESE TESTS, AFTER WHICH THE TESTS SHOULD BE COMPLETED AGAIN IN OTHER LOCATIONS. • SHOULD THE TRENCH WORK BE COMPLETED IN ADVANCE ON THE INSTALLATION OF THE GEOTEXTILE AND STONE, THE TRENCH SHOULD BE

• THE OVERLAP ON THE GEOTEXTILE SHALL BE A MINIMUM OF 0.3M. THE GEOTEXTILE SHALL BE WRAPPED OVERTOP OF THE STORE STORAGE

• ALL STONE INSTALLED IS TO BE TRIPLE WASHED TO PREVENT DUST FROM CLOGGING THE FABRIC AND SOIL PORES, STONE IS TO BE INSTALLED IN LIFTS OF 0.3M MAXIMUM. THESE LIFTS SHOULD BE LIGHTLY WORKED TO SETTLE THE STONE BUT MECHANICAL COMPACTION IS • ALL UNDERDRAIN PIPES ARE TO BE WRAPPED IN A SEDIMENT SOCK.

• IF THE FACILITY IS COMPLETED PRIOR TO SITE STABILIZATION, RUNOFF SHOULD BE DIRECTED AWAY FROM THE FACILITY TO PREVENT HEAVY SEDIMENTATION. EROSION CONTROLS SHOULD BE INSTALLED AS PER THE DIRECTION OF THE LID INSPECTOR.

• REMOVE ANY DEBRIS, GARBAGE, LEAVES, STICKS, OR OTHER ITEMS FROM THE FACILITY INLETS. THIS SHOULD BE DONE BIANNUALLY WITH SPECIAL ATTENTION IN FALL TO REMOVE FALLEN LEAVES;

• REMOVE ACCUMULATED SEDIMENT FROM THE BOTTOM OF THE FACILITY AS NEEDED BY FLUSHING; • MONITOR PERFORMANCE; OBSERVE WATER DEPTHS IN THE FACILITY DURING RAIN EVENTS BIANNUALLY.

### OIL GRIT SEPARATOR

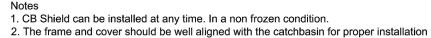
#### • ONCE INSTALLED. THE INLET TO THE OGS SHOULD BE SURROUNDED BY A FILTER SOCK RING TO REMOVE THE HEAVIEST SEDIMENT LOADS. THE OGS SHOULD BE INSPECTED BIWEEKLY DURING CONSTRUCTION AND CLEANED BY VACUUM TRUCK WHEN THE SUMP IS 50% FULL OF

• WHEN CONSTRUCTION IS COMPLETE, THE OGS SHOULD BE CLEANED OF ANY SEDIMENT.

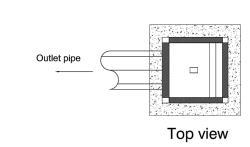
### INSPECTION SHOULD BE DONE BIANNUALLY;

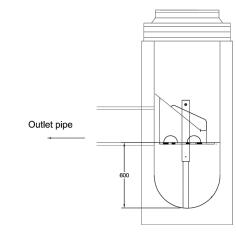
• REMOVE ACCUMULATED SEDIMENT FROM THE BOTTOM OF THE FACILITY WHEN 50% FULL BY VACUUM TRUCK; • REMOVAL OF ANY OILS OR FLOATABLES AS NEEDED, WITH SPECIAL ATTENTION PAID IN THE EVENT OF A DELETERIOUS SPILL.

> - APPROVED NATIVE BACKFILL STYROFOAM INSULATION WHERE SPECIFIED GRANULAR 'A' COMPACTED O 98% S.P.D. PIPE DIA: - 1/3 PIPE DIAMETER -150mm MIN. -300mm MAX. – UNDISTURBED GROUND TYP. PIPE BEDDING DETAIL



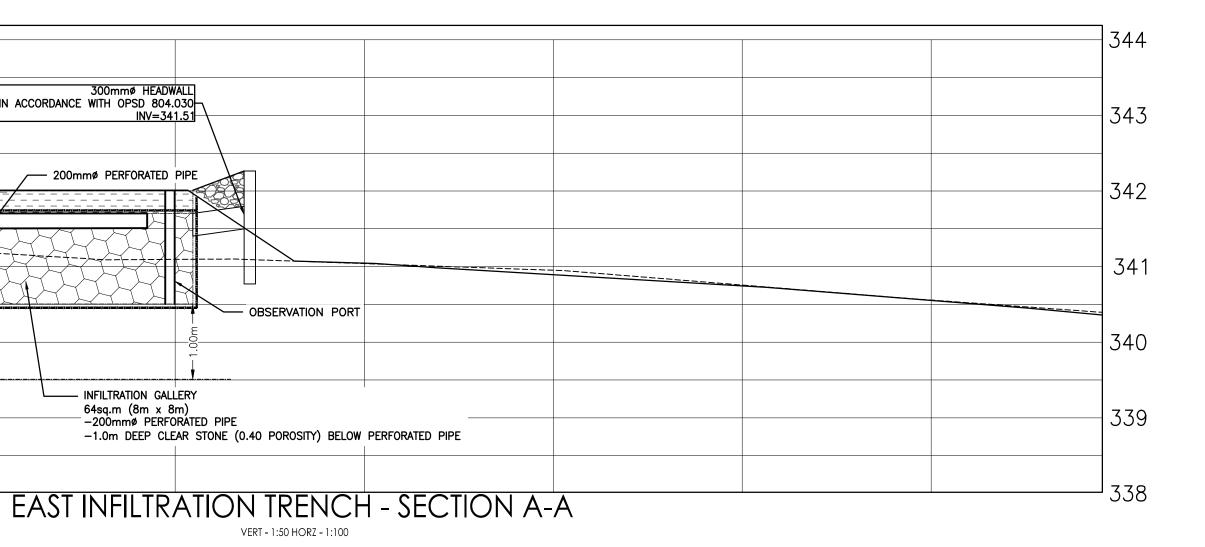
3. The catchbasin sump must be clean before installation 4. The grate should be at the same level as the standing water in the sump.





### Profile view

## CB Shield (600mm Sump)





Stantec 600-171 Queens Avenue London ON N6A 5J7 Tel. 519-645-2007 www.stantec.com

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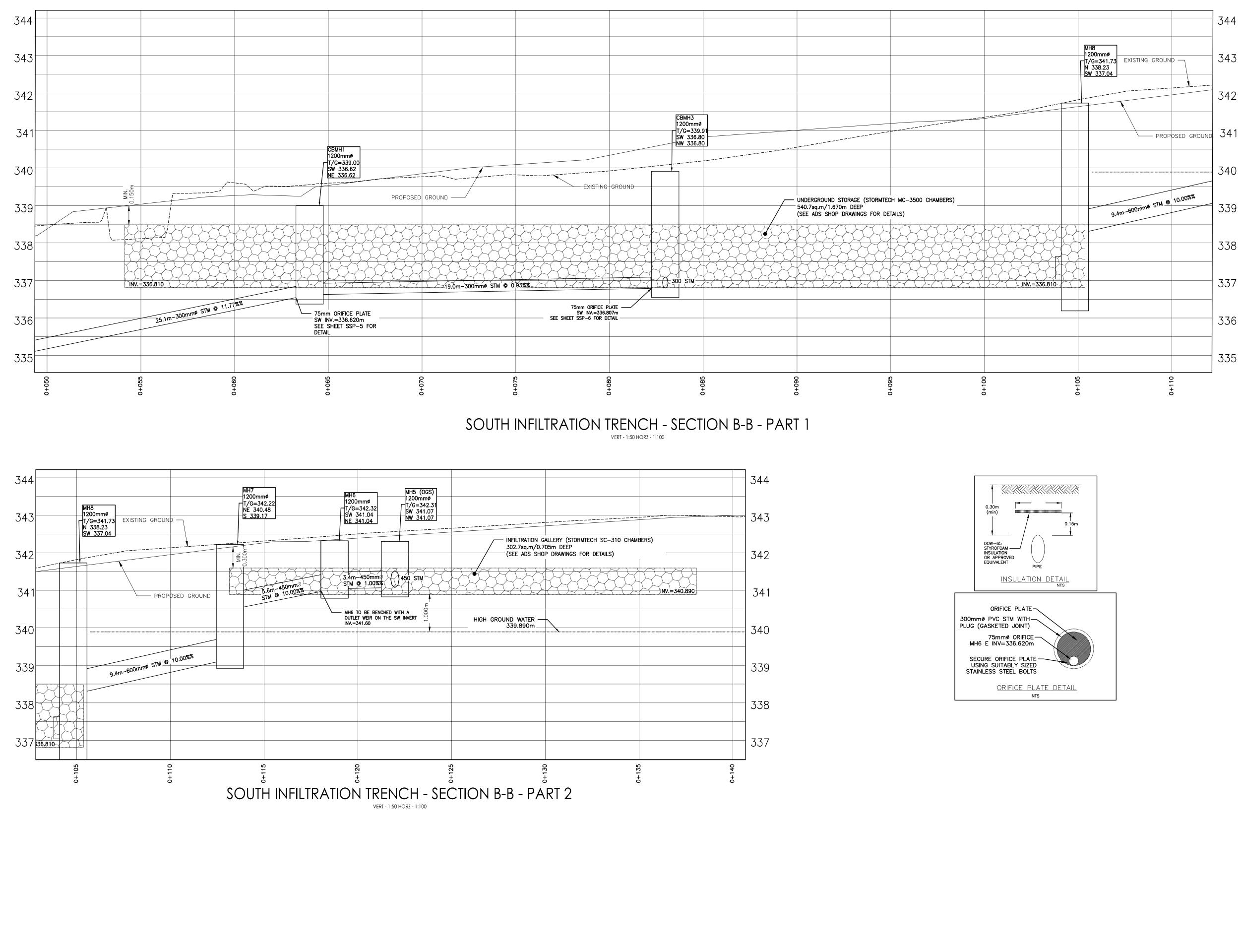
Notes

- CITY OF GUELPH BENCHMARK 225 ELEVATION 338.665 LOCATION: 1221 GORDON STREET
- EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014) THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER

Legend

1. PER CITY COMMENTS			JAC	CJH	22.05.3
Revision			Ву	Appd.	YY.MM.DI
2. ISSUED FOR DRAFT F	PLAN APPROVAL		 	 	22.05.3
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Permit-Seal		Dwn.	Chkd.	Dsgn.	YY.MM.D
Client/Project TRICAR DEVE 1242, 1250, 1 & 9 VALLEY F GUELPH, ON	260 GOR				
TRICAR DEVE 1242, 1250, 1 & 9 VALLEY F	260 GOR ROAD				
TRICAR DEVE 1242, 1250, 1 & 9 VALLEY F GUELPH, ON Title	260 GOR ROAD FAILS			3	5m
TRICAR DEVE 1242, 1250, 1 & 9 VALLEY F GUELPH, ON Title NOTES & DET Project No.	260 GOR ROAD FAILS	DON S		3 Revi	

\_\_\_\_\_ \_\_\_\_\_



ORIGINAL SHEET - ANSI D



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Liability Note: The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.

Notes

- CITY OF GUELPH BENCHMARK 225 ELEVATION 338.665 LOCATION: 1221 GORDON STREET EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014) THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER

Legend

1. PER CITY COMMENTS	S		JAC	CJH	22.05.31
Revision			Ву	Appd.	YY.MM.DE
2. ISSUED FOR DRAFT	PLAN APPROVAL		JAC	CJH	22.05.31
1. ISSUED FOR DRAFT	PLAN APPROVAL		JAC		21.08.24
Issued			Ву	Appd.	YY.MM.DE
File Name: 161413684_c-dt		JAC	CJH	JAC	21.07.23
Permit-Seal		Dwn.	Chkd.	Dsgn.	YY.MM.DE
	22				
Client/Project TRICAR DEVI 1242, 1250, 1 & 9 VALLEY F GUELPH, ON	ELOPMEN				
Client/Project TRICAR DEVI 1242, 1250, 1 & 9 VALLEY F GUELPH, ON	ELOPMEN 1260 GOR ROAD				
Client/Project TRICAR DEVI 1242, 1250, 1 & 9 VALLEY F GUELPH, ON Title	ELOPMEN ELOPMEN 1260 GOR ROAD TAILS			3	5m
Client/Project TRICAR DEVI 1242, 1250, 1 & 9 VALLEY F GUELPH, ON Title NOTES & DE Project No.	ELOPMEN ELOPMEN 1260 GOR ROAD TAILS	DON S		3 Revi	

\_\_\_\_ \_\_\_\_

# **APPENDIX B – DESIGN SHEETS**

Stantec		Tricar 250, 1260 Go	Develop ordon Stre		ey Road											DESIGN PA	ORM	1 IN	5	Years		
	DATE: DESIGNED I CHECKED B		May 1 JC CH	19, 2022		FILE NUMB			IJIILL	•						I = a / (( tc a= b= c=	0.00 0.00	MANNING'S MINIMUM C TIME OF EN	COVER:	0.000 48.000 10	m min	
LOCA	TION					DRAIN	AGE AREA									PIPE SELE	CTION					
Street	U/S	D/S	Area ID	5-Year Area Design (ha)	Runoff Coeff. Design	A x R	Accum. A x R	U/S T <sub>c</sub> (min)	Rainfall Intensity (mm/hr)	Total Flow (m <sup>3</sup> /s)	Length Design (m)	Design Size (mm)	Slope Design (%)	Full Capacity (m³/s)	Full Velocity (m/s)	Actual Velocity (m/s)	Time of Flow (min)	5-Year Q <sub>A</sub> /Q <sub>C</sub> (%)	Fall in Sewer (m)	Upper Inv. (m)	Lower Inv. (m)	Drop (m)
	<b></b>																					
Street A Street A	MH3 MH2	MH2 MH1	A26 A27	0.27	0.90	0.24	0.24	10.00 10.23	109.68 108.62	0.074 0.081	36.80 41.60	300 300	4.48 0.75	0.205	2.90 1.18	2.63 1.37	0.23	36.2% 97.3%	1.65 0.31	338.320 336.621	336.67 336.31	0.05
Street A			AZ7	0.05	0.90	0.05	0.27	10.25	108.02	0.081	41.00	500	0.75	0.084	1.10	1.57	0.50	97.5%	0.51	550.021	550.51	
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#### 1250 Gordon Street 161413684

Jun 8, 2022

#### FIRE FLOW CALCULATIONS AS PER OBC REQUIREMENTS

#### ONTARIO BUILDING CODE CLAUSE A-3.2.5.7.

#### $Q = K x V x S_{Tot}$

As per Table 2, Section A-3.2.5.7, OBC

	Required Minimum Water Supply Flow
OBC Part 3 Buildings under Building Code	Rate (L/min)
One-storey building with area ≤ 600 m2	1800
All other buildings	2700 (if Q ≤ 108,000 L)
	3600 (if Q >108,000 L and ≤ 135,000 L)
	4500 (if Q >135,000 L and ≤ 162,000 L)
	5400 (if Q >162,000 L and≤ 190,000 L)
	6300 (if Q >190,000 L and ≤ 270,000 L)
	9000 (if Q >270,000 L)

#### **Major Occupancy Classification**

Group C Residential Occupancies

 Water Supply Coefficient - K

 As per Table 1, Section A-3.2.5.7, OBC

 K= 10

#### **Total Building Volume**

Dida	Area	Flr Height	Volume
Bldg	(m <sup>2</sup> )	(m)	(m <sup>3</sup> )
2	23900	3.2	76480
			0
			0
Total			76480

\*Assuming single 10 storey Building #2 apartment is critical

#### Exposures

	Separation	
	(m)	Coeff
North	50	0.00
South	50	0.00
East	50	0.00
West	24	0.00
S <sub>tot</sub>		1.00

\*\*above separation distances conservative estimates.

Minimum Water Supply  $Q = K \times V \times S$ 

$Q = K x V x S_{Tot}$	Q=10 x	76480 x 1	1.00 =	764,800	L
si	nce Q > 270,000	) L	-		-
<b>Required Fire Flow (from Table</b>	2 above)		=	9000	L/min
			=	150	L/s

# APPENDIX C – EMAIL CORRESPONDENCE

Good Morning Chris, We will be retaining consultant in Q2. We will be reviewing the 1242-1270 Gordon Street development during the design of Gordon St.

Thanks.

Ike Umar, C.E.T. | Project Manager Engineering and Transportation Services | Infrastructure, Development and Enterprise City of Guelph

T 519-822-1260 X2242 E ike.umar@guelph.ca

From: Hendriksen, Chris (Vancouver) <Chris.Hendriksen@stantec.com>
Sent: Friday, March 11, 2022 9:51 AM
To: Ike Umar <Ike.Umar@guelph.ca>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Good morning lke. I wanted to follow up on the design progression of this work and to confirm that the design contributions from the proposed development at 1242-1270 Gordon Street and 9 Valley Road are being incorporated. Can you please provide an update?

Thanks

Chris

From: Ike Umar <<u>Ike.Umar@guelph.ca</u>>
Sent: Tuesday, August 10, 2021 8:01 AM
To: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Cc: Hendriksen, Chris (Vancouver) <<u>Chris.Hendriksen@stantec.com</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Good Morning Derrick, As per email below from Reg I do not have anything to add. We would know better once we have a schedule of construction in 2023.

Thanks Ike Umar, C.E.T. |Project Manager Engineering and Transportation Services | Infrastructure, Development and Enterprise City of Guelph

T 519-822-1260 X2242 E <u>ike.umar@guelph.ca</u>

From: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>

Sent: Thursday, August 5, 2021 4:47 PM
To: Ike Umar <<u>Ike.Umar@guelph.ca</u>>
Cc: Hendriksen, Chris (Vancouver) <<u>Chris.Hendriksen@stantec.com</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Good afternoon lke,

I am reaching out regarding the Gordon Street Sanitary Sewer works as per the correspondence below. We would like to confirm that the proposed sanitary sewer fronting the 1250 Gordon Street proposed development will be available as part of the construction work noted below which notes availability late 2023 to early 2024? Do you have any insight on anticipated Construction staging to better understand when the sewer servicing the 1250 site will be available? Any information on this would be greatly appreciated.

Thanks,

**Derrick Rice** P. Eng Project Engineer, Community Development

Direct: 519-675-6644 Cell: 519-630-3627 Derrick.Rice@stantec.com

Stantec 600-171 Queens Avenue London ON N6A 5J7



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From: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Sent: Wednesday, July 21, 2021 5:01 PM
To: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Cc: Hendriksen, Chris (Vancouver) <<u>Chris.Hendriksen@stantec.com</u>>; Ike Umar
<Ike.Umar@guelph.ca>; Mary Angelo <<u>Mary.Angelo@guelph.ca</u>>; Colleen Gammie
<Colleen.Gammie@guelph.ca>

Subject: RE: Gordon Street Sanitary Sewer upgrades

Derrick,

The Gordon St EA has been completed so we're moving ahead with implementation. The City is currently preparing a RFP to retain an engineering firm to undertake final design starting later this year and construction in 2023. The sewers will be available earliest as late 2023 or more likely in 2024. We'll know better once the final design is completed and staging of works is better understood.

Ike Umar (cc'd) is the City's PM for the works.

• Reg

Sent: July 21, 2021 8:31 AM

To: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>

**Cc:** Hendriksen, Chris (Vancouver) <<u>Chris.Hendriksen@stantec.com</u>>; Arun Hindupur

<arun.hindupur@guelph.ca>

Subject: RE: Gordon Street Sanitary Sewer upgrades

**[EXTERNAL EMAIL]** Do not click links or attachments unless you recognize the sender and know the content is safe.

Good morning Reg,

I reached out to you last year regarding the Gordon Street sanitary sewer upgrades and our client was hoping we could get an update on the work. I see from the links you provided me that design is scheduled for 2021 and construction 2023, could you give any further insight on progress for the project and if there is an anticipated date of when the new sewers will be in service?

Thanks,

Derrick Rice P. Eng Project Engineer, Community Development

Direct: 519-675-6644 Cell: 519-630-3627 Derrick.Rice@stantec.com

Stantec 600-171 Queens Avenue London ON N6A 5J7

?

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From: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Sent: Wednesday, March 4, 2020 3:54 PM
To: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Cc: Hendriksen, Chris <<u>Chris.Hendriksen@stantec.com</u>>; Arun Hindupur

<<u>arun.hindupur@guelph.ca</u>>

Subject: RE: Gordon Street Sanitary Sewer upgrades

Derrick,

I can't commit to keep you current on the status of works. Please monitor the City's webpages concerning the EA's and get added to the circulation list.

https://guelph.ca/city-hall/planning-and-development/community-plansstudies/environment-planning/environmental-assessments/gordon-street-improvements/

https://guelph.ca/plans-and-strategies/water-and-wastewater-servicing-master-plan/

• Reg

From: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Sent: March 4, 2020 3:22 PM
To: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Cc: Hendriksen, Chris <<u>Chris.Hendriksen@stantec.com</u>>; Arun Hindupur
<<u>Arun.Hindupur@guelph.ca</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Thanks for the quick response Reg,

If you could keep us in the loop as things progress it would be greatly appreciated.

Thanks,

**Derrick Rice** EIT Engineering Intern, Community Development

Direct: 519-675-6644 Cell: 519-630-3627 Derrick.Rice@stantec.com

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From: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Sent: Wednesday, March 4, 2020 2:50 PM
To: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Cc: Hendriksen, Chris <<u>Chris.Hendriksen@stantec.com</u>>; Arun Hindupur
<<u>arun.hindupur@guelph.ca</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Derrick,

The sizing of the sanitary system along Gordon Street is being considered within the overall Master Wastewater Servicing Plan currently underway. Sizing takes into account future growth including this development.

Funding is allocated in the capital budget for design to commence later this year, but I would not want to say construction will be completed in 2021. There is a large scope of work to complete plus two EA's to wrap up. We'll know much better when the new sewer will be in service once the road related EA and the Wastewater Servicing Master Plan EA are complete.

Reg Russwurm, MBA, P.Eng, **Manager, Design and Construction** Engineering and Transportation Services, **Infrastructure, Development and Enterprise City of Guelph** 519-822-1260 extension 2765

#### reg.russwurm@guelph.ca

guelph.ca facebook.com/cityofguelph @cityofguelph

• Reg

From: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Sent: March 4, 2020 11:44 AM
To: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Cc: Hendriksen, Chris <<u>Chris.Hendriksen@stantec.com</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

#### Hi Reg,

We had previously corresponded with Daryush Esmaili about the Gordon Street Sanitary Sewer upgrades to ensure that our development at 1250 Gordon Street (encompasses 9 Valley, 1242, 1250 and 1260 Gordon) would be considered in the sanitary sewer upgrade planned on Gordon Street. He had confirmed our development would be accommodated in the sizing of the planned upgrade back in June of 2019. I just wanted to contact you to find out if there are any updates on this project that you can provide?

If you have any questions please feel free to contact me.

Thanks,

Derrick Rice EIT Engineering Intern, Community Development

Direct: 519-675-6644 Cell: 519-630-3627 Derrick.Rice@stantec.com

Stantec 600-171 Queens Avenue London ON N6A 5J7

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From: Engineering General Delivery <<u>Engineering@guelph.ca</u>>
Sent: Wednesday, March 4, 2020 11:33 AM
To: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Cc: Reg Russwurm <<u>Reg.Russwurm@guelph.ca</u>>
Subject: RE: Gordon Street Sanitary Sewer upgrades

Good morning Mr. Rice,

Unfortunately Daryush Esmaili is no longer with the City of Guelph. Reg Russwurm is now the Manager of Design and Construction with Engineering and Transportation Services.

I have cc'ed him on this email in the hopes he can help provide the information you require.

Thank you,

**Steve Wark,** Clerical Assistant II Engineering and Transportation Services, **Infrastructure, Development and Enterprise City of Guelph** 519-822-1260 extension 2338 <u>steve.wark@guelph.ca</u>

From: Rice, Derrick <<u>Derrick.Rice@stantec.com</u>>
Sent: March 4, 2020 10:07 AM
To: Engineering General Delivery <<u>Engineering@guelph.ca</u>>
Subject: Gordon Street Sanitary Sewer upgrades

Hi,

I am trying to contact Daryush Esmaili regarding the Gordon Street Sanitary Sewer upgrades but seem to be getting a bounce back email from guelph.ca, could you please forward my contact information along to Daryush or let me know what I need to do to fix the issue?

Thanks,

#### **Derrick Rice EIT**

Engineering Intern, Community Development

Direct: 519-675-6644 Cell: 519-630-3627 Derrick.Rice@stantec.com

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## APPENDIX D – SWM FIGURES, MODELS & SUPPORTING DATA





ORIGINAL SHEET - ANSI D



#### Stantec 600-171 Queens Avenue

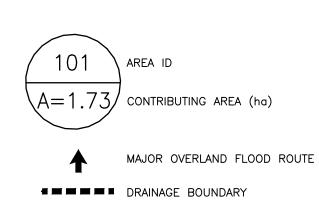
London ON N6A 5J7 Tel. 519-645-2007 www.stantec.com

Liability Note:

The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.

### Notes

- <u>CITY OF GUELPH BENCHMARK 225</u> <u>ELEVATION 338.665</u> LOCATION: 1221 GORDON STREET
   EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014)
   THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER
   SITE PLAN PREPARED BY STANTEC, DATED JANUARY, 2020.



1. SITE PLAN REVISIONS		JAC	CJH	21.05.14
Revision		Ву	Appd.	YY.MM.DD
2. FOR SITE PLAN APPROVAL		JAC	CJH	21.05.14
1. FOR SITE PLAN APPROVAL		JAC	CJH	20.03.24
Issued		Ву	Appd.	YY.MM.DD
File Name: 161413684_c-sd_ex	JAC	CJH	JAC	19.05.31
	Dwn.	Chkd.	Dsgn.	YY.MM.DD
Permit-Seal				

Client/Project TRICAR DEVELOPMENTS INC.

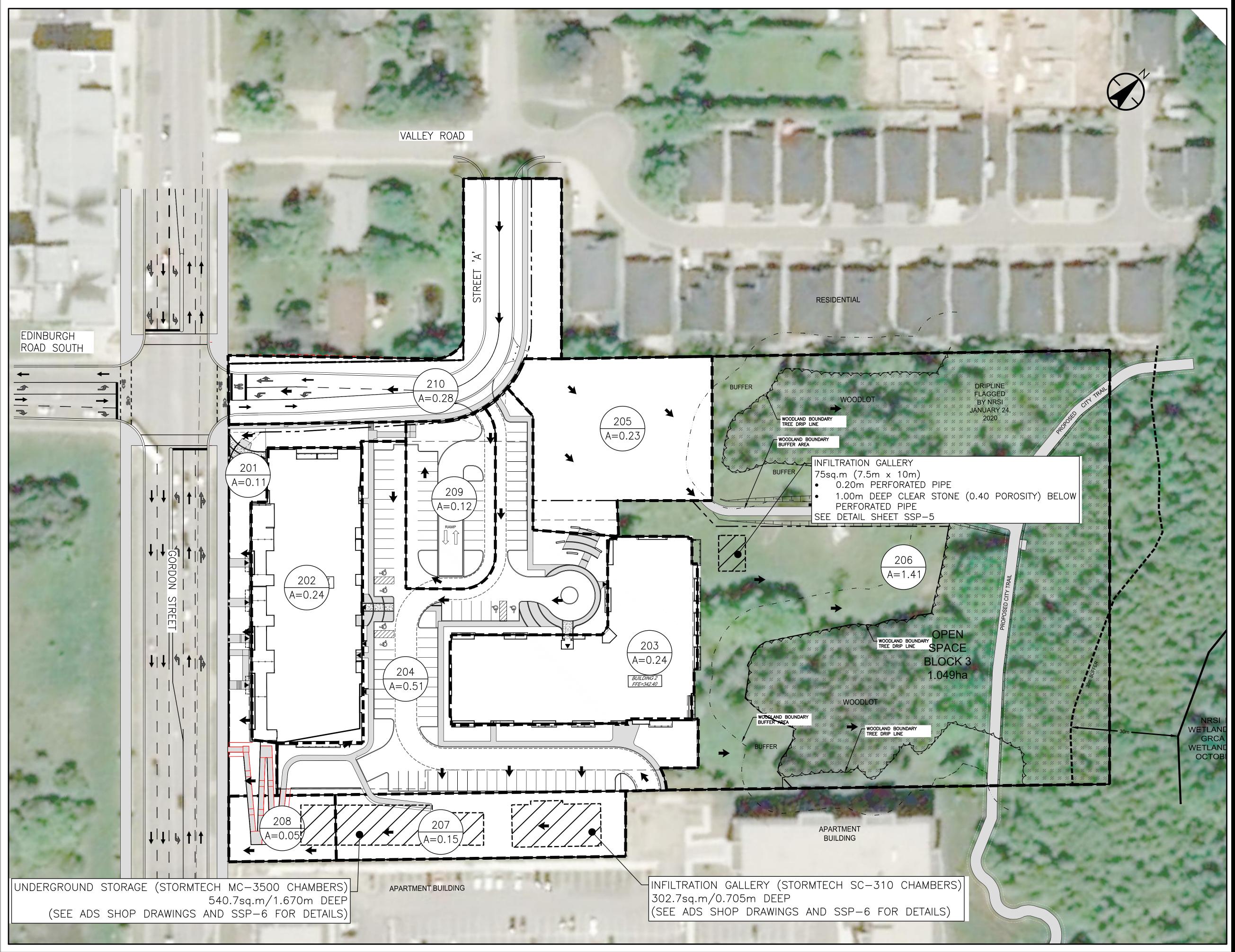
## 1250 GORDON STREET

### GUELPH, ON

### Title

## EXISTING STORM DRAINAGE CONDITIONS

Project No. 161413684	Scale 0 4 1:400	12 20m
Drawing No.	Sheet	Revision
1	1 of 2	1



ORIGINAL SHEET - ANSI D



#### Stantec 600-171 Queens Avenue

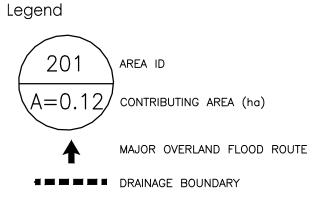
London ON N6A 5J7 Tel. 519-645-2007 www.stantec.com

Liability Note:

The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.

### Notes

- <u>CITY OF GUELPH BENCHMARK 225</u> <u>ELEVATION 338.665</u> LOCATION: 1221 GORDON STREET
   EXISTING SURVEY COMPLETED BY BSR&D (NOVEMBER, 4 2014)
   THE CONTRACTOR IS TO VERIFY ALL EXISTING ELEVATIONS AND EXISTING CONDITIONS AND TO REPORT ANY DISCREPANCIES TO THE CONSULTING ENGINEER
   SITE PLAN PREPARED BY STANTEC, DATED JANUARY, 2020.



2. SWM DESIGN REVISIONS		JAC	DW	22.05.31
2. SITE PLAN REVISIONS		JAC	CJH	21.07.30
1. SITE PLAN REVISIONS		JAC	CJH	21.05.14
Revision		Ву	Appd.	YY.MM.DD
File Name: 161413684_c-sd_prop	JAC	CJH	JAC	19.05.31
	Dwn.	Chkd.	Dsgn.	YY.MM.DD
Permit-Seal				

Client/Project TRICAR DEVELOPMENTS INC.

## 1250 GORDON STREET

### GUELPH, ON

### Title

### PROPOSED STORM DRAINAGE CONDITIONS

Project No. 161413684	Scale 0 4 1:400	12 20m
Drawing No.	Sheet	Revision
2	2 of 2	2

# HYDROLOGIC MODELING INPUTS

Subject:	MIDUSS Parameters
Project:	1242-1260 Gordon and 9 Valley
Project No.:	161413684
Client:	Tricar
Date:	June 6, 2022

Table 1: CN Values							Source		
Land Use				Hy	drologic Soil Typ	be			
		А	AB	В	BC	С	CD	D	
Meadow	"Good"	30	44	58	65	71	75	78	USDA
Woodlot	"Fair"	36	48	60	67	73	76	79	USDA
Lawns	"Good"	39	50	61	68	74	77	80	USDA
Pasture/Range		49	55	60	70	79	82	84	USDA
Crop		64	70	74	79	81	84	85	USDA
Gravel		76	81	85	87	89	90	91	USDA
Bare Soil (Fallow)		77	82	86	89	91	93	94	USDA
Impervious		98	98	98	98	98	98	98	USDA

USDA - United States Department of Agriculture (2004), National Engineering Handbook, Part 630 Hydrology,

## Table 2: Pre-Development Parameters

Area Description	Catchment Number	Area	Flow Path Length	CN	Slope	Impervious Coverage
		(ha)	(m)		(%)	(%)
To Gordon Street	101	1.33	70.00	67	2.50	10
To Torrance Watershed	102	1.72	150.00	67	5.00	1
TOTAL AREA		3.05				

## Table 3: Post-Development Parameters

Area Description	Catchment Number	Area	Flow Path Length	CN	Slope	Imperviousnes s
		(ha)	(m)		(%)	(%)
Uncontrolled to Gordon	201	0.11	6	68	2.0	70
West Building (Building 1)	202	0.24	15	68	0.5	99
East Buidling (Building 2)	203	0.24	15	68	0.5	99
Parking	204	0.51	10	68	2.0	90
Future Park	205	0.23	50	68	2.0	10
Uncontrolled to Torrance	206	1.41	120	68	5.0	0
Landscaped Area to Storage	207	0.15	75	68	3.0	50
Uncontrolled Landscape Area	208	0.05	35	68	25.0	70
Parking (Minor to Storage)	209	0.12	10	68	2.0	99
Street A (outside site limits)	210	0.28	-	-		
TOTAL AREA		3.34				

 Notes:
 3.34

 Slope measure from topographic contours and pre-development drainage plan Imperviousness estimated from development plan (existing buildings imperviouness estimated to be 99%) Street A is not included within the hydrologic model as it is outside the site boundaries



1242-1260 Gordon and 9 Valley Project: 161413684 Project Number: Project Location: Guelph Designer: DW Date: 6/6/2022 Pond Name: Subsurface Storage

# Stormwater Management Facility Design Calculations

			gement	I acinty D	esign calcul	ations				
	R	ating Curve		Estimated	Volume E				Outlet Structure Controls	6
	<b>F</b> lowether	Disalar	Storage	Detention		Active Storage		0.5	Demonst	
	Elevation (m)	Discharge (m <sup>3</sup> /s)	Active (m <sup>3</sup> )	Time (hrs)	Elevation (m)	Depth (m)	Elevation (m)	Orifice #1 (m³/s)	Paramet	ers
Drifice Invert	336.62	(1173)	(11)	(113)	336.62	(11)	336.6	(1173)	Orifice #1 Elev (m)	Orifice Coeff.
itone Invert	336.81	0.0047			336.81	0.19	336.8	0.005	336.62	0.620
	336.84	0.0051	5.49	0.3	336.84	0.2	336.8	0.005	Orifice #1-Midpoint (mm)	Perimeter (m)
	336.86	0.0055	10.98	0.6	336.86	0.2	336.9	0.005	336.66	0.236
	336.89	0.0058	16.47	0.9	336.89	0.3	336.9	0.006	Orifice Diameter (mm)	Area (m²)
	336.91 336.94	0.0061 0.0064	21.96 27.45	1.1 1.4	336.91 336.94	0.3 0.32	336.9 336.9	0.006 0.006	75 Weir Coeff. (Semi-Circular)	0.004 Orientation
	336.96	0.0004	32.94	1.4	336.96	0.32	337.0	0.000	1.62	Vertical
	336.99	0.0070	38.44	1.8	336.99	0.37	337.0	0.007	1.02	Vortiour
	337.01	0.0072	43.93	2.0	337.01	0.39	337.0	0.007		
ase of Chamber	337.04	0.0075	49.42	2.2	337.04	0.42	337.0	0.007		
	337.06	0.0077	61.00	2.7	337.06	0.44	337.1	0.008		
	337.09	0.0080	72.54	3.1	337.09	0.47	337.1	0.008		
	337.11	0.0082	84.03	3.5	337.11	0.49	337.1	0.008		
	337.14	0.0084	95.49	3.9	337.14	0.52	337.1	0.008		
	337.17	0.0086	106.91	4.2	337.17	0.55	337.2	0.009		
	337.19	0.0089	118.29	4.6	337.19	0.57	337.2 337.2	0.009		
	337.22 337.24	0.0091 0.0093	129.63 140.93	4.9 5.3	337.22 337.24	0.60 0.62	337.2 337.2	0.009 0.009		
	337.24	0.0095	140.93	5.6	337.24	0.65	337.3	0.009		
	337.29	0.0097	163.37	5.9	337.29	0.67	337.3	0.010		
	337.32	0.0099	174.52	6.3	337.32	0.70	337.3	0.010		
	337.34	0.0100	185.62	6.6	337.34	0.72	337.3	0.010		
	337.37	0.0102	196.66	6.9	337.37	0.75	337.4	0.010		
	337.39	0.0104	207.64	7.2	337.39	0.77	337.4	0.010		
	337.42 337.45	0.0106	218.55	7.5 7.7	337.42 337.45	0.80	337.4 337.4	0.011		
	337.45 337.47	0.0108 0.0109	229.40 240.19	7.7 8.0	337.45 337.47	0.83 0.85	337.4 337.5	0.011 0.011		
	337.50	0.0109	250.89	8.3	337.50	0.85	337.5	0.011		
	337.52	0.0113	261.53	8.5	337.52	0.90	337.5	0.011	1	
	337.55	0.0114	272.08	8.8	337.55	0.93	337.5	0.011		
	337.57	0.0116	282.55	9.1	337.57	0.95	337.6	0.012		
	337.60 337.62	0.0118 0.0119	292.93 303.21	9.3 9.5	337.60 337.62	0.98 1.00	337.6 337.6	0.012 0.012		
	337.65	0.0113	313.40	9.8	337.65	1.03	337.6	0.012		
	337.67	0.0122	323.48	10.0	337.67	1.05	337.7	0.012		
	337.70	0.0124	333.46	10.2	337.70	1.08	337.7	0.012		
	337.72	0.0125	343.31	10.5	337.72	1.10	337.7	0.013		
	337.75	0.0127	353.05	10.7	337.75	1.13	337.7	0.013		
	337.78 337.80	0.0128 0.0130	362.66 372.14	10.9 11.1	337.78 337.80	1.16 1.18	337.8 337.8	0.013 0.013		
	337.83	0.0130	381.46	11.3	337.83	1.10	337.8	0.013		
	337.85	0.0133	390.64	11.5	337.85	1.23	337.9	0.013		
	337.88	0.0134	399.65	11.7	337.88	1.26	337.9	0.013		
	337.90	0.0135	408.48	11.8	337.90	1.28	337.9	0.014		
	337.93	0.0137	417.12	12.0	337.93	1.31	337.9	0.014		
	337.95 337.98	0.0138 0.0139	425.55 433.75	12.2 12.4	337.95 337.98	1.33 1.36	338.0 338.0	0.014 0.014		
	338.00	0.0141	441.69	12.5	338.00	1.38	338.0	0.014		
	338.03	0.0142	449.32	12.7	338.03	1.41	338.0	0.014		
	338.05	0.0143	456.58	12.8	338.05	1.43	338.1	0.014		
	338.08	0.0145	463.26	12.9	338.08	1.46	338.1	0.014		
	338.11 338.13	0.0146 0.0147	469.45 475.45	13.0 13.2	338.11 338.13	1.49 1.51	338.1 338.1	0.015 0.015		
	338.16	0.0149	481.27	13.3	338.16	1.54	338.2	0.015		
op of Chamber	338.18	0.0150	486.86	13.4	338.18	1.56	338.2	0.015		
	338.21	0.0151	492.35	13.5	338.21	1.59	338.2	0.015		
	338.23	0.0152	497.84	13.6	338.23	1.61	338.2	0.015		
	338.26 338.28	0.0153 0.0155	503.33 508.82	13.7 13.8	338.26 338.28	1.64 1.66	338.3 338.3	0.015 0.015		
	JJ0.20	0.0100	JU0.02	13.0	000.20	1.00	000.0	0.010	1	
	338 31	0.0156	514 31	13.9	338 31	1.69		0.016		
	338.31 338.33	0.0156 0.0157	514.31 519.81	13.9 14.0	338.31 338.33	1.69 1.71	338.3 338.3	0.016 0.016		
							338.3			
	338.33 338.36 338.38	0.0157 0.0158 0.0159	519.81 525.30 530.79	14.0 14.1 14.2	338.33 338.36 338.38	1.71 1.74 1.76	338.3 338.3 338.4 338.4	0.016 0.016 0.016		
	338.33 338.36 338.38 338.41	0.0157 0.0158 0.0159 0.0161	519.81 525.30 530.79 536.28	14.0 14.1 14.2 14.3	338.33 338.36 338.38 338.41	1.71 1.74 1.76 1.79	338.3 338.3 338.4 338.4 338.4 338.4	0.016 0.016 0.016 0.016		
	338.33 338.36 338.38 338.41 338.44	0.0157 0.0158 0.0159 0.0161 0.0162	519.81 525.30 530.79 536.28 541.77	14.0 14.1 14.2 14.3 14.4	338.33 338.36 338.38 338.41 338.44	1.71 1.74 1.76 1.79 1.82	338.3 338.3 338.4 338.4 338.4 338.4 338.4	0.016 0.016 0.016 0.016 0.016		
op of Stone	338.33 338.36 338.38 338.41 338.44 338.44	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163	519.81 525.30 530.79 536.28 541.77 547.26	14.0 14.1 14.2 14.3 14.4 14.4	338.33 338.36 338.38 338.41 338.44 338.44	1.71 1.74 1.76 1.79 1.82 1.84	338.3 338.3 338.4 338.4 338.4 338.4 338.4 338.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016		
Top of Stone	338.33 338.36 338.38 338.41 338.44	0.0157 0.0158 0.0159 0.0161 0.0162	519.81 525.30 530.79 536.28 541.77	14.0 14.1 14.2 14.3 14.4	338.33 338.36 338.38 338.41 338.44	1.71 1.74 1.76 1.79 1.82	338.3 338.3 338.4 338.4 338.4 338.4 338.4	0.016 0.016 0.016 0.016 0.016		
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4	338.33 338.36 338.38 338.41 338.44 338.44	1.71 1.74 1.76 1.79 1.82 1.84 1.84 2.38	338.3 338.3 338.4 338.4 338.4 338.4 338.4 338.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016		
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 Greater than	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 339.49	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equat		
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 Greater than T=[v <sub>2</sub> -v <sub>1</sub> ]/[(Q <sub>2</sub>	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	$\begin{array}{c} 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.020\\ \end{array}$ Orifice flow equal $Q = C \cdot A \cdot (2 \cdot g \cdot H)^{0.1}$		
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.5 14.5 14.5 Greater than T=[v <sub>2</sub> -v <sub>1</sub> ]/[(Q <sub>2</sub> where	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	$\begin{array}{c} 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.016\\ 0.020\\\\\\ \end{array}$ Orifice flow equal $Q = C \cdot A \cdot (2 \cdot g \cdot H)^{0.1}\\ \text{where} \end{array}$	5	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.5 14.5 14.5 Greater than T=[v <sub>2</sub> -v <sub>1</sub> ]/[(Q <sub>2</sub> where T=drawdown	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equat $Q = C \cdot A \cdot (2 \cdot g \cdot H)^{0.1}$ where C = orifice coer	5 fficient	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2 + v_1)/[(Q_2 + v_1)/[(Q_2 + v_1)/[(Q_2 + v_1)/[(Q_2 + v_1)/[(Q_2 + v_1)/(Q_2 + v_1)/(Q$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal $Q = C \cdot A \cdot (2 \cdot g \cdot H)^{0.1}$ where C = orifice coee A = area of orif	5 fficient fice	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2^2)^2]$ where T=drawdown $v_2=starting p$ $v_2=ending pco$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orifid 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume and volume	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equations Q = C+A+(2+g+H) <sup>0.1</sup> where C = orifice coet A = area of orifi g = acceleration	<sup>5</sup> fficient fice n due to gravity	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2 + v_1)/[(Q_2 + v_2) + v_2)]$ where T=drawdown $v_2=starting pc$ $Q_2=starting fc$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orifid 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume ond volume low	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2+g-H) <sup>0.1</sup> where C = orifice coel A = area of orifi g = acceleratio H = head abov	5 fficient fice n due to gravity e centre line of orifice	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2^2)^2]$ where T=drawdown $v_2=starting p$ $v_2=ending pco$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orifid 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume ond volume low	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2+g-H) <sup>0.1</sup> where C = orifice coel A = area of orifi g = acceleratio H = head abov	<sup>5</sup> fficient fice n due to gravity	of the orifice diameter
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2 + v_1)/[(Q_2 + v_2)])$ where T=drawdown $v_2=starting pc$ $Q_2=starting for Q_1=ending for$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume low pw	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5 W Calculations:	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equation Q = C+A-(2-g-H) <sup>0.1</sup> where C = orifice coet A = area of orifice G = acceleration H = head abovy Note: used where	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4	of the orifice diameter
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 Greater than $T=[v_2-v_1]/[(Q_2 where T=drawdown v_2=starting p v_2=ending pc Q_2=starting f Q_1=ending flucture for the start of t$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume low ow 0.1 m above Orific	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2+g-H) <sup>0.1</sup> where C = orifice coe A = area of orifig g = acceleratio H = head abov Note: used who	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation	of the orifice diameter
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 14.5 T= $[v_2-v_1]/[(Q_2 where T=drawdown v_2=starting p c Q_2=starting f Q_1=ending f left Q_1=endin$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume low ow 0.1 m above Orific	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2-g-H) <sup>0.1</sup> where C = orifice coe A = area of orifi g = acceleratio H = head abov Note: used whe Sharp crested se Q=C*D <sup>2.5</sup> *(H/D) <sup>1.1</sup>	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation	of the orifice diameter
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 14.5 T= $[v_2-v_1]/[(Q_2 + Q_2) + Q_2 + Q$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific ond volume low ow 0.1 m above Orific low 0.1 m above Orific	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2-g-H) <sup>0.1</sup> where C = orifice coe A = area of orifi g = acceleratio H = head abov Note: used whe Sharp crested se Q=C*D <sup>2.5</sup> *(H/D) <sup>1.1</sup>	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 14.5 T= $[v_2-v_1]/[(Q_2 where T=drawdown v_2=starting p c_2=starting f Q_2=starting f Q_1=ending f Here T=drawdown v_2=v_1]/[(Q_2 where T=drawdown v_2=v_1)/(Q_2 where V_2=v_1)/$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific $_2+Q_1)/2]/3600$ time in hours ond volume low 0.1 m above Orifice 2)]/3600 time in hours	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2-g-H) <sup>0.1</sup> where C = orifice coe A = area of orifi g = acceleratio H = head abov Note: used whe Sharp crested se Q=C*D <sup>2.5</sup> *(H/D) <sup>1.1</sup> where C = sharp crest	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation 88 ted semi-circular weir coefficien	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.5 14.5 14.5 14.5 14.5 T= $[v_2-v_1]/[(Q_2 where T=drawdown v_2=starting p Q_2=starting f Q_1=ending f d Q_1=ending f d$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 20.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume how bow 0.1 m above Orific low bow 0.1 m above Orific low bow 0.1 m above Orific low bow	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equat Q = C+A-(2-g-H) <sup>0.1</sup> where C = orifice coer A = area of orifig g = acceleratio H = head abov Note: used whe Sharp crested se Q=C*D <sup>2.5</sup> *(H/D) <sup>1.1</sup> where C = sharp cress D = diameter of	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation 88 ted semi-circular weir coefficien of orifice	
op of Stone	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.00	0.0157 0.0158 0.0159 0.0161 0.0162 0.0163 0.0164 0.0204	519.81 525.30 530.79 536.28 541.77 547.26 552.75 552.75	14.0 14.1 14.2 14.3 14.4 14.4 14.5 14.5 14.5 14.5 T= $[v_2-v_1]/[(Q_2 where T=drawdown v_2=starting p c_2=starting f Q_2=starting f Q_1=ending f Here T=drawdown v_2=v_1]/[(Q_2 where T=drawdown v_2=v_1)/(Q_2 where V_2=v_1)/$	338.33 338.36 338.38 338.41 338.44 338.46 338.49 339.49 0.1 m above Orific 2+Q <sub>1</sub> )/2]/3600 time in hours ond volume low but volume low but time in hours ond volume time in hours ond volume time in hours ond volume	1.71 1.74 1.76 1.79 1.82 1.84 1.87 2.38 Orifice Flo	338.3 338.3 338.4 338.4 338.4 338.4 338.5 338.5 338.5 339.5	0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.016 0.020 Orifice flow equal Q = C+A+(2-g-H) <sup>0.1</sup> where C = orifice coe A = area of orifi g = acceleratio H = head abov Note: used who Sharp crested se Q=C+D <sup>2.5</sup> *(H/D) <sup>1.1</sup> where C = sharp cress D = diameter of H = head abov	5 fficient fice n due to gravity e centre line of orifice en water elevation is above 3/4 mi-circular weir equation 88 ted semi-circular weir coefficien of orifice	t

Тор	of	Stone

#### Rooftop Storage Calculations 1242-1260 Gordon and 9 Valley Subject: Project: Project No. 161413684 Client: Tricar

June 6, 2022 Date:

# Rating Curve for 1 ha

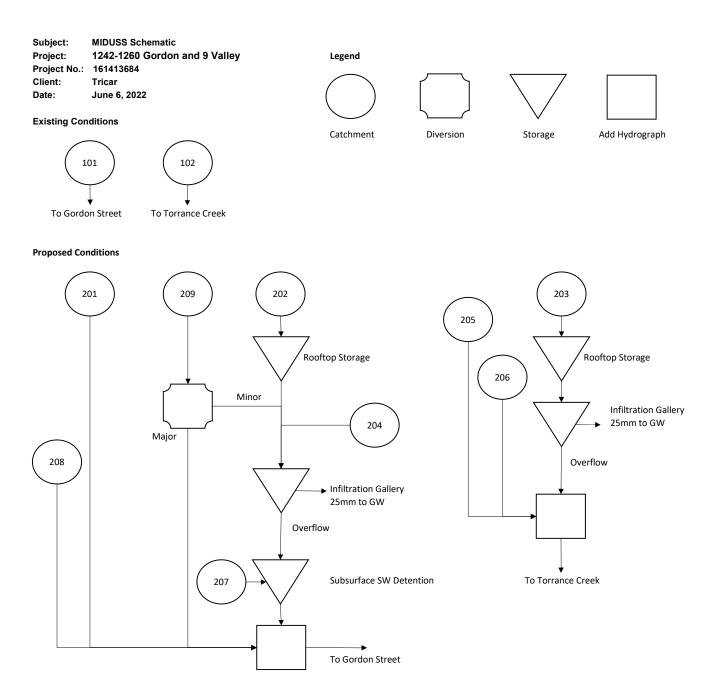
Q (m3/s)	Storage (ha-m)	Depth (m)
0.0226		0.023
0.0275	0.031	0.031
0.034	0.045	0.045
0.042	0.061	0.061
0.208	0.0625	0.0625

.

### Catchment 202/203 0 24

Site Ara

0.24		
Q (m3/s)	Storage (ha-m)	Depth (m)
0.0054	0.0055	0.023
0.0066	0.0074	0.031
0.0082	0.0108	0.045
0.0101	0.0146	0.061
0.0499	0.0150	0.063



# **MIDUSS FILES**

Stantec | 1250 Gordon

```
Output File (4.7) GOREX.out
                                   opened 2022-06-06 21:07
      Units used are defined by G =
                                    9.810
         300
              600
                      5.000
                                  are MAXDT MAXHYD & DTMIN values
      Licensee: Paragon Engineering Limited
35
      COMMENT
     5
           line(s) of comment
      1242-1260 Gordon Street and 9 Valley - 1614-13684
      Stormwater Management Modelling
      May 2022 - D. Williams
      START
14
          1=Zero; 2=Define
     1
35
      COMMENT
     7
           line(s) of comment
      *******
      25-mm STORM
      ******
2
      STORM
               1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
    509.000
               Coefficient a
      6.000
               Constant b
                             (min)
       .799
               Exponent c
       .400
               Fraction to peak r
    240.000
               Duration ó 1500 min
              25.028 mm
                           Total depth
3
      IMPERVIOUS
               Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
               Manning "n"
       .013
     98.000
               SCS Curve No or C
       .100
               Ia/S Coefficient
               Initial Abstraction
      2.000
14
      START
     1
           1=Zero; 2=Define
35
      COMMENT
           line(s) of comment
     3
      *****************************
      Catchment 101 - Existing to Gordon
      CATCHMENT
4
    101.000
               ID No.ó 99999
      1.330
               Area in hectares
               Length (PERV) metres
    110.000
      2.500
               Gradient (%)
     10.000
               Per cent Impervious
     70.000
               Length (IMPERV)
```

```
.000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
        .250
                Manning "n"
                SCS Curve No or C
     67.000
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .000
                                   .000
                                             .000 c.m/s
             .018
                        .736
             .110
                                   .173
                                           C perv/imperv/total
15
      ADD RUNOFF
             .018
                        .018
                                   .000
                                             .000 c.m/s
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
     3
           line(s) of comment
      Catchment 102 - Existing to Torrence
      *********
      CATCHMENT
4
    102.000
                ID No.ó 99999
      1.720
                Area in hectares
    150.000
                Length (PERV) metres
                Gradient (%)
      5.000
                Per cent Impervious
      1.000
                Length (IMPERV)
      1.000
                %Imp. with Zero Dpth
        .000
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
                Manning "n"
       .250
     67.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .005
                        .000
                                   .000
                                             .000 c.m/s
             .110
                        .650
                                   .116
                                           C perv/imperv/total
15
      ADD RUNOFF
                                             .000 c.m/s
             .005
                        .005
                                   .000
      START
14
     1
           1=Zero; 2=Define
35
      COMMENT
           line(s) of comment
     7
      ******
      2-Year STORM
      ********
      STORM
2
                1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
    743.000
                Coefficient a
```

```
6.000
                Constant b
                               (min)
        .798
                Exponent c
       .400
                Fraction to peak r
    180.000
                Duration ó 1500 min
               34.438 mm
                             Total depth
3
      IMPERVIOUS
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .013
                SCS Curve No or C
     98.000
                Ia/S Coefficient
       .100
      2.000
                Initial Abstraction
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
     3
           line(s) of comment
      *****************************
      Catchment 101 - Existing to Gordon
      *********
4
      CATCHMENT
     101.000
                ID No.ó 99999
      1.330
                Area in hectares
                Length (PERV) metres
     110.000
                Gradient (%)
      2.500
                Per cent Impervious
     10.000
                Length (IMPERV)
     70.000
        .000
                %Imp. with Zero Dpth
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
                Manning "n"
       .250
     67.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .027
                        .000
                                   .000
                                              .000 c.m/s
             .163
                        .799
                                   .226
                                           C perv/imperv/total
15
      ADD RUNOFF
                                              .000 c.m/s
             .027
                        .027
                                   .000
14
      START
     1
           1=Zero; 2=Define
35
      COMMENT
     3
           line(s) of comment
      Catchment 102 - Existing to Torrence
      CATCHMENT
4
     102.000
                ID No.ó 99999
      1.720
                Area in hectares
                Length (PERV) metres
     150.000
      5.000
                Gradient (%)
      1.000
                Per cent Impervious
      1.000
                Length (IMPERV)
```

```
.000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
        .250
                Manning "n"
                SCS Curve No or C
     67.000
                Ia/S Coefficient
        .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
           1
                        .000
                                   .000
                                              .000 c.m/s
              .015
                        .698
              .163
                                   .168
                                            C perv/imperv/total
15
      ADD RUNOFF
                        .015
                                   .000
                                              .000 c.m/s
              .015
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
      7
            line(s) of comment
       *******
      5-Year STORM
       ******
2
      STORM
                1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
                Coefficient a
    1593.000
     11.000
                Constant b
                               (min)
        .879
                Exponent c
        .400
                Fraction to peak r
     180.000
                Duration ó 1500 min
               47.240 mm
                             Total depth
3
      IMPERVIOUS
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
        .013
     98.000
                SCS Curve No or C
        .100
                Ia/S Coefficient
                Initial Abstraction
      2.000
      START
14
      1
            1=Zero; 2=Define
35
      COMMENT
      3
           line(s) of comment
       *****************************
      Catchment 101 - Existing to Gordon
       CATCHMENT
4
     101.000
                ID No.ó 99999
      1.330
                Area in hectares
     110.000
                Length (PERV) metres
      2.500
                Gradient (%)
     10.000
                Per cent Impervious
     70.000
                Length (IMPERV)
```

```
.000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
        .250
                Manning "n"
                SCS Curve No or C
     67.000
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .000
                                   .000
                                             .000 c.m/s
             .040
                        .841
             .226
                                   .287
                                           C perv/imperv/total
15
      ADD RUNOFF
             .040
                        .040
                                  .000
                                             .000 c.m/s
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
     3
           line(s) of comment
      Catchment 102 - Existing to Torrence
      *********
4
      CATCHMENT
    102.000
                ID No.ó 99999
      1.720
                Area in hectares
    150.000
                Length (PERV) metres
                Gradient (%)
      5.000
                Per cent Impervious
      1.000
                Length (IMPERV)
      1.000
                %Imp. with Zero Dpth
        .000
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
                Manning "n"
       .250
     67.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .038
                        .000
                                  .000
                                             .000 c.m/s
             .226
                        .739
                                   .231
                                           C perv/imperv/total
15
      ADD RUNOFF
                                             .000 c.m/s
             .038
                        .038
                                   .000
      START
14
     1
           1=Zero; 2=Define
35
      COMMENT
           line(s) of comment
     7
      ******
      100-Year STORM
      ********
2
      STORM
                1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
   4688.000
                Coefficient a
```

```
17.000
                Constant b
                               (min)
        .925
                Exponent c
        .400
                Fraction to peak r
     180.000
                Duration ó 1500 min
                             Total depth
              106.103 mm
3
      IMPERVIOUS
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .013
                SCS Curve No or C
     98.000
                Ia/S Coefficient
       .100
      2.000
                Initial Abstraction
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
      3
           line(s) of comment
      ******************************
      Catchment 101 - Existing to Gordon
      *********
4
      CATCHMENT
     101.000
                ID No.ó 99999
      1.330
                Area in hectares
                Length (PERV) metres
     110.000
                Gradient (%)
      2.500
                Per cent Impervious
     10.000
                Length (IMPERV)
     70.000
        .000
                %Imp. with Zero Dpth
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
                Manning "n"
       .250
      67.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .191
                        .000
                                   .000
                                              .000 c.m/s
                        .920
             .426
                                   .475
                                           C perv/imperv/total
15
      ADD RUNOFF
                                              .000 c.m/s
             .191
                        .191
                                   .000
14
      START
     1
           1=Zero; 2=Define
35
      COMMENT
      3
           line(s) of comment
      Catchment 102 - Existing to Torrence
      CATCHMENT
4
     102.000
                ID No.ó 99999
      1.720
                Area in hectares
                Length (PERV) metres
     150.000
      5.000
                Gradient (%)
      1.000
                Per cent Impervious
      1.000
                Length (IMPERV)
```

	.000	%Imp	. with Zero	Dpth		
	1	Opti	on 1=SCS CN/	C; 2=Horto	on; 3=Green-Ampt;	4=Repeat
	.250	Mann	ing "n"			
	67.000	SCS	Curve No or	С		
	.100	Ia/S	Coefficient	2		
	5.000	Init	ial Abstract	ion		
	1	Opti	on 1=Triang]	lr; 2=Recta	anglr; 3=SWM HYD;	4=Lin. Reserv
		.251	.000	.000	.000 c.m/s	
		.425	.808	.429	C perv/imperv/t	otal
15	ADD RUN	IOFF				
		.251	.251	.000	.000 c.m/s	
20	MANUAL					

```
Output File (4.7) GOR.out
                                   opened 2022-06-06 21:05
      Units used are defined by G =
                                     9.810
         300
              600
                      5.000
                                  are MAXDT MAXHYD & DTMIN values
      Licensee: Paragon Engineering Limited
35
      COMMENT
     5
           line(s) of comment
      1242-1260 Gordon Street and 9 Valley - 1614-13684
      Stormwater Management Modelling
      May 2022 - D. Williams
      START
14
     1
           1=Zero; 2=Define
35
      COMMENT
     7
           line(s) of comment
      *******
      25-mm STORM
      ******
2
      STORM
               1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
    509.000
               Coefficient a
      6.000
               Constant b
                             (min)
       .799
               Exponent c
       .400
               Fraction to peak r
    240.000
               Duration ó 1500 min
              25.028 mm
                           Total depth
3
      IMPERVIOUS
               Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
               Manning "n"
       .013
     98.000
               SCS Curve No or C
       .100
               Ia/S Coefficient
               Initial Abstraction
      2.000
      START
14
     1
           1=Zero; 2=Define
35
      COMMENT
           line(s) of comment
     3
      ******************************
      Catchment 202 - RFTOP
      ******
4
      CATCHMENT
    202.000
               ID No.ó 99999
       .240
               Area in hectares
               Length (PERV) metres
      1.000
       .500
               Gradient (%)
     99.000
               Per cent Impervious
     15.000
               Length (IMPERV)
```

.000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" SCS Curve No or C 68.000 Ia/S Coefficient .100 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .000 .000 c.m/s .031 .740 .114 .733 C perv/imperv/total 15 ADD RUNOFF .031 .031 .000 .000 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\* West Building - Rooftop Control \*\*\*\*\*\*\*\*\* 10 POND 6 Depth - Discharge - Volume sets .000 .000 .0 .023 .00540 55.2 .031 .00660 74.4 .045 .00820 108.0 .061 .0101 146.4 .063 .0499 150.0 Peak Outflow .003 c.m/s = Maximum Depth = .012 metres Maximum Storage = 28. c.m .031 .031 .003 .000 c.m/s 16 NEXT LINK .003 .003 .000 c.m/s .031 COMBINE 17 500 Junction Node No. .031 .003 .003 .003 c.m/s 14 START 1=Zero; 2=Define 1 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\* Catchment 209 - Min to Storage - Maj Uncontrolled \* 4 CATCHMENT 209.000 ID No.ó 99999 .120 Area in hectares Length (PERV) metres 5.000 Gradient (%) 2.000 Per cent Impervious 99.000 10.000 Length (IMPERV) .000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250

```
68.000
                 SCS Curve No or C
                 Ia/S Coefficient
        .100
       5.000
                 Initial Abstraction
                 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
           1
                         .000
                                    .003
                                                .003 c.m/s
              .018
              .115
                         .736
                                    .729
                                             C perv/imperv/total
15
       ADD RUNOFF
                                                .003 c.m/s
              .018
                         .018
                                    .003
       DIVERT
12
                 U/S Node No.ó 99999
           1
                 Threshold Discharge
        .038
        .038
                 Max. Outflow reqd.
            Omax & Vol.Diverted =
                                       .000 c.m/s
                                                            .0 c.m
            No flow diverted
              .018
                         .018
                                    .018
                                                .003 c.m/s
16
       NEXT LINK
              .018
                         .018
                                    .018
                                                .003 c.m/s
35
       COMMENT
      3
            line(s) of comment
       *******
       Catchment 204
       ********
 4
       CATCHMENT
                 ID No.ó 99999
     204.000
        .510
                 Area in hectares
       4.000
                 Length (PERV) metres
       2.000
                 Gradient (%)
                 Per cent Impervious
      90.000
      10.000
                 Length (IMPERV)
        .000
                 %Imp. with Zero Dpth
                 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
           1
        .250
                 Manning "n"
      68.000
                 SCS Curve No or C
        .100
                 Ia/S Coefficient
       5.000
                 Initial Abstraction
                 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
           1
                         .018
                                                .003 c.m/s
              .068
                                    .018
                         .736
                                     .674
                                             C perv/imperv/total
              .115
15
       ADD RUNOFF
              .068
                         .085
                                    .018
                                                .003 c.m/s
 9
       ROUTE
        .000
                 Conduit Length
                 No Conduit defined
        .000
                 Zero lag
        .000
                 Beta weighting factor
        .000
                 Routing timestep
        .000
                 No. of sub-reaches
           Ø
              .068
                         .085
                                                .003 c.m/s
                                    .085
17
       COMBINE
    500
            Junction Node No.
```

.068 .085 .085 .086 c.m/s 18 CONFLUENCE 500 Junction Node No. .068 .086 .085 .000 c.m/s 35 COMMENT line(s) of comment 3 Infiltration Chamber 10 POND 4 Depth - Discharge - Volume sets .000 .000 .0 .178 .00180 .1 .00190 .711 116.2 .712 .400 117.0 Peak Outflow .002 c.m/s = Maximum Depth = .685 metres Maximum Storage = 111. c.m .068 .086 .002 .000 c.m/s 16 NEXT LINK .068 .002 .002 .000 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\* Catchment 207 \*\*\*\*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 207.000 .150 Area in hectares 75.000 Length (PERV) metres Gradient (%) 3.000 50.000 Per cent Impervious 35.000 Length (IMPERV) .000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 68.000 SCS Curve No or C Ia/S Coefficient .100 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .010 .002 .002 .000 c.m/s .115 .740 .427 C perv/imperv/total 15 ADD RUNOFF .000 c.m/s .010 .012 .002 35 COMMENT 3 line(s) of comment Storage 10 POND

9 Depth - Discharge - Volume sets .000 .000 .0 .190 .00470 .1 .00750 .420 49.4 .880 .0111 250.9 1.380 .0141 441.7 1.560 .0150 486.9 1.870 .0164 552.8 2.380 .0204 553.0 2.390 .200 553.1 Peak Outflow .005 c.m/s = Maximum Depth .209 metres = Maximum Storage = 4. c.m .010 .012 .005 .000 c.m/s 17 COMBINE 500 Junction Node No. .010 .012 .005 .005 c.m/s 22 FILE HYDROGRAPH 1 1=READ: 2=WRITE 1 is Filename D 3 1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary .010 .012 .000 .005 c.m/s 17 COMBINE 500 Junction Node No. .010 .012 .000 .005 c.m/s START 14 1 1=Zero; 2=Define 35 COMMENT 3 line(s) of comment Uncontrolled Flow to Gordon Street 4 CATCHMENT 201.000 ID No.ó 99999 .110 Area in hectares 6.000 Length (PERV) metres 2.000 Gradient (%) Per cent Impervious 70.000 6.000 Length (IMPERV) .000 %Imp. with Zero Dpth 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat Manning "n" .250 68.000 SCS Curve No or C Ia/S Coefficient .100 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .012 .000 .005 c.m/s .115 .722 .540 C perv/imperv/total 15 ADD RUNOFF .012 .012 .000 .005 c.m/s

```
35
      COMMENT
          line(s) of comment
     3
      ************
      Uncontrolled Flow to Gordon Street
      ******
4
      CATCHMENT
               ID No.ó 99999
    208.000
               Area in hectares
       .050
               Length (PERV) metres
     35.000
     25.000
               Gradient (%)
               Per cent Impervious
     70.000
               Length (IMPERV)
      6.000
       .000
               %Imp. with Zero Dpth
               Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
         1
               Manning "n"
       .250
     68.000
               SCS Curve No or C
               Ia/S Coefficient
       .100
      5.000
               Initial Abstraction
               Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
            .005
                      .012
                                .000
                                          .005 c.m/s
                      .675
            .115
                                .507
                                        C perv/imperv/total
15
      ADD RUNOFF
            .005
                      .017
                                .000
                                          .005 c.m/s
9
      ROUTE
               Conduit Length
       .000
               No Conduit defined
       .000
       .000
               Zero lag
               Beta weighting factor
       .000
       .000
               Routing timestep
               No. of sub-reaches
         0
                      .017
                                .017
                                          .005 c.m/s
            .005
35
      COMMENT
          line(s) of comment
     3
      TOTAL FLOW TO GORDON
      17
      COMBINE
   500
          Junction Node No.
            .005
                      .017
                                .017
                                          .022 c.m/s
18
      CONFLUENCE
   500
          Junction Node No.
                                .017
            .005
                      .022
                                          .000 c.m/s
14
      START
     1
          1=Zero; 2=Define
35
      COMMENT
     3
          line(s) of comment
      Catchment 203 - RFTOP
      ******
4
      CATCHMENT
```

```
ID No.ó 99999
    203.000
       .240
                Area in hectares
      1.000
                Length (PERV) metres
                Gradient (%)
       .500
     99.000
                Per cent Impervious
     15.000
                Length (IMPERV)
                %Imp. with Zero Dpth
       .000
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .250
     68.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .031
                        .000
                                  .017
                                            .000 c.m/s
                        .740
                                  .733
                                          C perv/imperv/total
             .114
15
      ADD RUNOFF
             .031
                        .031
                                  .017
                                             .000 c.m/s
35
      COMMENT
     3
           line(s) of comment
      ********
      East Building - Rooftop Control
      10
      POND
     6 Depth - Discharge - Volume sets
         .000
                     .000
                                  .0
         .023
                   .00540
                                55.2
         .031
                   .00660
                                74.4
         .045
                   .00820
                               108.0
         .061
                    .0101
                               146.4
         .063
                    .0499
                               150.0
      Peak Outflow
                            .003 c.m/s
                     =
                            .012 metres
      Maximum Depth
                     =
      Maximum Storage =
                             28. c.m
             .031
                        .031
                                  .003
                                             .000 c.m/s
16
      NEXT LINK
                                             .000 c.m/s
             .031
                        .003
                                  .003
35
      COMMENT
     3
           line(s) of comment
      EAST LID
      **********
10
      POND
     3 Depth - Discharge - Volume sets
                     .000
         .000
                                  .0
                  .000700
                                30.0
        1.000
                    .0500
                                31.0
        1.001
      Peak Outflow
                     =
                            .001 c.m/s
      Maximum Depth
                     =
                            .929 metres
      Maximum Storage =
                             28. c.m
             .031
                        .003
                                  .001
                                             .000 c.m/s
```

```
16
      NEXT LINK
                        .001
                                   .001
                                              .000 c.m/s
              .031
35
      COMMENT
           line(s) of comment
      3
       ***********
      Catchment 206 - Uncontrolled To Torrence
       ******
4
      CATCHMENT
                ID No.ó 99999
    206.000
      1.410
                Area in hectares
     120.000
                Length (PERV) metres
                Gradient (%)
      5.000
      1.000
                Per cent Impervious
      5.000
                Length (IMPERV)
        .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
        .250
     68.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
              .005
                        .001
                                   .001
                                              .000 c.m/s
                        .700
                                            C perv/imperv/total
              .115
                                   .121
15
      ADD RUNOFF
              .005
                        .005
                                   .001
                                              .000 c.m/s
      COMMENT
35
     3
           line(s) of comment
       ********
      Catchment 205 - Park Block - Uncontrolled to Torrence
       ********
4
      CATCHMENT
                ID No.ó 99999
     205.000
                Area in hectares
       .230
     50.000
                Length (PERV) metres
      2.000
                Gradient (%)
                Per cent Impervious
      10.000
                Length (IMPERV)
      5.000
                %Imp. with Zero Dpth
        .000
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
        .250
                Manning "n"
      68.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .005
                                   .001
                                              .000 c.m/s
              .004
                        .716
                                            C perv/imperv/total
              .115
                                   .175
15
      ADD RUNOFF
              .004
                        .006
                                   .001
                                              .000 c.m/s
14
      START
           1=Zero; 2=Define
      1
```

```
35
      COMMENT
           line(s) of comment
     7
      ********
      2 Year STORM
      ******
2
      STORM
                1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
          1
    743.000
                Coefficient a
      6.000
                Constant b
                               (min)
       .798
                Exponent c
       .400
                Fraction to peak r
     180.000
                Duration ó 1500 min
               34.438 mm
                             Total depth
3
      IMPERVIOUS
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
        .013
                Manning "n"
     98.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      2.000
                Initial Abstraction
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
     3
           line(s) of comment
      *******
      Catchment 202 - RFTOP
      *******
4
      CATCHMENT
                ID No.ó 99999
     202.000
       .240
                Area in hectares
      1.000
                Length (PERV) metres
                Gradient (%)
       .500
                Per cent Impervious
     99.000
     15.000
                Length (IMPERV)
                %Imp. with Zero Dpth
        .000
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
        .250
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .000
                                   .000
                                              .000 c.m/s
             .051
                        .801
                                   .794
                                           C perv/imperv/total
             .168
15
      ADD RUNOFF
             .051
                        .051
                                   .001
                                              .000 c.m/s
35
      COMMENT
     3
           line(s) of comment
```

```
*********
      West Building - Rooftop Control
      ******
10
      POND
     6 Depth - Discharge - Volume sets
          .000
                     .000
                                   .0
          .023
                   .00540
                                 55.2
          .031
                   .00660
                                 74.4
          .045
                   .00820
                                108.0
         .061
                    .0101
                                146.4
          .063
                    .0499
                                150.0
      Peak Outflow
                      =
                             .004 c.m/s
      Maximum Depth
                             .019 metres
                      =
      Maximum Storage =
                              45. c.m
             .051
                        .051
                                   .004
                                              .000 c.m/s
16
      NEXT LINK
             .051
                        .004
                                   .004
                                              .000 c.m/s
17
      COMBINE
    500
           Junction Node No.
             .051
                        .004
                                   .004
                                              .004 c.m/s
14
      START
     1
           1=Zero; 2=Define
      COMMENT
35
     3
           line(s) of comment
      *********
      Catchment 209 - Min to Storage - Maj Uncontrolled
      ******
4
      CATCHMENT
     209.000
                ID No.ó 99999
       .120
                Area in hectares
      5.000
                Length (PERV) metres
      2.000
                Gradient (%)
     99.000
                Per cent Impervious
     10.000
                Length (IMPERV)
       .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .250
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
          1
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
                        .000
                                   .004
                                              .004 c.m/s
             .028
                        .787
             .168
                                   .781
                                           C perv/imperv/total
15
      ADD RUNOFF
             .028
                        .028
                                   .004
                                              .004 c.m/s
12
      DIVERT
                U/S Node No.ó 99999
          1
       .038
                Threshold Discharge
       .038
                Max. Outflow read.
           Qmax & Vol.Diverted =
                                      .000 c.m/s
                                                         .0 c.m
```

No flow diverted .028 .028 .028 .004 c.m/s 16 NEXT LINK .028 .028 .028 .004 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\* Catchment 204 \*\*\*\*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 204.000 .510 Area in hectares 4.000 Length (PERV) metres Gradient (%) 2.000 Per cent Impervious 90.000 10.000 Length (IMPERV) %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 68.000 SCS Curve No or C .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .108 .028 .028 .004 c.m/s .168 .787 .725 C perv/imperv/total 15 ADD RUNOFF .108 .136 .028 .004 c.m/s 9 ROUTE .000 Conduit Length No Conduit defined .000 .000 Zero lag .000 Beta weighting factor Routing timestep .000 0 No. of sub-reaches .108 .136 .136 .004 c.m/s 17 COMBINE Junction Node No. 500 .108 .136 .136 .137 c.m/s 18 CONFLUENCE 500 Junction Node No. .108 .136 .137 .000 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\* Infiltration Chamber \*\*\*\*\*\*\*\* 10 POND 4 Depth - Discharge - Volume sets .000 .000 .0 .178 .00180 .1

.711 .00190 116.2 .712 .400 117.0 Peak Outflow .022 c.m/s = Maximum Depth .711 metres = Maximum Storage = 116. c.m .108 .137 .022 .000 c.m/s 16 NEXT LINK .022 .000 c.m/s .108 .022 COMMENT 35 3 line(s) of comment \*\*\*\*\*\*\*\*\* Catchment 207 \*\*\*\*\*\* 4 CATCHMENT 207.000 ID No.ó 99999 .150 Area in hectares Length (PERV) metres 75.000 3.000 Gradient (%) Per cent Impervious 50.000 35.000 Length (IMPERV) %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 68.000 SCS Curve No or C Ia/S Coefficient .100 5.000 Initial Abstraction 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv .016 .022 .022 .000 c.m/s .169 .801 .485 C perv/imperv/total 15 ADD RUNOFF .025 .022 .000 c.m/s .016 35 COMMENT line(s) of comment 3 Storage \*\*\*\*\*\* 10 POND 9 Depth - Discharge - Volume sets .000 .000 .0 .190 .00470 .1 .420 .00750 49.4 250.9 .880 .0111 1.380 .0141 441.7 .0150 1.560 486.9 1.870 .0164 552.8 .0204 2.380 553.0 2.390 .200 553.1 Peak Outflow = .007 c.m/s Maximum Depth .396 metres = Maximum Storage = 44. c.m

.016 .025 .007 .000 c.m/s 17 COMBINE 500 Junction Node No. .016 .025 .007 .007 c.m/s 22 FILE HYDROGRAPH 1 1=READ: 2=WRITE is Filename 1 D 1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary 3 .000 .016 .025 .007 c.m/s 17 COMBINE 500 Junction Node No. .016 .025 .000 .007 c.m/s 14 START 1 1=Zero; 2=Define 35 COMMENT line(s) of comment 3 Uncontrolled Flow to Gordon Street \*\*\*\*\*\*\*\*\*\*\* 4 CATCHMENT 201.000 ID No.ó 99999 .110 Area in hectares Length (PERV) metres 6.000 2.000 Gradient (%) Per cent Impervious 70.000 6.000 Length (IMPERV) .000 %Imp. with Zero Dpth 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat .250 Manning "n" SCS Curve No or C 68.000 .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .019 .000 .007 c.m/s .168 .770 .590 C perv/imperv/total 15 ADD RUNOFF .019 .019 .000 .007 c.m/s 35 COMMENT line(s) of comment 3 Uncontrolled Flow to Gordon Street \*\*\*\*\*\* 4 CATCHMENT 208.000 ID No.ó 99999 Area in hectares .050 Length (PERV) metres 35.000 25.000 Gradient (%) Per cent Impervious 70.000 6.000 Length (IMPERV) .000 %Imp. with Zero Dpth

Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 68.000 SCS Curve No or C .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .019 .000 .008 .007 c.m/s .715 .551 C perv/imperv/total .168 15 ADD RUNOFF .027 .008 .000 .007 c.m/s 9 ROUTE Conduit Length .000 .000 No Conduit defined .000 Zero lag Beta weighting factor .000 Routing timestep .000 No. of sub-reaches 0 .008 .027 .027 .007 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\* TOTAL FLOW TO GORDON 17 COMBINE 500 Junction Node No. .008 .027 .027 .032 c.m/s 18 CONFLUENCE 500 Junction Node No. .008 .032 .027 .000 c.m/s 14 START 1=Zero; 2=Define 1 35 COMMENT 3 line(s) of comment Catchment 203 - RFTOP \*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 203.000 .240 Area in hectares 1.000 Length (PERV) metres .500 Gradient (%) 99.000 Per cent Impervious 15.000 Length (IMPERV) %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 68.000 SCS Curve No or C .100 Ia/S Coefficient 5.000 Initial Abstraction 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv

.051 .000 .027 .000 c.m/s .168 .794 C perv/imperv/total .801 15 ADD RUNOFF .051 .051 .027 .000 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\*\*\* East Building - Rooftop Control \*\*\*\*\*\*\*\*\* 10 POND 6 Depth - Discharge - Volume sets .000 .000 .0 .023 .00540 55.2 .031 74.4 .00660 .045 .00820 108.0 .061 .0101 146.4 .0499 .063 150.0 Peak Outflow .004 c.m/s = .019 metres Maximum Depth = Maximum Storage = 45. c.m .051 .051 .004 .000 c.m/s 16 NEXT LINK .051 .004 .004 .000 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\* EAST LID \*\*\*\*\*\* 10 POND 3 Depth - Discharge - Volume sets .000 .000 .0 1.000 .000700 30.0 1.001 .0500 31.0 Peak Outflow .003 c.m/s = Maximum Depth 1.000 metres = Maximum Storage = 30. c.m .051 .004 .003 .000 c.m/s 16 NEXT LINK .003 .003 .000 c.m/s .051 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\* Catchment 206 - Uncontrolled To Torrence \*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 206.000 1.410 Area in hectares 120.000 Length (PERV) metres 5.000 Gradient (%) Per cent Impervious 1.000

```
5.000
                Length (IMPERV)
        .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
        .250
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .014
                        .003
                                  .003
                                             .000 c.m/s
                        .738
                                   .175
                                           C perv/imperv/total
             .169
15
      ADD RUNOFF
             .014
                        .015
                                  .003
                                             .000 c.m/s
35
      COMMENT
     3
           line(s) of comment
      Catchment 205 - Park Block - Uncontrolled to Torrence
      *********
4
      CATCHMENT
                ID No.ó 99999
    205.000
       .230
                Area in hectares
     50.000
                Length (PERV) metres
      2.000
                Gradient (%)
                Per cent Impervious
     10.000
                Length (IMPERV)
      5.000
       .000
                %Imp. with Zero Dpth
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
       .250
                Manning "n"
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .015
                                  .003
             .006
                                             .000 c.m/s
             .169
                        .763
                                   .228
                                           C perv/imperv/total
15
      ADD RUNOFF
                        .017
                                  .003
                                             .000 c.m/s
             .006
14
      START
     1
           1=Zero; 2=Define
      COMMENT
35
           line(s) of comment
     7
      *******
      5 Year STORM
      *****
2
      STORM
          1
                1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
   1593.000
                Coefficient a
     11.000
                Constant b
                               (min)
```

```
.879
                Exponent c
       .400
                Fraction to peak r
     240.000
                Duration ó 1500 min
               49.540 mm
                             Total depth
3
      IMPERVIOUS
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .013
     98.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      2.000
                Initial Abstraction
14
      START
     1
           1=Zero; 2=Define
35
      COMMENT
      3
           line(s) of comment
      ************************
      Catchment 202 - RFTOP
      *********
4
      CATCHMENT
                ID No.ó 99999
     202.000
       .240
                Area in hectares
      1.000
                Length (PERV) metres
        .500
                Gradient (%)
                Per cent Impervious
     99.000
                Length (IMPERV)
     15.000
        .000
                %Imp. with Zero Dpth
          1
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
        .250
                Manning "n"
      68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                        .000
                                              .000 c.m/s
             .072
                                   .003
             .239
                        .854
                                   .847
                                           C perv/imperv/total
15
      ADD RUNOFF
                        .072
                                   .003
                                              .000 c.m/s
             .072
35
      COMMENT
      3
           line(s) of comment
      West Building - Rooftop Control
      **********
10
      POND
      6 Depth - Discharge - Volume sets
                                   .0
          .000
                     .000
          .023
                   .00540
                                 55.2
          .031
                   .00660
                                 74.4
          .045
                   .00820
                                108.0
          .061
                    .0101
                                146.4
                    .0499
          .063
                                150.0
      Peak Outflow
                             .006 c.m/s
                      =
      Maximum Depth
                      =
                             .029 metres
```

Maximum Storage = 69. c.m .072 .000 c.m/s .072 .006 16 NEXT LINK .072 .006 .006 .000 c.m/s 17 COMBINE 500 Junction Node No. .006 .006 c.m/s .072 .006 START 14 1=Zero; 2=Define 1 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\* Catchment 209 - Min to Storage - Maj Uncontrolled \*\*\*\*\* 4 CATCHMENT ID No.ó 99999 209.000 Area in hectares .120 5.000 Length (PERV) metres Gradient (%) 2.000 99.000 Per cent Impervious 10.000 Length (IMPERV) %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" 68.000 SCS Curve No or C Ia/S Coefficient .100 5.000 Initial Abstraction 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv .038 .000 .006 .006 c.m/s .833 .828 C perv/imperv/total .242 15 ADD RUNOFF .038 .006 .038 .006 c.m/s 12 DIVERT U/S Node No.ó 99999 1 .038 Threshold Discharge Max. Outflow reqd. .038 Qmax & Vol.Diverted = .000 c.m/s .0 c.m Majors From 209 .038 .038 .038 .006 c.m/s 16 NEXT LINK .038 .038 .038 .006 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\* Catchment 204 \*\*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 204.000 .510 Area in hectares 4.000 Length (PERV) metres

2.000 Gradient (%) Per cent Impervious 90.000 10.000 Length (IMPERV) %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" 68.000 SCS Curve No or C .100 Ia/S Coefficient Initial Abstraction 5.000 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .149 .038 .038 .006 c.m/s .774 .833 C perv/imperv/total .242 15 ADD RUNOFF .149 .187 .038 .006 c.m/s 9 ROUTE .000 Conduit Length No Conduit defined .000 .000 Zero lag Beta weighting factor .000 .000 Routing timestep No. of sub-reaches 0 .149 .187 .187 .006 c.m/s COMBINE 17 500 Junction Node No. .149 .187 .187 .190 c.m/s CONFLUENCE 18 500 Junction Node No. .149 .190 .187 .000 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\*\* Infiltration Chamber \*\*\*\*\* 10 POND 4 Depth - Discharge - Volume sets .000 .000 .0 .178 .00180 .1 116.2 .711 .00190 .712 .400 117.0 Peak Outflow .121 c.m/s = .711 metres Maximum Depth = Maximum Storage = 116. c.m .149 .190 .121 .000 c.m/s 16 NEXT LINK .121 .149 .121 .000 c.m/s 35 COMMENT 3 line(s) of comment \* Catchment 207 \*\*\*\*\*\*

```
4
      CATCHMENT
                ID No.ó 99999
     207.000
        .150
                 Area in hectares
                 Length (PERV) metres
      75.000
      3.000
                 Gradient (%)
      50.000
                 Per cent Impervious
      35.000
                 Length (IMPERV)
                %Imp. with Zero Dpth
        .000
                 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
           1
        .250
                 Manning "n"
                SCS Curve No or C
      68.000
        .100
                 Ia/S Coefficient
       5.000
                 Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
           1
              .023
                         .121
                                    .121
                                               .000 c.m/s
                         .854
                                    .549
                                            C perv/imperv/total
              .244
15
       ADD RUNOFF
                         .140
                                    .121
                                               .000 c.m/s
              .023
35
      COMMENT
            line(s) of comment
      3
       **********
       Storage
       10
       POND
      9 Depth - Discharge - Volume sets
          .000
                      .000
                                    .0
          .190
                    .00470
                                    .1
                    .00750
                                 49.4
          .420
          .880
                     .0111
                                 250.9
                     .0141
                                441.7
         1.380
         1.560
                     .0150
                                486.9
                     .0164
         1.870
                                552.8
         2.380
                     .0204
                                553.0
                      .200
         2.390
                                553.1
       Peak Outflow
                      =
                              .009 c.m/s
      Maximum Depth
                      =
                              .651 metres
      Maximum Storage =
                             150. c.m
              .023
                         .140
                                    .009
                                               .000 c.m/s
17
       COMBINE
    500
            Junction Node No.
                         .140
              .023
                                    .009
                                               .009 c.m/s
22
       FILE HYDROGRAPH
            1=READ: 2=WRITE
      1
                                 is Filename
      1
           D
            1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary
      3
              .023
                         .140
                                    .000
                                               .009 c.m/s
17
      COMBINE
            Junction Node No.
    500
              .023
                     .140
                                   .000
                                              .009 c.m/s
14
       START
```

```
1=Zero; 2=Define
     1
35
      COMMENT
           line(s) of comment
     3
      Uncontrolled Flow to Gordon Street
      ******
      CATCHMENT
4
    201.000
                ID No.ó 99999
       .110
                Area in hectares
                Length (PERV) metres
      6.000
      2.000
                Gradient (%)
                Per cent Impervious
     70.000
      6.000
                Length (IMPERV)
       .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
               Manning "n"
       .250
                SCS Curve No or C
     68.000
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .025
                       .000
                                  .000
                                            .009 c.m/s
             .243
                       .810
                                  .639
                                          C perv/imperv/total
15
      ADD RUNOFF
                       .025
                                  .000
                                            .009 c.m/s
             .025
35
      COMMENT
           line(s) of comment
     3
      Uncontrolled Flow to Gordon Street
      CATCHMENT
4
                ID No.ó 99999
    208.000
       .050
                Area in hectares
     35.000
                Length (PERV) metres
     25.000
                Gradient (%)
     70.000
                Per cent Impervious
      6.000
                Length (IMPERV)
                %Imp. with Zero Dpth
       .000
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
       .250
               Manning "n"
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
          1
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
                       .025
                                  .000
                                            .009 c.m/s
             .011
                       .756
             .243
                                          C perv/imperv/total
                                  .602
15
      ADD RUNOFF
                                  .000
             .011
                       .036
                                            .009 c.m/s
9
      ROUTE
       .000
                Conduit Length
       .000
                No Conduit defined
```

.000 Zero lag Beta weighting factor .000 .000 Routing timestep No. of sub-reaches 0 .011 .036 .036 .009 c.m/s 35 COMMENT line(s) of comment 3 TOTAL FLOW TO GORDON 17 COMBINE 500 Junction Node No. .011 .036 .036 .041 c.m/s 18 CONFLUENCE 500 Junction Node No. .011 .041 .036 .000 c.m/s 14 START 1=Zero; 2=Define 1 35 COMMENT line(s) of comment 3 \* Catchment 203 - RFTOP \*\*\*\*\*\*\* 4 CATCHMENT 203.000 ID No.ó 99999 .240 Area in hectares 1.000 Length (PERV) metres Gradient (%) .500 Per cent Impervious 99.000 Length (IMPERV) 15.000 %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 SCS Curve No or C 68,000 .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .036 .000 c.m/s .072 .239 .854 .847 C perv/imperv/total 15 ADD RUNOFF .072 .072 .036 .000 c.m/s 35 COMMENT 3 line(s) of comment East Building - Rooftop Control 10 POND 6 Depth - Discharge - Volume sets .000 .000 .0 55.2 .023 .00540

.031 .00660 74.4 .045 .00820 108.0 .061 .0101 146.4 .0499 .063 150.0 Peak Outflow .006 c.m/s = Maximum Depth = .029 metres Maximum Storage = 69. c.m .072 .072 .000 c.m/s .006 16 NEXT LINK .006 .006 .000 c.m/s .072 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\* EAST LID \*\*\*\*\*\*\*\*\*\* POND 10 3 Depth - Discharge - Volume sets .000 .000 .0 1.000 .000700 30.0 1.001 .0500 31.0 Peak Outflow = .006 c.m/s Maximum Depth = 1.000 metres Maximum Storage = 30. c.m .072 .006 .006 .000 c.m/s 16 NEXT LINK .072 .006 .006 .000 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\* Catchment 206 - Uncontrolled To Torrence \*\*\*\*\*\*\* 4 CATCHMENT ID No.ó 99999 206.000 1.410 Area in hectares 120.000 Length (PERV) metres Gradient (%) 5.000 Per cent Impervious 1.000 Length (IMPERV) 5.000 .000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" 68.000 SCS Curve No or C Ia/S Coefficient .100 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .038 .006 .006 .000 c.m/s .244 .776 .249 C perv/imperv/total 15 ADD RUNOFF .039 .006 .000 c.m/s .038 35 COMMENT

```
3
            line(s) of comment
       *************************************
      Catchment 205 - Park Block - Uncontrolled to Torrence
       ******
      CATCHMENT
 4
     205.000
                 ID No.ó 99999
        .230
                Area in hectares
      50.000
                 Length (PERV) metres
                 Gradient (%)
       2.000
                 Per cent Impervious
      10.000
       5.000
                 Length (IMPERV)
        .000
                %Imp. with Zero Dpth
                 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
           1
                 Manning "n"
        .250
      68.000
                SCS Curve No or C
                 Ia/S Coefficient
        .100
       5.000
                 Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
           1
              .008
                         .039
                                    .006
                                               .000 c.m/s
              .244
                         .800
                                    .300
                                            C perv/imperv/total
15
      ADD RUNOFF
              .008
                         .046
                                    .006
                                               .000 c.m/s
      START
14
            1=Zero; 2=Define
      1
35
      COMMENT
            line(s) of comment
      7
       ******
        100 Year STORM
       ********
 2
       STORM
                 1=Chicago;2=Huff;3=User;4=Cdn1hr;5=Historic
           1
    4688.000
                 Coefficient a
      17.000
                 Constant b
                                (min)
        .925
                 Exponent c
        .400
                 Fraction to peak r
     180.000
                Duration ó 1500 min
               106.103 mm
                             Total depth
       IMPERVIOUS
 3
           1
                 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
                 Manning "n"
        .013
                 SCS Curve No or C
      98.000
                 Ia/S Coefficient
        .100
       2.000
                 Initial Abstraction
14
      START
            1=Zero; 2=Define
      1
35
       COMMENT
```

```
line(s) of comment
     3
      *******
      Catchment 202 - RFTOP
      *****
      CATCHMENT
4
    202.000
                ID No.ó 99999
       .240
                Area in hectares
      1.000
                Length (PERV) metres
                Gradient (%)
       .500
     99.000
                Per cent Impervious
     15.000
                Length (IMPERV)
       .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
                Manning "n"
       .250
     68.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .155
                        .000
                                  .006
                                             .000 c.m/s
             .429
                        .920
                                  .915
                                          C perv/imperv/total
15
      ADD RUNOFF
             .155
                        .155
                                  .006
                                             .000 c.m/s
35
      COMMENT
           line(s) of comment
     3
      West Building - Rooftop Control
      **********
10
      POND
     6 Depth - Discharge - Volume sets
         .000
                     .000
                                  .0
                                55.2
         .023
                   .00540
         .031
                                74.4
                   .00660
         .045
                               108.0
                   .00820
         .061
                    .0101
                               146.4
         .063
                    .0499
                               150.0
      Peak Outflow
                     =
                            .049 c.m/s
      Maximum Depth
                     =
                            .062 metres
      Maximum Storage =
                            150. c.m
             .155
                       .155
                                             .000 c.m/s
                                  .049
16
      NEXT LINK
             .155
                        .049
                                  .049
                                             .000 c.m/s
17
      COMBINE
   500
           Junction Node No.
             .155
                        .049
                                  .049
                                             .049 c.m/s
14
      START
           1=Zero; 2=Define
     1
35
      COMMENT
     3
           line(s) of comment
      *********
      Catchment 209 - Min to Storage - Maj Uncontrolled
```

\*\*\*\*\*\*\*\*\* 4 CATCHMENT 209.000 ID No.ó 99999 .120 Area in hectares Length (PERV) metres 5.000 2.000 Gradient (%) Per cent Impervious 99.000 Length (IMPERV) 10.000 %Imp. with Zero Dpth .000 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" SCS Curve No or C 68.000 .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .049 .049 c.m/s .077 .429 .876 C perv/imperv/total .872 15 ADD RUNOFF .077 .077 .049 .049 c.m/s 12 DIVERT U/S Node No.ó 99999 1 .038 Threshold Discharge Max. Outflow reqd. .038 Qmax & Vol.Diverted = .039 c.m/s 14.9 c.m Majors From 209 .077 .077 .038 .049 c.m/s 16 NEXT LINK .077 .038 .038 .049 c.m/s 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\* Catchment 204 \* 4 CATCHMENT ID No.ó 99999 204.000 .510 Area in hectares Length (PERV) metres 4.000 Gradient (%) 2.000 90.000 Per cent Impervious 10.000 Length (IMPERV) .000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 Manning "n" .250 SCS Curve No or C 68.000 .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .307 .038 .038 .049 c.m/s .427 .876 .831 C perv/imperv/total 15 ADD RUNOFF

	.3	307	.345	.038	.049	c.m/s
9	ROUTE					
	.000	Conduit	Length			
	.000	No Cond	uit defir	ned		
	.000	Zero la	•			
	.000		ighting f			
	.000	Routing	-			
	0	No. of	sub-reach			
		307	.345	.345	.049	c.m/s
17	COMBINE					
		tion Nod				,
10		307	.345	.345	.352	c.m/s
18	CONFLUEN		- NI-			
		tion Nod		245	000	
25		307	.352	.345	.000	c.m/s
35	COMMENT 3 line	e(s) of c	ommon+			
		**********		****		
	Infiltrat	ion Cham	her			
		********		*****		
10	POND					
	4 Depth -	Discharg	e - Volur	ne sets		
	.000	.0		.0		
	.178	.001	80	.1		
	.711	.001	90	116.2		
		.40		117.0		
	Peak Out					
	Maximum [					
	Maximum S	storage =	117	7. c.m		1
10		307	.352	.351	.000	c.m/s
16	NEXT LINK		251	.351	000	c.m/s
35	COMMENT	07			.000	C.III/ 5
رر		e(s) of c	omment			
		********		***		
	Catchment	207				
	******	*******	*******	***		
4	CATCHMENT	Г				
	207.000	ID No.ó	99999			
	.150	Area in	hectares	5		
	75.000	Length	(PERV) me	etres		
	3.000	Gradien	t (%)			
	50.000		t Impervi	ious		
	35.000		(IMPERV)			
	.000	•	ith Zero			
	1			/C; 2=Horton;	3=Gree	en-Ampt; 4=Repeat
	.250	Manning		<u> </u>		
	68.000		ve No or			
	.100 5.000		efficient Abstract			
	סשט. כ	INICIAL	AUSTRACI			

Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 c.m/s .051 .351 .351 .436 .919 .678 C perv/imperv/total 15 ADD RUNOFF .051 .402 .351 .000 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\*\*\*\* Storage 10 POND 9 Depth - Discharge - Volume sets .000 .000 .0 .1 .190 .00470 .00750 49.4 .420 .880 .0111 250.9 1.380 .0141 441.7 1.560 .0150 486.9 1.870 .0164 552.8 2.380 .0204 553.0 .200 2.390 553.1 Peak Outflow = .016 c.m/s Maximum Depth = 1.677 metres Maximum Storage = 512. c.m .051 .000 c.m/s .402 .016 COMBINE 17 500 Junction Node No. .051 .402 .016 .016 c.m/s 22 FILE HYDROGRAPH 1=READ: 2=WRITE 1 1 is Filename D 3 1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary .051 .402 .039 .016 c.m/s 17 COMBINE 500 Junction Node No. .051 .402 .039 .047 c.m/s START 14 1 1=Zero; 2=Define 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\* Uncontrolled Flow to Gordon Street CATCHMENT 4 201.000 ID No.ó 99999 .110 Area in hectares 6.000 Length (PERV) metres Gradient (%) 2.000 70.000 Per cent Impervious 6.000 Length (IMPERV)

```
.000
               %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
       .250
                Manning "n"
     68.000
                SCS Curve No or C
                Ia/S Coefficient
       .100
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
                       .000
                                  .039
                                            .047 c.m/s
             .055
                       .841
             .432
                                  .718
                                          C perv/imperv/total
      ADD RUNOFF
15
             .055
                       .055
                                  .039
                                            .047 c.m/s
35
      COMMENT
           line(s) of comment
     3
      Uncontrolled Flow to Gordon Street
      4
      CATCHMENT
    208.000
               ID No.ó 99999
       .050
                Area in hectares
     35.000
                Length (PERV) metres
     25.000
                Gradient (%)
                Per cent Impervious
     70.000
      6.000
                Length (IMPERV)
       .000
                %Imp. with Zero Dpth
                Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
          1
               Manning "n"
       .250
     68.000
                SCS Curve No or C
       .100
                Ia/S Coefficient
      5.000
                Initial Abstraction
                Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .024
                       .055
                                 .039
                                            .047 c.m/s
             .433
                       .803
                                  .692
                                          C perv/imperv/total
15
      ADD RUNOFF
             .024
                                 .039
                       .080
                                            .047 c.m/s
9
      ROUTE
                Conduit Length
       .000
                No Conduit defined
       .000
       .000
                Zero lag
       .000
                Beta weighting factor
       .000
                Routing timestep
          0
                No. of sub-reaches
             .024
                       .080
                                  .080
                                            .047 c.m/s
35
      COMMENT
           line(s) of comment
     3
      TOTAL FLOW TO GORDON
      *****
17
      COMBINE
   500
           Junction Node No.
             .024
                       .080
                                  .080
                                            .127 c.m/s
```

18 CONFLUENCE Junction Node No. 500 .024 .080 .000 c.m/s .127 START 14 1=Zero; 2=Define 1 35 COMMENT 3 line(s) of comment \*\*\*\*\*\*\*\*\*\* Catchment 203 - RFTOP \*\*\*\*\*\*\*\*\* 4 CATCHMENT 203.000 ID No.ó 99999 .240 Area in hectares 1.000 Length (PERV) metres .500 Gradient (%) Per cent Impervious 99.000 Length (IMPERV) 15.000 .000 %Imp. with Zero Dpth Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat 1 .250 Manning "n" 68.000 SCS Curve No or C .100 Ia/S Coefficient 5.000 Initial Abstraction Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv 1 .000 .080 .000 c.m/s .155 .920 .429 .915 C perv/imperv/total 15 ADD RUNOFF .155 .155 .080 .000 c.m/s 35 COMMENT line(s) of comment 3 East Building - Rooftop Control 10 POND 6 Depth - Discharge - Volume sets .000 .000 .0 .023 .00540 55.2 .031 .00660 74.4 .045 .00820 108.0 .061 .0101 146.4 .0499 .063 150.0 Peak Outflow = .049 c.m/s Maximum Depth = .062 metres Maximum Storage = 150. c.m .155 .155 .049 .000 c.m/s 16 NEXT LINK .049 .155 .049 .000 c.m/s 35 COMMENT line(s) of comment 3 \*\*\*\*\*\*\*\*\*\*

```
EAST LID
      10
      POND
     3 Depth - Discharge - Volume sets
         .000
                    .000
                                 .0
        1.000
                  .000700
                               30.0
        1.001
                   .0500
                               31.0
      Peak Outflow
                     =
                            .030 c.m/s
                           1.001 metres
      Maximum Depth
                     =
      Maximum Storage =
                            31. c.m
             .155
                       .049
                                 .030
                                            .000 c.m/s
16
      NEXT LINK
                       .030
                                 .030
                                            .000 c.m/s
             .155
35
      COMMENT
     3
           line(s) of comment
      ***********
      Catchment 206 - Uncontrolled To Torrence
      ******
      CATCHMENT
4
    206.000
               ID No.ó 99999
      1.410
               Area in hectares
    120.000
               Length (PERV) metres
               Gradient (%)
      5.000
               Per cent Impervious
      1.000
               Length (IMPERV)
      5.000
       .000
               %Imp. with Zero Dpth
          1
               Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
               Manning "n"
       .250
     68.000
               SCS Curve No or C
       .100
               Ia/S Coefficient
      5.000
               Initial Abstraction
               Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
          1
             .229
                       .030
                                 .030
                                            .000 c.m/s
                       .813
             .436
                                 .440
                                          C perv/imperv/total
15
      ADD RUNOFF
             .229
                                            .000 c.m/s
                       .245
                                 .030
35
      COMMENT
     3
           line(s) of comment
      Catchment 205 - Park Block - Uncontrolled to Torrence
      ******
      CATCHMENT
4
               ID No.ó 99999
    205.000
               Area in hectares
       .230
               Length (PERV) metres
     50.000
               Gradient (%)
      2.000
     10.000
               Per cent Impervious
      5.000
               Length (IMPERV)
       .000
               %Imp. with Zero Dpth
          1
               Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
```

	.250	Mannin	g "n"		
	68.000	SCS Cu	rve No or C		
	.100	Ia/S C	oefficient		
	5.000	Initia	l Abstractio	n	
	1	Option	1=Trianglr;	2=Recta	nglr; 3=SWM HYD; 4=Lin. Reserv
		.043	.245	.030	.000 c.m/s
		.436	.831	.476	C perv/imperv/total
15	ADD RUN	OFF			
		.043	.283	.030	.000 c.m/s
20	MANUAL				

# **INFILTRATION GALLERY PARAMETERS**

Subject:Infiltration InformationProject:1242-1260 Gordon and 9 ValleyProject No.:161413684Client:TricarDate:June 6, 2022

### East Infiltration Gallery - Stone Gallery

Infiltration Rate	32 mm/hr
Void Ratio	0.4
Depth	1 m
Footprint Provided	75 m²
Volume	30 m <sup>3</sup>
Outflow Rate	0.0007 m³/s
Drawdown	12.5 hr

South Infiltration Gallery - StormTech® Infiltration Rate	23 mm/hr
Max Depth	0.705 m
Footprint Provided	302.7 m²
Voume	116.2 m³
Outflow Rate	0.0019 m³/s
Drawdown	16.7 hr

## WATER QUALITY

Stantec | 1250 Gordon



Page 1 of 2

Project Name:	1242-1260 Gordon St.		
<b>Consulting Engineer:</b>	Stantec		
Location:	Guelph, ON		
Sizing Completed By:	C. Neath	Email:	cody.neath@ads-pipe.com

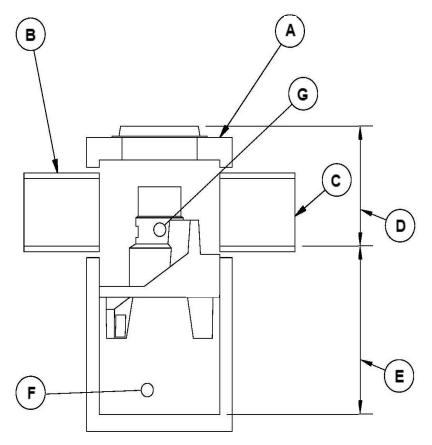
Treatment Requirements			
Treatment Goal:	Enhanced (MOE)		
Selected Parameters:	80% TSS 90% Volume		
Selected Unit: FD-4HC			

Summary of Results					
Model	TSS Removal	Volume Treated			
FD-4HC	87.0%	>90%			
FD-5HC	91.0%	>90%			
FD-6HC	93.0%	>90%			
FD-8HC	95.0%	>90%			
FD-10HC	97.0%	>90%			

FD-4HC Specification			
Unit Diameter (A):	1,200 mm		
Inlet Pipe Diameter (B):	450 mm		
Outlet Pipe Diameter (C):	450 mm		
Height, T/G to Outlet Invert (D):	1630 mm		
Height, Outlet Invert to Sump (E):	1515 mm		
Sediment Storage Capacity (F):	0.78 m³		
Oil Storage Capacity (G):	723 L		
Recommended Sediment Depth for Maintenance:	440 mm		
Max. Pipe Diameter:	600 mm		
Peak Flow Capacity:	510 L/s		

Site Elevat	ions:
Rim Elevation:	342.53
Inlet Pipe Elevation:	340.90
Outlet Pipe Elevation:	340.90

Site Details				
Site Area:	0.87 ha			
% Impervious:	95%			
Rational C:	0.87			
Rainfall Station:	Waterloo_Wellington			
Particle Size Distribution:	Fine			
Peak Flowrate:				



### Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



### Net Annual Removal Efficiency Summary: FD-4HC

Rainfall Intensity <sup>(1)</sup>	Fraction of Rainfall <sup>(1)</sup>	FD-4HC Removal Efficiency <sup>(2)</sup>	Weighted Net-Annual Removal Efficiency
mm/hr	%	%	%
0.50	0.3%	100.0%	0.3%
1.00	27.0%	97.0%	26.2%
1.50	3.2%	93.5%	3.0%
2.00	13.6%	91.0%	12.4%
2.50	7.2%	89.1%	6.4%
3.00	1.8%	87.6%	1.6%
3.50	6.7%	86.4%	5.8%
4.00	3.7%	85.3%	3.2%
4.50	1.5%	84.4%	1.3%
5.00	4.8%	83.6%	4.0%
6.00	3.3%	82.1%	2.7%
7.00	4.7%	81.0%	3.8%
8.00	2.8%	80.0%	2.2%
9.00	2.0%	79.1%	1.6%
10.00	2.5%	78.3%	2.0%
20.00	9.0%	73.4%	6.6%
30.00	3.1%	70.7%	2.2%
40.00	1.0%	68.9%	0.7%
50.00	0.8%	67.4%	0.5%
100.00	0.9%	63.2%	0.6%
150.00	0.1%	60.9%	0.1%
200.00	0.0%	59.3%	0.0%
	Total Net Annua	I Removal Efficiency:	87.0%
	99.9%		

### Notes:

- (1) Rainfall Data: 1981:2007,HLY03 6149387, Waterloo/Wellingotn Airport, ON
- (2) Based on third party verified data and appoximating the removal of a PSD similar to the STC Fine distribution
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.



## **ADS OGS Sizing Summary**

Page 1 of 2

Project Name:	1250 Gordon St. A		
Consulting Engineer:	Stantec		
Location:	Guelph, ON		
Sizing Completed By:	C. Neath	Email:	cody.neath@ads-pipe.com

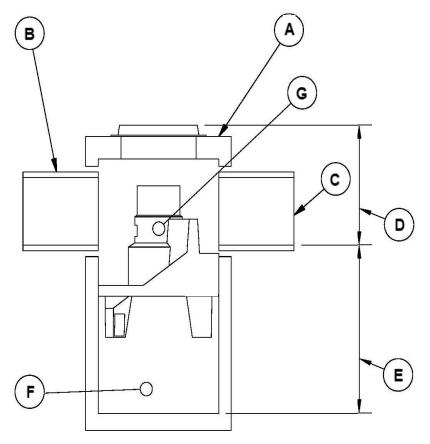
Treatment Requirements				
Treatment Goal:	Enhanced (MOE)			
Selected Parameters:	80% TSS 90% Volume			
Selected Unit:	FD-4HC			

Summary of Results					
Model TSS Removal Volume Trea					
FD-4HC	82.0%	>90%			
FD-5HC	83.0%	>90%			
FD-6HC	86.0%	>90%			
FD-8HC	91.0%	>90%			
FD-10HC	94.0%	>90%			

FD-4HC Specification	on
Unit Diameter (A):	1,200 mm
Inlet Pipe Diameter (B):	300 mm
Outlet Pipe Diameter (C):	300 mm
Height, T/G to Outlet Invert (D):	2000 mm
Height, Outlet Invert to Sump (E):	1515 mm
Sediment Storage Capacity (F):	0.78 m³
Oil Storage Capacity (G):	723 L
Recommended Sediment Depth for Maintenance:	440 mm
Max. Pipe Diameter:	600 mm
Peak Flow Capacity:	510 L/s

Site Elevations:		
Rim Elevation:	100.00	
Inlet Pipe Elevation:	98.00	
Outlet Pipe Elevation:	98.00	

Site Details		
Site Area:	0.3 ha	
% Impervious:	90%	
Rational C:	0.84	
Rainfall Station:	Waterloo_Wellington	
Particle Size Distribution:	NJDEP / ETV	
Peak Flowrate:		



### Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



## Net Annual Removal Efficiency Summary: FD-4HC

Rainfall Intensity <sup>(1)</sup>	Fraction of Rainfall <sup>(1)</sup>	FD-4HC Removal Efficiency <sup>(2)</sup>	Weighted Net-Annual Removal Efficiency
mm/hr	%	%	%
0.50	0.3%	105.5%	0.3%
1.00	27.0%	96.9%	26.1%
1.50	3.2%	91.9%	3.0%
2.00	13.6%	88.3%	12.0%
2.50	7.2%	85.6%	6.1%
3.00	1.8%	83.3%	1.5%
3.50	6.7%	81.4%	5.5%
4.00	3.7%	79.7%	2.9%
4.50	1.5%	78.3%	1.2%
5.00	4.8%	77.0%	3.7%
6.00	3.3%	74.7%	2.5%
7.00	4.7%	72.8%	3.4%
8.00	2.8%	71.1%	2.0%
9.00	2.0%	69.7%	1.4%
10.00	2.5%	68.4%	1.7%
20.00	9.0%	59.8%	5.4%
30.00	3.1%	54.7%	1.7%
40.00	1.0%	51.2%	0.5%
50.00	0.8%	48.4%	0.4%
100.00	0.9%	39.8%	0.4%
150.00	0.1%	0.0%	0.0%
200.00	0.0%	0.0%	0.0%
<b>I</b>	Total Net Annua	al Removal Efficiency:	82.0%
	Total Ru	unoff Volume Treated:	99.9%

### Notes:

- (1) Rainfall Data: 1981:2007,HLY03 6149387, Waterloo/Wellingotn Airport, ON
- (2) Based in NJDEP / ETV PSD, NJDEP Test Protocols 2013.
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.

# **STORMTECH DESIGN**

Stantec | 1250 Gordon

### **PROJECT INFORMATION**

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO.	



# 1242 - 1260 GORDON ST. GUELPH, CANADA

## SC-310 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC 310. 1.
- CHAMBERS SHALL BE ARCH SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT MODIFIED POLYPROPYLENE OR 2. POLYETHYLENE COPOLYMERS.
- CHAMBERS SHALL BE CERTIFIED TO CSA B1 4, "POLYMERIC SUB SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3. THE RE UIREMENTS OF ASTM F2922 POLETHYLENE OR ASTM F241 POLYPROPYLENE ."STANDARD SPECIFICATION FOR CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD Δ IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION RE UIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS. SECTION 12.12, ARE MET FOR 1 LONG DURATION DEAD LOADS AND 2 SHORT DURATION LIVE LOADS, BASED ON THE CSA S CL 2 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE 1 INSTANTANEOUS 1 MIN AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2 MA IMUM PERMANENT YR COVER LOAD AND 3 ALLOWABLE COVER WITH PARKED 1 WEEK AASHTO DESIGN TRUCK.
- RE UIREMENTS FOR HANDLING AND INSTALLATION
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 0 mm 2 .
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION. a THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION .2. OF ASTM F2922 SHALL BE GREATER THAN OR E UAL TO 400 LBS FT . AND TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES ABOVE 23 C 3 F, CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON RE UEST BY THE SITE DESIGN ENGINEER OR OWNER. THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS
  - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
  - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR E UAL TO 1.9 FOR DEAD LOAD AND 1. FOR LIVE LOAD, THE MINIMUM RE UIRED BY ASTM F2 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
  - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2922 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN E CEPT THAT IT SHALL BE THE YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 9

## **IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310 SYSTEM**

- STORMTECH SC 310 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER S REPRESENTATIVE HAS COMPLETED A 1 PRE CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2.
- 3 CHAMBERS ARE NOT TO BE BACKFILLED WITH A DO ER OR AN E CAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS
  - STONESHOOTER LOCATED OFF THE CHAMBER BED.
  - BACKFILL AS ROWS ARE BUILT USING AN E CAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
  - BACKFILL FROM OUTSIDE THE E CAVATION USING A LONG BOOM HOE OR E CAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- MAINTAIN MINIMUM 1 0 mm " SPACING BETWEEN THE CHAMBER ROWS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20 0 mm 3 4 2" .
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN. ENGINEER.
- ADS RECOMMENDS THE USE OF "FLE STORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

### NOTES FOR CONSTRUCTION EQUIPMENT

- 1.
- 2. THE USE OF CONSTRUCTION E UIPMENT OVER SC 310 SC 40 CHAMBERS IS LIMITED
  - NO E UIPMENT IS ALLOWED ON BARE CHAMBERS.
  - WITH THE "STORMTECH SC 310 SC 40 DC 0 CONSTRUCTION GUIDE".
- 3. FULL 900 mm 3 " OF STABILI ED COVER MATERIALS OVER THE CHAMBERS IS RE UIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

### USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1 92 2 94 WITH ANY UESTIONS ON INSTALLATION RE UIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION E UIPMENT.





STORMTECH SC 310 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC 310 SC 40 DC 0 CONSTRUCTION GUIDE".

STORMTECH SC 310 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC 310 SC 40 DC 0 CONSTRUCTION GUIDE".

NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR E CAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE

WEIGHT LIMITS FOR CONSTRUCTION E UIPMENT CAN BE FOUND IN THE "STORMTECH SC 310 SC 40 DC 0 CONSTRUCTION GUIDE".

### **PROJECT INFORMATION**

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO.	



# 1242 - 1260 GORDON ST. GUELPH, CANADA

## MC-3500 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC 3 00. 1.
- CHAMBERS SHALL BE ARCH SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT MODIFIED POLYPROPYLENE 2. COPOLYMERS.
- CHAMBERS SHALL BE CERTIFIED TO CSA B1 4, "POLYMERIC SUB SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3. THE RE UIREMENTS OF ASTM F241 "STANDARD SPECIFICATION FOR POLYPROPYLENE PP CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 4 DESIGNATION SS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD Δ IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION RE UIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS. SECTION 12.12, ARE MET FOR 1 LONG DURATION DEAD LOADS AND 2 SHORT DURATION LIVE LOADS, BASED ON THE CSA S CL 2 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE 1 INSTANTANEOUS 1 MIN AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2 MA IMUM PERMANENT YR COVER LOAD AND 3 ALLOWABLE COVER WITH PARKED 1 WEEK AASHTO DESIGN TRUCK.
- RE UIREMENTS FOR HANDLING AND INSTALLATION
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN mm 3.
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION. a THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION .2. OF ASTM F241 SHALL BE GREATER THAN OR E UAL TO 4 0 LBS FT . AND TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES ABOVE 23 C 3 F, CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON RE UEST BY THE SITE DESIGN ENGINEER OR OWNER. THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS
  - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
  - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR E UAL TO 1.9 FOR DEAD LOAD AND 1. FOR LIVE LOAD, THE MINIMUM RE UIRED BY ASTM F2 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
  - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F241 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN E CEPT THAT IT SHALL BE THE YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 9

## **IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM**

- STORMTECH MC 3 00 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER S REPRESENTATIVE HAS COMPLETED A PRE CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH MC 3 00 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC 3 00 MC 4 00 CONSTRUCTION GUIDE". 2.
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DO ER OR AN E CAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS
  - STONESHOOTER LOCATED OFF THE CHAMBER BED.
  - BACKFILL AS ROWS ARE BUILT USING AN E CAVATOR ON THE FOUNDATION STONE OR SUBGRADE. BACKFILL FROM OUTSIDE THE E CAVATION USING A LONG BOOM HOE OR E CAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- MAINTAIN MINIMUM 1 0 mm " SPACING BETWEEN THE CHAMBER ROWS.
- INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 300 mm 12" INTO CHAMBER END CAPS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE WELL GRADED BETWEEN 3/4" AND 2" 20 0 mm .
- 9. STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING.
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN 10. FNGINFFR
- ADS RECOMMENDS THE USE OF "FLE STORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 11. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

### NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH MC 3 00 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC 3 00 MC 4 00 CONSTRUCTION GUIDE". 1
- THE USE OF E UIPMENT OVER MC 3 00 CHAMBERS IS LIMITED 2
  - NO E UIPMENT IS ALLOWED ON BARE CHAMBERS.
  - NO RUBBER TIRED LOADER, DUMP TRUCK, OR E CAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE .
  - WITH THE "STORMTECH MC 3 00 MC 4 00 CONSTRUCTION GUIDE". WEIGHT LIMITS FOR CONSTRUCTION E UIPMENT CAN BE FOUND IN THE "STORMTECH MC 3 00 MC 4 00 CONSTRUCTION GUIDE".
- 3. FULL 900 mm 3 " OF STABILI ED COVER MATERIALS OVER THE CHAMBERS IS RE UIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

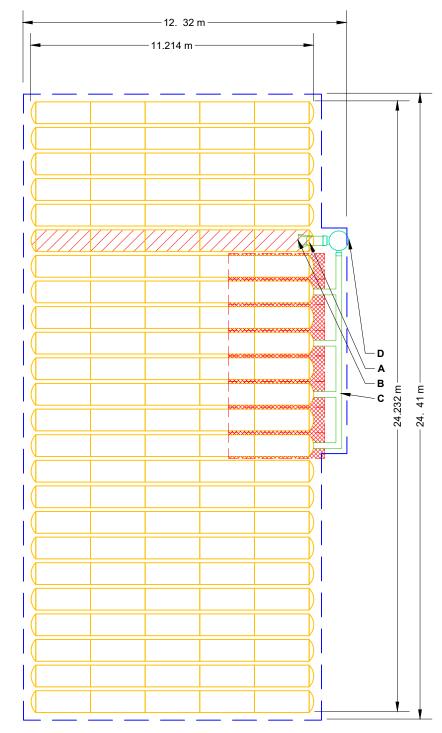
### USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY

CONTACT STORMTECH AT 1 92 2 94 WITH ANY UESTIONS ON INSTALLATION RE UIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION E UIPMENT.





PROP	OSED LAYOUT: INFILTRAT	PROPOSED ELEVATIONS: INFILTRAT				
	STORMTECH SC 310 CHAMBERS	MA IMUM ALLOWABLE GRADE TOP OF PAVEMENT UNPAVED	343. 24	PART TYPE	ITEM ON	DESCRIPTION
	STORMTECH SC 310 END CAPS	MINIMUM ALLOWABLE GRADE UNPAVED WITH TRAFFIC	341.9	PREFABRICATED E END CAP	Δ	300 mm BOTTOM PREFABRICATED E END CAP, PART SC310ECE
· -	STONE BELOW mm STONE VOID	MINIMUM ALLOWABLE GRADE TOP OF RIGID CONCRETE PAVEMENT	341. 43	FLAMP	В	BOTTOM CONNECTIONS AND ISOLATOR PLUS ROWS INSTALL FLAMP ON 300 mm ACCESS PIPE PART SC31012RAMP
	INSTALLED SYSTEM VOLUME m	TOP OF STONE	341.43	MANIFOLD	С	200 mm 200 mm TOP MANIFOLD, MOLDED FITTINGS
11 .2	PERIMETER STONE INCLUDED	TOP OF SC 310 CHAMBER 200 mm 200 mm TOP MANIFOLD INVERT	<u>341.2</u> 340.9	PLUS ROW	D	0 mm DIAMETER 10 mm SUMP MIN
	BASE STONE INCLUDED	300 mm ISOLATOR ROW PLUS INVERT	340.902	2		
002.	SYSTEM AREA m SYSTEM PERIMETER m	BOTTOM OF SC 310 CHAMBER BOTTOM OF STONE	<u>340.</u> 340. 2			

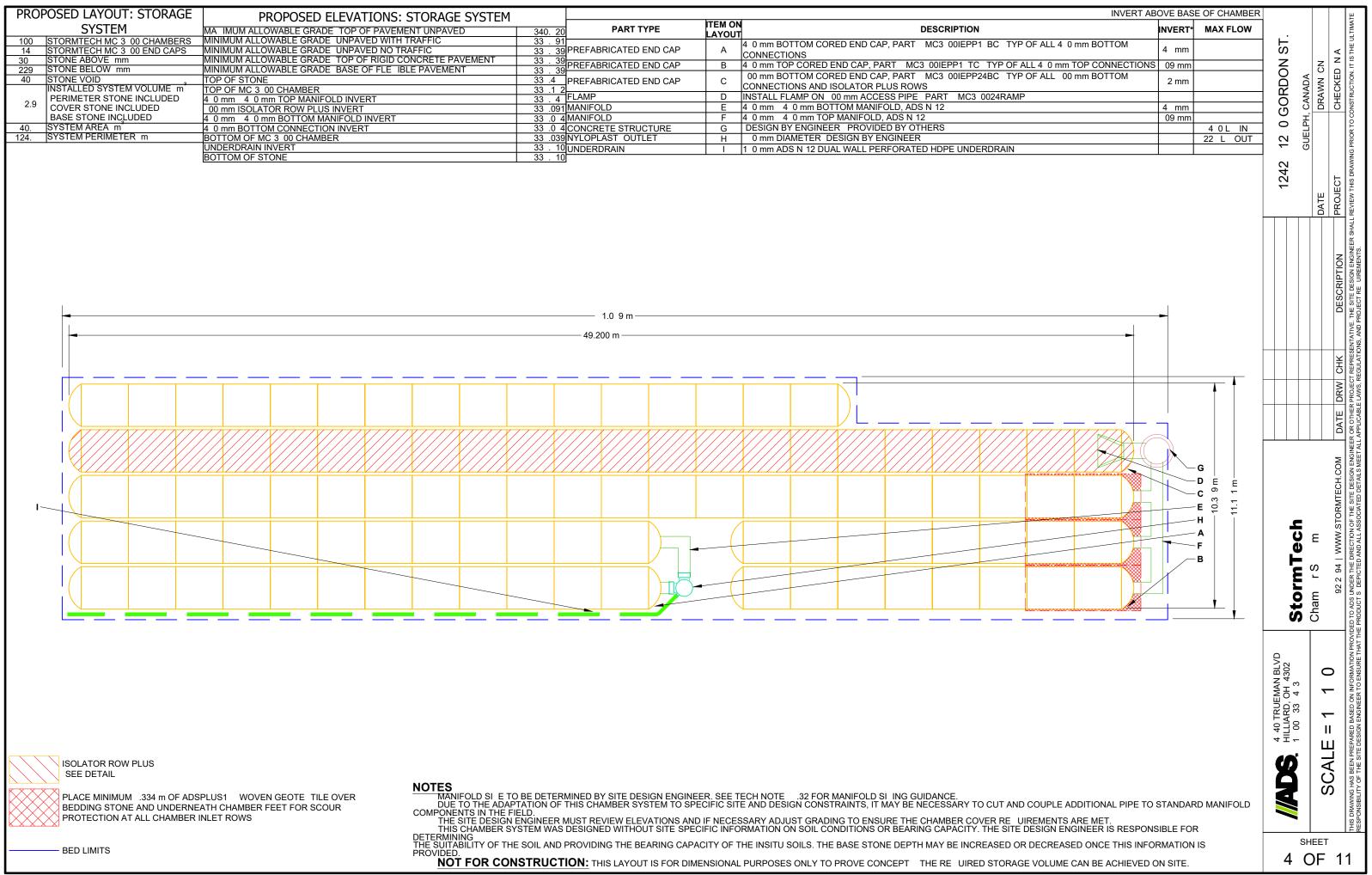




PLACE MINIMUM 3. 10 m OF ADSPLUS12 WOVEN GEOTE TILE OVER BEDDING STONE AND UNDERNEATH CHAMBER FEET FOR SCOUR PROTECTION AT ALL CHAMBER INLET ROWS

- BED LIMITS

INVERT ABOVE BASE OF CHAMBER				MATE
TYP OF ALL 300 mm 23 mm	ST.		A	THE ULT
	Z	CN	z g	N. IT IS
9 mm L IN	RD(	CANAUA DRAWN CN	CHECKED N A	<b>IRUCTIO</b>
I _ I	1242 12 0 GORDON ST.	GUELPH, CANAUA DRAWN	R	O CONST
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	0 7	<u>ر</u>		AWING F
	124		СT	THIS DR
		DATE	PROJECT	EVIEW.
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			Ž	NGINEER ENTS.
			DESCRIPTION	UIREME
			ESCF	SITE DE ECT RE
				IVE. THE UD PROJ
				ESENTAT IONS, AN
			CHK	r REPRE EGULAT
			DRW	PROJECT LAWS, R
			DATE	OTHER F ICABLE
			DA	NEER OR ( ALL APPL
	StormTech	Cham r S m	92 2 94   WWW.STORMTECH.COM	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THE PRODUCT S DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT RE UREMENTS.
LE ADDITIONAL PIPE TO STANDARD MANIFOLD NTS ARE MET.	HADS 4 40 TRUEMAN BLVD HILLIARD, OH 4302 1 00 33 4 3			IS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PR SPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT
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## ACCEPTABLE FILL MATERIALS: STORMTECH SC-310 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPA
D	FINAL FILL: FILL MATERIAL FOR LAYER D STARTS FROM THE TOP OF THE C LAYER TO THE BOTTOM OF FLE IBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE D LAYER.	ANY SOIL ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE RE UIREMENTS.	NA	PREPAR INSTALL
с	INITIAL FILL: FILL MATERIAL FOR LAYER C STARTS FROM THE TOP OF THE EMBEDMENT STONE B LAYER TO 1 " 4 0 mm ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE C LAYER.	GRANULAR WELL GRADED SOIL AGGREGATE MI TURES, 3 FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M14 <sup>1</sup> A 1, A 2 4, A 3 OR AASHTO M43 <sup>1</sup> 3, 3 , 4, 4 , , , , , , , , , , , , 9, 9, 10	BEGIN COM THE CHAMBE " 1 0 mm WELL GRA PROCES VEHICLE WI
В	<b>EMBEDMENT STONE:</b> FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE A LAYER TO THE C LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 3	
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT BOTTOM OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 3 , 4, 4 , , , ,	PLATE CO

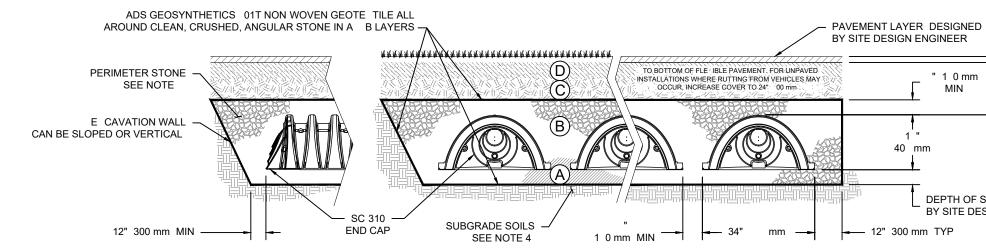
PLEASE NOTE

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR E AMPLE, A SPECIFICATION FOR 4 STONE WOULD STATE "CLEAN, CRUSHED, ANGULAR NO. 4 AASHTO M43 STONE".

2. STORMTECH COMPACTION RE UIREMENTS ARE MET FOR A LOCATION MATERIALS WHEN PLACED AND COMPACTED IN " 1 0 mm MA LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.

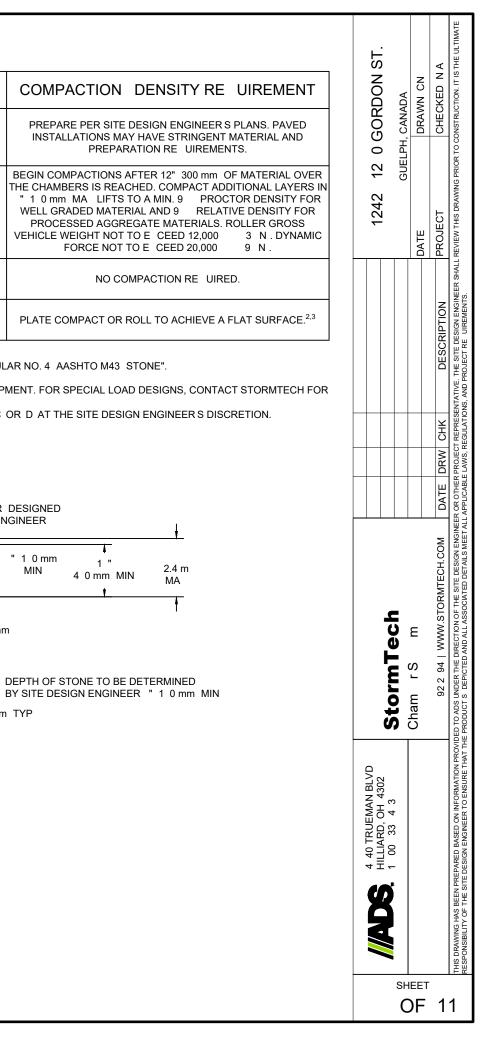
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION E UIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION RE UIPMENTS.

4. ONCE LAYER C IS PLACED, ANY SOIL MATERIAL CAN BE PLACED IN LAYER D UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL RE UIREMENTS OF LAYER C OR D AT THE SITE DESIGN ENGINEERS DISCRETION.



## NOTES:

- 1. CHAMBERS SHALL MEET THE RE UIREMENTS OF ASTM F2922 POLETHYLENE OR ASTM F241 POLYPROPYLENE, "STANDARD SPECIFICATION FOR CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. SC 310 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE ALLOWABLE BEARING CAPACITY OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF E PECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE E TENDED HORI ONTALLY TO THE E CAVATION WALL FOR BOTH VERTICAL AND SLOPED E CAVATION WALLS.
- . RE UIREMENTS FOR HANDLING AND INSTALLATION
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2 .
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR E UAL TO 400 LBS FT . THE ASC IS DEFINED IN SECTION .2. OF ASTM F241 . AND TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES ABOVE 3 F 23 C, CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.



## ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

MATERIAL LOCATION		DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPA
D	<b>FINAL FILL</b> : FILL MATERIAL FOR LAYER D STARTS FROM THE TOP OF THE C LAYER TO THE BOTTOM OF FLE IBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE D LAYER	ANY SOIL ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE RE UIREMENTS.	N A	PREPAR INSTALL
с	INITIAL FILL: FILL MATERIAL FOR LAYER C STARTS FROM THE TOP OF THE EMBEDMENT STONE B LAYER TO 24" 00 mm ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE C LAYER.	GRANULAR WELL GRADED SOIL AGGREGATE MI TURES, 3 FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M14 <sup>1</sup> A 1, A 2 4, A 3 OR AASHTO M43 <sup>1</sup> 3, 3 , 4, 4 , , , , , , , , , , , , 9, 9, 10	BEGIN COM THE CHAMBI 12" 300 mm WELL GRA
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE A LAYER TO THE C LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 4	
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT BOTTOM OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 <sup>1</sup> 3, 4	PLATE CO

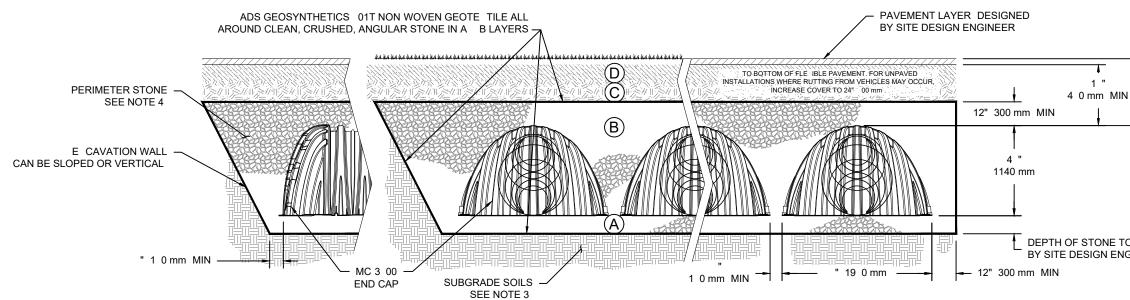
PLEASE NOTE

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR E AMPLE, A SPECIFICATION FOR 4 STONE WOULD STATE "CLEAN, CRUSHED, ANGULAR NO. 4 AASHTO M43 STONE".

2. STORMTECH COMPACTION RE UIREMENTS ARE MET FOR A LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" 230 mm MA LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.

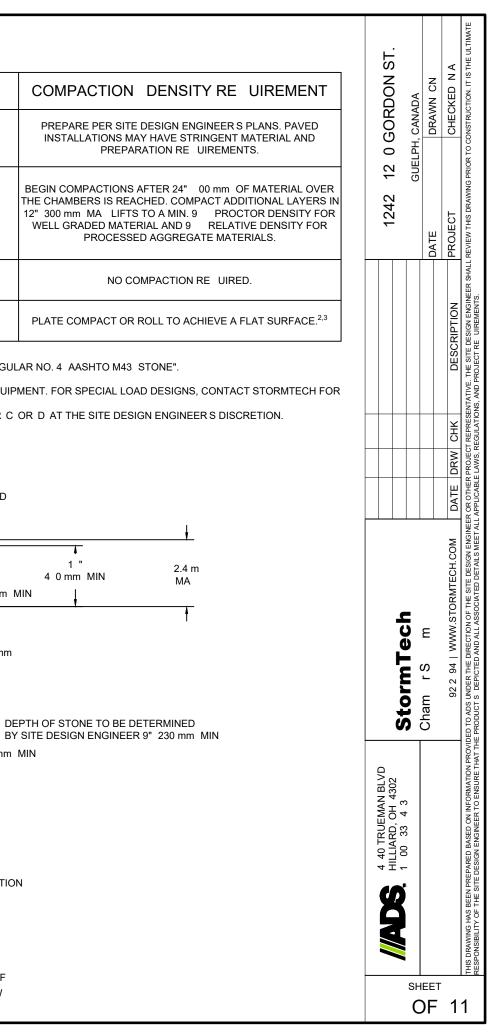
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION E UIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION RE UIREMENTS.

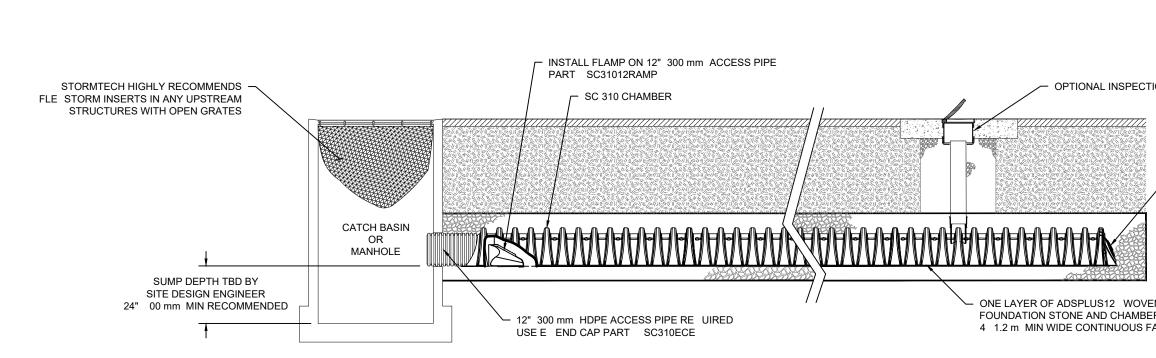
4. ONCE LAYER C IS PLACED, ANY SOIL MATERIAL CAN BE PLACED IN LAYER D UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL RE UIREMENTS OF LAYER C OR D AT THE SITE DESIGN ENGINEERS DISCRETION.



## NOTES:

- 1. CHAMBERS SHALL MEET THE RE UIREMENTS OF ASTM F241, "STANDARD SPECIFICATION FOR POLYPROPYLENE PP CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 4 DESIGNATION SS.
- 2. MC 3 00 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE ALLOWABLE BEARING CAPACITY OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF E PECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE E TENDED HORI ONTALLY TO THE E CAVATION WALL FOR BOTH VERTICAL AND SLOPED E CAVATION WALLS.
- . RE UIREMENTS FOR HANDLING AND INSTALLATION
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3 .
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR E UAL TO 4 0 LBS FT . THE ASC IS DEFINED IN SECTION .2. OF ASTM F241 . AND TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES ABOVE 3 F 23 C, CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.





### SC-310 ISOLATOR ROW PLUS DETAIL

NTS

### **INSPECTION & MAINTENANCE**

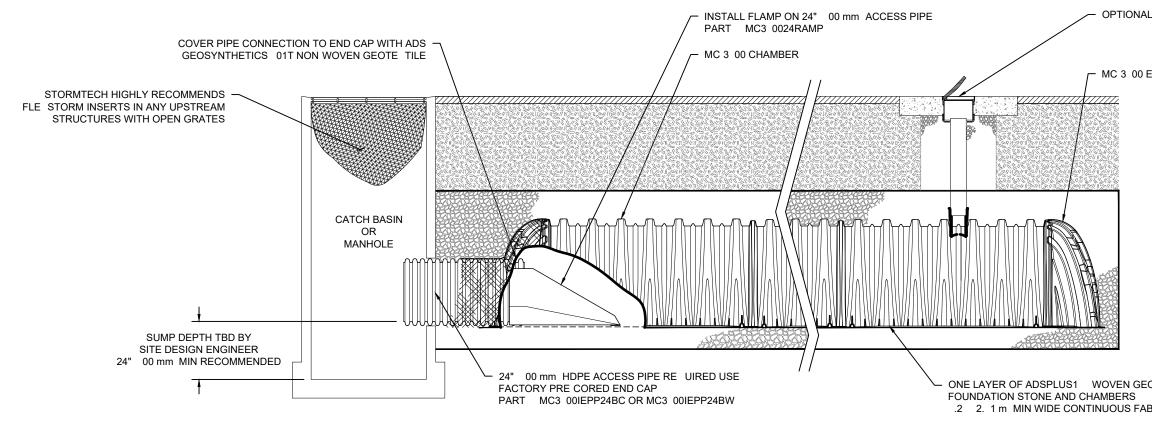
### STEP 1 INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- A. INSPECTION PORTS IF PRESENT
  - A.1. REMOVE OPEN LID ON NYLOPLAST INLINE DRAIN
  - A.2. REMOVE AND CLEAN FLE STORM FILTER IF INSTALLED
  - A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
  - A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS OPTIONAL
  - A. IF SEDIMENT IS AT, OR ABOVE, 3" 0 mm PROCEED TO STEP 2, IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
- FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3" 0 mm PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2 CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
  - A. A FI ED CULVERT CLEANING NO LE WITH REAR FACING SPREAD OF 4 " 1.1 m OR MORE IS PREFERRED
  - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
  - C. VACUUM STRUCTURE SUMP AS RE UIRED
- STEP 3 REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS RECORD OBSERVATIONS AND ACTIONS.
- STEP 4 INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

### NOTES

- 1. INSPECT EVERY MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

	-			ABRIC WITHOUT SEAMS	V N GEOTE TILE BETWEEN RS	ON PORT SC 310 END CAP
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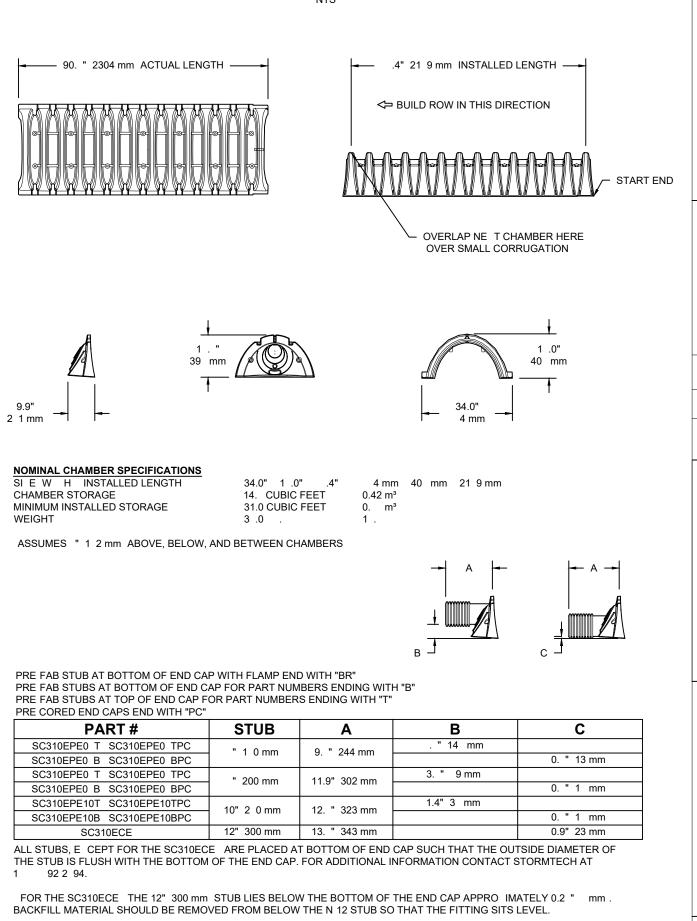
MC-3500 ISOLATOR ROW PLUS DETAIL

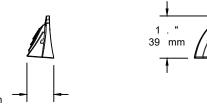
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### **SC-310 TECHNICAL SPECIFICATION**

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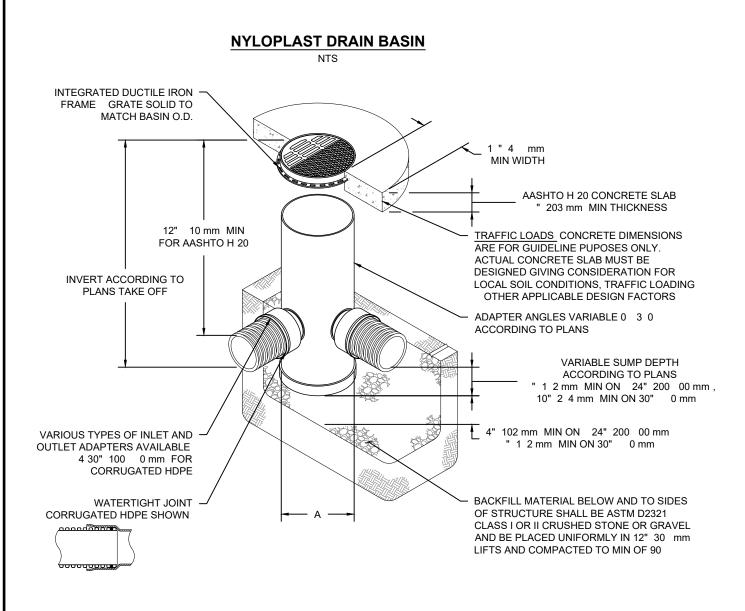
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PART #	STUB	Α	
SC310EPE0 T SC310EPE0 TPC	"10mm	9. " 244 mm	
SC310EPE0 B SC310EPE0 BPC	i o min	5. 244 mm	
SC310EPE0 T SC310EPE0 TPC	" 200 mm	11.9" 302 mm	
SC310EPE0 B SC310EPE0 BPC	200 11111	11.9 302 1111	
SC310EPE10T SC310EPE10TPC	10" 2 0 mm	12. " 323 mm	
SC310EPE10B SC310EPE10BPC		12. 525 11111	
SC310ECE	12" 300 mm	13. " 343 mm	

NOTE ALL DIMENSIONS ARE NOMINAL



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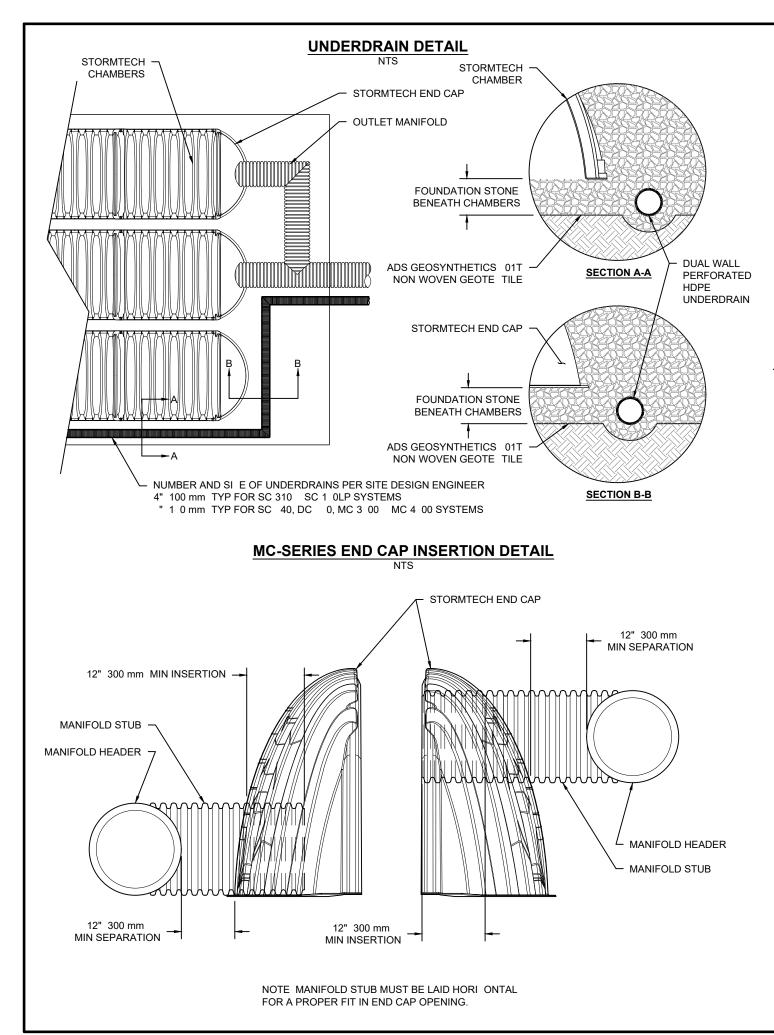


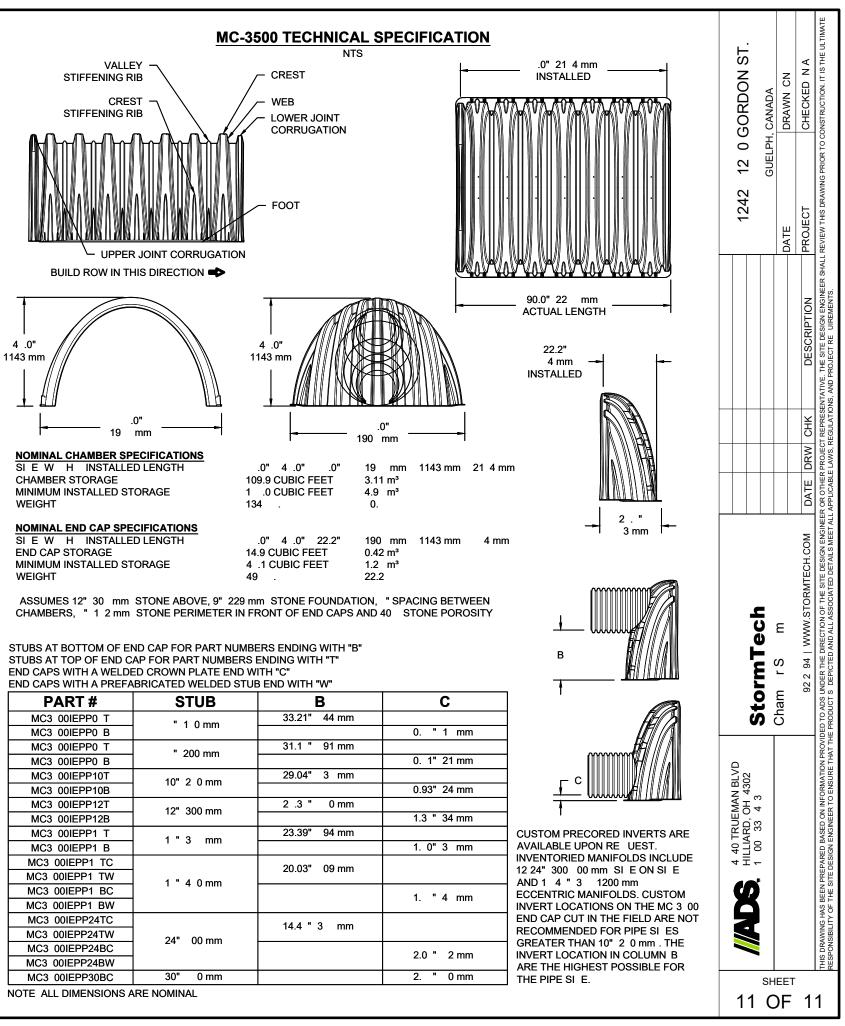
## NOTES

- 1. 30" 200 0 mm GRATES SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A 3 GRADE 0 00
- 2. 12 30" 300 0 mm FRAMES SHALL BE DUCTILE IRON PER ASTM A 3 GRADE 0 0 0 3. DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 4.
- FOR CORRUGATED HDPE ADS HANCOR DUAL WALL SDR 3 PVC FOR COMPLETE DESIGN AND PRODUCT INFORMATION WWW.NYLOPLAST-US.COM . TO ORDER CALL 800-821-6710

Α	PART	GRATE SOLID COVER OPTIONS		
" 200 mm	2 0 AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
10" 2 0 mm	2 10AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
12"	2 12AG	PEDESTRIAN	STANDARD AASHTO	SOLID
300 mm		AASHTO H 10	H 20	AASHTO H 20
1 "	2 1 AG	PEDESTRIAN	STANDARD AASHTO	SOLID
3 mm		AASHTO H 10	H 20	AASHTO H 20
1 "	2 1 AG	PEDESTRIAN	STANDARD AASHTO	SOLID
4 0 mm		AASHTO H 10	H 20	AASHTO H 20
24"	2 24AG	PEDESTRIAN	STANDARD AASHTO	SOLID
00 mm		AASHTO H 10	H 20	AASHTO H 20
30"	2 30AG	PEDESTRIAN	STANDARD AASHTO	SOLID
0 mm		AASHTO H 20	H 20	AASHTO H 20

1242 12 0 GORDON ST.	GUELPH, CANADA	DRAWN CN	CHECKED NA	R TO CONSTRUCTION. IT IS THE ULTIMATE
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	Nyiopiast		0 932 2443   WWW.NYLOPLAST US.COM	THS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT S DEPICTED AND ALL ASSOCIATED DETALS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT RE UREMENTS.
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STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" END CAPS WITH A WELDED CROWN PLATE END WITH "C" END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART #	STUB	В	
MC3 00IEPP0 T	"10mm	33.21" 44 mm	
MC3 00IEPP0 B	1 10mm		0.
MC3 00IEPP0 T	" 200 mm	31.1 " 91 mm	
MC3 00IEPP0 B	200 11111		0. 1
MC3 00IEPP10T	10" 2 0 mm	29.04" 3 mm	
MC3 00IEPP10B			0.93
MC3 00IEPP12T	12" 300 mm	2 .3 " 0 mm	
MC3 00IEPP12B	12 300 11111		1.3
MC3 00IEPP1 T	1 " 3 mm	23.39" 94 mm	
MC3 00IEPP1 B	1"3 mm		1. 0
MC3 00IEPP1 TC		20.03" 09 mm	
MC3 00IEPP1 TW	1"40mm	20.03 09 1111	
MC3 00IEPP1 BC			1.
MC3 00IEPP1 BW			1.
MC3 00IEPP24TC		14.4 " 3 mm	
MC3 00IEPP24TW		14.4 5 11111	
MC3 00IEPP24BC	24 00 11111		2.0
MC3 00IEPP24BW	1		2.0
MC3 00IEPP30BC	30" 0 mm		2.

NOTE ALL DIMENSIONS ARE NOMINAL

